# Drainage Narrative

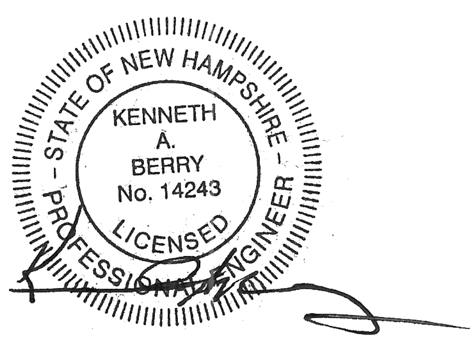
## 49 Winkley Pond Road
## Barrington, NH
## Tax Map 253, Lot 14

Prepared for

Hambone, LLC
242 Central Ave
Dover, NH 03820

Prepared By


Berry Surveying & Engineering
335 Second Crown Point Road
Barrington, NH  03825
603-332-2863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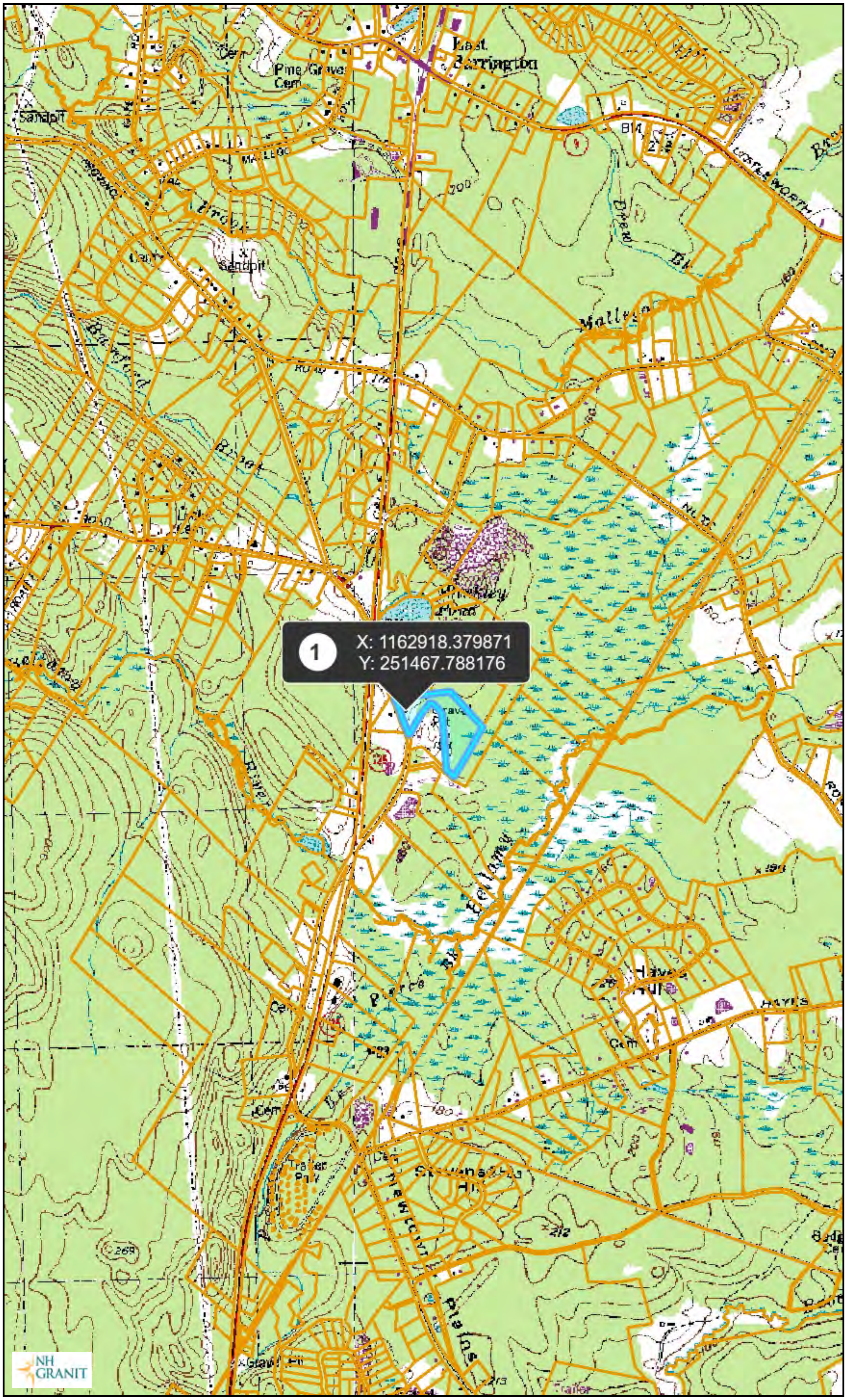
# Map by NH GRANIT




## Legend

Parcels
- Parcel Polygons
- Attributes for Additional Lines
- State
- County
- City/Town

Map Scale

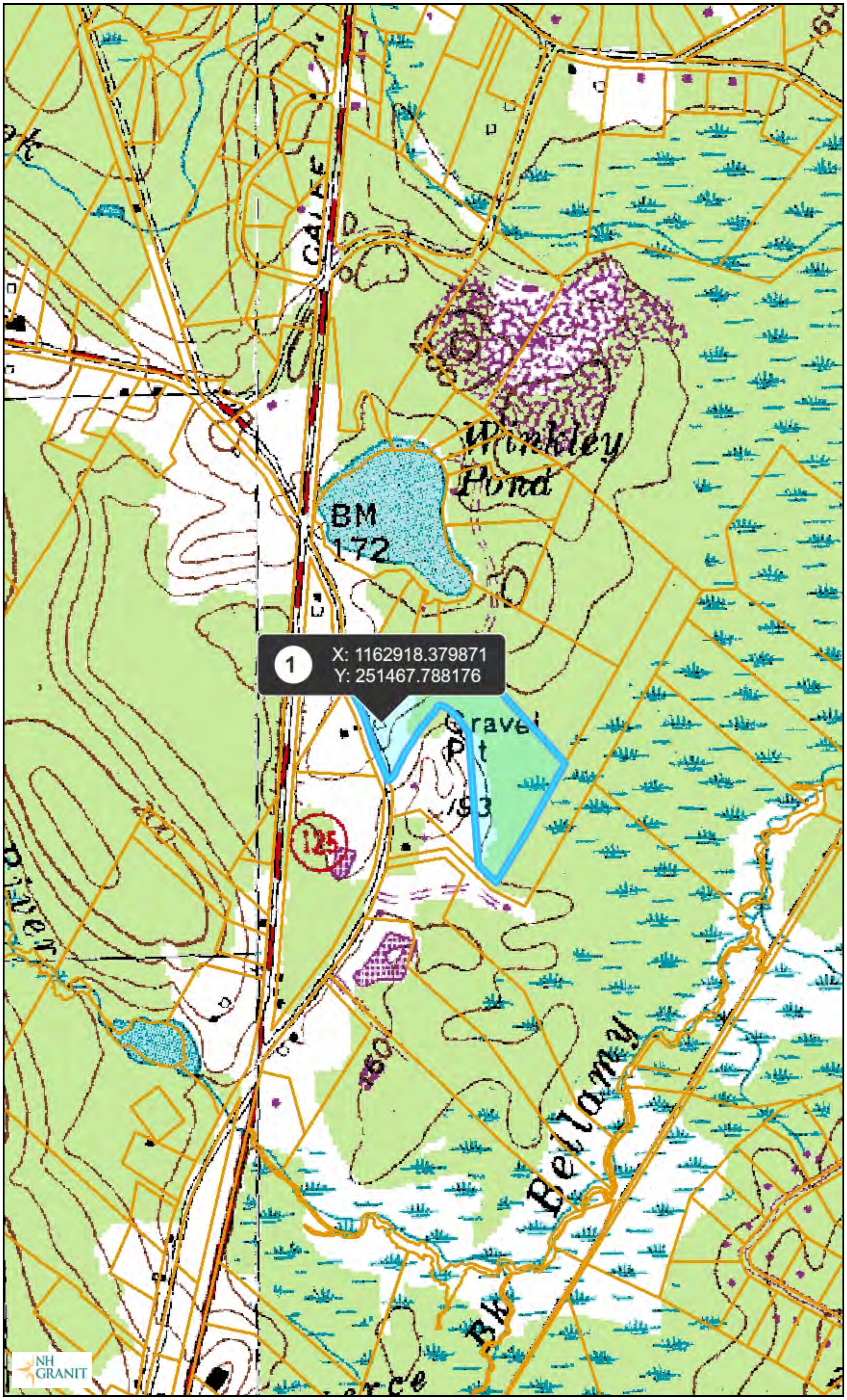
1: 24,000



Map Generated: 3/3/2022

Notes

# Map by NH GRANIT




Legend

Parcels
Parcel Polygons
Attributes for Additional Lines
State
County
City/Town

Map Scale
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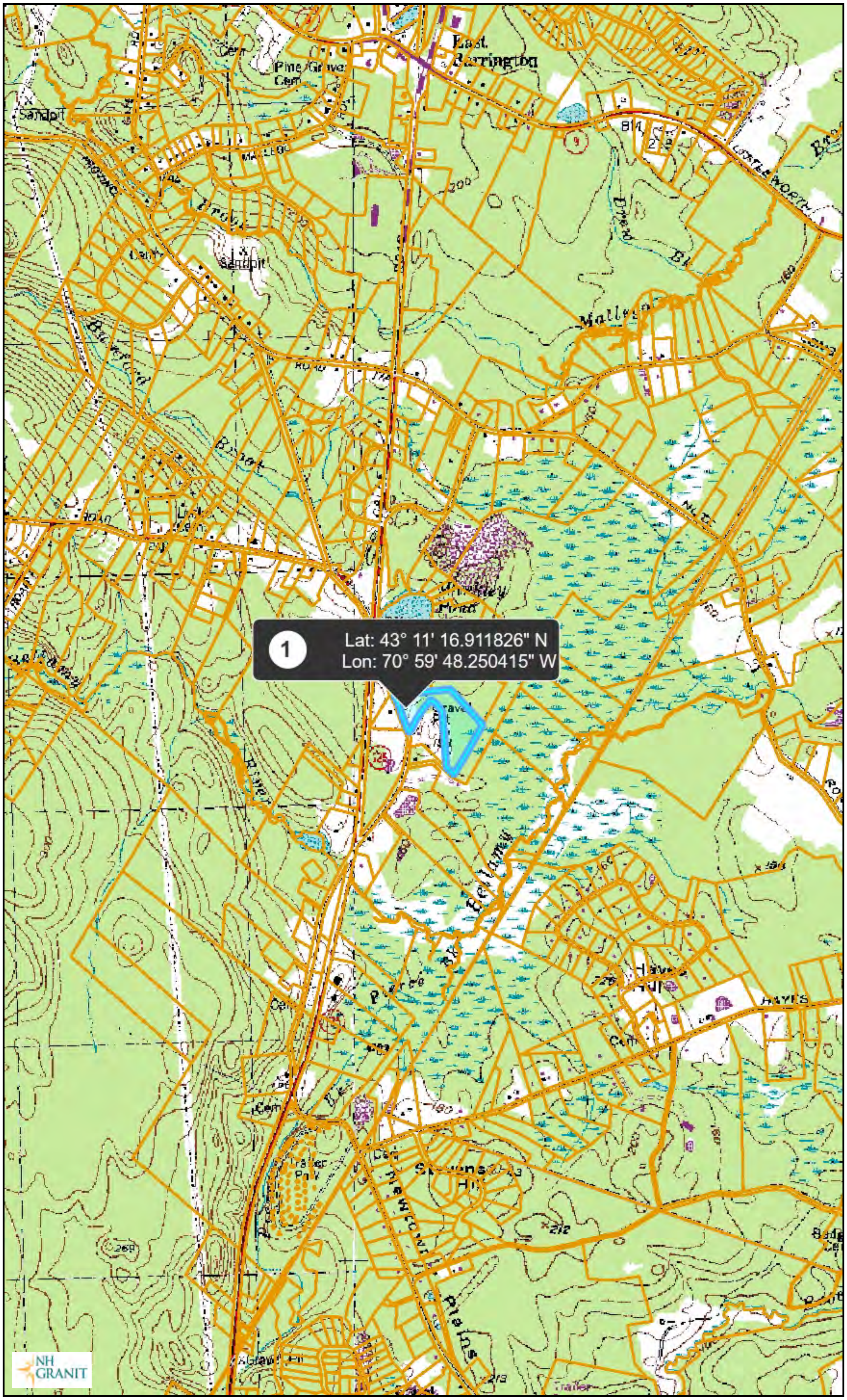
Map Generated: 3/3/2022

Notes

# Map by NH GRANIT




## Legend

Parcels

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- Attributes for Additional Lines

- State
- County
- City/Town

Map Scale

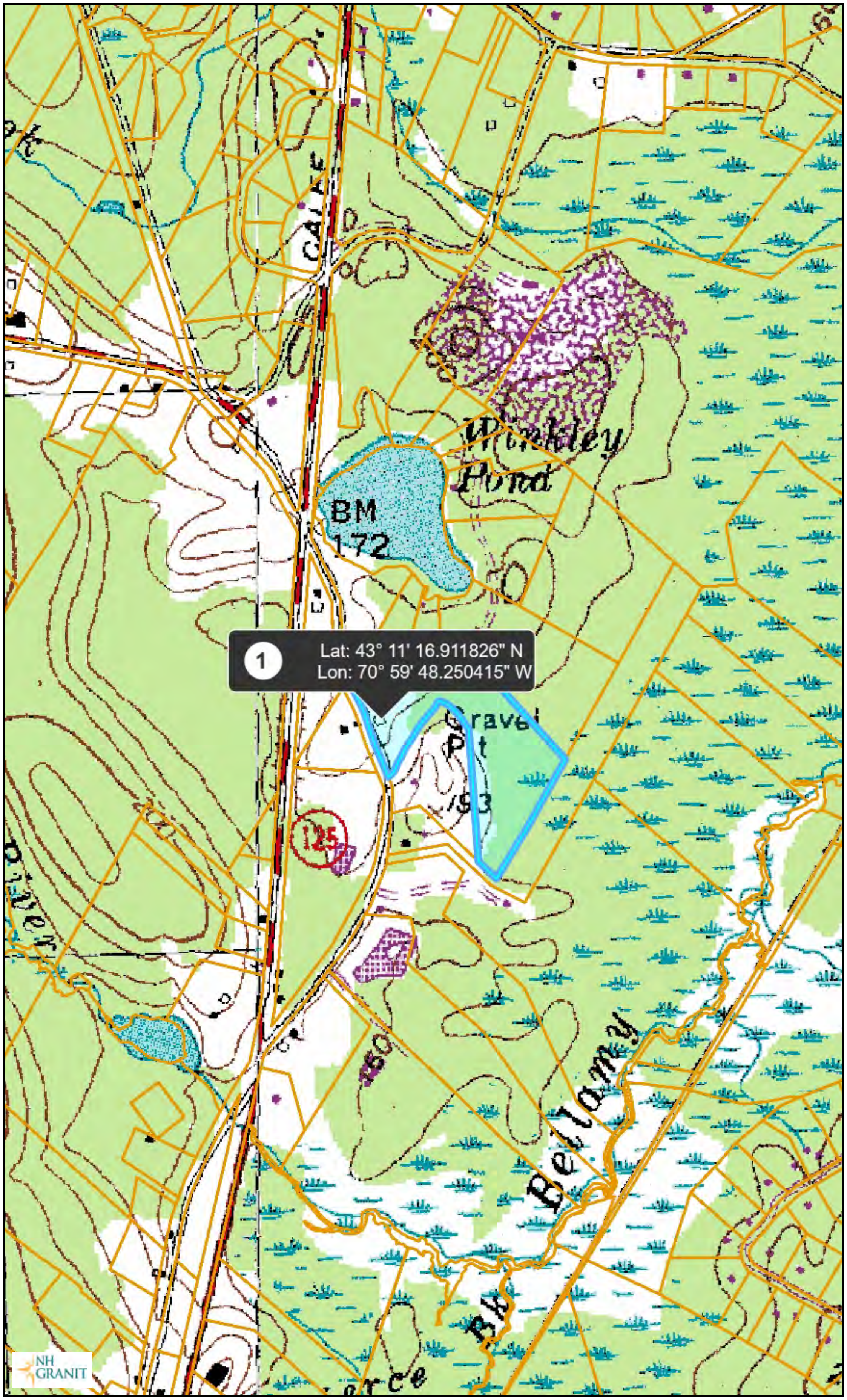
1: 24,000



Map Generated: 3/3/2022

Notes

# Map by NH GRANIT




Legend

Parcels
- Parcel Polygons
- Attributes for Additional Lines

State
County
City/Town

Map Scale
1: 10,000



Map Generated: 3/3/2022

Notes

## DESIGN METHOD OBJECTIVES

The owner / developer of Tax Map 253, Lot 14, Hambone, LLC is proposing to develop the property at 49 Winkley Pond Road. The site is currently a single family lot including a house and a barn which are both proposed to be removed. Six of the seven proposed units will two-bedroom townhouse style construction, with one unit as a one-bedroom townhouse style construction.

On-site topography survey was completed by field crews of Berry Surveying & Engineering in October of 2022 and a Site Specific Soil Survey was completed by John P. Hayes with a report generated on July 26, 2023. Soils on site are included in three hydrologic soil groups: HSG B, HSG C, and HSG D. (See attached report). A wetland delineation was completed as part of the existing conditions package. The off-site land which drains onto the locus parcel has been delineated by USDA / NRCS soils in Websoil and USGS Equivalent contours from public sources. (Google Tin & NH Lidar)

An Existing and Proposed Conditions analysis was conducted for the purpose of estimating the peak rate of stormwater run-off and to subsequently design adequate mitigation of drainage. There is one existing drainage discharge point which was identified in the existing analysis and duplicated in the proposed conditions analysis. Designing two watershed models we have compared the differences in these rates of peak run-off and surface water volume. Sheet W1, Existing Conditions Watershed Plan, outlines the characteristics of the site in its existing or pre-construction conditions. The second analysis displays the proposed (post-construction) conditions (See Sheet W2). HydroCAD uses a series of node suffixes for numbering purposes (S = Subcatchment, P = Pond Device, R = Reach), to simplify annotation these suffixes are left off the watershed plans and node type is denoted by the symbol shape according to the displayed legend which coincides with HydroCAD graphics. The analysis was conducted using data for; 2 Yr - 24 Hr (3.08”), 10 Yr - 24 Hr (4.63”), 25 Yr - 24 Hr (5.85”), 50 Yr - 24 Hr (6.99”), and 100 YR - 24 Hr (8.36”) storm events. Storm event analysis was accomplished using the USDA SCS TR-20 method within the HydroCAD Stormwater Modeling System environment. Rainfall quantities are based on the Extreme Precipitation Table for this location from the Northeast Regional Climate Center / Cornell University (http://precip.eas.cornell.edu).

## 1.0 Existing Conditions Analysis:

Reference: Sheet W1 - Existing Conditions Watershed Plan (Enclosed)
Existing Conditions Plan

The existing parcel currently consists of 2 residential structures. The soils within the locus parcel are made up of multiple soil types, containing Hydrologic Soil Group (HSG) B, C, & D. See Site Specific Soils Map and report for more information. The land cover types involved are grassed land, woods, buildings, and road pavement. Off-site soils are likewise HSG A & C and again based on USDA / NRCS Websoil.

The land area analyzed consists of 2.03 acres of the 13.47 acre parcel as well as 2.72 acres of offsite land. The land analyzed is made up of a single subcatchment analyzed at an individual final reach.

**Final Reach #100**

**Subcatchment #1** is land area in the northwestern portion of the property and drains to a delineated wetland being analyzed at **Final Reach #100** which eventually flows offsite.

## 2.0 Proposed Conditions Analysis:

Reference: Sheet W2 - Proposed Conditions Watershed Plan (Enclosed)
Proposed Grading & Drainage Plan

The client is proposing to develop the roadside portion of the parcel with 7 dwelling units and a dead end road consisting of 208 feet of roadway. The proposal is supported by an infiltration pond to help comply with groundwater recharge volume requirements and a closed drainage system of catch basins and drain manholes all directed to a single rain garden for treatment of onsite paved surfaces.

**Final Reach #100**

**Subcatchment #1** is reduced in size due to the proposed development of the parcel and the construction of drainage practices. Runoff still flows to the wetland analyzed as **Final Reach #100**.

**Subcatchment #11** is made up of the land directly surrounding and flowing to **Rain Garden #101** (**Pond #101**) extending to a portion of Winkley Pond Road. Runoff is directed through an outlet structure to the wetland analyzed as **Final Reach #100** through an overland reach (**Reach #101**).

**Subcatchment #12** consists of the land directly surrounding and flowing to **Infiltration Basin #102** extending to portions of Winkley Pond Road as well as extending offsite to a high point north of the parcel. Runoff is infiltrated into the ground with any future excess runoff overflowing directly into **Rain Garden #101** and subsequently directed through an outlet structure and overland reach to the wetland analyzed as **Final Reach #100**.

**Subcatchments #21-#24** encompass a majority of the impervious area of the proposed development. Runoff is collected in four catch basins (**Ponds #C01-#C04** respectively). **Catch Basins #2-#4** individually outlet into **Rain Garden #101** and eventually to **Final Reach #100**. **Catch Basin #1** collects runoff from the southeastern portion of the roadway as well as the front portions of the roofs of units **#6 & #7** and directs the runoff to **Catch Basin #2** and subsequently to **Final Reach #100**.

**Subcatchment #25** is made up of a small portion of Winkley Pond Road and the paved apron of the proposed fire cistern. Runoff flows to **Catch Basin #5** (**Pond #C05**) and into **Rain Garden #101** through Drain Manhole #1 (**Pond #D01**).

### 3.0a Stormwater Treatment:

Treatment takes place within the rain garden and infiltration basin designed to support the development on site. Pre-treatment will be provided in the sediment forebay of the infiltration basin and the deep sump catch basins before entering the rain arden. The stormwater quality volume capability is treated within provided treatment area of the practices.

### 3.0b Stormwater Infiltration:

Groundwater recharge volume requirements are satisfied by Infiltration Basin #102 (Pond #102) (Sheet P-102). See Infiltration Feasibility Study also prepared by Berry Surveying & Engineering and published on the same day.

### 3.1 FULL COMPARATIVE ANALYSIS

ANALYSIS COMPONENT: PEAK RATE DISCHARGE (Cubic Feet / Second)

| | | 2 Yr | 10 Yr | 25 Yr | 50 Yr | 100 Yr |
|---|---|---|---|---|---|---|
| Final Reach #100 | Existing | 0.12 | 1.41 | 3.21 | 5.30 | 8.14 |
| | Proposed | 0.11 | 1.08 | 2.28 | 3.62 | 6.14 |

ANALYSIS COMPONENT: VOLUME (Acre Feet)

| | | 2 Yr | 10 Yr | 25 Yr | 50 Yr | 100 Yr |
|---|---|---|---|---|---|---|
| Final Reach #100 | Existing | 0.057 | 0.252 | 0.475 | 0.722 | 1.058 |
| | Proposed | 0.091 | 0.251 | 0.423 | 0.610 | 0.860 |

## 4.0 EROSION and SEDIMENT CONTROL PLAN & BEST MANAGEMENT PRACTICES (BMP's)

Reference: Proposed Site Plan and Grading Plan
Erosion & Sediment Control Plan
Erosion & Sediment Control Details

The proposed site development is protected from erosion and the abutting properties are protected from sediment by the use of Best Management Practices as outlined in the New Hampshire Stormwater Manual, Volume 2, Post-Construction Best Management Practices Selection & Design (December 2008, NHDES & US EPA). Any area disturbed by construction will be re-stabilized within 30 days and abutting properties will not be adversely affected by this development. All swales and drainage structures will be constructed and stabilized prior to having run-off directed to them. Reference is also made to the Stormwater System Management: Inspection & Maintenance Manual and Stormwater Operations, Inspection & Maintenance Plan which has been developed specifically for this project and available to the owner.

### Perimeter Control (Silt Fence / SiltSoxx / Erosion Control Mix Berm)

The plan set demonstrates the location of perimeter sediment control. The Erosion and Sediment Control Details, Sheet E-101, has the specifications for installation and maintenance of the silt fence, Filtrexx mulch filled SiltSoxx (or approved equal), and Erosion Control Mix Berm. There are locations on the site, for example bio-media rain garden protection, where SiltSoxx protection is specified. An area of permanent perimeter control is shown by the well house for wetland buffer protection from steeper slopes.

### Bio-Retention System (Rain-Garden)

Description: A bioretention system (sometimes referred to as a "rain garden") is a type of filtration BMP designed to collect and filter moderate amounts of stormwater runoff using conditioned planting soil beds, gravel beds and vegetation within shallow depressions. The bioretention system may be designed with an underdrain, to collect treated water and convey it to discharge, or it may be designed to infiltrate the treated water directly to the subsoil. Bioretention cells are capable of reducing sediment, nutrients, oil and grease, and trace metals. Bioretention systems should be sited in close proximity to the origin of the stormwater runoff to be treated. The major difference between bioretention systems and other filtration systems is the use of vegetation. A typical surface sand filter is designed to be maintained with no vegetation, whereas a bioretention cell is planted with a variety of shrubs and perennials whose roots assist with pollutant uptake. The use of vegetation allows these systems to blend in with other landscaping features. See SWM Volume 2, 4-3.4c, Treatment Practices, Bio-Retention System, page 110.

Construction Considerations: After the stone and bio-media has been installed, Filtrexx Silt Soxx or approved equal, will be installed at the toe of slope intersection between the berm and bio-media and will remain until the slopes of the berm are stable.

Maintenance Considerations: Systems should be inspected at least twice annually, and following any rainfall event exceeding 2.5 inches in a 24 hour period, with maintenance or rehabilitation conducted as warranted by such inspection. Pretreatment measures should be inspected at least twice annually, and cleaned of accumulated sediment as warranted by inspection, but no less than once annually. Trash and debris should be removed at each inspection. At least once annually, system should be inspected for drawdown time. If bioretention system does not drain within 72-hours following a rainfall event, then a qualified professional should assess the condition of the facility to determine measures required to restore filtration function or infiltration function (as applicable), including but not limited to removal of accumulated sediments or reconstruction of the filter media. Vegetation should be inspected at least annually, and maintained in healthy condition, including pruning, removal and replacement of dead or diseased vegetation, and removal of invasive species. The rain garden is equipped with an underdrain and end cap assembly which will need to be routinely inspected for obstructions.

See the Stormwater Management Inspection and Maintenance Manual for more details.

## In-Ground Infiltration Basin

Description: Infiltration basins are impoundments designed to temporarily store runoff, allowing all or a portion of the water to infiltrate into the ground. An infiltration basin is designed to completely drain between storm events. An infiltration basin is specifically designed to retain and infiltrate the entire Water Quality Volume. Some infiltration basins may infiltrate additional volumes during larger storm events, but many will be designed to release stormwater exceeding the water quality volume from the larger storms. In a properly sited and designed infiltration basin, water quality treatment is provided by runoff pollutants binding to soil particles beneath the basin as water percolates into the subsurface. Biological and chemical processes occurring in the soil also contribute to the breakdown of pollutants. Infiltrated water is used by plants to support growth or it is recharged to the underlying groundwater. As with all impoundment BMPs, surface infiltration basins should be designed with an outlet structure to pass peak flows during a range of storm events, as well as with an emergency spillway to pass peak flows around the embankment during extreme storm events that exceed the combined infiltration capacity and outlet structure capacity of the facility. See SWM Volume 2, 4-3.3b, Treatment Practices, In-Ground Infiltration Basin, page 88.

Maintenance Considerations: Removal of debris from inlet and outlet structures. Removal of accumulated sediment. Inspection and repair of outlet structures and appurtenances. Inspection of infiltration components at least twice annually, and following any rainfall event exceeding 2.5 inches in a 24 hour period, with maintenance or rehabilitation conducted as warranted by such inspection. Inspection of pretreatment measures at least twice annually, and removal of accumulated sediment as warranted by inspection, but no less than once annually. Periodic mowing of embankments. Removal of woody vegetation from embankments. Inspection and repair of embankments and spillways. If an infiltration system does not drain within 72-hours following a rainfall event, then a qualified professional should assess the condition of the facility to determine measures required to restore infiltration function, including but not limited to removal of accumulated sediments or reconstruction of the infiltration trench.

## Vegetated Stabilization

All areas that are disturbed during construction will be stabilized with vegetated material within 30 days of breaking ground. Construction will be managed in such a manner that erosion is prevented and that no abutter's property will be subjected to any siltation, unless otherwise permitted. All areas to be planted with grass for long-term cover will follow the specification and on Sheet E-102 using seeding mixture C, as follows:

| Mixture | Pounds per Acre | Pounds per 1,000 Sq. Ft. |
|---|---|---|
| Tall Fescue | 24 | 0.55 |
| Creeping Red Fescue | 24 | 0.55 |
| **Total** | **48** | **1.10** |

## Conservation Mix

| | | |
|---|---|---|
| Virginia Wild Rye | Native | FACW- |
| Little Bluestem | Native | FACU |
| Big Bluestem | Native | FAC |
| Red Fescue | Native | FACU |
| Switch Grass | Native | FAC |
| Partridge Pea | Native | FACU |
| Showy Tick Trefoil | Native | FAC |
| Butterfly Milkweed | Native | NI |
| Beggar Ticks | Native | FACW |
| Purple Joe Pye Weed | Native | FAC |
| Black Eyed Susan | Native | FACU- |
| **Total** | **25** | **0.57** |

Conservation Mix to be provided by New England Wetland Plants, Inc., Amherst, MA as outline in their New England Conservation / Wildlife Mix or approved equal. Mix to be applied at a rate of 25 lbs. per acre or one-lb. per 1750 square feet. Ratio of seed is proprietary and substitutions are not allowed.

Conservation Mix will used to stabilize all 2:1 slopes and all land area disturbed within the wetland buffer. (If applicable).

## Stabilized Construction Entrance

A temporary gravel construction entrance provides an area where mud can be dislodged from tires before the vehicle leaves the construction site to reduce the amount of mud and sediment transported onto paved municipal and state roads. The stone size for the pad should be 3” coarse aggregate, and the pad itself constructed to a minimum length of 75’ for the full width of the access road. The aggregate should be placed at least six inches thick. A plan view and profile are shown on Sheet E-101- Erosion & Sediment Control Detail Plan. (If applicable).

## Environmental Dust Control

Dust will be controlled on the site by the use of multiple Best Management Practices. Mulching and temporary seeding will be the first line of protection to be utilized where problems occur. If dust problems are not solved by these applications, the use of water and calcium chloride can be applied. Calcium chloride will be applied at a rate that will keep the surface moist but not cause pollution.

## Drainage Swales / Stormwater Conveyance Channels / Conveyance Swales

Description: Conveyance swales are stabilized channels designed to convey runoff at non-erosive velocities. They may be stabilized using vegetation, riprap, or a combination, or with an alternative lining designed to accommodate design flows while protecting the integrity of the sides and bottom of the channel. Conveyance channels may provide incidental water quality benefits, but are not specifically designed to provide treatment. Conveyance swales are not considered a Treatment or Pretreatment Practice under the AoT regulations, unless they are also designed to meet the requirements of an acceptable Treatment/Pretreatment Practice as described elsewhere in this Chapter. See SWM Volume 2, 4-6.3 Conveyance Practices, Conveyance Swale, page 166.

Maintenance Considerations: Grassed channels should be inspected periodically (at least annually) for sediment accumulation, erosion, and condition of surface lining (vegetation or riprap). Repairs, including stone or vegetation replacement, should be made based on this inspection. Remove sediment and debris annually, or more frequently as warranted by inspection. Mow vegetated channels based on frequency specified by design. Mowing at least once per year is required to control establishment of woody vegetation. It is recommended to cut grass no shorter than 4 inches.

## Construction Sequence

1. Cut and remove trees in construction area only as required.

2. Construct and/or install temporary and permanent sediment erosion and detention control facilities as specified. Erosion and sediment control measures shall be installed prior to any soil land disturbance and must be reviewed and approved by the community services department.

3. Erosion, sediment and detention control facility shall be installed & stabilized prior to directing runoff to them, temporary diversions may be required. Post construction storm water management practices must be initiated and stabilized early in the process.

4. Clear, cut and dispose of debris in approved facility.

5. Construct temporary water diversions (swales, basins, etc.) as needed until site is stabilized.

6. All swales are to be installed prior to rough grading of the site. Temporary water diversion (swales, etc.) must be used as necessary until areas are stabilized.

7. Construct roadways for access to desired construction areas. All roads shall be stabilized immediately.

8. Install pipe and construction associated appurtenances as required or directed. Install rain gardens. All disturbed areas shall stabilized immediately after grading.

9. Begin permanent and temporary seeding and mulching. All cut and fill slopes and disturbed areas shall be seeded or mulched as required, or directed. Any area disturbed by construction will be re-stabilized within 45 days (Env-Wq 1504.16) and abutting properties will not be adversely affected by this development. All swales and drainage structures will be constructed and stabilized prior to having run-off directed to them. Iaw EPA 2022 CGP 2.2.14, site stabilization will be initiated immediately in any areas of exposed soil where construction activities have permanently ceased or will be temporarily inactive for 14 or more calendar days. The installation of stabilization will be completed as soon as practicable but no later than 14 calendar days. All roadways and parking areas shall be stabilized within 72 hours of achieving finished grades. All cut and fill slopes shall be stabilized within 72 hours of achieving finished grades.

10. Construct temporary berms, drains ditches, silt fences, sediment traps, etc. Mulch and seed as required.

11. Inspect and maintain all erosion and sediment control measures during construction. All SWPPP inspections must be conducted by a qualified professional such as a professional engineer (PE), a certified professional in erosion and sediment control (CPESC), a certified erosion sediment and storm water inspector (CESSWI), or a certified professional in storm water quality (CPSWQ). Inspection reports shall be submitted to the community services department. Inspections shall be conducted weekly and within 24 hours of a 0.25 inch rain event.

12. Complete permanent seeding and landscaping.

13. Remove temporary erosion control measures after seeding areas have established themselves and site improvements are complete.

14. Smooth and revegetate all disturbed areas. Stabilization should occur within 14 days or removing temporary measures.

15. Finish graveling all roadways.

## Temporary Erosion Control Measures

1. The smallest practical area of land shall be exposed at any one time.

2. Erosion, sediment control measures shall be installed as shown on the plans and at locations as required, or directed by the engineer.

3. All disturbed areas shall be returned to original grades and elevations. Disturbed areas shall be loamed with a minimum of 4" of loam and seeded with not less than 1.10 pound of seed per 1,000 square feet (48 pounds per acre) of area.

4. Silt fences and other barriers shall be inspected periodically and after every rainstorm during the life of the project. All damaged areas shall be repaired, sediment deposits shall periodically be removed and properly disposed of.

5. After all disturbed areas have been stabilized, the temporary erosion control measures are to be removed and the area disturbed by the removal smoothed and re-vegetated.

6. Areas must be seeded and mulched within 5 days of final grading, permanently stabilized within 15 days of final grading, or temporarily stabilized within 30 days of initial disturbance of soil.

### Inspection and Maintenance Schedule

Perimeter control and catch basin inlet protection will be inspected during and after storm events of 0.25" or greaterto ensure that the BMP still has integrity and is not allowing sediment to pass. Depending on SWPPP criteria, all BMP controls will be inspected once every 7 days and after storm events. Inspection reports must be submitted to Town of Barrington Planning Department. See also Stormwater System Management: Inspection and Maintenance Manual with accompanying plan published separately also by Berry Surveying & Engineering. See also Storm Water Pollution Prevention Plan (SWPPP) developed in accordance with EPA NPDES requirements & the Town of Barrington Stormwater regulations.

Corrective Action measures will be made in accordance with SWPPP requirements and records maintained on site by the Contractor.

## 5.0 CONCLUSION

Peak rates of runoff flow are modeled to be reduced in the post-construction analysis, as compared to the pre-construction analysis. This reduction occurs at all storm events due to the installation of the low impact development stormwater devices.

The volume of stormwater discharge from the site at the final reach is minimally increased in the 2 Yr.-24 Hr. and reduced in all other events due to construction grading, the retention in the rain garden, and infiltration in the infiltration basin. The 2Yr.-24Hr. volume increase is less than 0.100 acre feet, allowed by NHDES AoT Bureau for Channel Protection Volume purposes.

A Site Specific, Terrain Alteration Permit (RSA 485: A-17) is not required for this site plan due to the area of disturbance being less than 100,000 SF. The impact is approximately 53,500 square feet, so that an EPA Notice of Intent will be required to be filed prior to construction and a Stormwater Pollution Prevention Plan prepared.

Respectfully Submitted,
BERRY SURVEYING & ENGINEERING

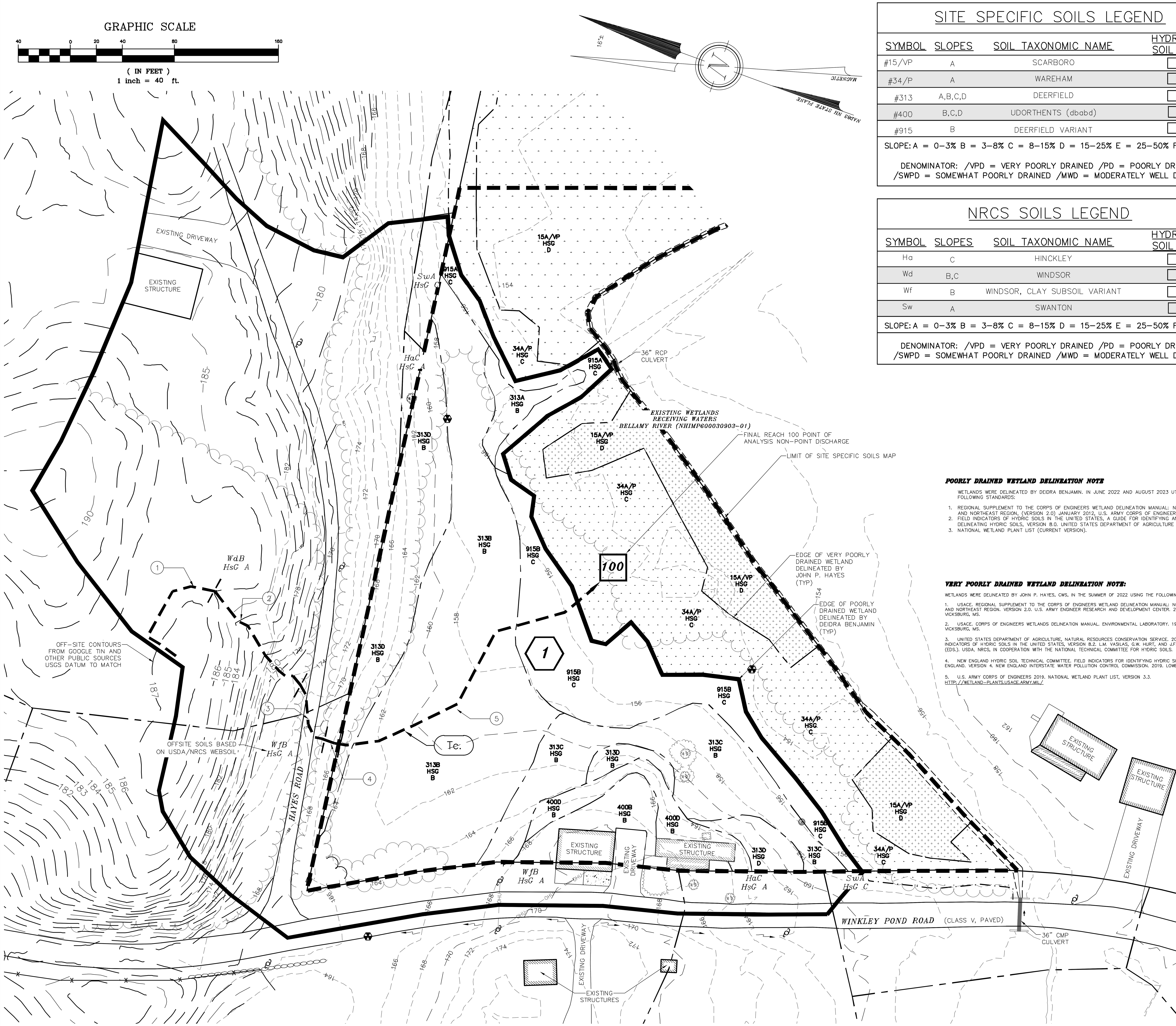
Christopher R. Berry, SIT 567
Principal, President

Kenneth A. Berry PE, LLS,
CPSWQ, CPESC, CESSWI
Principal, VP - Technical Operations

Kevin R. Poulin, PE
Design Engineer

## **Appendix I –**Existing Conditions Analysis

25 Yr - 24 Hr. Full Summary
2 Yr - 24 Hr. Node Listing
10 Yr -24 Hr. Node Listing
25 Yr -24 Hr. Node Listing
50 Yr - 24 Hr. Node Listing
100 Yr -24 Hr. Node Listing




## SITE SPECIFIC SOILS LEGEND

| SYMBOL | SLOPES | SOIL TAXONOMIC NAME | HYDROLOGIC SOIL GROUP |
|---|---|---|---|
| #15/VP | A | SCARBORO | D |
| #34/P | A | WAREHAM | C |
| #313 | A,B,C,D | DEERFIELD | B |
| #400 | B,C,D | UDORTHENTS (dbabd) | B |
| #915 | B | DEERFIELD VARIANT | C |

SLOPE: A = 0–3% B = 3–8% C = 8–15% D = 15–25% E = 25–50% F = 50%+

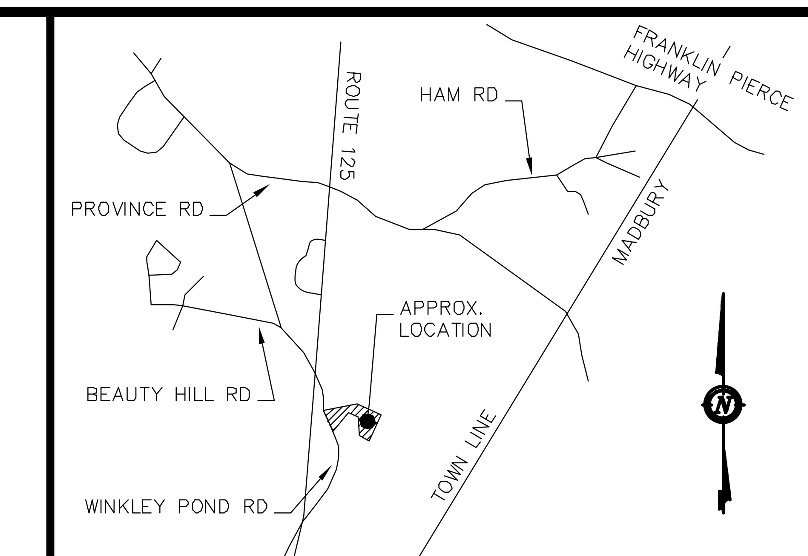
DENOMINATOR: /VPD = VERY POORLY DRAINED /PD = POORLY DRAINED /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED

## NRCS SOILS LEGEND

| SYMBOL | SLOPES | SOIL TAXONOMIC NAME | HYDROLOGIC SOIL GROUP |
|---|---|---|---|
| Ha | C | HINCKLEY | A |
| Wd | B,C | WINDSOR | A |
| Wf | B | WINDSOR, CLAY SUBSOIL VARIANT | A |
| Sw | A | SWANTON | C |

SLOPE: A = 0–3% B = 3–8% C = 8–15% D = 15–25% E = 25–50% F = 50%+

DENOMINATOR: /VPD = VERY POORLY DRAINED /PD = POORLY DRAINED /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED



LOCUS MAP
BARRINGTON, N.H.
(NOT TO SCALE)

## NOTES:

1.) OWNER: HAMBONE LLC
242 CENTRAL AVE
DOVER, NH 03820

2.) TAX MAP: TAX MAP 253, LOT 14

3.) LOT AREA: 586,793 Sq. Ft., 13.47 Ac.
330,912 Sq.Ft., 7.60 Ac., TOTAL UPLAND

4.) S.C.R.D. BOOK 4976, PAGE 1023

5.) I HEREBY CERTIFY THAT, TO THE BEST OF MY KNOWLEDGE & BELIEF, A PORTION OF THIS PARCEL FALLS WITHIN THE FLOOD PLAIN FLOOD HAZARD REF.: FEMA, COMMUNITY# 330178, MAP# 33017C0305E, DATED: SEPTEMBER 30, 2015.

6.) VERTICAL DATUM BASED ON NAVD88 ELEVATIONS. HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED USING CARLSON BRX7 SURVEY GRADE GPS RECEIVERS.

7.) THE INTENT OF THIS PLAN IS TO SHOW THE EXISTING DRAINAGE CONDITIONS OF TAX MAP 253, LOT 14 AS OF THE DATE OF THE SURVEY.

8.) HYDROCAD USES A SERIES OF NODE SUFFIXES FOR NUMBERING PURPOSES (S=SUBCATCHMENT, P=POND DEVICE, R=REACH), TO SIMPLIFY ANNOTATION THESE SUFFIXES ARE LEFT OFF THE WATERSHED PLANS AND NODE TYPE IS DENOTED BY THE SYMBOL SHAPE ACCORDING TO THE DISPLAYED LEGEND WHICH COINCIDES WITH HYDROCAD GRAPHICS.

### POORLY DRAINED WETLAND DELINEATION NOTE

WETLANDS WERE DELINEATED BY DEIDRA BENJAMIN. IN JUNE 2022 AND AUGUST 2023 UTILIZING THE FOLLOWING STANDARDS:

1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

### VERY POORLY DRAINED WETLAND DELINEATION NOTE:

WETLANDS WERE DELINEATED BY JOHN P. HAYES, CWS, IN THE SUMMER OF 2022 USING THE FOLLOWING CRITERIA:

1. USACE. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION. VERSION 2.0. U.S. ARMY ENGINEER RESEARCH AND DEVELOPMENT CENTER. 2012. VICKSBURG, MS.

2. USACE. CORPS OF ENGINEERS WETLANDS DELINEATION MANUAL. ENVIRONMENTAL LABORATORY. 1987. VICKSBURG, MS.

3. UNITED STATES DEPARTMENT OF AGRICULTURE, NATURAL RESOURCES CONSERVATION SERVICE. 2018. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, VERSION 8.2. L.M. VASILAS, G.W. HURT, AND J.F. BERKOWITZ (EDS.). USDA, NRCS, IN COOPERATION WITH THE NATIONAL TECHNICAL COMMITTEE FOR HYDRIC SOILS.

4. NEW ENGLAND HYDRIC SOIL TECHNICAL COMMITTEE. FIELD INDICATORS FOR IDENTIFYING HYDRIC SOILS IN NEW ENGLAND. VERSION 4. NEW ENGLAND INTERSTATE WATER POLLUTION CONTROL COMMISSION. 2019. LOWELL, MA.

5. U.S. ARMY CORPS OF ENGINEERS 2019. NATIONAL WETLAND PLANT LIST, VERSION 3.3. HTTP://WETLAND-PLANTS.USACE.ARMY.MIL/

STATE OF NEW HAMPSHIRE DEIDRA L. BENJAMIN No. 295 CERTIFIED WETLAND SCIENTIST

DEIDRA BENJAMIN, CWS #295

JOHN P. HAYES III No. 087 CERTIFIED SOIL SCIENTIST

JOHN P. HAYES, III CSS #87

STATE OF NEW HAMPSHIRE JOHN P. HAYES, III CERTIFIED WETLAND SCIENTIST

JOHN P. HAYES III, CWS #18

### LEGEND:

- EXISTING CONTOUR MINOR (299)
- EXISTING CONTOUR MAJOR (300)
- STONE WALL
- WETLAND LINE
- PROPERTY LINE
- SOIL LINE
- SOIL SERIES (448A)
- NRCS SOIL LINE
- NRCS SOIL LABEL (HfB)
- LIMIT OF WATERSHED/SUBCATCHMENT
- TIME OF CONCENTRATION PATH
- FLOW REACH
- MATCH LINE
- S.C.R.D. STRAFFORD COUNTY REGISTRY OF DEEDS
- TYP. TYPICAL
- FND FOUND
- TBR TO BE REMOVED

### SYMBOLS LEGEND:

- # SUBCATCHMENT AREA SYMBOL
- # FLOW REACH SYMBOL
- # POND DEVICE SYMBOL
- Tc. # TIME OF CONCENTRATION SEGMENT

| REVISION | DATE | DESCRIPTION |
|---|---|---|
| | | |

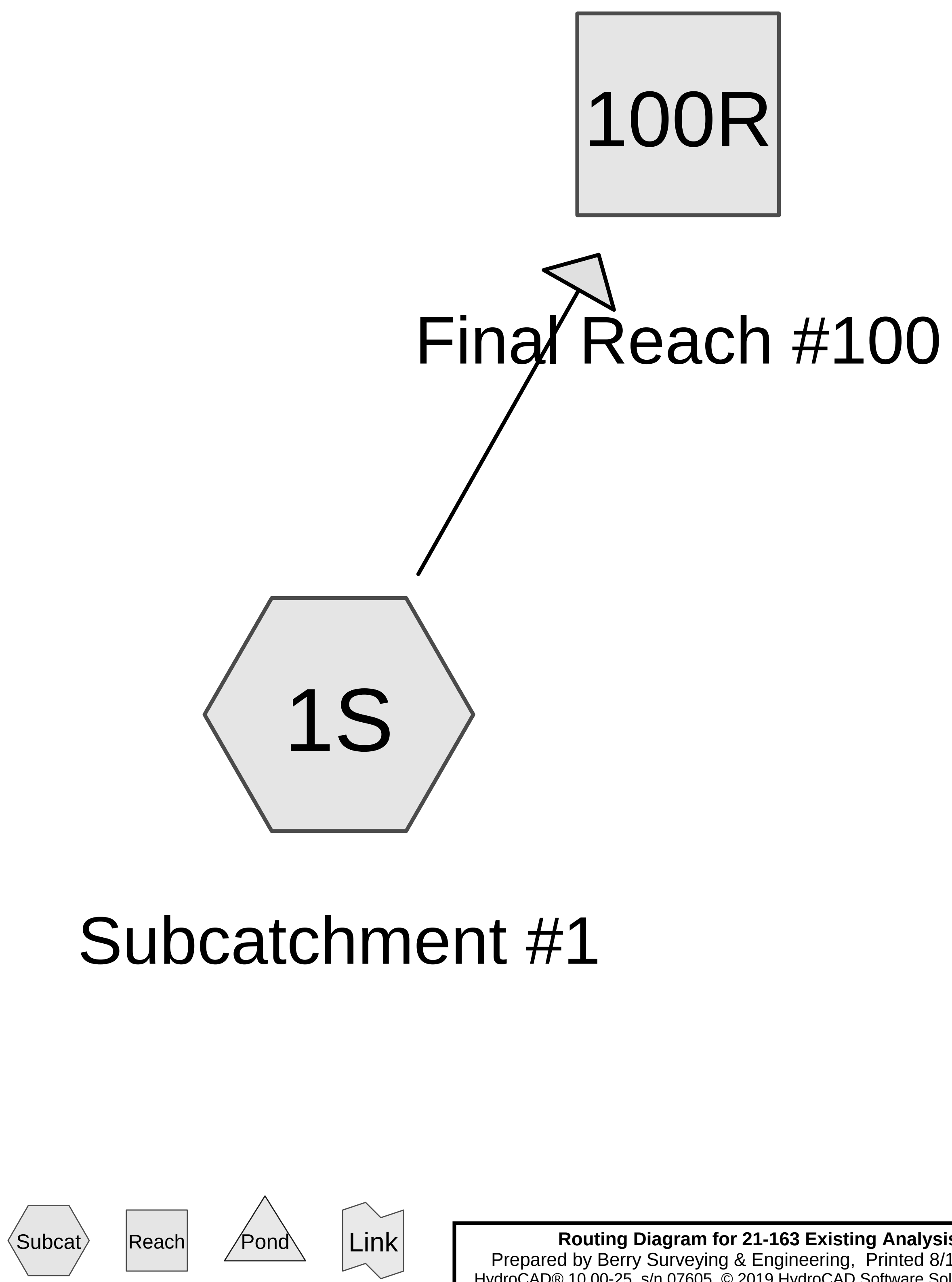
SWPPP EPA SITE MAP (EXISTING)

W-1 EXISTING WATERSHED CONDITIONS PLAN
LAND OF
HAMBONE LLC
49 WINKLEY POND ROAD
BARRINGTON, N.H.
*TAX MAP 253, LOT 14*

BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863

SCALE : 1 IN. EQUALS 40 FT.
DATE : JULY 16, 2023
FILE NO. : DB 2021-163

STATE OF NEW HAMPSHIRE KENNETH A. BERRY No. 14246 LICENSED PROFESSIONAL ENGINEER




**Routing Diagram for 21-163 Existing Analysis**
Prepared by Berry Surveying & Engineering, Printed 8/14/2023

## Area Listing (all nodes)

| Area (acres) | CN | Description (subcatchment-numbers) |
|---|---|---|
| 0.930 | 39 | >75% Grass cover, Good, HSG A (1S) |
| 1.319 | 61 | >75% Grass cover, Good, HSG B (1S) |
| 0.326 | 74 | >75% Grass cover, Good, HSG C (1S) |
| 0.220 | 96 | Gravel surface, HSG A (1S) |
| 0.015 | 96 | Gravel surface, HSG B (1S) |
| 0.095 | 98 | Paved parking, HSG A (1S) |
| 0.000 | 98 | Paved parking, HSG C (1S) |
| 0.058 | 98 | Roofs, HSG A (1S) |
| 0.051 | 98 | Roofs, HSG B (1S) |
| 1.360 | 30 | Woods, Good, HSG A (1S) |
| 0.264 | 55 | Woods, Good, HSG B (1S) |
| 0.110 | 70 | Woods, Good, HSG C (1S) |
| **4.746** | **52** | **TOTAL AREA** |

## Soil Listing (all nodes)

| Area (acres) | Soil Group | Subcatchment Numbers |
|---|---|---|
| 2.663 | HSG A | 1S |
| 1.648 | HSG B | 1S |
| 0.436 | HSG C | 1S |
| 0.000 | HSG D | |
| 0.000 | Other | |
| **4.746** | | **TOTAL AREA** |

## Ground Covers (all nodes)

| HSG-A (acres) | HSG-B (acres) | HSG-C (acres) | HSG-D (acres) | Other (acres) | Total (acres) | Ground Cover | Subcatchment Numbers |
|---|---|---|---|---|---|---|---|
| 0.930 | 1.319 | 0.326 | 0.000 | 0.000 | 2.574 | >75% Grass cover, Good | 1S |
| 0.220 | 0.015 | 0.000 | 0.000 | 0.000 | 0.235 | Gravel surface | 1S |
| 0.095 | 0.000 | 0.000 | 0.000 | 0.000 | 0.096 | Paved parking | 1S |
| 0.058 | 0.051 | 0.000 | 0.000 | 0.000 | 0.109 | Roofs | 1S |
| 1.360 | 0.264 | 0.110 | 0.000 | 0.000 | 1.733 | Woods, Good | 1S |
| **2.663** | **1.648** | **0.436** | **0.000** | **0.000** | **4.746** | **TOTAL AREA** | |

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=206,757 sf 4.31% Impervious Runoff Depth>1.20"
Flow Length=508' Tc=28.8 min CN=52 Runoff=3.21 cfs 0.475 af

**Reach 100R: Final Reach #100** Inflow=3.21 cfs 0.475 af
Outflow=3.21 cfs 0.475 af

**Total Runoff Area = 4.746 ac Runoff Volume = 0.475 af Average Runoff Depth = 1.20"**
**95.69% Pervious = 4.542 ac 4.31% Impervious = 0.205 ac**

## Summary for Subcatchment 1S: Subcatchment #1

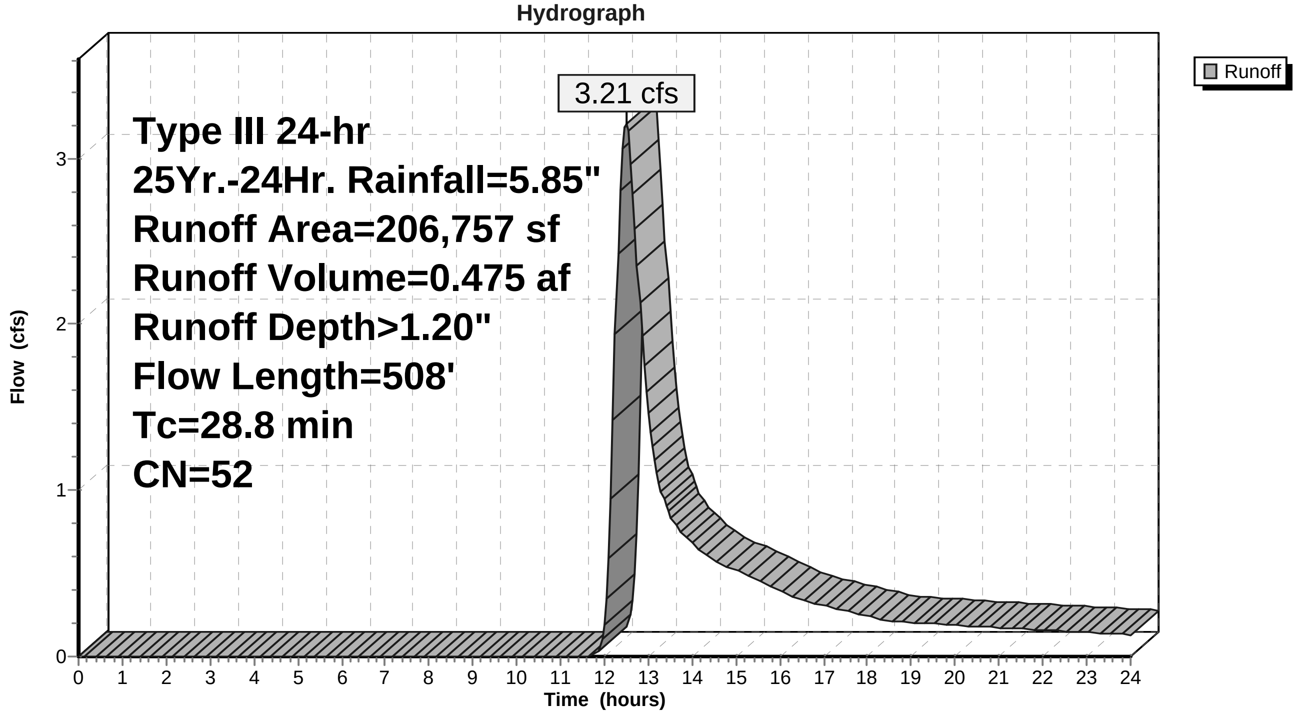
Runoff = 3.21 cfs @ 12.48 hrs, Volume= 0.475 af, Depth> 1.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25Yr.-24Hr. Rainfall=5.85"

| Area (sf) | CN | Description |
|---|---|---|
| 40,505 | 39 | >75% Grass cover, Good, HSG A |
| 57,435 | 61 | >75% Grass cover, Good, HSG B |
| 14,195 | 74 | >75% Grass cover, Good, HSG C |
| 4,152 | 98 | Paved parking, HSG A |
| 8 | 98 | Paved parking, HSG C |
| 2,534 | 98 | Roofs, HSG A |
| 2,217 | 98 | Roofs, HSG B |
| 9,565 | 96 | Gravel surface, HSG A |
| 653 | 96 | Gravel surface, HSG B |
| 59,229 | 30 | Woods, Good, HSG A |
| 11,485 | 55 | Woods, Good, HSG B |
| 4,779 | 70 | Woods, Good, HSG C |
| 206,757 | 52 | Weighted Average |
| 197,846 | | 95.69% Pervious Area |
| 8,911 | | 4.31% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 24.6 | 100 | 0.0150 | 0.07 | | **Sheet Flow, Segment #1**<br>Woods: Light underbrush n= 0.400 P2= 3.08" |
| 1.0 | 102 | 0.1176 | 1.71 | | **Shallow Concentrated Flow, Segment #2**<br>Woodland Kv= 5.0 fps |
| 0.2 | 50 | 0.0800 | 4.55 | | **Shallow Concentrated Flow, Segment #3**<br>Unpaved Kv= 16.1 fps |
| 0.1 | 13 | 0.2300 | 2.40 | | **Shallow Concentrated Flow, Segment #4**<br>Woodland Kv= 5.0 fps |
| 2.9 | 243 | 0.0391 | 1.38 | | **Shallow Concentrated Flow, Segment #5**<br>Short Grass Pasture Kv= 7.0 fps |
| 28.8 | 508 | Total | | | |

## Subcatchment 1S: Subcatchment #1



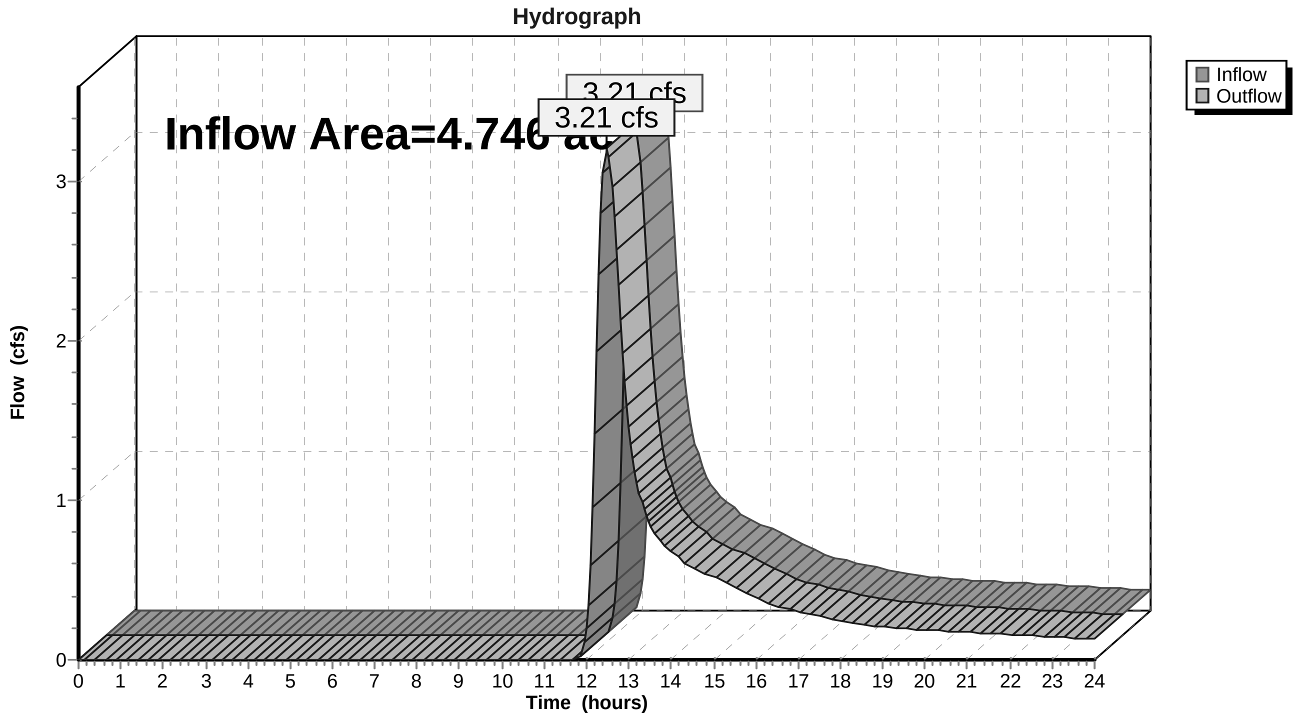
## Summary for Reach 100R: Final Reach #100

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 4.746 ac, 4.31% Impervious, Inflow Depth > 1.20" for 25Yr.-24Hr. event
Inflow = 3.21 cfs @ 12.48 hrs, Volume= 0.475 af
Outflow = 3.21 cfs @ 12.48 hrs, Volume= 0.475 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

### Reach 100R: Final Reach #100



Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=206,757 sf 4.31% Impervious Runoff Depth>0.14"
Flow Length=508' Tc=28.8 min CN=52 Runoff=0.12 cfs 0.057 af

**Reach 100R: Final Reach #100** Inflow=0.12 cfs 0.057 af
Outflow=0.12 cfs 0.057 af

**Total Runoff Area = 4.746 ac Runoff Volume = 0.057 af Average Runoff Depth = 0.14"**
**95.69% Pervious = 4.542 ac 4.31% Impervious = 0.205 ac**

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=206,757 sf 4.31% Impervious Runoff Depth>0.64"
Flow Length=508' Tc=28.8 min CN=52 Runoff=1.41 cfs 0.252 af

**Reach 100R: Final Reach #100** Inflow=1.41 cfs 0.252 af
Outflow=1.41 cfs 0.252 af

**Total Runoff Area = 4.746 ac Runoff Volume = 0.252 af Average Runoff Depth = 0.64"**
**95.69% Pervious = 4.542 ac 4.31% Impervious = 0.205 ac**

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=206,757 sf 4.31% Impervious Runoff Depth>1.20"
Flow Length=508' Tc=28.8 min CN=52 Runoff=3.21 cfs 0.475 af

**Reach 100R: Final Reach #100** Inflow=3.21 cfs 0.475 af
Outflow=3.21 cfs 0.475 af

**Total Runoff Area = 4.746 ac Runoff Volume = 0.475 af Average Runoff Depth = 1.20"**
**95.69% Pervious = 4.542 ac 4.31% Impervious = 0.205 ac**

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=206,757 sf 4.31% Impervious Runoff Depth>1.83"
Flow Length=508' Tc=28.8 min CN=52 Runoff=5.30 cfs 0.722 af

**Reach 100R: Final Reach #100** Inflow=5.30 cfs 0.722 af
Outflow=5.30 cfs 0.722 af

**Total Runoff Area = 4.746 ac Runoff Volume = 0.722 af Average Runoff Depth = 1.83"**
**95.69% Pervious = 4.542 ac 4.31% Impervious = 0.205 ac**

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=206,757 sf 4.31% Impervious Runoff Depth>2.67"
Flow Length=508' Tc=28.8 min CN=52 Runoff=8.14 cfs 1.058 af

**Reach 100R: Final Reach #100** Inflow=8.14 cfs 1.058 af
Outflow=8.14 cfs 1.058 af

**Total Runoff Area = 4.746 ac Runoff Volume = 1.058 af Average Runoff Depth = 2.67"**
**95.69% Pervious = 4.542 ac 4.31% Impervious = 0.205 ac**

**Appendix II -** Proposed Conditions Analysis

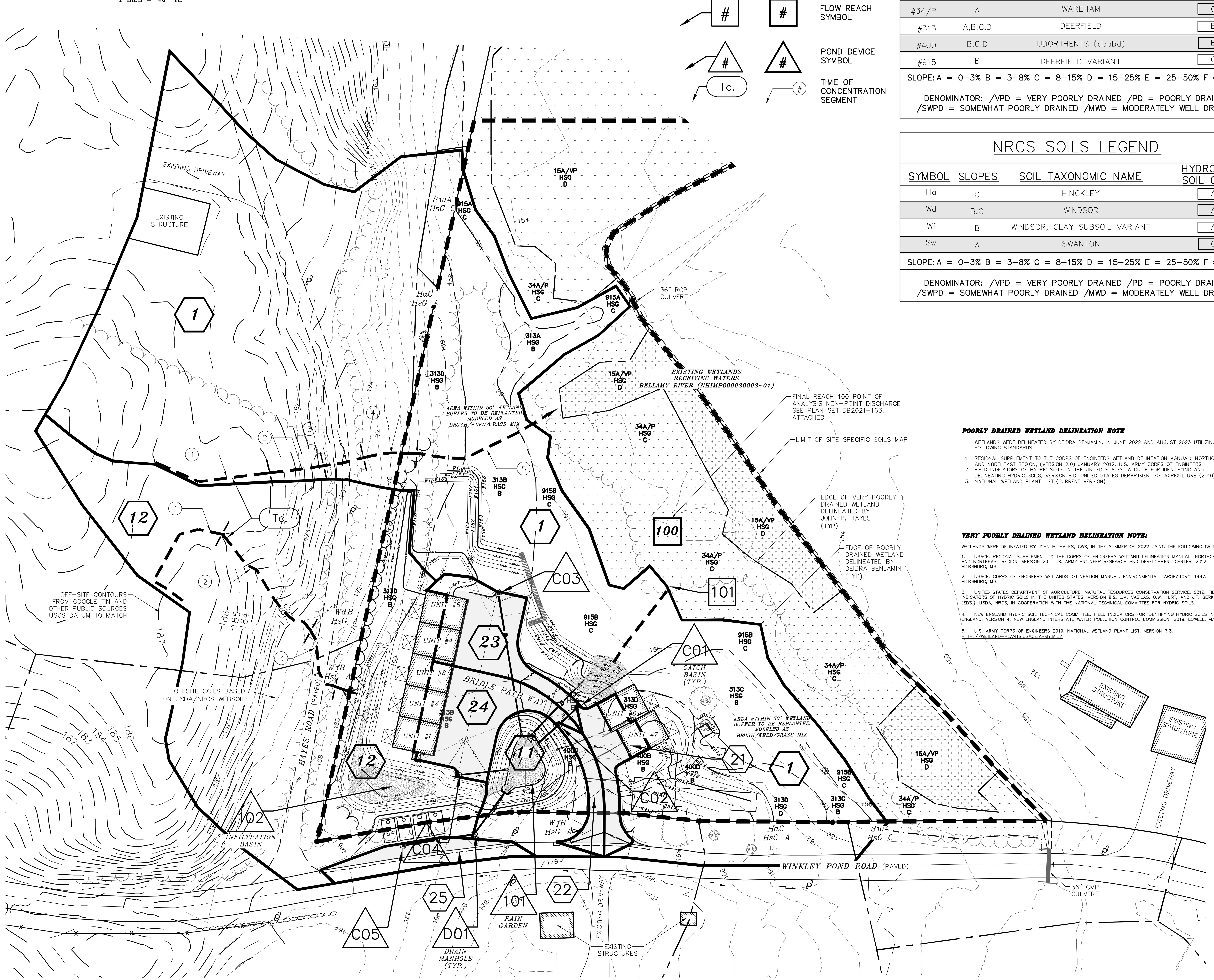
25 Yr - 24 Hr. Full Summary
2 Yr - 24 Hr. Node Listing
10 Yr -24 Hr. Node Listing
25 Yr -24 Hr. Node Listing
50 Yr - 24 Hr. Node Listing
100 Yr -24 Hr. Node Listing

GRAPHIC SCALE

( IN FEET )
1 inch = 40 ft.

**SYMBOLS LEGEND:**

- SUBCATCHMENT AREA SYMBOL
- FLOW REACH SYMBOL
- POND DEVICE SYMBOL
- TIME OF CONCENTRATION SEGMENT




## SITE SPECIFIC SOILS LEGEND

| SYMBOL | SLOPES | SOIL TAXONOMIC NAME | HYDROLOGIC SOIL GROUP |
|---|---|---|---|
| #15/VP | A | SCARBORO | D |
| #34/P | A | WAREHAM | C |
| #313 | A,B,C,D | DEERFIELD | B |
| #400 | B,C,D | UDORTHENTS (dbabd) | B |
| #915 | B | DEERFIELD VARIANT | C |

SLOPE: A = 0–3% B = 3–8% C = 8–15% D = 15–25% E = 25–50% F = 50%+

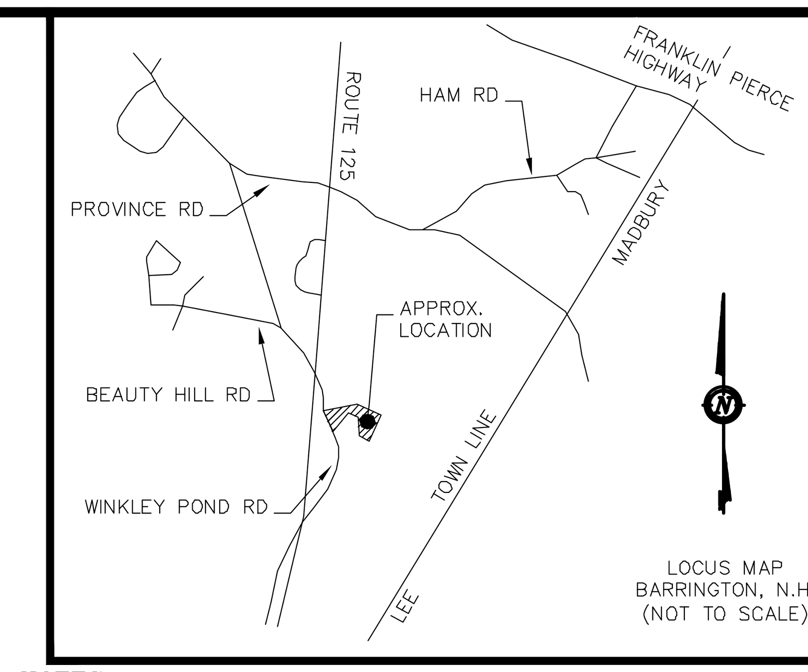
DENOMINATOR: /VPD = VERY POORLY DRAINED /PD = POORLY DRAINED /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED

## NRCS SOILS LEGEND

| SYMBOL | SLOPES | SOIL TAXONOMIC NAME | HYDROLOGIC SOIL GROUP |
|---|---|---|---|
| Ha | C | HINCKLEY | A |
| Wd | B,C | WINDSOR | A |
| Wf | B | WINDSOR, CLAY SUBSOIL VARIANT | A |
| Sw | A | SWANTON | C |

SLOPE: A = 0–3% B = 3–8% C = 8–15% D = 15–25% E = 25–50% F = 50%+

DENOMINATOR: /VPD = VERY POORLY DRAINED /PD = POORLY DRAINED /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED




***NOTES:***

1.) OWNER: HAMBONE LLC, 242 CENTRAL AVE, DOVER, NH 03820

2.) TAX MAP: TAX MAP 253, LOT 14

3.) LOT AREA: 586,793 Sq. Ft., 13.47 Ac.; 330,912 Sq.Ft., 7.60 Ac., TOTAL UPLAND

4.) S.C.R.D. BOOK 4976, PAGE 1023

5.) I HEREBY CERTIFY THAT, TO THE BEST OF MY KNOWLEDGE & BELIEF, A PORTION OF THIS PARCEL FALLS WITHIN THE FLOOD PLAIN FLOOD HAZARD REF.: FEMA, COMMUNITY# 330178, MAP# 33017C0305E, DATED: SEPTEMBER 30, 2015.

6.) VERTICAL DATUM BASED ON NAVD88 ELEVATIONS. HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED USING CARLSON BRX7 SURVEY GRADE GPS RECEIVERS.

7.) THE INTENT OF THIS PLAN IS TO SHOW THE POST CONSTRUCTION DRAINAGE CONDITIONS OF TAX MAP 253, LOT 14.

8.) SEE PROPOSED GRADING & DRAINAGE PLAN FOR SLOPES & EROSION & SEDIMENT CONTROL PLAN FOR STOCKPILE AREA AND CONSTRUCTION ENTRANCE.

9.) HYDROCAD USES A SERIES OF NODE SUFFIXES FOR NUMBERING PURPOSES (S=SUBCATCHMENT, P=POND DEVICE, R=REACH), TO SIMPLIFY ANNOTATION THESE SUFFIXES ARE LEFT OFF THE WATERSHED PLANS AND NODE TYPE IS DENOTED BY THE SYMBOL SHAPE ACCORDING TO THE DISPLAYED LEGEND WHICH COINCIDES WITH HYDROCAD GRAPHICS.

***POORLY DRAINED WETLAND DELINEATION NOTE***

WETLANDS WERE DELINEATED BY DEIDRA BENJAMIN. IN JUNE 2022 AND AUGUST 2023 UTILIZING THE FOLLOWING STANDARDS:

1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

***VERY POORLY DRAINED WETLAND DELINEATION NOTE:***

WETLANDS WERE DELINEATED BY JOHN P. HAYES, CWS, IN THE SUMMER OF 2022 USING THE FOLLOWING CRITERIA:

1. USACE. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION. VERSION 2.0. U.S. ARMY ENGINEER RESEARCH AND DEVELOPMENT CENTER. 2012. VICKSBURG, MS.

2. USACE. CORPS OF ENGINEERS WETLANDS DELINEATION MANUAL. ENVIRONMENTAL LABORATORY. 1987. VICKSBURG, MS.

3. UNITED STATES DEPARTMENT OF AGRICULTURE, NATURAL RESOURCES CONSERVATION SERVICE. 2018. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, VERSION 8.2. L.M. VASILAS, G.W. HURT, AND J.F. BERKOWITZ (EDS.). USDA, NRCS, IN COOPERATION WITH THE NATIONAL TECHNICAL COMMITTEE FOR HYDRIC SOILS.

4. NEW ENGLAND HYDRIC SOIL TECHNICAL COMMITTEE. FIELD INDICATORS FOR IDENTIFYING HYDRIC SOILS IN NEW ENGLAND. VERSION 4. NEW ENGLAND INTERSTATE WATER POLLUTION CONTROL COMMISSION. 2019. LOWELL, MA.

5. U.S. ARMY CORPS OF ENGINEERS 2019. NATIONAL WETLAND PLANT LIST, VERSION 3.3. HTTP://WETLAND-PLANTS.USACE.ARMY.MIL/

STATE OF NEW HAMPSHIRE – DEIDRA L. BENJAMIN – No. 295 – CERTIFIED WETLAND SCIENTIST

DEIDRA BENJAMIN, CWS #295

STATE OF NEW HAMPSHIRE – JOHN P. HAYES III – No. 087 – CERTIFIED SOIL SCIENTIST

JOHN P. HAYES, III CSS #87

STATE OF NEW HAMPSHIRE – JOHN P. HAYES III – No. 18 – CERTIFIED WETLAND SCIENTIST

JOHN P. HAYES III, CWS #18

***LEGEND:***

- EXISTING CONTOUR MINOR
- EXISTING CONTOUR MAJOR
- STONE WALL
- WETLAND LINE
- PROPERTY LINE
- SOIL LINE
- SOIL SERIES (448A)
- NRCS SOIL LINE
- NRCS SOIL LABEL (HfB)
- LIMIT OF WATERSHED/SUBCATCHMENT
- TIME OF CONCENTRATION PATH
- FLOW REACH
- MATCH LINE
- S.C.R.D. STRAFFORD COUNTY REGISTRY OF DEEDS
- TYP. TYPICAL
- FND FOUND
- TBR TO BE REMOVED
- DRAIN MANHOLE W/STRUCTURE
- CATCH BASIN W/ STRUCTURE
- STORMWATER BMP OUTLET STRUCTURE
- DRAIN CULVERT W/ FLARED END SECTION (F.E.S.)
- UNDERDRAIN (U.D)

| REVISION | DATE | DESCRIPTION |
|---|---|---|
| | | |

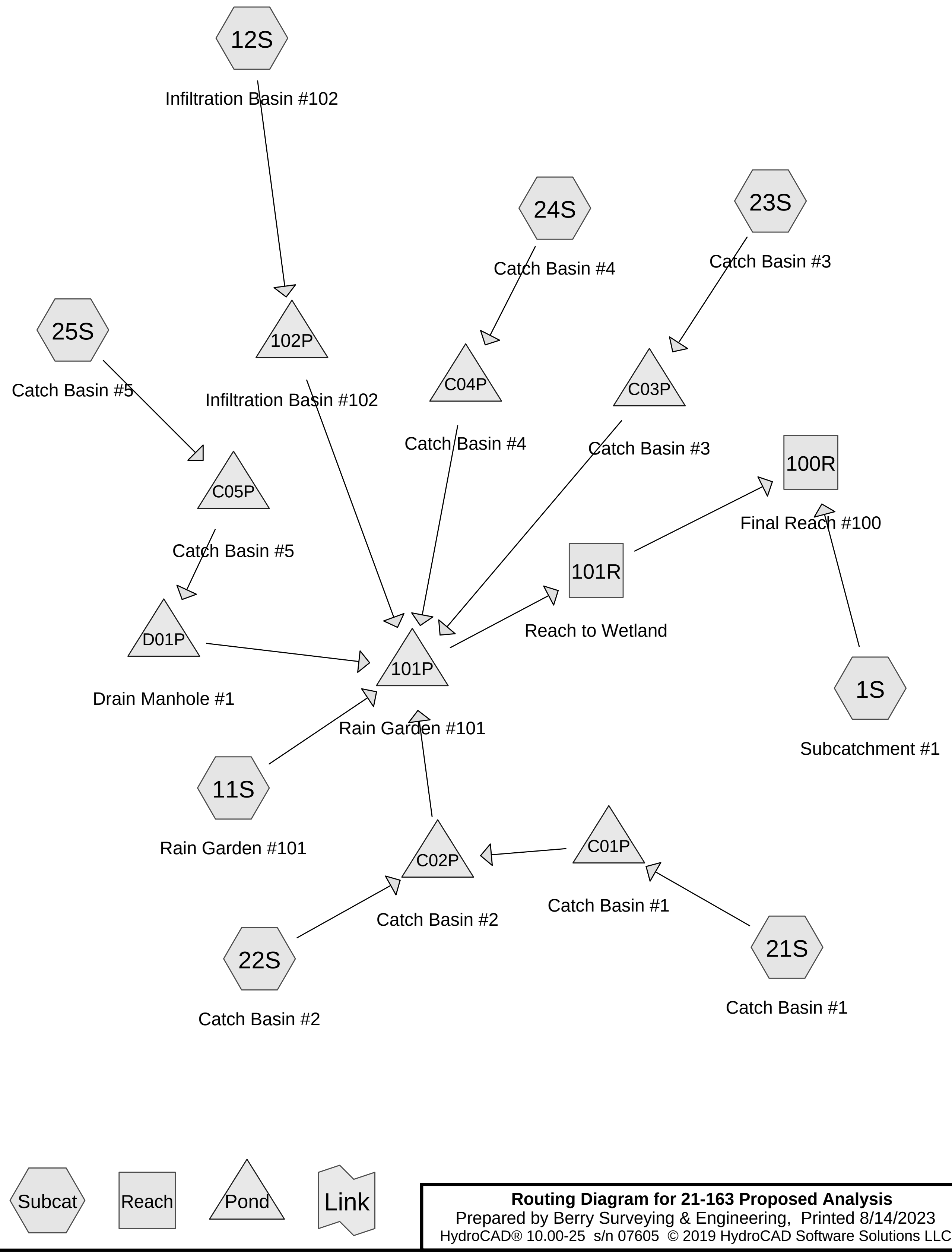
SWPPP EPA SITE MAP (PROPOSED)

W-2 PROPOSED WATERSHED CONDITIONS PLAN
LAND OF
HAMBONE LLC
49 WINKLEY POND ROAD
BARRINGTON, N.H.
*TAX MAP 253, LOT 14*


BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863


SCALE : 1 IN. EQUALS 40 FT.
DATE : JULY 16, 2023
FILE NO. : DB 2021-163

STATE OF NEW HAMPSHIRE – KENNETH A. BERRY – No. 12746 – LICENSED PROFESSIONAL ENGINEER




**Routing Diagram for 21-163 Proposed Analysis**
Prepared by Berry Surveying & Engineering, Printed 8/14/2023

## Area Listing (all nodes)

| Area (acres) | CN | Description (subcatchment-numbers) |
|---|---|---|
| 0.919 | 39 | >75% Grass cover, Good, HSG A (1S, 11S, 12S) |
| 0.814 | 61 | >75% Grass cover, Good, HSG B (1S, 11S, 12S, 23S) |
| 0.010 | 74 | >75% Grass cover, Good, HSG C (1S) |
| 0.303 | 48 | Brush, Good, HSG B (1S) |
| 0.316 | 65 | Brush, Good, HSG C (1S) |
| 0.213 | 96 | Gravel surface, HSG A (1S, 11S, 12S) |
| 0.018 | 96 | Gravel surface, HSG B (1S, 11S, 12S, 23S) |
| 0.129 | 98 | Paved parking, HSG A (1S, 11S, 21S, 22S, 25S) |
| 0.226 | 98 | Paved parking, HSG B (21S, 22S, 23S, 24S) |
| 0.000 | 98 | Paved parking, HSG C (1S) |
| 0.047 | 98 | Roofs, HSG A (1S) |
| 0.140 | 98 | Roofs, HSG B (1S, 12S, 21S, 23S, 24S) |
| 1.355 | 30 | Woods, Good, HSG A (1S, 12S) |
| 0.145 | 55 | Woods, Good, HSG B (1S, 12S) |
| 0.110 | 70 | Woods, Good, HSG C (1S) |
| **4.746** | **53** | **TOTAL AREA** |

## Soil Listing (all nodes)

| Area (acres) | Soil Group | Subcatchment Numbers |
|---|---|---|
| 2.663 | HSG A | 1S, 11S, 12S, 21S, 22S, 25S |
| 1.648 | HSG B | 1S, 11S, 12S, 21S, 22S, 23S, 24S |
| 0.436 | HSG C | 1S |
| 0.000 | HSG D | |
| 0.000 | Other | |
| **4.746** | | **TOTAL AREA** |

## Ground Covers (all nodes)

| HSG-A (acres) | HSG-B (acres) | HSG-C (acres) | HSG-D (acres) | Other (acres) | Total (acres) | Ground Cover | Subcatchment Numbers |
|---|---|---|---|---|---|---|---|
| 0.919 | 0.814 | 0.010 | 0.000 | 0.000 | 1.743 | >75% Grass cover, Good | 1S, 11S, 12S, 23S |
| 0.000 | 0.303 | 0.316 | 0.000 | 0.000 | 0.620 | Brush, Good | 1S |
| 0.213 | 0.018 | 0.000 | 0.000 | 0.000 | 0.231 | Gravel surface | 1S, 11S, 12S, 23S |
| 0.129 | 0.226 | 0.000 | 0.000 | 0.000 | 0.355 | Paved parking | 1S, 11S, 21S, 22S, 23S, 24S, 25S |
| 0.047 | 0.140 | 0.000 | 0.000 | 0.000 | 0.187 | Roofs | 1S, 12S, 21S, 23S, 24S |
| 1.355 | 0.145 | 0.110 | 0.000 | 0.000 | 1.610 | Woods, Good | 1S, 12S |
| **2.663** | **1.648** | **0.436** | **0.000** | **0.000** | **4.746** | **TOTAL AREA** | |

## Pipe Listing (all nodes)

| Line# | Node Number | In-Invert (feet) | Out-Invert (feet) | Length (feet) | Slope (ft/ft) | n | Diam/Width (inches) | Height (inches) | Inside-Fill (inches) |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 101P | 157.30 | 157.00 | 60.0 | 0.0050 | 0.012 | 15.0 | 0.0 | 0.0 |
| 2 | C01P | 162.47 | 162.32 | 16.0 | 0.0094 | 0.012 | 15.0 | 0.0 | 0.0 |
| 3 | C02P | 162.22 | 161.00 | 17.5 | 0.0697 | 0.012 | 15.0 | 0.0 | 0.0 |
| 4 | C03P | 160.42 | 159.80 | 103.5 | 0.0060 | 0.012 | 15.0 | 0.0 | 0.0 |
| 5 | C04P | 160.23 | 160.00 | 32.0 | 0.0072 | 0.012 | 15.0 | 0.0 | 0.0 |
| 6 | C05P | 161.00 | 160.35 | 50.0 | 0.0130 | 0.012 | 15.0 | 0.0 | 0.0 |
| 7 | D01P | 160.25 | 159.80 | 37.0 | 0.0122 | 0.012 | 15.0 | 0.0 | 0.0 |

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=123,825 sf 3.77% Impervious Runoff Depth>1.13"
Flow Length=308' Tc=26.7 min CN=51 Runoff=1.82 cfs 0.268 af

**Subcatchment 11S: Rain Garden #101** Runoff Area=6,863 sf 6.35% Impervious Runoff Depth>1.90"
Tc=6.0 min CN=61 Runoff=0.33 cfs 0.025 af

**Subcatchment 12S: Infiltration Basin #102** Runoff Area=59,399 sf 4.02% Impervious Runoff Depth>0.67"
Flow Length=265' Tc=25.9 min CN=44 Runoff=0.40 cfs 0.077 af

**Subcatchment 21S: Catch Basin #1** Runoff Area=2,597 sf 100.00% Impervious Runoff Depth>5.61"
Tc=6.0 min CN=98 Runoff=0.33 cfs 0.028 af

**Subcatchment 22S: Catch Basin #2** Runoff Area=1,343 sf 100.00% Impervious Runoff Depth>5.61"
Tc=6.0 min CN=98 Runoff=0.17 cfs 0.014 af

**Subcatchment 23S: Catch Basin #3** Runoff Area=4,735 sf 89.00% Impervious Runoff Depth>5.14"
Tc=6.0 min CN=94 Runoff=0.59 cfs 0.047 af

**Subcatchment 24S: Catch Basin #4** Runoff Area=5,442 sf 100.00% Impervious Runoff Depth>5.61"
Tc=6.0 min CN=98 Runoff=0.70 cfs 0.058 af

**Subcatchment 25S: Catch Basin #5** Runoff Area=2,550 sf 100.00% Impervious Runoff Depth>5.61"
Tc=6.0 min CN=98 Runoff=0.33 cfs 0.027 af

**Reach 100R: Final Reach #100** Inflow=2.28 cfs 0.423 af
Outflow=2.28 cfs 0.423 af

**Reach 101R: Reach to Wetland** Avg. Flow Depth=0.07' Max Vel=0.99 fps Inflow=0.46 cfs 0.156 af
n=0.035 L=66.5' S=0.0301 '/' Capacity=29.48 cfs Outflow=0.46 cfs 0.156 af

**Pond 101P: Rain Garden #101** Peak Elev=162.58' Storage=3,901 cf Inflow=2.39 cfs 0.198 af
Outflow=0.46 cfs 0.156 af

**Pond 102P: Infiltration Basin #102** Peak Elev=162.09' Storage=883 cf Inflow=0.40 cfs 0.077 af
Discarded=0.11 cfs 0.072 af Primary=0.00 cfs 0.000 af Outflow=0.11 cfs 0.072 af

**Pond C01P: Catch Basin #1** Peak Elev=162.76' Storage=0.000 af Inflow=0.33 cfs 0.028 af
15.0" Round Culvert n=0.012 L=16.0' S=0.0094 '/' Outflow=0.33 cfs 0.028 af

**Pond C02P: Catch Basin #2** Peak Elev=162.59' Storage=0.000 af Inflow=0.51 cfs 0.042 af
15.0" Round Culvert n=0.012 L=17.5' S=0.0697 '/' Outflow=0.51 cfs 0.042 af

**Pond C03P: Catch Basin #3** Peak Elev=162.58' Storage=0.001 af Inflow=0.59 cfs 0.047 af
15.0" Round Culvert n=0.012 L=103.5' S=0.0060 '/' Outflow=0.57 cfs 0.046 af

**Pond C04P: Catch Basin #4** Peak Elev=162.58' Storage=0.001 af Inflow=0.70 cfs 0.058 af
15.0" Round Culvert n=0.012 L=32.0' S=0.0072 '/' Outflow=0.68 cfs 0.058 af

**Pond C05P: Catch Basin #5** Peak Elev=162.58' Storage=0.000 af Inflow=0.33 cfs 0.027 af
15.0" Round Culvert n=0.012 L=50.0' S=0.0130 '/' Outflow=0.32 cfs 0.027 af

**Pond D01P: Drain Manhole #1** Peak Elev=162.58' Storage=0.001 af Inflow=0.32 cfs 0.027 af
15.0" Round Culvert n=0.012 L=37.0' S=0.0122 '/' Outflow=0.30 cfs 0.027 af

**Total Runoff Area = 4.746 ac Runoff Volume = 0.544 af Average Runoff Depth = 1.38"**
**88.57% Pervious = 4.204 ac 11.43% Impervious = 0.543 ac**

## Summary for Subcatchment 1S: Subcatchment #1

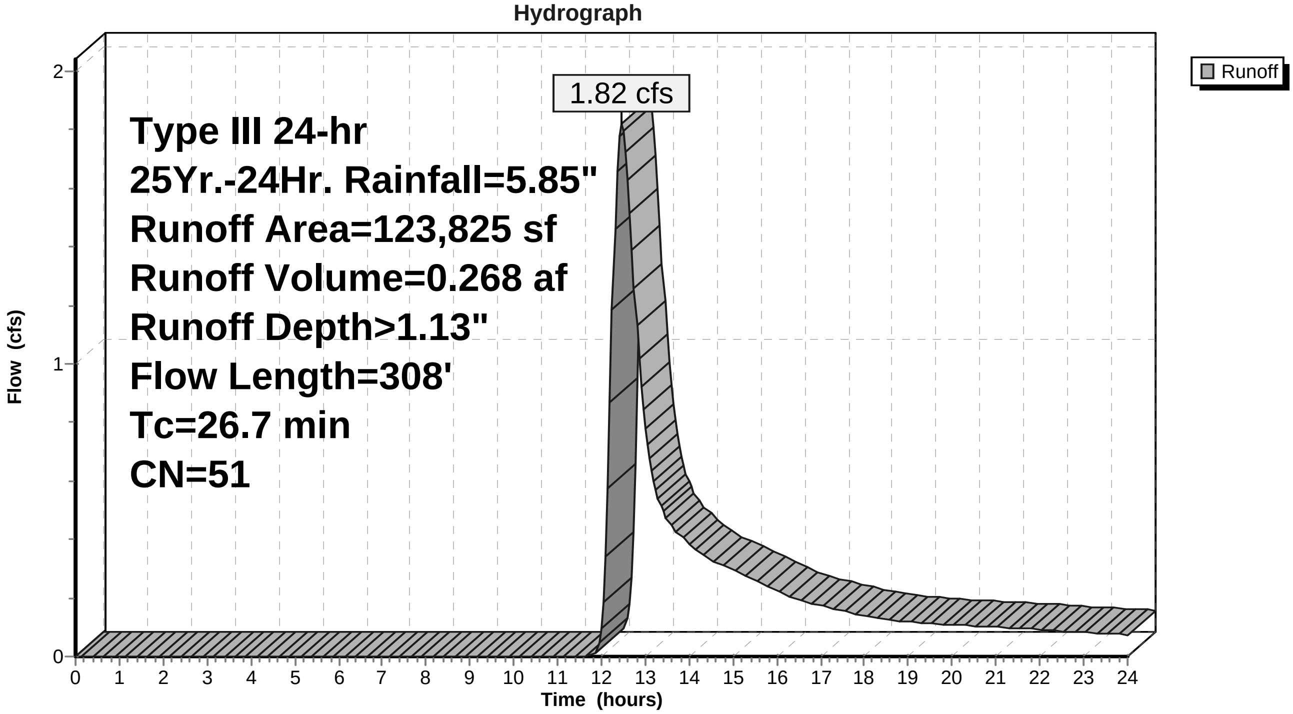
Runoff = 1.82 cfs @ 12.46 hrs, Volume= 0.268 af, Depth> 1.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25Yr.-24Hr. Rainfall=5.85"

| Area (sf) | CN | Description |
|---|---|---|
| 32,716 | 39 | >75% Grass cover, Good, HSG A |
| 19,106 | 61 | >75% Grass cover, Good, HSG B |
| 422 | 74 | >75% Grass cover, Good, HSG C |
| 13,215 | 48 | Brush, Good, HSG B |
| 13,773 | 65 | Brush, Good, HSG C |
| 1,593 | 98 | Paved parking, HSG A |
| 8 | 98 | Paved parking, HSG C |
| 2,050 | 98 | Roofs, HSG A |
| 1,012 | 98 | Roofs, HSG B |
| 5,392 | 96 | Gravel surface, HSG A |
| 335 | 96 | Gravel surface, HSG B |
| 23,832 | 30 | Woods, Good, HSG A |
| 5,592 | 55 | Woods, Good, HSG B |
| 4,779 | 70 | Woods, Good, HSG C |
| 123,825 | 51 | Weighted Average |
| 119,162 | | 96.23% Pervious Area |
| 4,663 | | 3.77% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 25.1 | 89 | 0.0112 | 0.06 | | **Sheet Flow, Segment #1**<br>Woods: Light underbrush n= 0.400 P2= 3.08" |
| 0.4 | 41 | 0.1463 | 1.91 | | **Shallow Concentrated Flow, Segment #2**<br>Woodland Kv= 5.0 fps |
| 0.1 | 30 | 0.1333 | 5.88 | | **Shallow Concentrated Flow, Segment #3**<br>Unpaved Kv= 16.1 fps |
| 0.2 | 40 | 0.3000 | 2.74 | | **Shallow Concentrated Flow, Segment #4**<br>Woodland Kv= 5.0 fps |
| 0.9 | 108 | 0.0833 | 2.02 | | **Shallow Concentrated Flow, Segment #5**<br>Short Grass Pasture Kv= 7.0 fps |
| 26.7 | 308 | Total | | | |

## Subcatchment 1S: Subcatchment #1



## Summary for Subcatchment 11S: Rain Garden #101

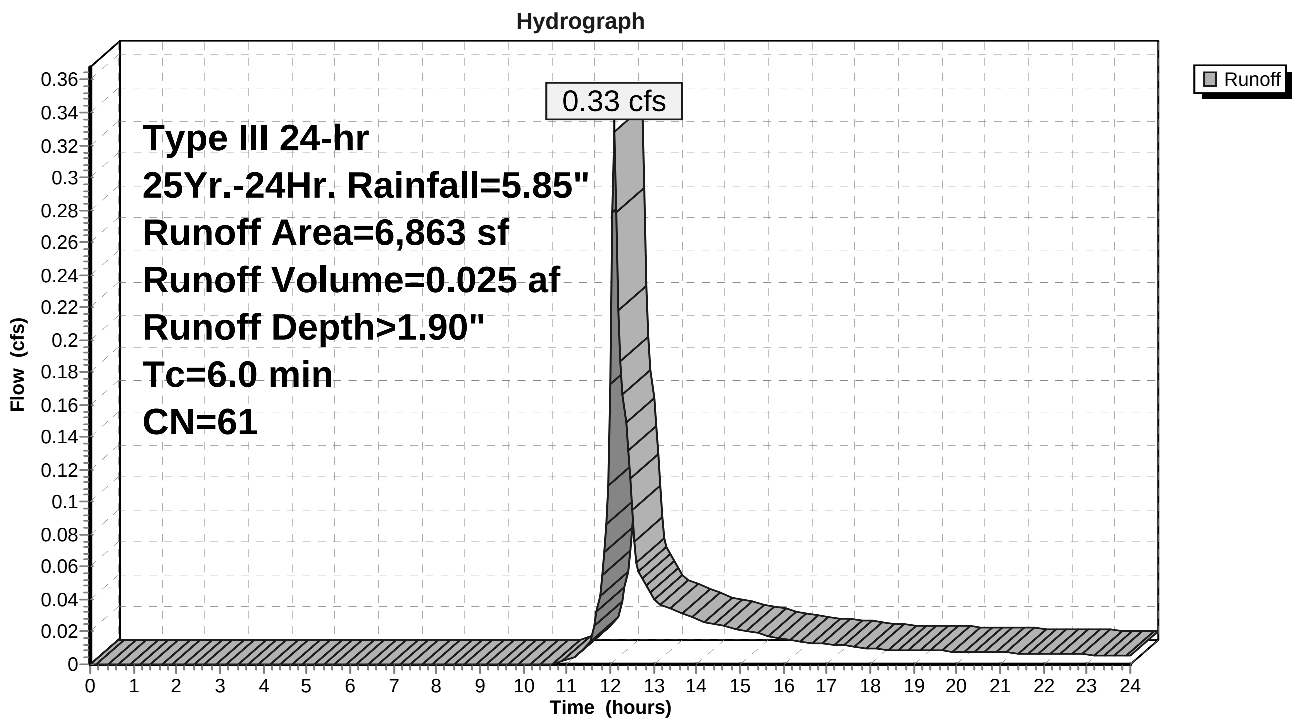
Runoff = 0.33 cfs @ 12.10 hrs, Volume= 0.025 af, Depth> 1.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25Yr.-24Hr. Rainfall=5.85"

| Area (sf) | CN | Description |
|---|---|---|
| 1,573 | 39 | >75% Grass cover, Good, HSG A |
| 4,387 | 61 | >75% Grass cover, Good, HSG B |
| 436 | 98 | Paved parking, HSG A |
| 139 | 96 | Gravel surface, HSG A |
| 328 | 96 | Gravel surface, HSG B |
| 6,863 | 61 | Weighted Average |
| 6,427 | | 93.65% Pervious Area |
| 436 | | 6.35% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 6.0 | | | | | **Direct Entry, Direct Entry** |

### Subcatchment 11S: Rain Garden #101



## Summary for Subcatchment 12S: Infiltration Basin #102

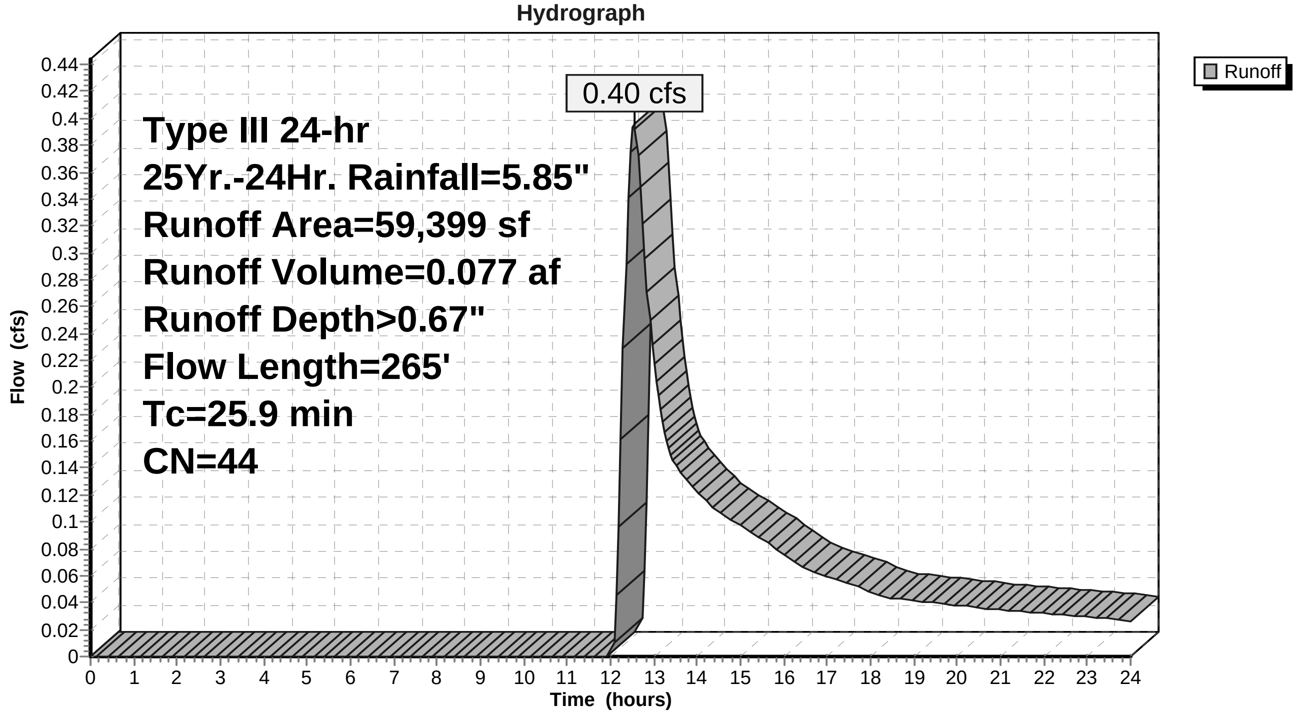
Runoff = 0.40 cfs @ 12.54 hrs, Volume= 0.077 af, Depth> 0.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25Yr.-24Hr. Rainfall=5.85"

| Area (sf) | CN | Description |
|---|---|---|
| 5,750 | 39 | >75% Grass cover, Good, HSG A |
| 11,488 | 61 | >75% Grass cover, Good, HSG B |
| 2,388 | 98 | Roofs, HSG B |
| 3,751 | 96 | Gravel surface, HSG A |
| 95 | 96 | Gravel surface, HSG B |
| 35,187 | 30 | Woods, Good, HSG A |
| 740 | 55 | Woods, Good, HSG B |
| 59,399 | 44 | Weighted Average |
| 57,011 | | 95.98% Pervious Area |
| 2,388 | | 4.02% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 24.6 | 100 | 0.0150 | 0.07 | | **Sheet Flow, Segment #1** Woods: Light underbrush n= 0.400 P2= 3.08" |
| 1.0 | 102 | 0.1176 | 1.71 | | **Shallow Concentrated Flow, Segment #2** Woodland Kv= 5.0 fps |
| 0.2 | 50 | 0.0800 | 4.55 | | **Shallow Concentrated Flow, Segment #3** Unpaved Kv= 16.1 fps |
| 0.1 | 13 | 0.2300 | 2.40 | | **Shallow Concentrated Flow, Segment #4** Woodland Kv= 5.0 fps |
| 25.9 | 265 | Total | | | |

## Subcatchment 12S: Infiltration Basin #102



## Summary for Subcatchment 21S: Catch Basin #1

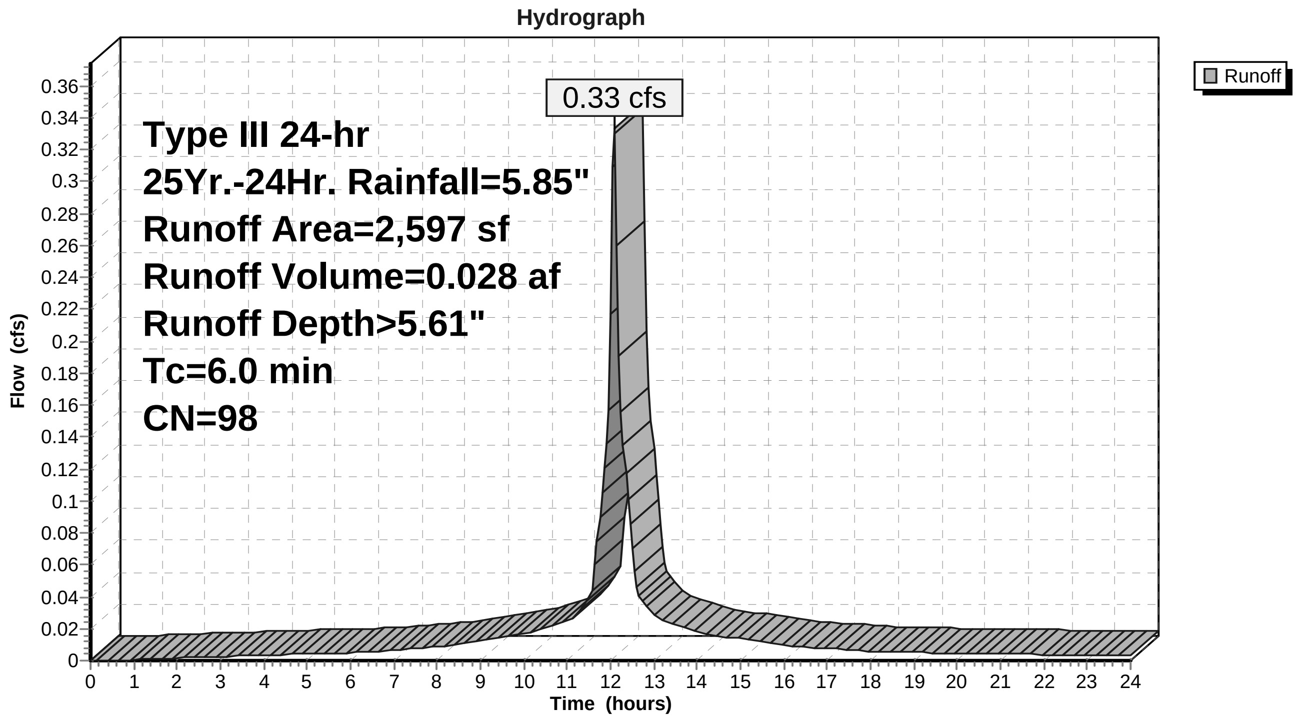
Runoff = 0.33 cfs @ 12.09 hrs, Volume= 0.028 af, Depth> 5.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25Yr.-24Hr. Rainfall=5.85"

| Area (sf) | CN | Description |
|---|---|---|
| 456 | 98 | Paved parking, HSG A |
| 1,373 | 98 | Paved parking, HSG B |
| 768 | 98 | Roofs, HSG B |
| 2,597 | 98 | Weighted Average |
| 2,597 | | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 6.0 | | | | | **Direct Entry, Direct Entry** |

## Subcatchment 21S: Catch Basin #1



## Summary for Subcatchment 22S: Catch Basin #2

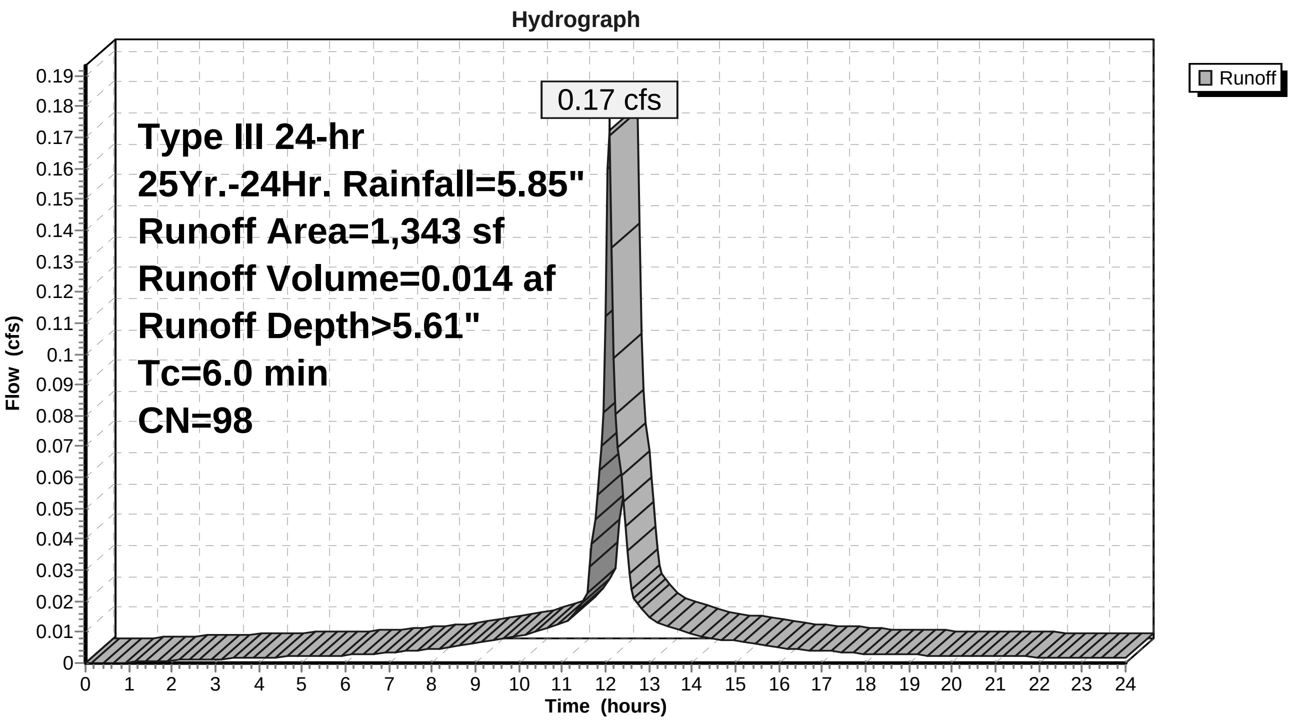
Runoff = 0.17 cfs @ 12.09 hrs, Volume= 0.014 af, Depth> 5.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25Yr.-24Hr. Rainfall=5.85"

| Area (sf) | CN | Description |
|---|---|---|
| 580 | 98 | Paved parking, HSG A |
| 763 | 98 | Paved parking, HSG B |
| 1,343 | 98 | Weighted Average |
| 1,343 | | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 6.0 | | | | | **Direct Entry, Direct Entry** |

## Subcatchment 22S: Catch Basin #2



## Summary for Subcatchment 23S: Catch Basin #3

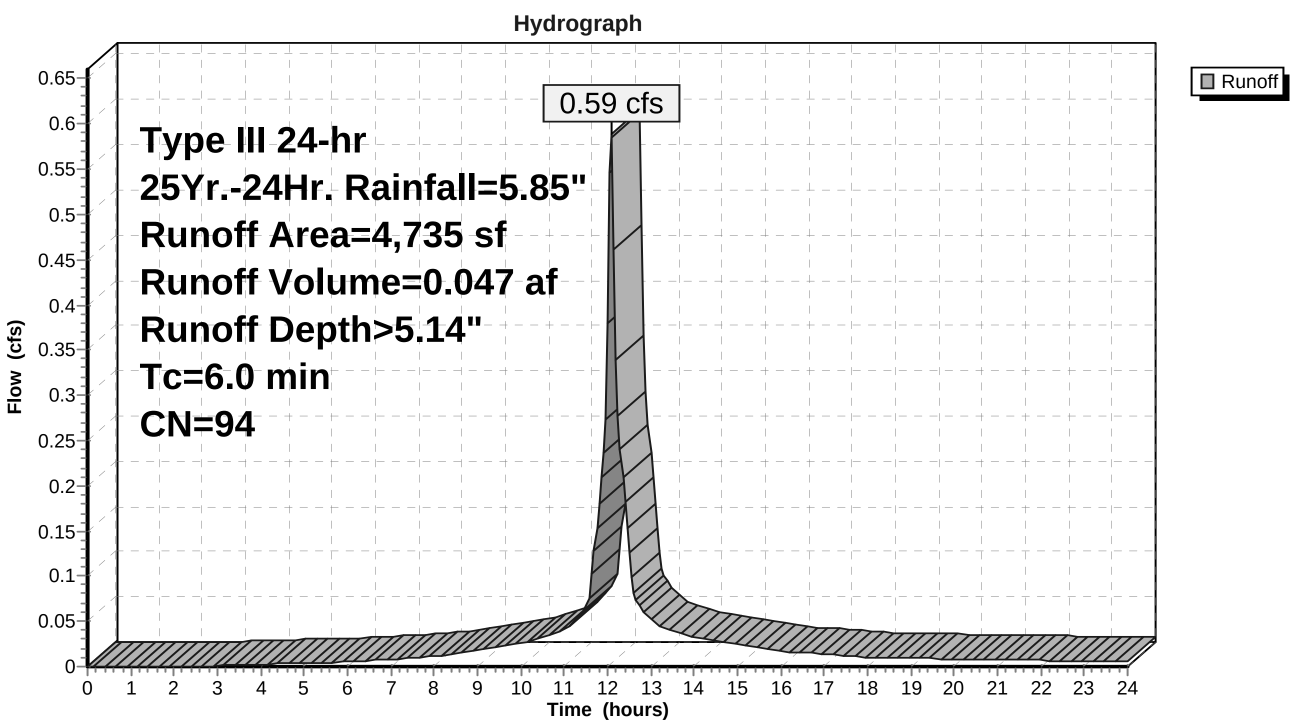
Runoff = 0.59 cfs @ 12.09 hrs, Volume= 0.047 af, Depth> 5.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25Yr.-24Hr. Rainfall=5.85"

| Area (sf) | CN | Description |
|---|---|---|
| 479 | 61 | >75% Grass cover, Good, HSG B |
| 3,398 | 98 | Paved parking, HSG B |
| 42 | 96 | Gravel surface, HSG B |
| 816 | 98 | Roofs, HSG B |
| 4,735 | 94 | Weighted Average |
| 521 | | 11.00% Pervious Area |
| 4,214 | | 89.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 6.0 | | | | | **Direct Entry, Direct Entry** |

## Subcatchment 23S: Catch Basin #3



## Summary for Subcatchment 24S: Catch Basin #4

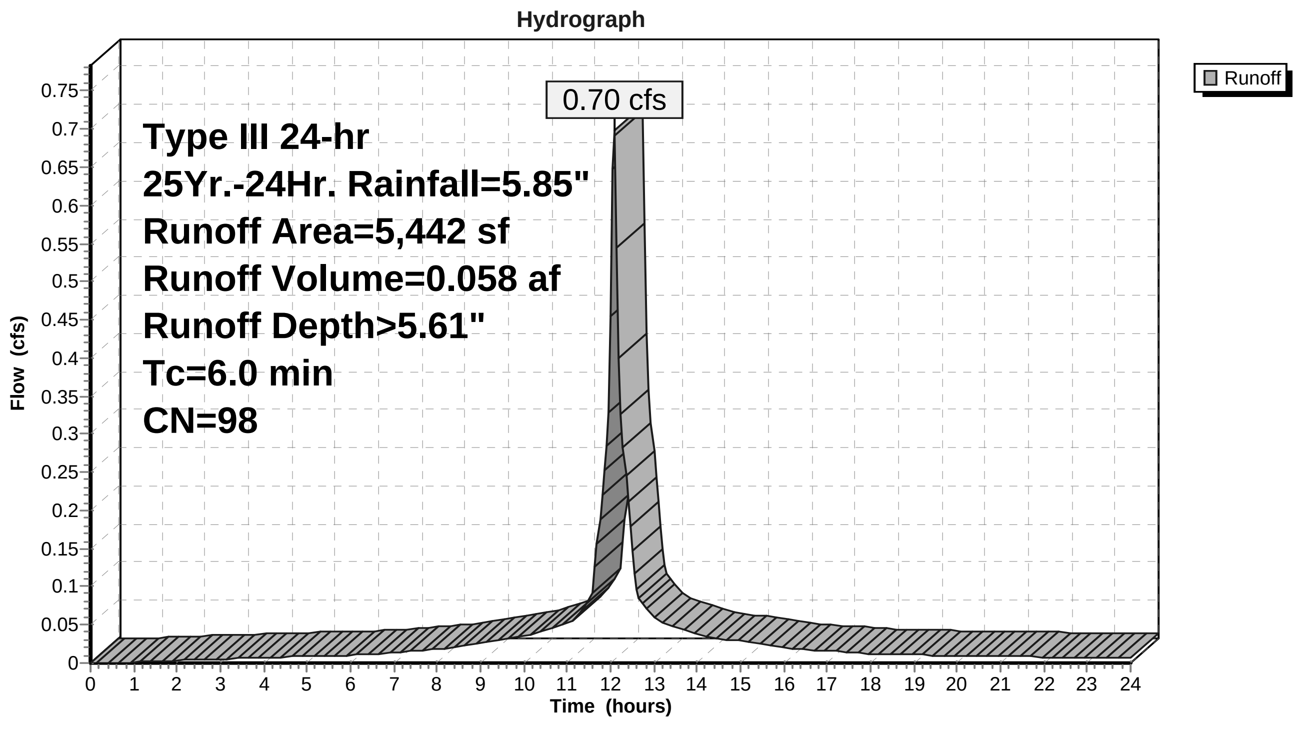
Runoff = 0.70 cfs @ 12.09 hrs, Volume= 0.058 af, Depth> 5.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25Yr.-24Hr. Rainfall=5.85"

| Area (sf) | CN | Description |
|---|---|---|
| 4,320 | 98 | Paved parking, HSG B |
| 1,122 | 98 | Roofs, HSG B |
| 5,442 | 98 | Weighted Average |
| 5,442 | | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 6.0 | | | | | **Direct Entry, Direct Entry** |

## Subcatchment 24S: Catch Basin #4



## Summary for Subcatchment 25S: Catch Basin #5

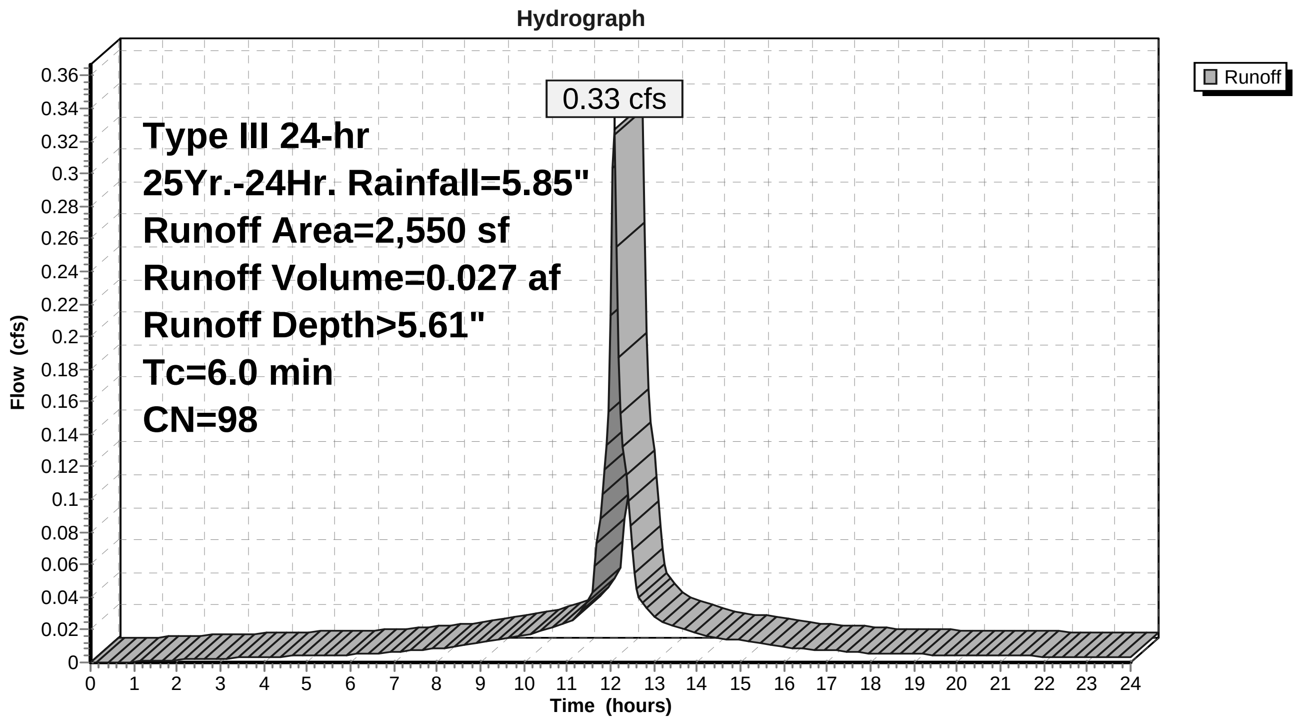
Runoff = 0.33 cfs @ 12.09 hrs, Volume= 0.027 af, Depth> 5.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25Yr.-24Hr. Rainfall=5.85"

| Area (sf) | CN | Description |
|---|---|---|
| 2,550 | 98 | Paved parking, HSG A |
| 2,550 | | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 6.0 | | | | | **Direct Entry, Direct Entry** |

## Subcatchment 25S: Catch Basin #5



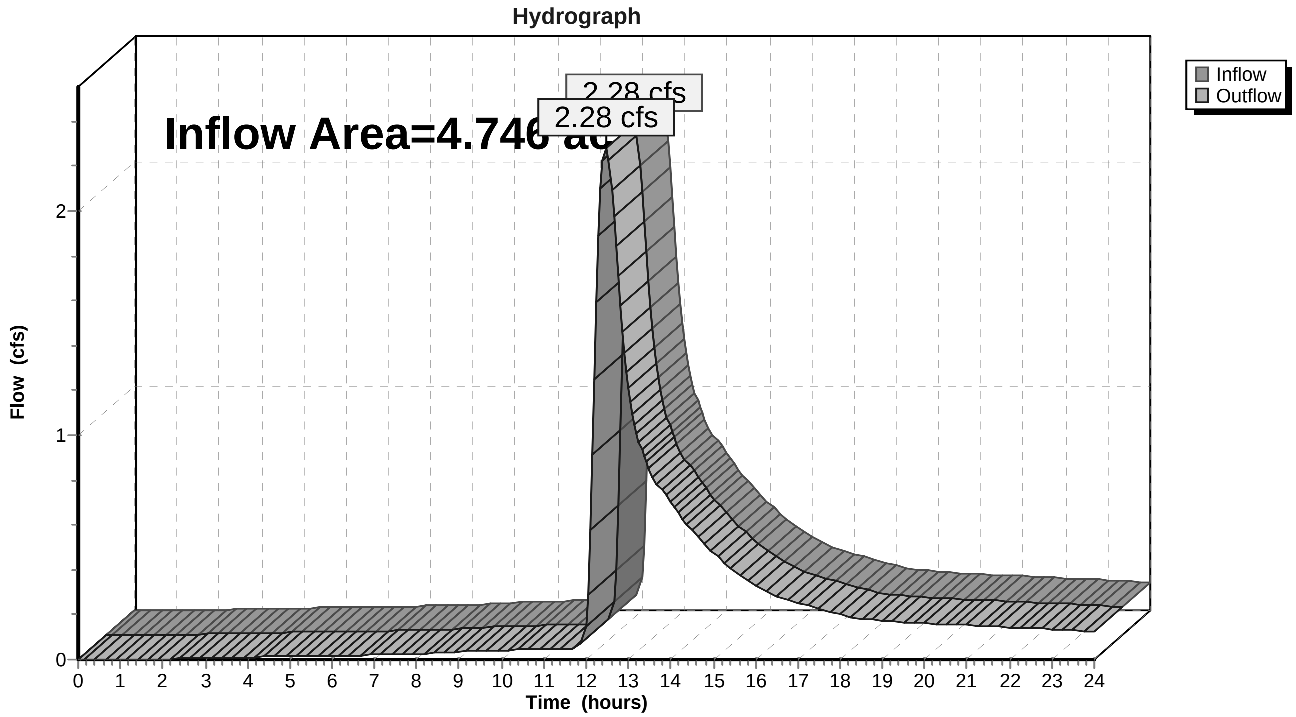
## Summary for Reach 100R: Final Reach #100

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 4.746 ac, 11.43% Impervious, Inflow Depth > 1.07" for 25Yr.-24Hr. event
Inflow = 2.28 cfs @ 12.46 hrs, Volume= 0.423 af
Outflow = 2.28 cfs @ 12.46 hrs, Volume= 0.423 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

### Reach 100R: Final Reach #100



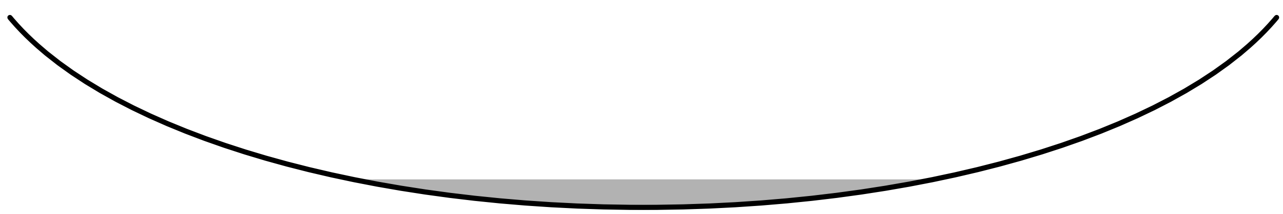
## Summary for Reach 101R: Reach to Wetland

Inflow Area = 1.904 ac, 22.87% Impervious, Inflow Depth > 0.98" for 25Yr.-24Hr. event
Inflow = 0.46 cfs @ 12.54 hrs, Volume= 0.156 af
Outflow = 0.46 cfs @ 12.55 hrs, Volume= 0.156 af, Atten= 0%, Lag= 0.8 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Max. Velocity= 0.99 fps, Min. Travel Time= 1.1 min
Avg. Velocity = 0.50 fps, Avg. Travel Time= 2.2 min

Peak Storage= 31 cf @ 12.55 hrs
Average Depth at Peak Storage= 0.07'
Bank-Full Depth= 0.50' Flow Area= 8.3 sf, Capacity= 29.48 cfs

25.00' x 0.50' deep Parabolic Channel, n= 0.035 Earth, dense weeds
Length= 66.5' Slope= 0.0301 '/'
Inlet Invert= 157.00', Outlet Invert= 155.00'



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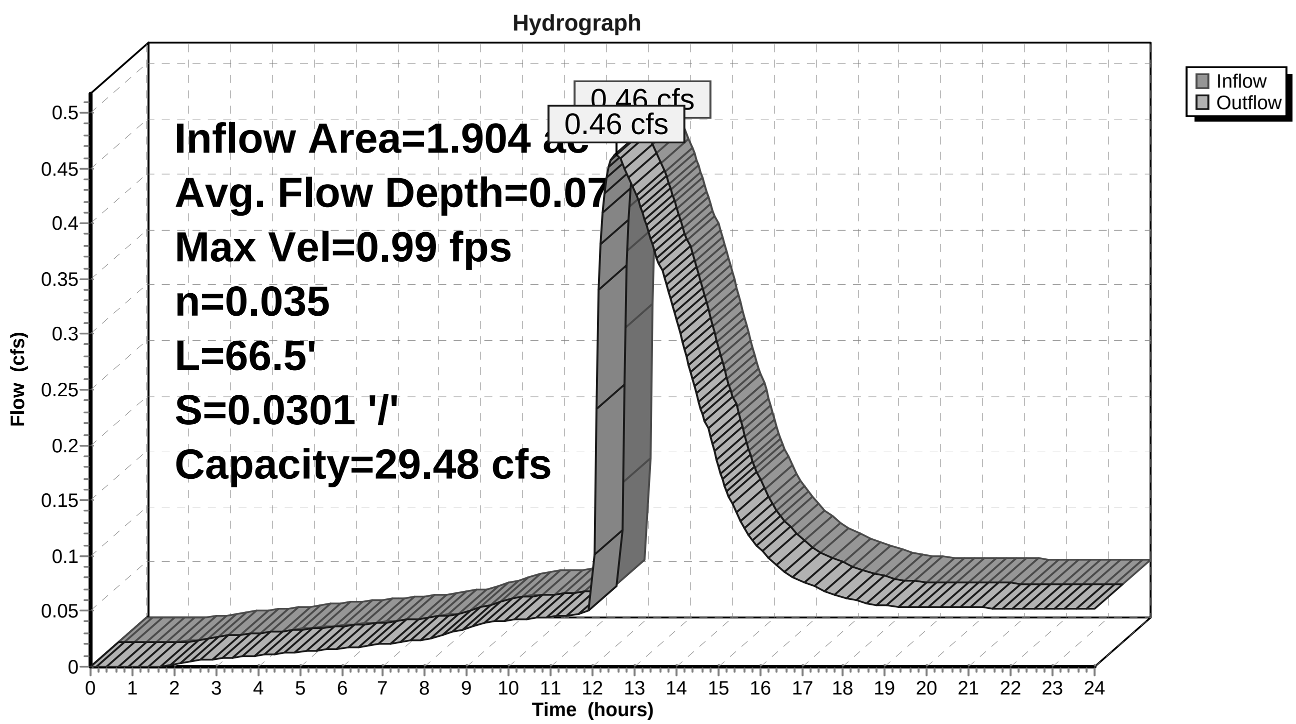
### Reach 101R: Reach to Wetland



## Summary for Pond 101P: Rain Garden #101

[80] Warning: Exceeded Pond C02P by 0.01' @ 12.45 hrs (0.07 cfs 0.001 af)
[80] Warning: Exceeded Pond C03P by 0.23' @ 12.10 hrs (2.59 cfs 0.119 af)
[80] Warning: Exceeded Pond C04P by 0.24' @ 12.10 hrs (2.87 cfs 0.237 af)
[80] Warning: Exceeded Pond D01P by 0.25' @ 12.10 hrs (2.93 cfs 0.540 af)

Inflow Area = 1.904 ac, 22.87% Impervious, Inflow Depth > 1.25" for 25Yr.-24Hr. event
Inflow = 2.39 cfs @ 12.09 hrs, Volume= 0.198 af
Outflow = 0.46 cfs @ 12.54 hrs, Volume= 0.156 af, Atten= 81%, Lag= 26.9 min
Primary = 0.46 cfs @ 12.54 hrs, Volume= 0.156 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 162.58' @ 12.54 hrs Surf.Area= 636 sf Storage= 3,901 cf
Flood Elev= 163.50' Surf.Area= 636 sf Storage= 5,797 cf

Plug-Flow detention time= 184.9 min calculated for 0.156 af (79% of inflow)
Center-of-Mass det. time= 102.2 min ( 869.5 - 767.3 )

| Volume | Invert | Avail.Storage | Storage Description |
|---|---|---|---|
| #1 | 157.30' | 254 cf | **Stone (Irregular)** Listed below (Recalc)<br>636 cf Overall x 40.0% Voids |
| #2 | 158.30' | 191 cf | **BioMedia (Irregular)** Listed below (Recalc) -Impervious<br>954 cf Overall x 20.0% Voids |
| #3 | 159.80' | 5,352 cf | **Open Water Storage (Irregular)** Listed below (Recalc) -Impervious |
| | | 5,797 cf | Total Available Storage |

| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 157.30 | 636 | 110.2 | 0 | 0 | 636 |
| 158.30 | 636 | 110.2 | 636 | 636 | 746 |

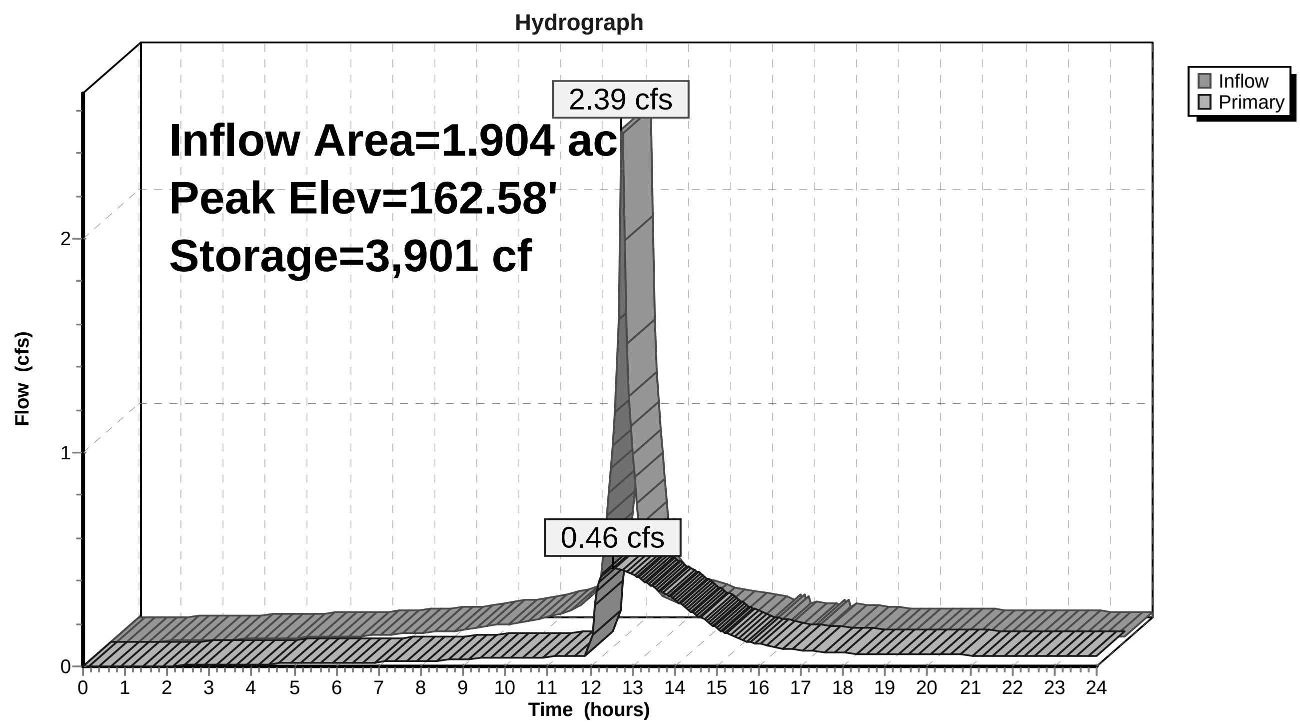
| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 158.30 | 636 | 110.2 | 0 | 0 | 636 |
| 159.80 | 636 | 110.2 | 954 | 954 | 801 |

| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 159.80 | 636 | 110.2 | 0 | 0 | 636 |
| 160.00 | 806 | 118.2 | 144 | 144 | 783 |
| 161.00 | 1,145 | 130.3 | 971 | 1,114 | 1,053 |
| 162.00 | 1,569 | 149.8 | 1,351 | 2,466 | 1,509 |
| 163.00 | 2,047 | 168.6 | 1,803 | 4,269 | 2,012 |
| 163.50 | 2,290 | 177.8 | 1,084 | 5,352 | 2,280 |

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 157.30' | **15.0" Round 15" HDPE N-12**<br>L= 60.0' CPP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 157.30' / 157.00' S= 0.0050 '/' Cc= 0.900<br>n= 0.012, Flow Area= 1.23 sf |
| #2 | Device 1 | 157.30' | **1.0" Vert. 1" Orifice** C= 0.600 |
| #3 | Device 2 | 157.30' | **10.000 in/hr Filtration thru media over Surface area** |
| #4 | Device 1 | 161.50' | **4.0" Vert. 4" Orifice** C= 0.600 |
| #5 | Device 1 | 163.00' | **48.0" Vert. 48" Outlet Structure** C= 0.600 |

**Primary OutFlow** Max=0.46 cfs @ 12.54 hrs HW=162.58' TW=157.07' (Dynamic Tailwater)
**1=15" HDPE N-12** (Passes 0.46 cfs of 12.49 cfs potential flow)
**2=1" Orifice** (Orifice Controls 0.06 cfs @ 11.02 fps)
**3=Filtration thru media** (Passes 0.06 cfs of 0.15 cfs potential flow)
**4=4" Orifice** (Orifice Controls 0.40 cfs @ 4.60 fps)
**5=48" Outlet Structure** ( Controls 0.00 cfs)

## Pond 101P: Rain Garden #101



## Summary for Pond 102P: Infiltration Basin #102

Inflow Area = 1.364 ac, 4.02% Impervious, Inflow Depth > 0.67" for 25Yr.-24Hr. event
Inflow = 0.40 cfs @ 12.54 hrs, Volume= 0.077 af
Outflow = 0.11 cfs @ 14.30 hrs, Volume= 0.072 af, Atten= 72%, Lag= 105.9 min
Discarded = 0.11 cfs @ 14.30 hrs, Volume= 0.072 af
Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 162.09' @ 14.30 hrs Surf.Area= 1,613 sf Storage= 883 cf
Flood Elev= 164.00' Surf.Area= 7,916 sf Storage= 6,779 cf

Plug-Flow detention time= 125.0 min calculated for 0.072 af (94% of inflow)
Center-of-Mass det. time= 97.9 min ( 1,037.6 - 939.7 )

| Volume | Invert | Avail.Storage | Storage Description |
|---|---|---|---|
| #1 | 161.00' | 2,058 cf | **Infiltration Cell (Irregular)**Listed below (Recalc) |
| #2 | 162.00' | 821 cf | **Sediment Forebay (Irregular)**Listed below (Recalc) |
| #3 | 163.00' | 3,901 cf | **Open Water Storage (Irregular)**Listed below (Recalc) |
| | | 6,779 cf | Total Available Storage |

| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 161.00 | 459 | 96.0 | 0 | 0 | 459 |
| 162.00 | 1,055 | 144.0 | 737 | 737 | 1,384 |
| 163.00 | 1,606 | 197.4 | 1,321 | 2,058 | 2,844 |

| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 162.00 | 453 | 176.0 | 0 | 0 | 453 |
| 163.00 | 1,255 | 237.0 | 821 | 821 | 2,468 |

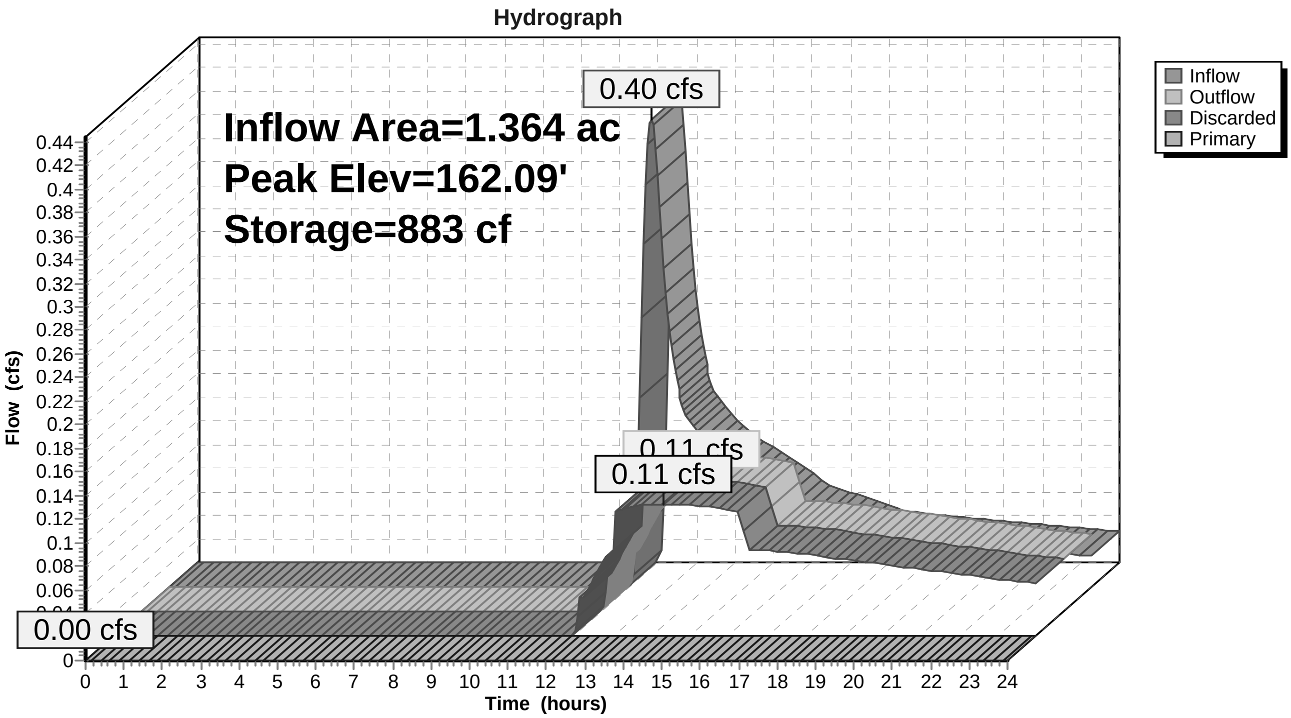
| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 163.00 | 3,128 | 393.2 | 0 | 0 | 3,128 |
| 163.50 | 3,732 | 407.7 | 1,713 | 1,713 | 4,074 |
| 164.00 | 5,055 | 470.9 | 2,188 | 3,901 | 8,498 |

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Discarded | 161.00' | **3.000 in/hr Infiltration over Surface area** |
| #2 | Primary | 163.50' | **5.0' long x 10.0' breadth Overflow**<br>Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60<br>Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64 |

**Discarded OutFlow** Max=0.11 cfs @ 14.30 hrs HW=162.09' (Free Discharge)
└─**1=Infiltration** (Exfiltration Controls 0.11 cfs)

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=161.00' TW=157.30' (Dynamic Tailwater)
└─**2=Overflow** ( Controls 0.00 cfs)

## Pond 102P: Infiltration Basin #102



## Summary for Pond C01P: Catch Basin #1

Inflow Area = 0.060 ac,100.00% Impervious, Inflow Depth > 5.61" for 25Yr.-24Hr. event
Inflow = 0.33 cfs @ 12.09 hrs, Volume= 0.028 af
Outflow = 0.33 cfs @ 12.09 hrs, Volume= 0.028 af, Atten= 0%, Lag= 0.1 min
Primary = 0.33 cfs @ 12.09 hrs, Volume= 0.028 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 162.76' @ 12.09 hrs Surf.Area= 0.000 ac Storage= 0.000 af
Flood Elev= 166.97' Surf.Area= 0.000 ac Storage= 0.001 af

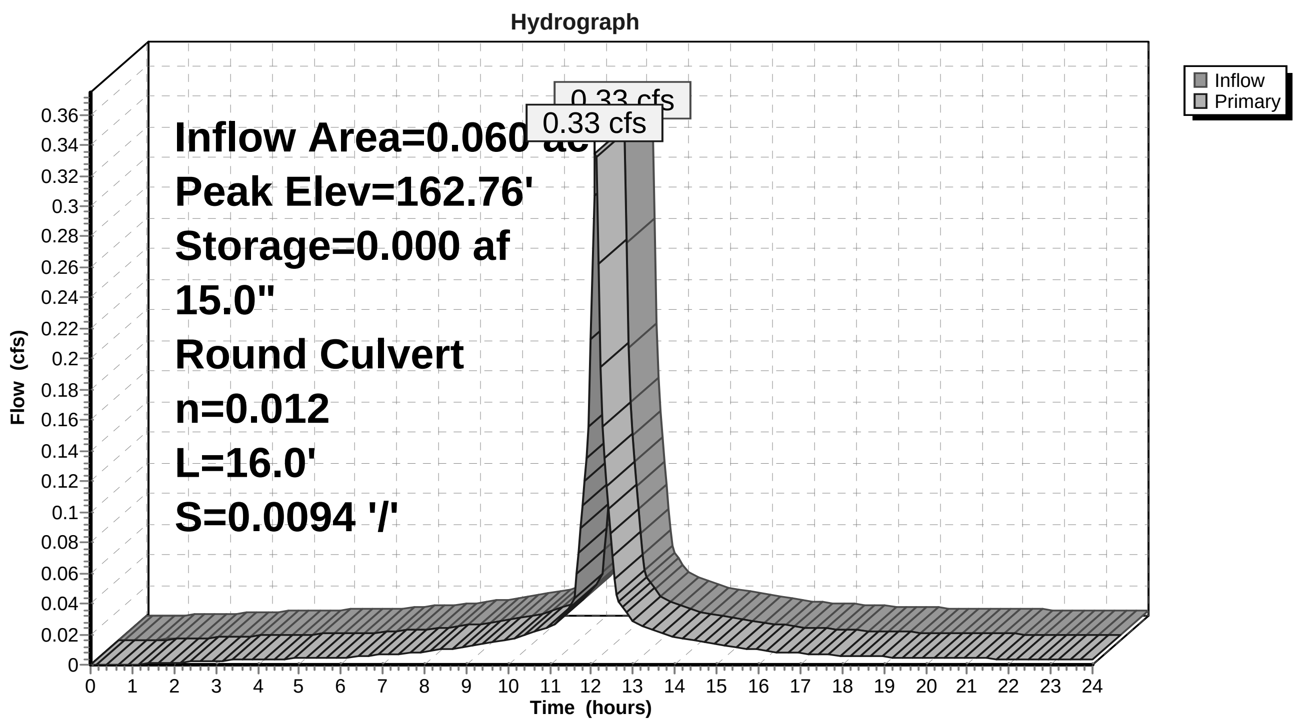
Plug-Flow detention time= 0.7 min calculated for 0.028 af (100% of inflow)
Center-of-Mass det. time= 0.5 min ( 745.6 - 745.1 )

| Volume | Invert | Avail.Storage | Storage Description |
|---|---|---|---|
| #1 | 162.47' | 0.001 af | **4.00'D x 4.50'H 4' Structure** |

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 162.47' | **15.0" Round 15" HDPE N-12**<br>L= 16.0' CPP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 162.47' / 162.32' S= 0.0094 '/' Cc= 0.900<br>n= 0.012, Flow Area= 1.23 sf |

**Primary OutFlow** Max=0.32 cfs @ 12.09 hrs HW=162.75' TW=162.55' (Dynamic Tailwater)
└─**1=15" HDPE N-12** (Outlet Controls 0.32 cfs @ 2.29 fps)

### Pond C01P: Catch Basin #1



## Summary for Pond C02P: Catch Basin #2

Inflow Area = 0.090 ac,100.00% Impervious, Inflow Depth > 5.61" for 25Yr.-24Hr. event
Inflow = 0.51 cfs @ 12.09 hrs, Volume= 0.042 af
Outflow = 0.51 cfs @ 12.09 hrs, Volume= 0.042 af, Atten= 0%, Lag= 0.1 min
Primary = 0.51 cfs @ 12.09 hrs, Volume= 0.042 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 162.59' @ 12.58 hrs Surf.Area= 0.000 ac Storage= 0.000 af
Flood Elev= 166.97' Surf.Area= 0.000 ac Storage= 0.001 af

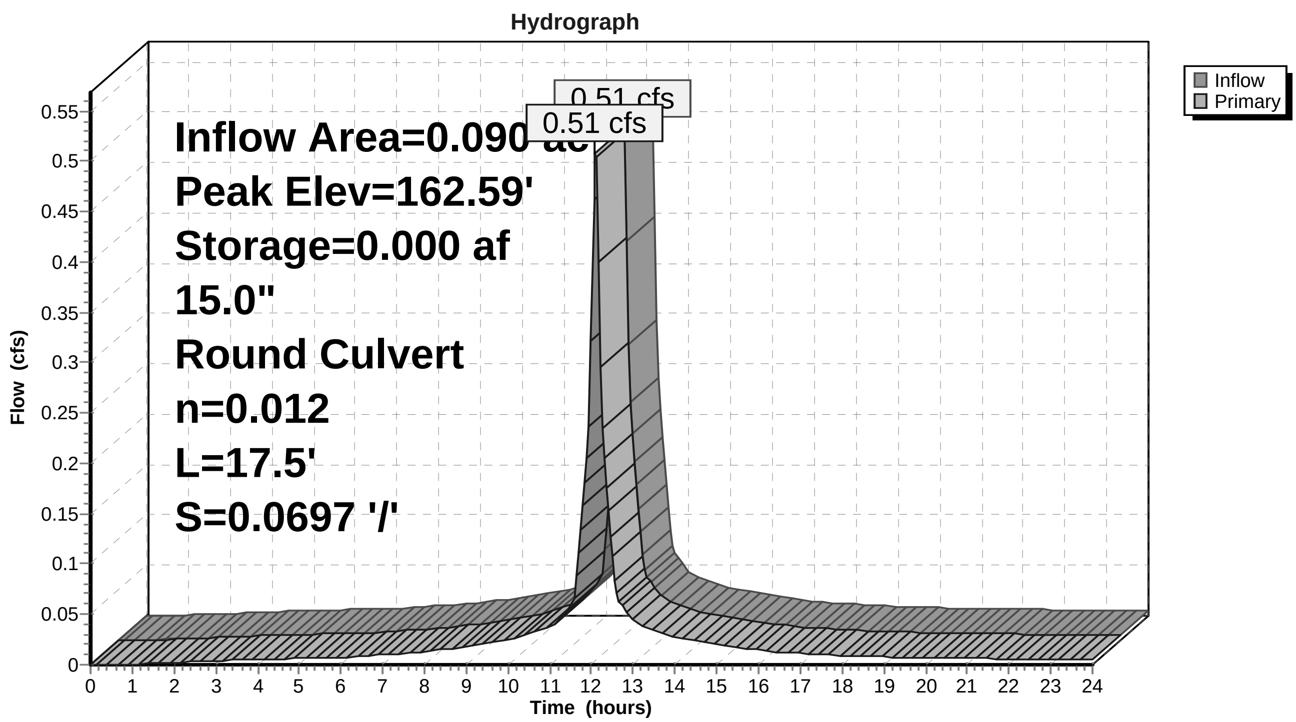
Plug-Flow detention time= 0.6 min calculated for 0.042 af (100% of inflow)
Center-of-Mass det. time= 0.4 min ( 745.9 - 745.4 )

| Volume | Invert | Avail.Storage | Storage Description |
|---|---|---|---|
| #1 | 162.22' | 0.001 af | **4.00'D x 4.75'H 4' Structure** |

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 162.22' | **15.0" Round 15" HDPE N-12**<br>L= 17.5' CPP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 162.22' / 161.00' S= 0.0697 '/' Cc= 0.900<br>n= 0.012, Flow Area= 1.23 sf |

**Primary OutFlow** Max=0.49 cfs @ 12.09 hrs HW=162.55' TW=161.90' (Dynamic Tailwater)
↑—**1=15" HDPE N-12** (Inlet Controls 0.49 cfs @ 1.94 fps)

### Pond C02P: Catch Basin #2



## Summary for Pond C03P: Catch Basin #3

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=20)

Inflow Area = 0.109 ac, 89.00% Impervious, Inflow Depth > 5.14" for 25Yr.-24Hr. event
Inflow = 0.59 cfs @ 12.09 hrs, Volume= 0.047 af
Outflow = 0.57 cfs @ 12.09 hrs, Volume= 0.046 af, Atten= 3%, Lag= 0.0 min
Primary = 0.57 cfs @ 12.09 hrs, Volume= 0.046 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 162.58' @ 12.59 hrs Surf.Area= 0.000 ac Storage= 0.001 af
Flood Elev= 163.92' Surf.Area= 0.000 ac Storage= 0.001 af

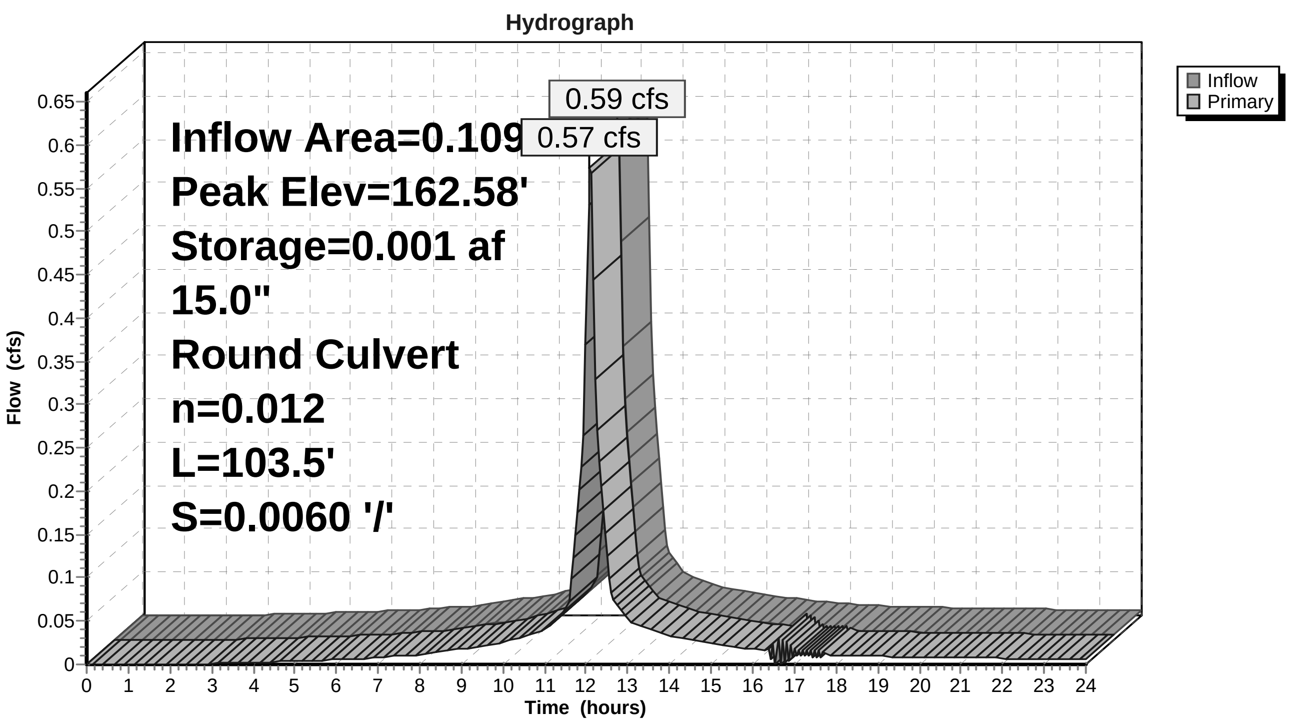
Plug-Flow detention time= 6.0 min calculated for 0.046 af (99% of inflow)
Center-of-Mass det. time= 2.3 min ( 771.0 - 768.7 )

| Volume | Invert | Avail.Storage | Storage Description |
|---|---|---|---|
| #1 | 160.42' | 0.001 af | **4.00'D x 3.50'H 4' Structure** |

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 160.42' | **15.0" Round 15" HDPE N-12**<br>L= 103.5' CPP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 160.42' / 159.80' S= 0.0060 '/' Cc= 0.900<br>n= 0.012, Flow Area= 1.23 sf |

**Primary OutFlow** Max=0.00 cfs @ 12.09 hrs HW=161.66' TW=161.89' (Dynamic Tailwater)
└─**1=15" HDPE N-12** ( Controls 0.00 cfs)

### Pond C03P: Catch Basin #3



## Summary for Pond C04P: Catch Basin #4

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=28)

Inflow Area = 0.125 ac,100.00% Impervious, Inflow Depth > 5.61" for 25Yr.-24Hr. event
Inflow = 0.70 cfs @ 12.09 hrs, Volume= 0.058 af
Outflow = 0.68 cfs @ 12.09 hrs, Volume= 0.058 af, Atten= 2%, Lag= 0.0 min
Primary = 0.68 cfs @ 12.09 hrs, Volume= 0.058 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 162.58' @ 12.59 hrs Surf.Area= 0.000 ac Storage= 0.001 af
Flood Elev= 163.73' Surf.Area= 0.000 ac Storage= 0.001 af

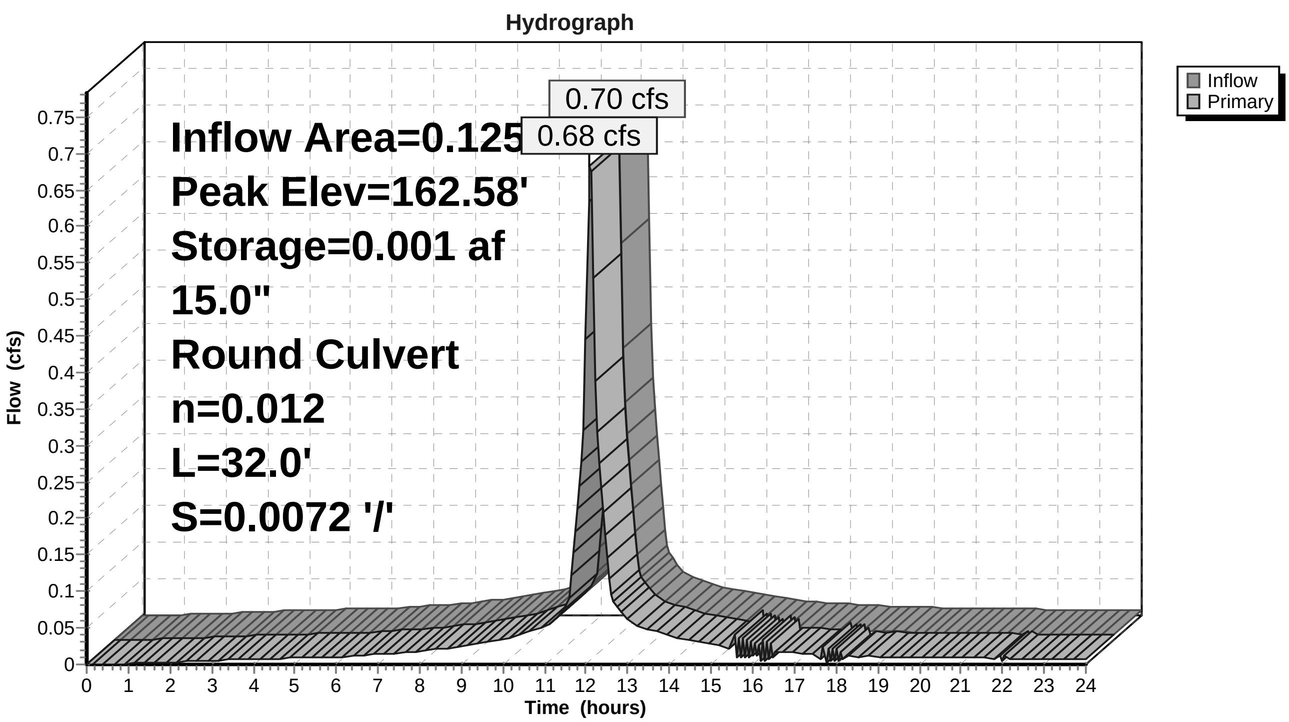
Plug-Flow detention time= 6.0 min calculated for 0.058 af (99% of inflow)
Center-of-Mass det. time= 1.4 min ( 746.5 - 745.1 )

| Volume | Invert | Avail.Storage | Storage Description |
|---|---|---|---|
| #1 | 160.23' | 0.001 af | **4.00'D x 3.50'H 4' Structure** |

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 160.23' | **15.0" Round 15" HDPE N-12**<br>L= 32.0' CPP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 160.23' / 160.00' S= 0.0072 '/' Cc= 0.900<br>n= 0.012, Flow Area= 1.23 sf |

**Primary OutFlow** Max=0.00 cfs @ 12.09 hrs HW=161.66' TW=161.89' (Dynamic Tailwater)
↑—**1=15" HDPE N-12** ( Controls 0.00 cfs)

### Pond C04P: Catch Basin #4



## Summary for Pond C05P: Catch Basin #5

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=99)

Inflow Area = 0.059 ac,100.00% Impervious, Inflow Depth > 5.61" for 25Yr.-24Hr. event
Inflow = 0.33 cfs @ 12.09 hrs, Volume= 0.027 af
Outflow = 0.32 cfs @ 12.08 hrs, Volume= 0.027 af, Atten= 3%, Lag= 0.0 min
Primary = 0.32 cfs @ 12.08 hrs, Volume= 0.027 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 162.58' @ 12.64 hrs Surf.Area= 0.000 ac Storage= 0.000 af
Flood Elev= 163.00' Surf.Area= 0.000 ac Storage= 0.001 af

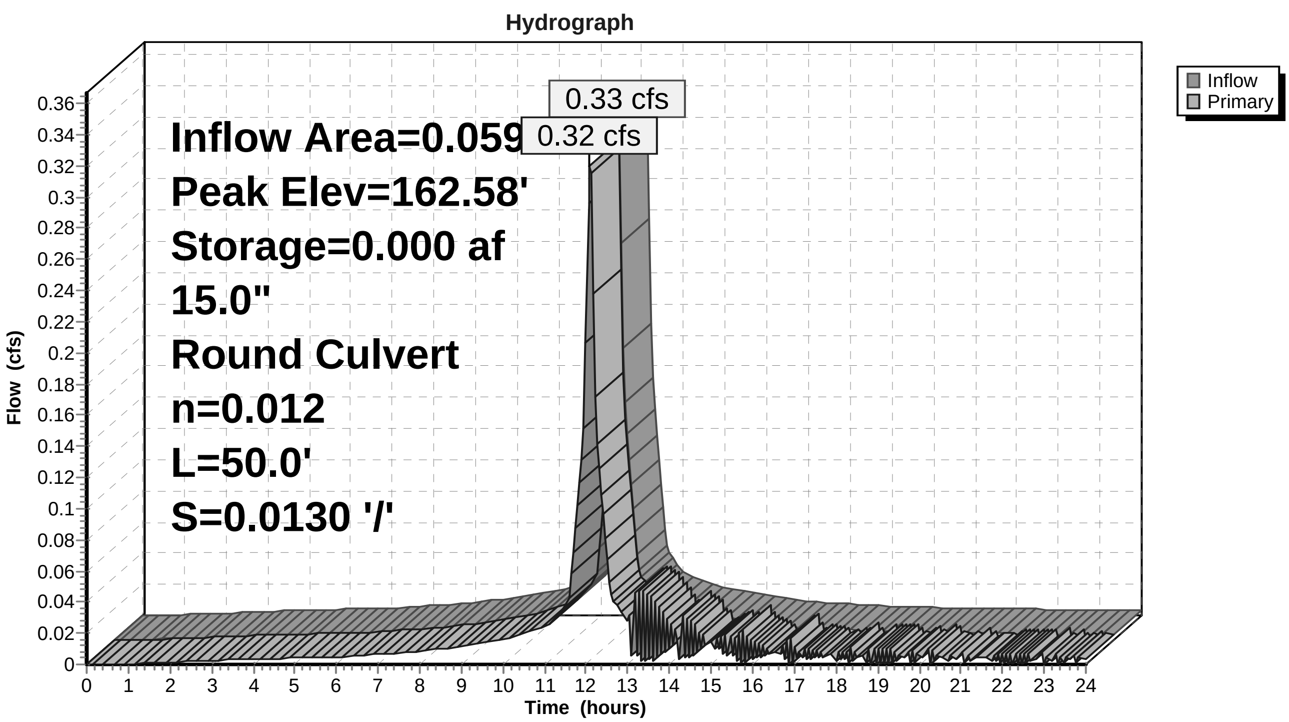
Plug-Flow detention time= 7.2 min calculated for 0.027 af (99% of inflow)
Center-of-Mass det. time= 2.9 min ( 748.0 - 745.1 )

| Volume | Invert | Avail.Storage | Storage Description |
|---|---|---|---|
| #1 | 161.00' | 0.001 af | **4.00'D x 4.50'H 4' Structure** |

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 161.00' | **15.0" Round 15" HDPE N-12**<br>L= 50.0' CPP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 161.00' / 160.35' S= 0.0130 '/' Cc= 0.900<br>n= 0.012, Flow Area= 1.23 sf |

**Primary OutFlow** Max=0.00 cfs @ 12.08 hrs HW=161.49' TW=161.64' (Dynamic Tailwater)
└─**1=15" HDPE N-12** ( Controls 0.00 cfs)

### Pond C05P: Catch Basin #5



## Summary for Pond D01P: Drain Manhole #1

[80] Warning: Exceeded Pond C05P by 0.24' @ 12.15 hrs (1.86 cfs 0.090 af)

Inflow Area = 0.059 ac,100.00% Impervious, Inflow Depth > 5.57" for 25Yr.-24Hr. event
Inflow = 0.32 cfs @ 12.08 hrs, Volume= 0.027 af
Outflow = 0.30 cfs @ 12.08 hrs, Volume= 0.027 af, Atten= 5%, Lag= 0.0 min
Primary = 0.30 cfs @ 12.08 hrs, Volume= 0.027 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 162.58' @ 12.59 hrs Surf.Area= 0.000 ac Storage= 0.001 af
Flood Elev= 166.75' Surf.Area= 0.000 ac Storage= 0.002 af

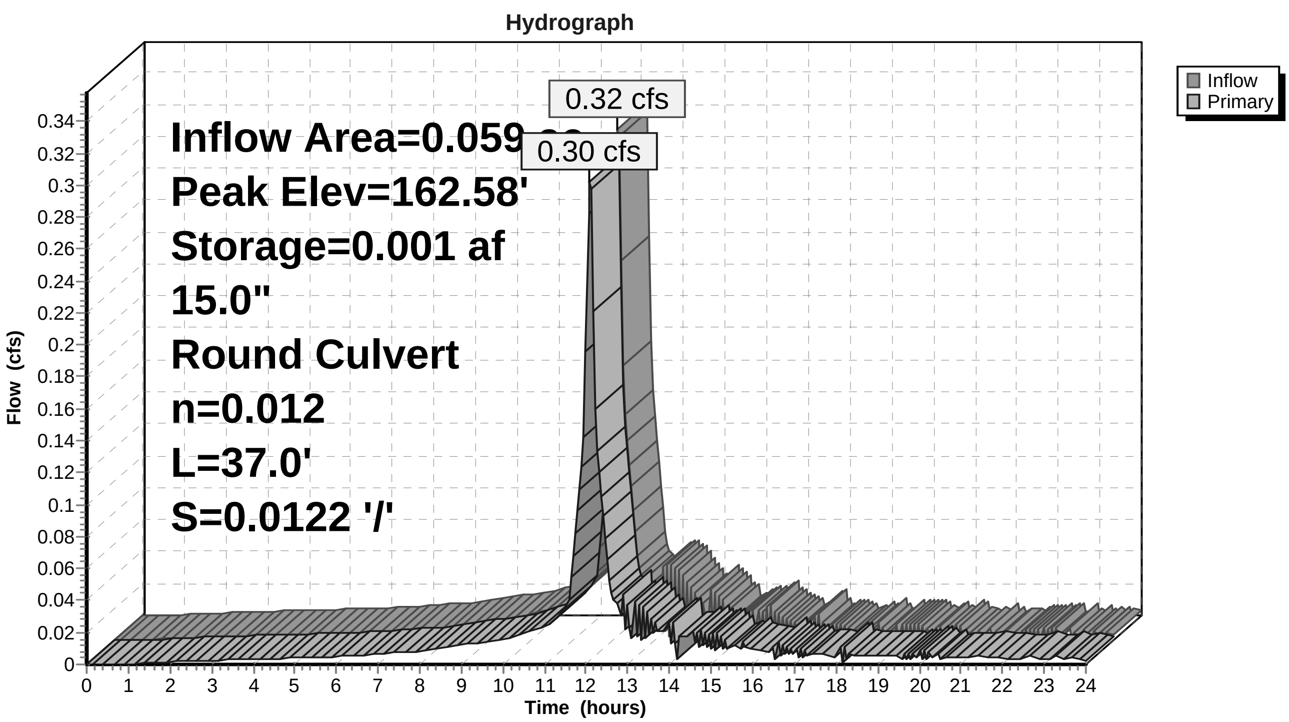
Plug-Flow detention time= 12.2 min calculated for 0.027 af (99% of inflow)
Center-of-Mass det. time= 4.0 min ( 751.9 - 748.0 )

| Volume | Invert | Avail.Storage | Storage Description |
|---|---|---|---|
| #1 | 160.25' | 0.002 af | **4.00'D x 6.50'H 4' Structure** |

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 160.25' | **15.0" Round 15" HDPE N-12**<br>L= 37.0' CPP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 160.25' / 159.80' S= 0.0122 '/' Cc= 0.900<br>n= 0.012, Flow Area= 1.23 sf |

**Primary OutFlow** Max=0.00 cfs @ 12.08 hrs HW=161.63' TW=161.87' (Dynamic Tailwater)
└**1=15" HDPE N-12** ( Controls 0.00 cfs)

### Pond D01P: Drain Manhole #1



Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=123,825 sf 3.77% Impervious Runoff Depth>0.12"
Flow Length=308' Tc=26.7 min CN=51 Runoff=0.05 cfs 0.029 af

**Subcatchment 11S: Rain Garden #101** Runoff Area=6,863 sf 6.35% Impervious Runoff Depth>0.40"
Tc=6.0 min CN=61 Runoff=0.04 cfs 0.005 af

**Subcatchment 12S: Infiltration Basin #102** Runoff Area=59,399 sf 4.02% Impervious Runoff Depth>0.02"
Flow Length=265' Tc=25.9 min CN=44 Runoff=0.00 cfs 0.002 af

**Subcatchment 21S: Catch Basin #1** Runoff Area=2,597 sf 100.00% Impervious Runoff Depth>2.85"
Tc=6.0 min CN=98 Runoff=0.17 cfs 0.014 af

**Subcatchment 22S: Catch Basin #2** Runoff Area=1,343 sf 100.00% Impervious Runoff Depth>2.85"
Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af

**Subcatchment 23S: Catch Basin #3** Runoff Area=4,735 sf 89.00% Impervious Runoff Depth>2.43"
Tc=6.0 min CN=94 Runoff=0.29 cfs 0.022 af

**Subcatchment 24S: Catch Basin #4** Runoff Area=5,442 sf 100.00% Impervious Runoff Depth>2.85"
Tc=6.0 min CN=98 Runoff=0.36 cfs 0.030 af

**Subcatchment 25S: Catch Basin #5** Runoff Area=2,550 sf 100.00% Impervious Runoff Depth>2.85"
Tc=6.0 min CN=98 Runoff=0.17 cfs 0.014 af

**Reach 100R: Final Reach #100** Inflow=0.11 cfs 0.091 af
Outflow=0.11 cfs 0.091 af

**Reach 101R: Reach to Wetland** Avg. Flow Depth=0.03' Max Vel=0.51 fps Inflow=0.05 cfs 0.063 af
n=0.035 L=66.5' S=0.0301 '/' Capacity=29.48 cfs Outflow=0.05 cfs 0.062 af

**Pond 101P: Rain Garden #101** Peak Elev=161.50' Storage=2,184 cf Inflow=1.12 cfs 0.092 af
Outflow=0.05 cfs 0.063 af

**Pond 102P: Infiltration Basin #102** Peak Elev=161.00' Storage=0 cf Inflow=0.00 cfs 0.002 af
Discarded=0.00 cfs 0.002 af Primary=0.00 cfs 0.000 af Outflow=0.00 cfs 0.002 af

**Pond C01P: Catch Basin #1** Peak Elev=162.67' Storage=0.000 af Inflow=0.17 cfs 0.014 af
15.0" Round Culvert n=0.012 L=16.0' S=0.0094 '/' Outflow=0.17 cfs 0.014 af

**Pond C02P: Catch Basin #2** Peak Elev=162.46' Storage=0.000 af Inflow=0.26 cfs 0.021 af
15.0" Round Culvert n=0.012 L=17.5' S=0.0697 '/' Outflow=0.26 cfs 0.021 af

**Pond C03P: Catch Basin #3** Peak Elev=161.50' Storage=0.000 af Inflow=0.29 cfs 0.022 af
15.0" Round Culvert n=0.012 L=103.5' S=0.0060 '/' Outflow=0.29 cfs 0.022 af

**Pond C04P: Catch Basin #4** Peak Elev=161.50' Storage=0.000 af Inflow=0.36 cfs 0.030 af
15.0" Round Culvert n=0.012 L=32.0' S=0.0072 '/' Outflow=0.36 cfs 0.029 af

**Pond C05P: Catch Basin #5** Peak Elev=161.50' Storage=0.000 af Inflow=0.17 cfs 0.014 af
15.0" Round Culvert n=0.012 L=50.0' S=0.0130 '/' Outflow=0.17 cfs 0.014 af

**Pond D01P: Drain Manhole #1** Peak Elev=161.50' Storage=0.000 af Inflow=0.17 cfs 0.014 af
15.0" Round Culvert n=0.012 L=37.0' S=0.0122 '/' Outflow=0.17 cfs 0.014 af

**Total Runoff Area = 4.746 ac Runoff Volume = 0.124 af Average Runoff Depth = 0.31"**
**88.57% Pervious = 4.204 ac 11.43% Impervious = 0.543 ac**

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=123,825 sf 3.77% Impervious Runoff Depth>0.59"
Flow Length=308' Tc=26.7 min CN=51 Runoff=0.76 cfs 0.140 af

**Subcatchment 11S: Rain Garden #101** Runoff Area=6,863 sf 6.35% Impervious Runoff Depth>1.15"
Tc=6.0 min CN=61 Runoff=0.19 cfs 0.015 af

**Subcatchment 12S: Infiltration Basin #102** Runoff Area=59,399 sf 4.02% Impervious Runoff Depth>0.29"
Flow Length=265' Tc=25.9 min CN=44 Runoff=0.10 cfs 0.033 af

**Subcatchment 21S: Catch Basin #1** Runoff Area=2,597 sf 100.00% Impervious Runoff Depth>4.39"
Tc=6.0 min CN=98 Runoff=0.26 cfs 0.022 af

**Subcatchment 22S: Catch Basin #2** Runoff Area=1,343 sf 100.00% Impervious Runoff Depth>4.39"
Tc=6.0 min CN=98 Runoff=0.14 cfs 0.011 af

**Subcatchment 23S: Catch Basin #3** Runoff Area=4,735 sf 89.00% Impervious Runoff Depth>3.94"
Tc=6.0 min CN=94 Runoff=0.46 cfs 0.036 af

**Subcatchment 24S: Catch Basin #4** Runoff Area=5,442 sf 100.00% Impervious Runoff Depth>4.39"
Tc=6.0 min CN=98 Runoff=0.55 cfs 0.046 af

**Subcatchment 25S: Catch Basin #5** Runoff Area=2,550 sf 100.00% Impervious Runoff Depth>4.39"
Tc=6.0 min CN=98 Runoff=0.26 cfs 0.021 af

**Reach 100R: Final Reach #100** Inflow=1.08 cfs 0.251 af
Outflow=1.08 cfs 0.251 af

**Reach 101R: Reach to Wetland** Avg. Flow Depth=0.06' Max Vel=0.88 fps Inflow=0.32 cfs 0.112 af
n=0.035 L=66.5' S=0.0301 '/' Capacity=29.48 cfs Outflow=0.32 cfs 0.112 af

**Pond 101P: Rain Garden #101** Peak Elev=162.06' Storage=3,011 cf Inflow=1.81 cfs 0.150 af
Outflow=0.32 cfs 0.112 af

**Pond 102P: Infiltration Basin #102** Peak Elev=161.39' Storage=221 cf Inflow=0.10 cfs 0.033 af
Discarded=0.05 cfs 0.033 af Primary=0.00 cfs 0.000 af Outflow=0.05 cfs 0.033 af

**Pond C01P: Catch Basin #1** Peak Elev=162.72' Storage=0.000 af Inflow=0.26 cfs 0.022 af
15.0" Round Culvert n=0.012 L=16.0' S=0.0094 '/' Outflow=0.26 cfs 0.022 af

**Pond C02P: Catch Basin #2** Peak Elev=162.51' Storage=0.000 af Inflow=0.40 cfs 0.033 af
15.0" Round Culvert n=0.012 L=17.5' S=0.0697 '/' Outflow=0.40 cfs 0.033 af

**Pond C03P: Catch Basin #3** Peak Elev=162.06' Storage=0.000 af Inflow=0.46 cfs 0.036 af
15.0" Round Culvert n=0.012 L=103.5' S=0.0060 '/' Outflow=0.45 cfs 0.035 af

**Pond C04P: Catch Basin #4** Peak Elev=162.06' Storage=0.001 af Inflow=0.55 cfs 0.046 af
15.0" Round Culvert n=0.012 L=32.0' S=0.0072 '/' Outflow=0.54 cfs 0.045 af

**Pond C05P: Catch Basin #5** Peak Elev=162.06' Storage=0.000 af Inflow=0.26 cfs 0.021 af
15.0" Round Culvert n=0.012 L=50.0' S=0.0130 '/' Outflow=0.26 cfs 0.021 af

**Pond D01P: Drain Manhole #1** Peak Elev=162.06' Storage=0.001 af Inflow=0.26 cfs 0.021 af
15.0" Round Culvert n=0.012 L=37.0' S=0.0122 '/' Outflow=0.24 cfs 0.021 af

**Total Runoff Area = 4.746 ac Runoff Volume = 0.324 af Average Runoff Depth = 0.82"**
**88.57% Pervious = 4.204 ac 11.43% Impervious = 0.543 ac**

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=123,825 sf 3.77% Impervious Runoff Depth>1.13"
Flow Length=308' Tc=26.7 min CN=51 Runoff=1.82 cfs 0.268 af

**Subcatchment 11S: Rain Garden #101** Runoff Area=6,863 sf 6.35% Impervious Runoff Depth>1.90"
Tc=6.0 min CN=61 Runoff=0.33 cfs 0.025 af

**Subcatchment 12S: Infiltration Basin #102** Runoff Area=59,399 sf 4.02% Impervious Runoff Depth>0.67"
Flow Length=265' Tc=25.9 min CN=44 Runoff=0.40 cfs 0.077 af

**Subcatchment 21S: Catch Basin #1** Runoff Area=2,597 sf 100.00% Impervious Runoff Depth>5.61"
Tc=6.0 min CN=98 Runoff=0.33 cfs 0.028 af

**Subcatchment 22S: Catch Basin #2** Runoff Area=1,343 sf 100.00% Impervious Runoff Depth>5.61"
Tc=6.0 min CN=98 Runoff=0.17 cfs 0.014 af

**Subcatchment 23S: Catch Basin #3** Runoff Area=4,735 sf 89.00% Impervious Runoff Depth>5.14"
Tc=6.0 min CN=94 Runoff=0.59 cfs 0.047 af

**Subcatchment 24S: Catch Basin #4** Runoff Area=5,442 sf 100.00% Impervious Runoff Depth>5.61"
Tc=6.0 min CN=98 Runoff=0.70 cfs 0.058 af

**Subcatchment 25S: Catch Basin #5** Runoff Area=2,550 sf 100.00% Impervious Runoff Depth>5.61"
Tc=6.0 min CN=98 Runoff=0.33 cfs 0.027 af

**Reach 100R: Final Reach #100** Inflow=2.28 cfs 0.423 af
Outflow=2.28 cfs 0.423 af

**Reach 101R: Reach to Wetland** Avg. Flow Depth=0.07' Max Vel=0.99 fps Inflow=0.46 cfs 0.156 af
n=0.035 L=66.5' S=0.0301 '/' Capacity=29.48 cfs Outflow=0.46 cfs 0.156 af

**Pond 101P: Rain Garden #101** Peak Elev=162.58' Storage=3,901 cf Inflow=2.39 cfs 0.198 af
Outflow=0.46 cfs 0.156 af

**Pond 102P: Infiltration Basin #102** Peak Elev=162.09' Storage=883 cf Inflow=0.40 cfs 0.077 af
Discarded=0.11 cfs 0.072 af Primary=0.00 cfs 0.000 af Outflow=0.11 cfs 0.072 af

**Pond C01P: Catch Basin #1** Peak Elev=162.76' Storage=0.000 af Inflow=0.33 cfs 0.028 af
15.0" Round Culvert n=0.012 L=16.0' S=0.0094 '/' Outflow=0.33 cfs 0.028 af

**Pond C02P: Catch Basin #2** Peak Elev=162.59' Storage=0.000 af Inflow=0.51 cfs 0.042 af
15.0" Round Culvert n=0.012 L=17.5' S=0.0697 '/' Outflow=0.51 cfs 0.042 af

**Pond C03P: Catch Basin #3** Peak Elev=162.58' Storage=0.001 af Inflow=0.59 cfs 0.047 af
15.0" Round Culvert n=0.012 L=103.5' S=0.0060 '/' Outflow=0.57 cfs 0.046 af

**Pond C04P: Catch Basin #4** Peak Elev=162.58' Storage=0.001 af Inflow=0.70 cfs 0.058 af
15.0" Round Culvert n=0.012 L=32.0' S=0.0072 '/' Outflow=0.68 cfs 0.058 af

**Pond C05P: Catch Basin #5** Peak Elev=162.58' Storage=0.000 af Inflow=0.33 cfs 0.027 af
15.0" Round Culvert n=0.012 L=50.0' S=0.0130 '/' Outflow=0.32 cfs 0.027 af

**Pond D01P: Drain Manhole #1** Peak Elev=162.58' Storage=0.001 af Inflow=0.32 cfs 0.027 af
15.0" Round Culvert n=0.012 L=37.0' S=0.0122 '/' Outflow=0.30 cfs 0.027 af

**Total Runoff Area = 4.746 ac Runoff Volume = 0.544 af Average Runoff Depth = 1.38"**
**88.57% Pervious = 4.204 ac 11.43% Impervious = 0.543 ac**

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=123,825 sf 3.77% Impervious Runoff Depth>1.74"
Flow Length=308' Tc=26.7 min CN=51 Runoff=3.07 cfs 0.411 af

**Subcatchment 11S: Rain Garden #101** Runoff Area=6,863 sf 6.35% Impervious Runoff Depth>2.69"
Tc=6.0 min CN=61 Runoff=0.48 cfs 0.035 af

**Subcatchment 12S: Infiltration Basin #102** Runoff Area=59,399 sf 4.02% Impervious Runoff Depth>1.14"
Flow Length=265' Tc=25.9 min CN=44 Runoff=0.82 cfs 0.130 af

**Subcatchment 21S: Catch Basin #1** Runoff Area=2,597 sf 100.00% Impervious Runoff Depth>6.75"
Tc=6.0 min CN=98 Runoff=0.40 cfs 0.034 af

**Subcatchment 22S: Catch Basin #2** Runoff Area=1,343 sf 100.00% Impervious Runoff Depth>6.75"
Tc=6.0 min CN=98 Runoff=0.21 cfs 0.017 af

**Subcatchment 23S: Catch Basin #3** Runoff Area=4,735 sf 89.00% Impervious Runoff Depth>6.27"
Tc=6.0 min CN=94 Runoff=0.71 cfs 0.057 af

**Subcatchment 24S: Catch Basin #4** Runoff Area=5,442 sf 100.00% Impervious Runoff Depth>6.75"
Tc=6.0 min CN=98 Runoff=0.84 cfs 0.070 af

**Subcatchment 25S: Catch Basin #5** Runoff Area=2,550 sf 100.00% Impervious Runoff Depth>6.75"
Tc=6.0 min CN=98 Runoff=0.39 cfs 0.033 af

**Reach 100R: Final Reach #100** Inflow=3.62 cfs 0.610 af
Outflow=3.62 cfs 0.610 af

**Reach 101R: Reach to Wetland** Avg. Flow Depth=0.08' Max Vel=1.06 fps Inflow=0.58 cfs 0.199 af
n=0.035 L=66.5' S=0.0301 '/' Capacity=29.48 cfs Outflow=0.58 cfs 0.199 af

**Pond 101P: Rain Garden #101** Peak Elev=163.05' Storage=4,813 cf Inflow=2.96 cfs 0.245 af
Outflow=0.58 cfs 0.199 af

**Pond 102P: Infiltration Basin #102** Peak Elev=162.64' Storage=1,944 cf Inflow=0.82 cfs 0.130 af
Discarded=0.16 cfs 0.118 af Primary=0.00 cfs 0.000 af Outflow=0.16 cfs 0.118 af

**Pond C01P: Catch Basin #1** Peak Elev=163.05' Storage=0.000 af Inflow=0.40 cfs 0.034 af
15.0" Round Culvert n=0.012 L=16.0' S=0.0094 '/' Outflow=0.40 cfs 0.034 af

**Pond C02P: Catch Basin #2** Peak Elev=163.05' Storage=0.000 af Inflow=0.61 cfs 0.051 af
15.0" Round Culvert n=0.012 L=17.5' S=0.0697 '/' Outflow=0.61 cfs 0.051 af

**Pond C03P: Catch Basin #3** Peak Elev=163.05' Storage=0.001 af Inflow=0.71 cfs 0.057 af
15.0" Round Culvert n=0.012 L=103.5' S=0.0060 '/' Outflow=0.69 cfs 0.056 af

**Pond C04P: Catch Basin #4** Peak Elev=163.05' Storage=0.001 af Inflow=0.84 cfs 0.070 af
15.0" Round Culvert n=0.012 L=32.0' S=0.0072 '/' Outflow=0.82 cfs 0.070 af

**Pond C05P: Catch Basin #5** Peak Elev=163.05' Storage=0.001 af Inflow=0.39 cfs 0.033 af
15.0" Round Culvert n=0.012 L=50.0' S=0.0130 '/' Outflow=0.38 cfs 0.033 af

**Pond D01P: Drain Manhole #1** Peak Elev=163.05' Storage=0.001 af Inflow=0.38 cfs 0.033 af
15.0" Round Culvert n=0.012 L=37.0' S=0.0122 '/' Outflow=0.36 cfs 0.032 af

**Total Runoff Area = 4.746 ac Runoff Volume = 0.787 af Average Runoff Depth = 1.99"**
**88.57% Pervious = 4.204 ac 11.43% Impervious = 0.543 ac**

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Subcatchment #1** Runoff Area=123,825 sf 3.77% Impervious Runoff Depth>2.57"
Flow Length=308' Tc=26.7 min CN=51 Runoff=4.79 cfs 0.608 af

**Subcatchment 11S: Rain Garden #101** Runoff Area=6,863 sf 6.35% Impervious Runoff Depth>3.72"
Tc=6.0 min CN=61 Runoff=0.67 cfs 0.049 af

**Subcatchment 12S: Infiltration Basin #102** Runoff Area=59,399 sf 4.02% Impervious Runoff Depth>1.81"
Flow Length=265' Tc=25.9 min CN=44 Runoff=1.48 cfs 0.206 af

**Subcatchment 21S: Catch Basin #1** Runoff Area=2,597 sf 100.00% Impervious Runoff Depth>8.12"
Tc=6.0 min CN=98 Runoff=0.48 cfs 0.040 af

**Subcatchment 22S: Catch Basin #2** Runoff Area=1,343 sf 100.00% Impervious Runoff Depth>8.12"
Tc=6.0 min CN=98 Runoff=0.25 cfs 0.021 af

**Subcatchment 23S: Catch Basin #3** Runoff Area=4,735 sf 89.00% Impervious Runoff Depth>7.64"
Tc=6.0 min CN=94 Runoff=0.86 cfs 0.069 af

**Subcatchment 24S: Catch Basin #4** Runoff Area=5,442 sf 100.00% Impervious Runoff Depth>8.12"
Tc=6.0 min CN=98 Runoff=1.00 cfs 0.084 af

**Subcatchment 25S: Catch Basin #5** Runoff Area=2,550 sf 100.00% Impervious Runoff Depth>8.12"
Tc=6.0 min CN=98 Runoff=0.47 cfs 0.040 af

**Reach 100R: Final Reach #100** Inflow=6.14 cfs 0.860 af
Outflow=6.14 cfs 0.860 af

**Reach 101R: Reach to Wetland** Avg. Flow Depth=0.12' Max Vel=1.39 fps Inflow=1.40 cfs 0.253 af
n=0.035 L=66.5' S=0.0301 '/' Capacity=29.48 cfs Outflow=1.40 cfs 0.253 af

**Pond 101P: Rain Garden #101** Peak Elev=163.30' Storage=5,349 cf Inflow=3.64 cfs 0.302 af
Outflow=1.40 cfs 0.253 af

**Pond 102P: Infiltration Basin #102** Peak Elev=163.05' Storage=3,021 cf Inflow=1.48 cfs 0.206 af
Discarded=0.42 cfs 0.186 af Primary=0.00 cfs 0.000 af Outflow=0.42 cfs 0.186 af

**Pond C01P: Catch Basin #1** Peak Elev=163.30' Storage=0.000 af Inflow=0.48 cfs 0.040 af
15.0" Round Culvert n=0.012 L=16.0' S=0.0094 '/' Outflow=0.48 cfs 0.040 af

**Pond C02P: Catch Basin #2** Peak Elev=163.30' Storage=0.000 af Inflow=0.72 cfs 0.061 af
15.0" Round Culvert n=0.012 L=17.5' S=0.0697 '/' Outflow=0.72 cfs 0.061 af

**Pond C03P: Catch Basin #3** Peak Elev=163.30' Storage=0.001 af Inflow=0.86 cfs 0.069 af
15.0" Round Culvert n=0.012 L=103.5' S=0.0060 '/' Outflow=0.84 cfs 0.069 af

**Pond C04P: Catch Basin #4** Peak Elev=163.30' Storage=0.001 af Inflow=1.00 cfs 0.084 af
15.0" Round Culvert n=0.012 L=32.0' S=0.0072 '/' Outflow=0.98 cfs 0.084 af

**Pond C05P: Catch Basin #5** Peak Elev=163.30' Storage=0.001 af Inflow=0.47 cfs 0.040 af
15.0" Round Culvert n=0.012 L=50.0' S=0.0130 '/' Outflow=0.46 cfs 0.039 af

**Pond D01P: Drain Manhole #1** Peak Elev=163.30' Storage=0.001 af Inflow=0.46 cfs 0.039 af
15.0" Round Culvert n=0.012 L=37.0' S=0.0122 '/' Outflow=0.44 cfs 0.039 af

**Total Runoff Area = 4.746 ac Runoff Volume = 1.116 af Average Runoff Depth = 2.82"**
**88.57% Pervious = 4.204 ac 11.43% Impervious = 0.543 ac**

**Appendix III** - Calculations, Charts, & Graphs

Extreme Precipitation Tables
Rip-Rap Calculations
NHDES AoT Spreadsheet
USDA / NRCS Websoil
Site Specific Soil Survey Report & Plan
Stormwater System Management: Inspection and Maintenance
Watershed Report Card, 303(d) List, & ORW List
Infiltration Feasibility Study
KSat NH Manual
Manual Filtrexx Silt Soxx Specifications Cut Sheets

# Extreme Precipitation Tables

## Northeast Regional Climate Center

***Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.***

| | |
|---|---|
| **Smoothing** | Yes |
| **State** | New Hampshire |
| **Location** | |
| **Longitude** | 70.995 degrees West |
| **Latitude** | 43.187 degrees North |
| **Elevation** | 0 feet |
| **Date/Time** | Wed, 02 Mar 2022 12:30:12 -0500 |

## Extreme Precipitation Estimates

| | 5min | 10min | 15min | 30min | 60min | 120min | | 1hr | 2hr | 3hr | 6hr | 12hr | 24hr | 48hr | | 1day | 2day | 4day | 7day | 10day | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| **1yr** | 0.26 | 0.40 | 0.50 | 0.65 | 0.81 | 1.03 | **1yr** | 0.70 | 0.98 | 1.20 | 1.53 | 1.98 | 2.57 | 2.81 | **1yr** | 2.27 | 2.70 | 3.11 | 3.83 | 4.41 | **1yr** |
| **2yr** | 0.32 | 0.49 | 0.61 | 0.80 | 1.01 | 1.28 | **2yr** | 0.87 | 1.16 | 1.49 | 1.89 | 2.41 | 3.09 | 3.43 | **2yr** | 2.73 | 3.30 | 3.80 | 4.52 | 5.15 | **2yr** |
| **5yr** | 0.37 | 0.57 | 0.72 | 0.96 | 1.23 | 1.57 | **5yr** | 1.06 | 1.44 | 1.84 | 2.36 | 3.03 | 3.90 | 4.39 | **5yr** | 3.45 | 4.22 | 4.83 | 5.71 | 6.46 | **5yr** |
| **10yr** | 0.40 | 0.63 | 0.80 | 1.09 | 1.42 | 1.84 | **10yr** | 1.22 | 1.69 | 2.17 | 2.80 | 3.61 | 4.66 | 5.29 | **10yr** | 4.12 | 5.09 | 5.81 | 6.81 | 7.66 | **10yr** |
| **25yr** | 0.46 | 0.74 | 0.94 | 1.29 | 1.72 | 2.26 | **25yr** | 1.49 | 2.09 | 2.69 | 3.50 | 4.55 | 5.89 | 6.78 | **25yr** | 5.21 | 6.52 | 7.41 | 8.60 | 9.62 | **25yr** |
| **50yr** | 0.52 | 0.83 | 1.06 | 1.48 | 2.00 | 2.66 | **50yr** | 1.73 | 2.45 | 3.17 | 4.15 | 5.42 | 7.04 | 8.18 | **50yr** | 6.23 | 7.87 | 8.91 | 10.27 | 11.43 | **50yr** |
| **100yr** | 0.58 | 0.94 | 1.21 | 1.71 | 2.33 | 3.12 | **100yr** | 2.01 | 2.88 | 3.74 | 4.92 | 6.45 | 8.42 | 9.87 | **100yr** | 7.45 | 9.50 | 10.71 | 12.27 | 13.58 | **100yr** |
| **200yr** | 0.64 | 1.05 | 1.36 | 1.96 | 2.71 | 3.67 | **200yr** | 2.34 | 3.39 | 4.42 | 5.85 | 7.69 | 10.07 | 11.92 | **200yr** | 8.91 | 11.47 | 12.88 | 14.66 | 16.15 | **200yr** |
| **500yr** | 0.76 | 1.25 | 1.63 | 2.36 | 3.31 | 4.54 | **500yr** | 2.86 | 4.21 | 5.49 | 7.33 | 9.70 | 12.76 | 15.31 | **500yr** | 11.30 | 14.72 | 16.46 | 18.57 | 20.33 | **500yr** |

## Lower Confidence Limits

| | 5min | 10min | 15min | 30min | 60min | 120min | | 1hr | 2hr | 3hr | 6hr | 12hr | 24hr | 48hr | | 1day | 2day | 4day | 7day | 10day | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| **1yr** | 0.24 | 0.36 | 0.45 | 0.60 | 0.74 | 0.90 | **1yr** | 0.64 | 0.88 | 0.92 | 1.25 | 1.53 | 1.95 | 2.49 | **1yr** | 1.73 | 2.40 | 2.92 | 3.30 | 3.97 | **1yr** |
| **2yr** | 0.31 | 0.49 | 0.60 | 0.81 | 1.00 | 1.18 | **2yr** | 0.86 | 1.15 | 1.36 | 1.82 | 2.34 | 3.00 | 3.33 | **2yr** | 2.65 | 3.20 | 3.68 | 4.41 | 5.03 | **2yr** |
| **5yr** | 0.35 | 0.54 | 0.67 | 0.92 | 1.16 | 1.40 | **5yr** | 1.01 | 1.37 | 1.61 | 2.14 | 2.77 | 3.61 | 4.04 | **5yr** | 3.20 | 3.89 | 4.49 | 5.35 | 6.02 | **5yr** |
| **10yr** | 0.38 | 0.59 | 0.73 | 1.02 | 1.32 | 1.60 | **10yr** | 1.14 | 1.56 | 1.82 | 2.44 | 3.13 | 4.14 | 4.68 | **10yr** | 3.67 | 4.50 | 5.20 | 6.20 | 6.88 | **10yr** |
| **25yr** | 0.44 | 0.67 | 0.83 | 1.19 | 1.56 | 1.91 | **25yr** | 1.35 | 1.87 | 2.12 | 2.84 | 3.65 | 4.94 | 5.65 | **25yr** | 4.38 | 5.43 | 6.33 | 7.53 | 8.33 | **25yr** |
| **50yr** | 0.49 | 0.74 | 0.92 | 1.32 | 1.78 | 2.19 | **50yr** | 1.54 | 2.14 | 2.37 | 3.21 | 4.10 | 5.65 | 6.51 | **50yr** | 5.00 | 6.26 | 7.35 | 8.71 | 9.61 | **50yr** |
| **100yr** | 0.54 | 0.82 | 1.03 | 1.49 | 2.04 | 2.52 | **100yr** | 1.76 | 2.46 | 2.66 | 3.60 | 4.58 | 6.44 | 7.49 | **100yr** | 5.70 | 7.20 | 8.54 | 10.08 | 11.00 | **100yr** |
| **200yr** | 0.61 | 0.91 | 1.16 | 1.67 | 2.34 | 2.88 | **200yr** | 2.02 | 2.82 | 2.98 | 4.05 | 5.12 | 7.34 | 8.91 | **200yr** | 6.50 | 8.57 | 9.94 | 11.66 | 12.62 | **200yr** |
| **500yr** | 0.71 | 1.06 | 1.36 | 1.98 | 2.81 | 3.48 | **500yr** | 2.43 | 3.40 | 3.48 | 4.72 | 5.97 | 8.68 | 10.81 | **500yr** | 7.68 | 10.39 | 12.15 | 14.16 | 15.07 | **500yr** |

## Upper Confidence Limits

| | 5min | 10min | 15min | 30min | 60min | 120min | | 1hr | 2hr | 3hr | 6hr | 12hr | 24hr | 48hr | | 1day | 2day | 4day | 7day | 10day | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| **1yr** | 0.28 | 0.43 | 0.53 | 0.71 | 0.87 | 1.07 | **1yr** | 0.75 | 1.05 | 1.23 | 1.73 | 2.19 | 2.77 | 3.03 | **1yr** | 2.45 | 2.91 | 3.34 | 4.12 | 4.74 | **1yr** |
| **2yr** | 0.33 | 0.50 | 0.62 | 0.84 | 1.03 | 1.24 | **2yr** | 0.89 | 1.21 | 1.46 | 1.94 | 2.50 | 3.20 | 3.54 | **2yr** | 2.83 | 3.41 | 3.92 | 4.65 | 5.30 | **2yr** |
| **5yr** | 0.39 | 0.60 | 0.75 | 1.02 | 1.30 | 1.57 | **5yr** | 1.13 | 1.54 | 1.84 | 2.47 | 3.16 | 4.19 | 4.73 | **5yr** | 3.71 | 4.55 | 5.19 | 6.06 | 6.87 | **5yr** |
| **10yr** | 0.45 | 0.70 | 0.87 | 1.21 | 1.56 | 1.90 | **10yr** | 1.35 | 1.86 | 2.21 | 3.01 | 3.80 | 5.17 | 5.89 | **10yr** | 4.58 | 5.67 | 6.44 | 7.41 | 8.36 | **10yr** |
| **25yr** | 0.55 | 0.84 | 1.05 | 1.49 | 1.97 | 2.45 | **25yr** | 1.70 | 2.39 | 2.84 | 3.90 | 4.87 | 6.85 | 7.89 | **25yr** | 6.06 | 7.59 | 8.54 | 9.74 | 10.77 | **25yr** |
| **50yr** | 0.64 | 0.97 | 1.21 | 1.74 | 2.34 | 2.95 | **50yr** | 2.02 | 2.88 | 3.45 | 4.74 | 5.89 | 8.48 | 9.87 | **50yr** | 7.50 | 9.49 | 10.60 | 11.95 | 13.16 | **50yr** |
| **100yr** | 0.74 | 1.12 | 1.41 | 2.03 | 2.79 | 3.56 | **100yr** | 2.41 | 3.48 | 4.17 | 5.79 | 7.14 | 10.50 | 12.35 | **100yr** | 9.29 | 11.87 | 13.14 | 14.68 | 16.06 | **100yr** |
| **200yr** | 0.86 | 1.30 | 1.64 | 2.38 | 3.32 | 4.30 | **200yr** | 2.86 | 4.21 | 5.07 | 7.07 | 8.63 | 13.04 | 15.10 | **200yr** | 11.54 | 14.52 | 16.29 | 18.02 | 19.65 | **200yr** |
| **500yr** | 1.05 | 1.57 | 2.02 | 2.93 | 4.16 | 5.51 | **500yr** | 3.59 | 5.38 | 6.53 | 9.22 | 11.13 | 17.41 | 20.24 | **500yr** | 15.41 | 19.46 | 21.64 | 23.68 | 25.66 | **500yr** |

Powered by ACIS
Northeast Regional Climate Center

# RIP RAP CALCULATIONS

21-163 49 Winkley Pond Road
Hambone LLC
Barrington, NH

**Berry Surveying & Engineering**
335 Second Crown Point Road
Barrington, NH
16-Aug-23

Rip Rap equations were obtained from the *Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire.* Rip Rap was sized for the 25 year storm event. (Some d50 sizes and T values have been modified)

---

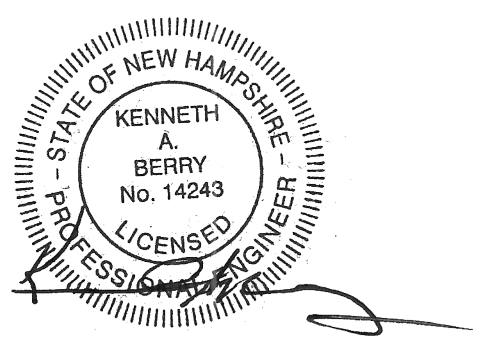
**TAILWATER < HALF THE Do**

La = (1.8 x Q) / Do 3/2 + (7 x Do)     Q = Peak Flow & Do is Pipe Diameter
W = La + 3*Do or defined channel width
d50 = (0.02 x Q4/3) / (Tw x Do)     Tw = Tailwater Depth
T = Largest Stone Size x 1.5

| Culvert or Catch Basin | Tailwater (Feet) Tw | Discharge (C.F.S.) Q | Diameter of Pipe Do | Length of Rip Rap La (feet) | Width of Rip Rap W (feet) | d50-Stone Rip Rap d50(ft.) | Actual Size | Thickness |
|---|---|---|---|---|---|---|---|---|
| 15" HDPE (Pond #D01P) | 0.25 | 0.30 | 1.25 | 9.1 | 12.9 | 0.01 | 0.50 | 1.20 |
| 15" HDPE (Pond #C02P) | 0.25 | 0.51 | 1.25 | 9.4 | 13.2 | 0.03 | 0.50 | 1.20 |
| 15" HDPE (Pond #C03P) | 0.25 | 0.57 | 1.25 | 9.5 | 13.2 | 0.03 | 0.50 | 1.20 |
| 15" HDPE (Pond #C04P) | 0.25 | 0.68 | 1.25 | 9.6 | 13.4 | 0.04 | 0.50 | 1.20 |
| 15" HDPE (Pond #101P) | 0.25 | 0.46 | 1.25 | 9.3 | 13.1 | 0.02 | 0.50 | 1.20 |

Please note that the designer chose to use the 25 Year Event for the dimensional calculations.

| Table 7-24 -- Recommended Rip Rap Gradation Ranges | | | | |
|---|---|---|---|---|
| | | | | |
| d50 Size = | 0.5 | Feet | 6 | Inches |
| % of Weight Smaller | | Size of Stone (Inches) | | |
| Than the Given d50 Size | | From | | To |
| 100% | | 9 | | 12 |
| 85% | | 8 | | 11 |
| 50% | | 6 | | 9 |
| 15% | | 2 | | 3 |



# GROUNDWATER RECHARGE VOLULME (GRV) CALCULATION
## (Env-Wq 1507.04)

| | | | |
|---|---|---|---|
| 0.02 | ac | Area of HSG A soil that was replaced by impervious cover | 0.40" |
| 0.32 | ac | Area of HSG B soil that was replaced by impervious cover | 0.25" |
| - | ac | Area of HSG C soil that was replaced by impervious cover | 0.10" |
| - | ac | Area of HSG D soil or impervious cover that was replaced by impervious cover | 0.0" |
| 0.26 | inches | Rd = Weighted groundwater recharge depth | |
| 0.088 | ac-in | GRV = AI * Rd | |
| 319 | cf | GRV conversion (ac-in x 43,560 sf/ac x 1ft/12”) | |

**Provide calculations below showing that the project meets the groundwater recharge requirements (Env-Wq 1507.04):**

4,591 Cf Infiltrated in Infiltration Basin #102

NEW HAMPSHIRE DEPARTMENT OF Environmental Services

# FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

**Type/Node Name:** **Rain Garden #101**

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

| Value | Unit | Description | Criteria |
|---|---|---|---|
| Yes | | Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.07(a). | |
| 1.90 | ac | A = Area draining to the practice | |
| 0.44 | ac | $A_I$ = Impervious area draining to the practice | |
| 0.23 | decimal | I = Percent impervious area draining to the practice, in decimal form | |
| 0.26 | unitless | Rv = Runoff coefficient = 0.05 + (0.9 x I) | |
| 0.49 | ac-in | WQV= 1” x Rv x A | |
| 1,768 | cf | WQV conversion (ac-in x 43,560 sf/ac x 1ft/12”) | |
| 442 | cf | 25% x WQV (check calc for sediment forebay volume) | |
| 1,326 | cf | 75% x WQV (check calc for surface sand filter volume) | |
| Deep Sump | | Method of Pretreatment? (not required for clean or roof runoff) | |
| N/A | cf | $V_{SED}$ = Sediment forebay volume, if used for pretreatment | **≥ 25%WQV** |
| **Calculate time to drain if system IS NOT underdrained:** | | | |
| | sf | $A_{SA}$ = Surface area of the practice | |
| | iph | $Ksat_{DESIGN}$ = Design infiltration rate[1] | |
| | Yes/No | If Ksat (prior to factor of safety) is < 0.50 iph, has an underdrain been provided? (Use the calculations below) | |
| - | hours | $T_{DRAIN}$ = Drain time = V / ($A_{SA}$ * $I_{DESIGN}$) | **≤ 72-hrs** |
| **Calculate time to drain if system IS underdrained:** | | | |
| 161.39 | ft | $E_{WQV}$ = Elevation of WQV (attach stage-storage table) | |
| 0.05 | cfs | $Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) | |
| 19.65 | hours | $T_{DRAIN}$ = Drain time = 2WQV/$Q_{WQV}$ | **≤ 72-hrs** |
| 158.30 | feet | $E_{FC}$ = Elevation of the bottom of the filter course material[2] | |
| 157.30 | feet | $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable | |
| 159.67 | feet | $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pit) | |
| 156.33 | feet | $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test pit) | |
| 1.00 | feet | $D_{FC\ to\ UD}$ = Depth to UD from the bottom of the filter course | **≥ 1'** |
| 1.97 | feet | $D_{FC\ to\ ROCK}$ = Depth to bedrock from the bottom of the filter course | **≥ 1'** |
| (1.37) | feet | $D_{FC\ to\ SHWT}$ = Depth to SHWT from the bottom of the filter course | **≥ 1'** |
| 163.05 | ft | Peak elevation of the 50-year storm event (infiltration can be used in analysis) | |
| 163.50 | ft | Elevation of the top of the practice | |
| YES | | 50 peak elevation ≤ Elevation of the top of the practice | **← yes** |
| **If a surface sand filter or underground sand filter is proposed:** | | | |
| YES | ac | Drainage Area check. | **< 10 ac** |
| | cf | V = Volume of storage[3] (attach a stage-storage table) | **≥ 75%WQV** |
| | inches | $D_{FC}$ = Filter course thickness | **18", or 24" if within GPA** |
| Sheet | | Note what sheet in the plan set contains the filter course specification. | |
| | Yes/No | Access grate provided? | **← yes** |

| | | | |
|---|---|---|---|
| **If a bioretention area is proposed:** | | | |
| YES | ac | Drainage Area no larger than 5 ac? | **← yes** |
| 1,928 | cf | V = Volume of storage[3] (attach a stage-storage table) | **≥ WQV** |
| 18.0 | inches | $D_{FC}$ = Filter course thickness | **18", or 24" if within GPA** |
| Sheet | P101 | Note what sheet in the plan set contains the filter course specification | |
| 3.0 | :1 | Pond side slopes | **≥ 3:1** |
| Sheet | P101 | Note what sheet in the plan set contains the planting plans and surface cover | |
| **If porous pavement is proposed:** | | | |
| | | Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.) | |
| | acres | $A_{SA}$ = Surface area of the pervious pavement | |
| | :1 | Ratio of the contributing area to the pervious surface area | **≤ 5:1** |
| | inches | $D_{FC}$ = Filter course thickness | **12", or 18" if within GPA** |
| Sheet | | Note what sheet in the plan set contains the filter course spec. | **mod. 304.1 (see spec)** |

1. Rate of the limiting layer (either the filter course or the underlying soil). $Ksat_{design}$ includes factor of safey. See Env-Wq 1504.14 for guidance on determining the infiltration rate.

2. See lines 34, 40 and 48 for required depths of filter media.

3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes: ______________________________

## Summary for Pond 101P: Rain Garden #101

[80] Warning: Exceeded Pond C02P by 0.09' @ 12.20 hrs (0.54 cfs 0.018 af)
[80] Warning: Exceeded Pond C03P by 0.24' @ 12.10 hrs (2.58 cfs 0.154 af)
[80] Warning: Exceeded Pond C04P by 0.24' @ 12.10 hrs (2.92 cfs 0.257 af)
[80] Warning: Exceeded Pond D01P by 0.26' @ 12.10 hrs (3.00 cfs 0.547 af)

Inflow Area = 1.904 ac, 22.87% Impervious, Inflow Depth > 1.54" for 50Yr.-24Hr. event
Inflow = 2.96 cfs @ 12.09 hrs, Volume= 0.245 af
Outflow = 0.58 cfs @ 12.53 hrs, Volume= 0.199 af, Atten= 80%, Lag= 26.6 min
Primary = 0.58 cfs @ 12.53 hrs, Volume= 0.199 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 163.05' @ 12.53 hrs Surf.Area= 636 sf Storage= 4,813 cf
Flood Elev= 163.50' Surf.Area= 636 sf Storage= 5,797 cf

Plug-Flow detention time= 171.7 min calculated for 0.199 af (81% of inflow)
Center-of-Mass det. time= 95.8 min ( 860.7 - 764.9 )

| Volume | Invert | Avail.Storage | Storage Description |
|---|---|---|---|
| #1 | 157.30' | 254 cf | **Stone (Irregular)** Listed below (Recalc)<br>636 cf Overall x 40.0% Voids |
| #2 | 158.30' | 191 cf | **BioMedia (Irregular)** Listed below (Recalc) -Impervious<br>954 cf Overall x 20.0% Voids |
| #3 | 159.80' | 5,352 cf | **Open Water Storage (Irregular)** Listed below (Recalc) -Impervious |
| | | 5,797 cf | Total Available Storage |

| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 157.30 | 636 | 110.2 | 0 | 0 | 636 |
| 158.30 | 636 | 110.2 | 636 | 636 | 746 |

| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 158.30 | 636 | 110.2 | 0 | 0 | 636 |
| 159.80 | 636 | 110.2 | 954 | 954 | 801 |

| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 159.80 | 636 | 110.2 | 0 | 0 | 636 |
| 160.00 | 806 | 118.2 | 144 | 144 | 783 |
| 161.00 | 1,145 | 130.3 | 971 | 1,114 | 1,053 |
| 162.00 | 1,569 | 149.8 | 1,351 | 2,466 | 1,509 |
| 163.00 | 2,047 | 168.6 | 1,803 | 4,269 | 2,012 |
| 163.50 | 2,290 | 177.8 | 1,084 | 5,352 | 2,280 |

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 157.30' | **15.0" Round 15" HDPE N-12**<br>L= 56.7' CPP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 157.30' / 157.00' S= 0.0053 '/' Cc= 0.900<br>n= 0.012, Flow Area= 1.23 sf |
| #2 | Device 1 | 157.30' | **1.0" Vert. 1" Orifice** C= 0.600 |
| #3 | Device 2 | 157.30' | **10.000 in/hr Filtration thru media over Surface area** |
| #4 | Device 1 | 161.50' | **4.0" Vert. 4" Orifice** C= 0.600 |
| #5 | Device 1 | 163.00' | **48.0" Vert. 48" Outlet Structure** C= 0.600 |

**Primary OutFlow** Max=0.58 cfs @ 12.53 hrs HW=163.05' TW=157.08' (Dynamic Tailwater)
└─**1=15" HDPE N-12** (Passes 0.58 cfs of 13.31 cfs potential flow)
  ├─**2=1" Orifice** (Orifice Controls 0.06 cfs @ 11.50 fps)
  │ └─**3=Filtration thru media** (Passes 0.06 cfs of 0.15 cfs potential flow)
  ├─**4=4" Orifice** (Orifice Controls 0.49 cfs @ 5.66 fps)
  └─**5=48" Outlet Structure** (Orifice Controls 0.02 cfs @ 0.74 fps)

## Stage-Area-Storage for Pond 101P: Rain Garden #101

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---:|---:|---:|
| 157.30 | **636** | 0 |
| 157.40 | 636 | 25 |
| 157.50 | 636 | 51 |
| 157.60 | 636 | 76 |
| 157.70 | 636 | 102 |
| 157.80 | 636 | 127 |
| 157.90 | 636 | 153 |
| 158.00 | 636 | 178 |
| 158.10 | 636 | 204 |
| 158.20 | 636 | 229 |
| 158.30 | 636 | 254 |
| 158.40 | 636 | 267 |
| 158.50 | 636 | 280 |
| 158.60 | 636 | 293 |
| 158.70 | 636 | 305 |
| 158.80 | 636 | 318 |
| 158.90 | 636 | 331 |
| 159.00 | 636 | 343 |
| 159.10 | 636 | 356 |
| 159.20 | 636 | 369 |
| 159.30 | 636 | 382 |
| 159.40 | 636 | 394 |
| 159.50 | 636 | 407 |
| 159.60 | 636 | 420 |
| 159.70 | 636 | 432 |
| 159.80 | 636 | 445 |
| 159.90 | 636 | 513 |
| 160.00 | 636 | 589 |
| 160.10 | 636 | 671 |
| 160.20 | 636 | 757 |
| 160.30 | 636 | 845 |
| 160.40 | 636 | 937 |
| 160.50 | 636 | 1,032 |
| 160.60 | 636 | 1,130 |
| 160.70 | 636 | 1,232 |
| 160.80 | 636 | 1,338 |
| 160.90 | 636 | 1,447 |
| 161.00 | 636 | 1,560 |
| 161.10 | 636 | 1,676 |
| 161.20 | 636 | 1,797 |
| 161.30 | 636 | 1,921 |
| 161.40 | 636 | 2,050 |
| 161.50 | 636 | 2,182 |
| 161.60 | 636 | 2,319 |
| 161.70 | 636 | 2,461 |
| 161.80 | 636 | 2,606 |
| 161.90 | 636 | 2,756 |
| 162.00 | 636 | 2,911 |
| 162.10 | 636 | 3,070 |
| 162.20 | 636 | 3,234 |
| 162.30 | 636 | 3,402 |
| 162.40 | 636 | 3,575 |
| 162.50 | 636 | 3,753 |
| 162.60 | 636 | 3,935 |
| 162.70 | 636 | 4,122 |
| 162.80 | 636 | 4,314 |
| 162.90 | 636 | 4,512 |
| 163.00 | 636 | 4,714 |
| 163.10 | 636 | 4,921 |
| 163.20 | 636 | 5,133 |
| 163.30 | 636 | 5,349 |
| 163.40 | 636 | 5,571 |
| 163.50 | 636 | **5,797** |
| 163.60 | 636 | 5,797 |
| 163.70 | 636 | 5,797 |
| 163.80 | 636 | 5,797 |
| 163.90 | 636 | 5,797 |
| 164.00 | 636 | 5,797 |
| 164.10 | 636 | 5,797 |
| 164.20 | 636 | 5,797 |
| 164.30 | 636 | 5,797 |
| 164.40 | 636 | 5,797 |
| 164.50 | 636 | 5,797 |
| 164.60 | 636 | 5,797 |
| 164.70 | 636 | 5,797 |
| 164.80 | 636 | 5,797 |
| 164.90 | 636 | 5,797 |
| 165.00 | 636 | 5,797 |
| 165.10 | 636 | 5,797 |
| 165.20 | 636 | 5,797 |
| 165.30 | 636 | 5,797 |
| 165.40 | 636 | 5,797 |
| 165.50 | 636 | 5,797 |
| 165.60 | 636 | 5,797 |
| 165.70 | 636 | 5,797 |
| 165.80 | 636 | 5,797 |
| 165.90 | 636 | 5,797 |
| 166.00 | 636 | 5,797 |
| 166.10 | 636 | 5,797 |
| 166.20 | 636 | 5,797 |
| 166.30 | 636 | 5,797 |
| 166.40 | 636 | 5,797 |
| 166.50 | 636 | 5,797 |
| 166.60 | 636 | 5,797 |
| 166.70 | 636 | 5,797 |
| 166.80 | 636 | 5,797 |
| 166.90 | 636 | 5,797 |
| 167.00 | 636 | 5,797 |

Elev: 158.3 Invert Stone (254 CF)
Elev: 161.5 Lowest Outlet (2,182 CF)
2,182 CF - 254 CF = 1,928 CF Storage

## Stage-Area-Storage for Pond 101P: Rain Garden #101

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---|---|---|---|---|---|
| 157.30 | **636** | 0 | 162.60 | 636 | 3,935 |
| 157.40 | 636 | 25 | 162.70 | 636 | 4,122 |
| 157.50 | 636 | 51 | 162.80 | 636 | 4,314 |
| 157.60 | 636 | 76 | 162.90 | 636 | 4,512 |
| 157.70 | 636 | 102 | 163.00 | 636 | 4,714 |
| 157.80 | 636 | 127 | 163.10 | 636 | 4,921 |
| 157.90 | 636 | 153 | 163.20 | 636 | 5,133 |
| 158.00 | 636 | 178 | 163.30 | 636 | 5,349 |
| 158.10 | 636 | 204 | 163.40 | 636 | 5,571 |
| 158.20 | 636 | 229 | 163.50 | 636 | **5,797** |
| 158.30 | 636 | 254 | 163.60 | 636 | 5,797 |
| 158.40 | 636 | 267 | 163.70 | 636 | 5,797 |
| 158.50 | 636 | 280 | 163.80 | 636 | 5,797 |
| 158.60 | 636 | 293 | 163.90 | 636 | 5,797 |
| 158.70 | 636 | 305 | 164.00 | 636 | 5,797 |
| 158.80 | 636 | 318 | 164.10 | 636 | 5,797 |
| 158.90 | 636 | 331 | 164.20 | 636 | 5,797 |
| 159.00 | 636 | 343 | 164.30 | 636 | 5,797 |
| 159.10 | 636 | 356 | 164.40 | 636 | 5,797 |
| 159.20 | 636 | 369 | 164.50 | 636 | 5,797 |
| 159.30 | 636 | 382 | 164.60 | 636 | 5,797 |
| 159.40 | 636 | 394 | 164.70 | 636 | 5,797 |
| 159.50 | 636 | 407 | 164.80 | 636 | 5,797 |
| 159.60 | 636 | 420 | 164.90 | 636 | 5,797 |
| 159.70 | 636 | 432 | 165.00 | 636 | 5,797 |
| 159.80 | 636 | 445 | 165.10 | 636 | 5,797 |
| 159.90 | 636 | 513 | 165.20 | 636 | 5,797 |
| 160.00 | 636 | 589 | 165.30 | 636 | 5,797 |
| 160.10 | 636 | 671 | 165.40 | 636 | 5,797 |
| 160.20 | 636 | 757 | 165.50 | 636 | 5,797 |
| 160.30 | 636 | 845 | 165.60 | 636 | 5,797 |
| 160.40 | 636 | 937 | 165.70 | 636 | 5,797 |
| 160.50 | 636 | 1,032 | 165.80 | 636 | 5,797 |
| 160.60 | 636 | 1,130 | 165.90 | 636 | 5,797 |
| 160.70 | 636 | 1,232 | 166.00 | 636 | 5,797 |
| 160.80 | 636 | 1,338 | 166.10 | 636 | 5,797 |
| 160.90 | 636 | 1,447 | 166.20 | 636 | 5,797 |
| 161.00 | 636 | 1,560 | 166.30 | 636 | 5,797 |
| 161.10 | 636 | 1,676 | 166.40 | 636 | 5,797 |
| 161.20 | 636 | 1,797 | 166.50 | 636 | 5,797 |
| 161.30 | 636 | 1,921 | 166.60 | 636 | 5,797 |
| 161.40 | 636 | 2,050 | 166.70 | 636 | 5,797 |
| 161.50 | 636 | 2,182 | 166.80 | 636 | 5,797 |
| 161.60 | 636 | 2,319 | 166.90 | 636 | 5,797 |
| 161.70 | 636 | 2,461 | 167.00 | 636 | 5,797 |
| 161.80 | 636 | 2,606 | | | |
| 161.90 | 636 | 2,756 | | | |
| 162.00 | 636 | 2,911 | | | |
| 162.10 | 636 | 3,070 | | | |
| 162.20 | 636 | 3,234 | | | |
| 162.30 | 636 | 3,402 | | | |
| 162.40 | 636 | 3,575 | | | |
| 162.50 | 636 | 3,753 | | | |

1,768 CF Required for WQV
Elev: 158.3 Invert Stone (254 (CF))
254 CF + 1,768 CF = 2,022 CF
WQV Elev: 161.39

## Stage-Discharge for Pond 101P: Rain Garden #101

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---|---|---|---|
| 157.30 | 0.00 | 162.60 | 0.47 |
| 157.40 | 0.01 | 162.70 | 0.49 |
| 157.50 | 0.01 | 162.80 | 0.51 |
| 157.60 | 0.01 | 162.90 | 0.53 |
| 157.70 | 0.02 | 163.00 | 0.55 |
| 157.80 | 0.02 | 163.10 | 0.66 |
| 157.90 | 0.02 | 163.20 | 0.94 |
| 158.00 | 0.02 | 163.30 | 1.40 |
| 158.10 | 0.02 | 163.40 | 2.03 |
| 158.20 | 0.02 | 163.50 | 2.82 |
| 158.30 | 0.03 | 163.60 | 3.77 |
| 158.40 | 0.03 | 163.70 | 4.87 |
| 158.50 | 0.03 | 163.80 | 6.13 |
| 158.60 | 0.03 | 163.90 | 7.53 |
| 158.70 | 0.03 | 164.00 | 9.07 |
| 158.80 | 0.03 | 164.10 | 10.75 |
| 158.90 | 0.03 | 164.20 | 12.56 |
| 159.00 | 0.03 | 164.30 | 14.50 |
| 159.10 | 0.03 | 164.40 | 15.04 |
| 159.20 | 0.04 | 164.50 | 15.15 |
| 159.30 | 0.04 | 164.60 | 15.27 |
| 159.40 | 0.04 | 164.70 | 15.38 |
| 159.50 | 0.04 | 164.80 | 15.49 |
| 159.60 | 0.04 | 164.90 | 15.61 |
| 159.70 | 0.04 | 165.00 | 15.72 |
| 159.80 | 0.04 | 165.10 | 15.83 |
| 159.90 | 0.04 | 165.20 | 15.94 |
| 160.00 | 0.04 | 165.30 | 16.05 |
| 160.10 | 0.04 | 165.40 | 16.16 |
| 160.20 | 0.04 | 165.50 | 16.26 |
| 160.30 | 0.05 | 165.60 | 16.37 |
| 160.40 | 0.05 | 165.70 | 16.48 |
| 160.50 | 0.05 | 165.80 | 16.58 |
| 160.60 | 0.05 | 165.90 | 16.69 |
| 160.70 | 0.05 | 166.00 | 16.79 |
| 160.80 | 0.05 | 166.10 | 16.89 |
| 160.90 | 0.05 | 166.20 | 17.00 |
| 161.00 | 0.05 | 166.30 | 17.10 |
| 161.10 | 0.05 | 166.40 | 17.20 |
| 161.20 | 0.05 | 166.50 | 17.30 |
| 161.30 | 0.05 | 166.60 | 17.40 |
| 161.40 | 0.05 | 166.70 | 17.50 |
| 161.50 | 0.05 | 166.80 | 17.60 |
| 161.60 | 0.08 | 166.90 | 17.70 |
| 161.70 | 0.14 | 167.00 | **17.80** |
| 161.80 | 0.21 | | |
| 161.90 | 0.26 | | |
| 162.00 | 0.30 | | |
| 162.10 | 0.33 | | |
| 162.20 | 0.36 | | |
| 162.30 | 0.39 | | |
| 162.40 | 0.42 | | |
| 162.50 | 0.44 | | |

WQV Elev: 161.39
WQV Discharge: 0.05 CFS

# INFILTRATION PRACTICE CRITERIA
# (Env-Wq 1508.06)

NEW HAMPSHIRE DEPARTMENT OF Environmental Services

**Type/Node Name:** **Infiltration Basin #102**

Enter the type of infiltration practice (e.g., basin, trench) and the node name in the drainage analysis, if applicable.

| Value | Unit | Description | Criteria |
|---|---|---|---|
| ***Yes*** | | Have you reviewed Env-Wq 1508.06(a) to ensure that infiltration is allowed? | **← yes** |
| 1.41 | ac | A = Area draining to the practice | |
| 0.05 | ac | $A_I$ = Impervious area draining to the practice | |
| 0.04 | decimal | I = Percent impervious area draining to the practice, in decimal form | |
| 0.09 | unitless | Rv = Runoff coefficient = 0.05 + (0.9 x I) | |
| 0.12 | ac-in | WQV= 1" x Rv x A | |
| 435 | cf | WQV conversion (ac-in x 43,560 sf/ac x 1ft/12") | |
| 109 | cf | 25% x WQV (check calc for sediment forebay volume) | |
| Sediment Forebay | | Method of pretreatment? (not required for clean or roof runoff) | |
| 821 | cf | $V_{SED}$ = Sediment forebay volume, if used for pretreatment | **≥ 25%WQV** |
| 4,591 | cf | V = Volume[1] (attach a stage-storage table) | **≥ WQV** |
| 459 | sf | $A_{SA}$ = Surface area of the bottom of the pond | |
| 3.00 | iph | $Ksat_{DESIGN}$ = Design infiltration rate[2] | |
| 3.8 | hours | $T_{DRAIN}$ = Drain time = V / ($A_{SA}$ * $I_{DESIGN}$) | **≤ 72-hrs** |
| 161.00 | feet | $E_{BTM}$ = Elevation of the bottom of the basin | |
| 160.00 | feet | $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pit) | |
| 157.00 | feet | $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test pit) | |
| 1.00 | feet | $D_{SHWT}$ = Separation from SHWT | **≥ *** [3] |
| 4.0 | feet | $D_{ROCK}$ = Separation from bedrock | **≥ *** [3] |
| | ft | $D_{amend}$ = Depth of amended soil, if applicable due high infiltation rate | **≥ 24"** |
| | ft | $D_T$ = Depth of trench, if trench proposed | **4 - 10 ft** |
| | Yes/No | If a trench or underground system is proposed, has observation well been provided? | **←yes** |
| | | If a trench is proposed, does materialmeet Env-Wq 1508.06(k)(2) requirements.[4] | **← yes** |
| Yes | Yes/No | If a basin is proposed, Is the perimeter curvilinear, and basin floor flat? | **← yes** |
| 3.0 | :1 | If a basin is proposed, pond side slopes. | **≥3:1** |
| 161.39 | ft | Peak elevation of the 10-year storm event (infiltration can be used in analysis) | |
| 162.64 | ft | Peak elevation of the 50-year storm event (infiltration can be used in analysis) | |
| 164.00 | ft | Elevation of the top of the practice (if a basin, this is the elevation of the berm) | |
| YES | | 10 peak elevation ≤ Elevation of the top of the trench?[5] | **← yes** |
| YES | | If a basin is proposed, 50-year peak elevation ≤ Elevation of berm? | **← yes** |

1. Volume below the lowest invert of the outlet structure and excludes forebay volume
2. $Ksat_{DESIGN}$ includes a factor of safety. See Env-Wq 1504.14 for requirements for determining the infiltr. rate
3. 1' separation if treatment not required; 4' for treatment in GPAs & WSIPAs; & 3' in all other areas.
4. Clean, washed well graded diameter of 1.5 to 3 inches above the in-situ soil.
5. If 50-year peak elevation exceeds top of trench, the overflow must be routed in HydroCAD as secondary discharge.

**Designer's Notes:**

## Summary for Pond 102P: Infiltration Basin #102

Inflow Area = 1.364 ac, 4.02% Impervious, Inflow Depth > 1.14" for 50Yr.-24Hr. event
Inflow = 0.82 cfs @ 12.47 hrs, Volume= 0.130 af
Outflow = 0.16 cfs @ 14.66 hrs, Volume= 0.118 af, Atten= 81%, Lag= 131.8 min
Discarded = 0.16 cfs @ 14.66 hrs, Volume= 0.118 af
Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 162.64' @ 14.66 hrs Surf.Area= 2,312 sf Storage= 1,944 cf
Flood Elev= 164.00' Surf.Area= 7,916 sf Storage= 6,779 cf

Plug-Flow detention time= 163.0 min calculated for 0.118 af (91% of inflow)
Center-of-Mass det. time= 121.7 min ( 1,038.9 - 917.3 )

| Volume | Invert | Avail.Storage | Storage Description |
|---|---|---|---|
| #1 | 161.00' | 2,058 cf | **Infiltration Cell (Irregular)**Listed below (Recalc) |
| #2 | 162.00' | 821 cf | **Sediment Forebay (Irregular)**Listed below (Recalc) |
| #3 | 163.00' | 3,901 cf | **Open Water Storage (Irregular)**Listed below (Recalc) |
| | | 6,779 cf | Total Available Storage |

| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 161.00 | 459 | 96.0 | 0 | 0 | 459 |
| 162.00 | 1,055 | 144.0 | 737 | 737 | 1,384 |
| 163.00 | 1,606 | 197.4 | 1,321 | 2,058 | 2,844 |

| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 162.00 | 453 | 176.0 | 0 | 0 | 453 |
| 163.00 | 1,255 | 237.0 | 821 | 821 | 2,468 |

| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|---|---|---|---|---|---|
| 163.00 | 3,128 | 393.2 | 0 | 0 | 3,128 |
| 163.50 | 3,732 | 407.7 | 1,713 | 1,713 | 4,074 |
| 164.00 | 5,055 | 470.9 | 2,188 | 3,901 | 8,498 |

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Discarded | 161.00' | **3.000 in/hr Infiltration over Surface area** |
| #2 | Primary | 163.50' | **5.0' long x 10.0' breadth Overflow**<br>Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60<br>Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64 |

**Discarded OutFlow** Max=0.16 cfs @ 14.66 hrs HW=162.64' (Free Discharge)
└─**1=Infiltration** (Exfiltration Controls 0.16 cfs)

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=161.00' TW=157.30' (Dynamic Tailwater)
└─**2=Overflow** ( Controls 0.00 cfs)

## Stage-Area-Storage for Pond 102P: Infiltration Basin #102

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---|---|---|
| 161.00 | 459 | 0 |
| 161.05 | 483 | 24 |
| 161.10 | 508 | 48 |
| 161.15 | 533 | 74 |
| 161.20 | 559 | 102 |
| 161.25 | 585 | 130 |
| 161.30 | 612 | 160 |
| 161.35 | 640 | 191 |
| 161.40 | 668 | 224 |
| 161.45 | 697 | 258 |
| 161.50 | 726 | 294 |
| 161.55 | 757 | 331 |
| 161.60 | 787 | 369 |
| 161.65 | 819 | 410 |
| 161.70 | 851 | 451 |
| 161.75 | 883 | 495 |
| 161.80 | 916 | 540 |
| 161.85 | 950 | 586 |
| 161.90 | 984 | 635 |
| 161.95 | 1,019 | 685 |
| 162.00 | 1,508 | 737 |
| 162.05 | 1,563 | 813 |
| 162.10 | 1,620 | 893 |
| 162.15 | 1,678 | 975 |
| 162.20 | 1,737 | 1,061 |
| 162.25 | 1,798 | 1,149 |
| 162.30 | 1,860 | 1,241 |
| 162.35 | 1,923 | 1,335 |
| 162.40 | 1,987 | 1,433 |
| 162.45 | 2,053 | 1,534 |
| 162.50 | 2,120 | 1,638 |
| 162.55 | 2,188 | 1,746 |
| 162.60 | 2,258 | 1,857 |
| 162.65 | 2,329 | 1,972 |
| 162.70 | 2,401 | 2,090 |
| 162.75 | 2,474 | 2,212 |
| 162.80 | 2,549 | 2,338 |
| 162.85 | 2,625 | 2,467 |
| 162.90 | 2,703 | 2,600 |
| 162.95 | 2,781 | 2,737 |
| 163.00 | 5,989 | 2,878 |
| 163.05 | 6,047 | 3,036 |
| 163.10 | 6,106 | 3,197 |
| 163.15 | 6,165 | 3,360 |
| 163.20 | 6,224 | 3,527 |
| 163.25 | 6,284 | 3,697 |
| 163.30 | 6,345 | 3,870 |
| 163.35 | 6,406 | 4,045 |
| 163.40 | 6,468 | 4,224 |
| 163.45 | 6,530 | 4,406 |
| 163.50 | 6,593 | 4,591 |
| 163.55 | 6,716 | 4,781 |
| 163.60 | 6,842 | 4,977 |
| 163.65 | 6,969 | 5,179 |
| 163.70 | 7,098 | 5,387 |
| 163.75 | 7,229 | 5,602 |
| 163.80 | 7,363 | 5,824 |
| 163.85 | 7,498 | 6,053 |
| 163.90 | 7,635 | 6,288 |
| 163.95 | 7,775 | 6,530 |
| 164.00 | **7,916** | **6,779** |

Spillway Elev: 163.50
4,591 CF Stored in BMP

# Custom Soil Resource Report
## Soil Map

## MAP LEGEND

**Area of Interest (AOI)**

Area of Interest (AOI)

**Soils**

Soil Map Unit Polygons

Soil Map Unit Lines

Soil Map Unit Points

**Special Point Features**

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot

Other

Special Line Features

**Water Features**

Streams and Canals

**Transportation**

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

**Background**

Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Strafford County, New Hampshire
Survey Area Data: Version 22, Aug 31, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Dec 31, 2009—Sep 9, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# Map Unit Legend

| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI |
|---|---|---|---|
| Fa | Fresh water marsh | 2.8 | 2.5% |
| GlB | Gloucester fine sandy loam, 3 to 8 percent slopes | 3.3 | 3.0% |
| GsB | Gloucester very stony fine sandy loam, 3 to 8 percent slopes | 28.0 | 25.5% |
| Gv | Gravel and borrow pits | 2.0 | 1.9% |
| HaC | Hinckley loamy sand, 8 to 15 percent slopes | 6.9 | 6.3% |
| Mp | Freetown and Swansea mucky peats, 0 to 2 percent slopes | 1.8 | 1.7% |
| Sb | Saugatuck loamy sand | 12.1 | 11.0% |
| ScA | Scantic silt loam, 0 to 3 percent slopes | 1.7 | 1.5% |
| SwA | Swanton fine sandy loam, 0 to 3 percent slopes | 11.9 | 10.9% |
| W | Water | 2.5 | 2.3% |
| WdA | Windsor loamy sand, 0 to 3 percent slopes | 5.3 | 4.8% |
| WdC | Windsor loamy sand, 8 to 15 percent slopes | 12.6 | 11.5% |
| WfB | Windsor loamy fine sand, clay subsoil variant, 0 to 8 percent slopes | 18.8 | 17.1% |
| **Totals for Area of Interest** | | **109.7** | **100.0%** |

# Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

**John P. Hayes III CSS, CWS,**
**7 Limestone Way**
**North Hampton, NH 03862**
**603-205-4396**
**johnphayes@comcast.net**

**8/4/23**
**Christopher Berry** **Job # 22-006**
**Berry Surveying and Engineering**
**335 Second Crown Point Road**
**Barrington NH 03825**

**Site Specific Soil Survey 7/26/23**
**Map 253 Lot 14**
**49 Winkley Pond Road**
**Barrington, NH**

Dear Chris,

This report presents the findings of a Site Specific Soil Survey conducted on the referenced properties by John P. Hayes III on July 26, 2023. The soil survey was conducted in accordance with the New Hampshire Supplement of the Site-Specific Soil Mapping Standard For New Hampshire and Vermont, Special Publication # 3, Version 7.0 July 2021, published by the Society of Soil Scientist of Northern New England. Soil series information was also taken from the Soil Survey of Strafford County New Hampshire issued March 1973.

The property that is subject of the soil survey is located on the southeast side of Winkley Pond road, southwest of Hayes road, and east of Route 125, in Barrington, NH. The lot is approximately 7.8 acres in size. Only a portion of the parcel, on the easterly side, near Winkley Pond road, has been mapped. The plans used for these soil maps are a 30 scale plan, where 1 inch equals 30 feet, with two foot contours.

The purpose of the soil survey is to provide the client with soils information for urban and suburban or rural land planning. Soil characteristics on the property were evaluated through observation of numerous test pits, and hand auger probes conducted throughout the property. Slope phases were determined with the use of the topography provided on the plan. The Site-specific Soil Map Units identified are taken from the New Hampshire State-Wide Numerical Soils Legend, Issue #10 January 2011, and are briefly described below. Official Series Descriptions (OSD) for each of these soil series are enclosed with this report. The soil map units comply with the Range In Characteristics described in the OSD. Any limiting inclusions on the site, do not exceed 15 percent of any of the soil map units. Dissimilar inclusions, if any, will be noted in the report. Limits of the Site Specific mapping units are highlighted on the plan. The Hydrological Soil Groups for each of the soil series was determined using SSSNNE Publication No. 5 Ksat Values for New Hampshire Soils September 2009. Limits of the Site Specific mapping units are highlighted on the plan.

Portions of the soil map with the map unit denominator of P and VP contain poorly drained soils, and very poorly drained soils respectively. Portions of the soil map with the map unit 400, contain disturbed soils that have been excavated and/or regraded, that are moderately well drained, and are sandy in texture. A Disturbed Soil Mapping Unit Supplement for New Hampshire DES AoT Site Specific Soil Maps is also included. This supplement explains the additional information given about each disturbed soil map units that are present on the site.

| MAP UNIT # | SOIL TAXANOMI C NAME | SLOPES | HYDRO LOGIC SOIL GROUP | DESCRIPTION |
|---|---|---|---|---|
| **15**<br>**VP** | **Scarboro** | **A** | **D** | The Scarboro series consists of very deep, very poorly drained soils in sandy glaciofluvial deposits, on outwash plains. These soils are located in the wetland areas, in the southeast portion of the mapped area of the property. The soil texture consists of 4 to 16 inches of organic material over sand. These soils are deep to bedrock. The saturated hydraulic conductivity is high or very high. Some inclusions of poorly drained Wareham and Shaker soils may be present, but are less than 10 percent of the mapped area. These soils are semi permanantly to permanately saturated. |
| **34**<br>**P** | **Wareham** | **A** | **C** | The Wareham series consists of very deep, poorly drained sandy soils formed in outwash on plains, deltas, and terraces. These soils are located in the southeastern portion of the mapped area of the lot.. The soil texture is loamy sand over coarse sand. These soils are deep to bedrock. Permeability is rapid throughout the soil profile. Some inclusions of very poorly drained Scarboro soils, poorly drained Shaker soils, and the somewhat poorly drained Deerfield Variant soils may be present, but are less than 10 percent of the mapped area. Estimated seasonal high water tables in these soils range from 0 to 10 inches. |
| **313** | **Deerfield** | **A B C D** | **B** | The Deerfield series consists of very deep, moderately well drained soils formed in glaciofluvial deposits. These soils are located in the upland area on the northwestern portion of the mapped area. The soil textures on this soil series on this site consist of loamy sand over sand and/or fine sand, and loamy sand over stratified very fine sand and silt. These soils are deep to bedrock. The saturated hydraulic conductivity is high or very high. Some inclusions of excessively well drained Windsor, moderately well drained Eldridge, and somewhat poorly drained Deerfield Variant, soils may be present, but are less than 10 percent of the mapped area. Estimated seasonal high water tables in these soils range from 15 to 38 inches. |
| **400**<br>**(dbadb)** | **Udorthents (sandy or gravelly)** | **B C D** | **B** | Udorthents are disturbed soils that have been excavated and/or regraded, and are sandy or gravelly in texture. These soils are located in the northwest |

| MAP UNIT # | SOIL TAXANOMIC NAME | SLOPES | HYDRO LOGIC SOIL GROUP | DESCRIPTION |
|---|---|---|---|---|
| 400 (dbadb) | **Udorthents (sandy or gravelly)** | **B C D** | **B** | portion of the mapped area, around the 2 structures, and adjacent to Winkley Pond road. These disturbed soils are mostly likelyderived from the surrounding Deerfield soil series. These soils are moderately well drained, and are deep to bedrock. Saturated hydraulic conductivity is high or very high. Estimated seasonal high water tables in these soils range from 20 to 38 inches. |
| 915 | **Deerfield Variant (somewhat poorly drained)** | **B** | **C** | The Deerfield Variant series consists of very deep, somewhat poorly drained soils formed in glaciofluvial deposits. These soils are located in the northeast portion of the property, adjacent to the wetlands. The soil texture is loamy sand over stratified very fine sand and silt. These soils are deep to bedrock. Saturated hydraulic conductivity is high to very high. Some inclusions of moderately well drained Deerfield, somewhat poorly drained Eldridge Variant, and poorly drained Wareham soils may be present, but are less than 10 percent of the mapped area. Estimated seasonal high water tables in these soils range from 11 to 15 inches. |

**Slope Phases**

| Alpha Slope Symbol | Range |
|---|---|
| A | 0 – 3% |
| B | 3 – 8% |
| C | 8 – 15% |
| D | 15 – 25% |
| E | 25 – 50% |
| F | > 50% |

I trust that this Soil Survey and report meet your current planning needs. Please do not hesitate to contact me if you have any questions.

Sincerely:

John P. Hayes III


John P. Hayes III CSS, CWS

## TEST PIT DATA:

TEST PITS WERE OBSERVED BY JOHN P. HAYES III, CSS, CWS
DATE : FEBRUARY 24, 2022

**TEST PIT #1**
0–10 10YR 3/2 VERY DARK GRAYISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
10–13 7.5YR 6/1 GRAY, LOAMY SAND, GRANULAR, FRIABLE
13–18 5YR 3/3 DARK REDDISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
18–36 10 YR 5/4 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
36–72 10YR 6/2 LIGHT BROWNISH GRAY, FINE SAND WITH REDOX. FEATURES PRESENT, GRANULAR, FRIABLE
E.S.H.W.T. @ 36"
RESTRICTIVE LAYER @ NONE
GROUND WATER @ 50"
TERMINATED @ 72"
REFUSAL @ NONE
PERC RATE : 5 MIN/INCH

**TEST PIT #2**
0–14 10YR 3/2 VERY DARK GRAYISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
14–28 10YR 5/6 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
28–36 10YR 5/4 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
36–75 10YR 6/2 LIGHT BROWNISH GRAY, VERY FINE SAND WITH REDOX. FEATURES PRESENT, MASSIVE, FRIABLE
E.S.H.W.T. @ 36"
RESTRICTIVE LAYER @ NONE
GROUND WATER @ N/A
TERMINATED @ 75"
REFUSAL @ NONE
PERC RATE : 4 MIN/INCH

**TEST PIT #3**
0–14 10YR 3/2 VERY DARK GRAYISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
14–22 10YR 5/6 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
22–28 10YR 5/4 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
28–31 7.5YR 6/1 GRAY, LOAMY SAND WITH REDOX. FEATURES PRESENT, GRANULAR, FRIABLE
31–36 5YR 3/3 DARK REDDISH BROWN, LOAMY SAND WITH REDOX. FEATURES PRESENT, GRANULAR, FRIABLE
36–58 5Y 5/2 OLIVE GRAY, STRATIFIED VERY FINE SAND AND SILT WITH REDOX. FEATURES PRESENT, MASSIVE, FRIABLE
58–75 10YR 6/2 LIGHT BROWNISH GRAY, FINE SAND WITH REDOX. FEATURES PRESENT, GRANULAR, FRIABLE
E.S.H.W.T. @ 28"
RESTRICTIVE LAYER @ NONE
GROUND WATER @ 60"
TERMINATED @ 75"
REFUSAL @ NONE
PERC RATE : 5 MIN/INCH

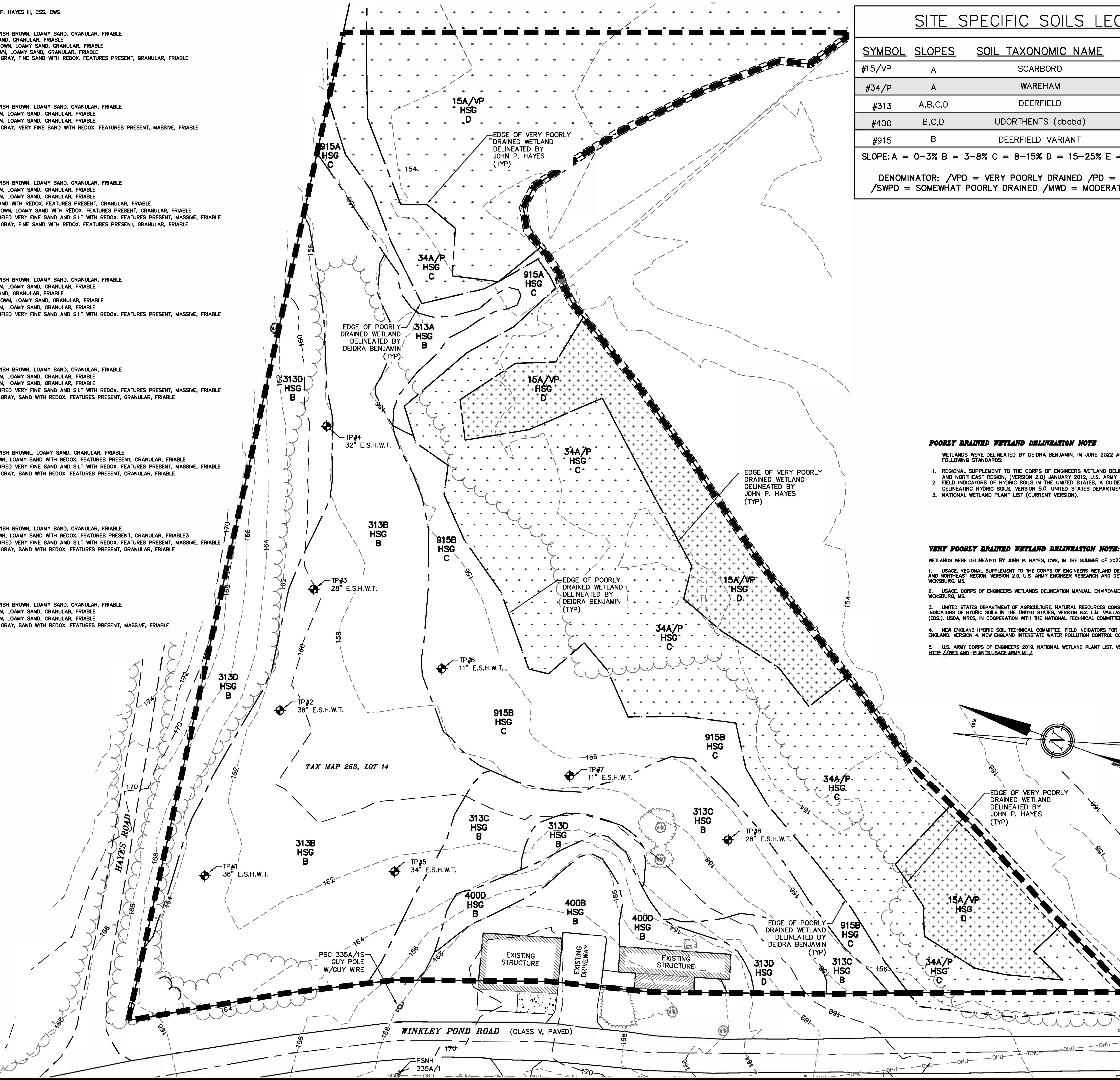
**TEST PIT #4**
0–14 10YR 3/2 VERY DARK GRAYISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
14–20 10YR 5/6 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
20–24 7.5YR 6/1 GRAY, LOAMY SAND, GRANULAR, FRIABLE
24–28 5YR 3/3 DARK REDDISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
28–32 10YR 5/4 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
32–72 5Y 5/2 OLIVE GRAY, STRATIFIED VERY FINE SAND AND SILT WITH REDOX. FEATURES PRESENT, MASSIVE, FRIABLE
E.S.H.W.T. @ 32"
RESTRICTIVE LAYER @ NONE
GROUND WATER @ 48"
TERMINATED @ 72"
REFUSAL @ NONE
PERC RATE : 5 MIN/INCH

**TEST PIT #5**
0–14 10YR 3/2 VERY DARK GRAYISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
14–22 10YR 5/6 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
22–34 10YR 5/4 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
34–48 5Y 5/2 OLIVE GRAY, STRATIFIED VERY FINE SAND AND SILT WITH REDOX. FEATURES PRESENT, MASSIVE, FRIABLE
48–74 10YR 6/2 LIGHT BROWNISH GRAY, SAND WITH REDOX. FEATURES PRESENT, GRANULAR, FRIABLE
E.S.H.W.T. @ 34"
RESTRICTIVE LAYER @ NONE
GROUND WATER @ N/A
TERMINATED @ 48"
REFUSAL @ NONE
PERC RATE : 4 MIN/INCH

**TEST PIT #6**
0–11 10YR 3/2 VERY DARK GRAYISH BROWNL, LOAMY SAND, GRANULAR, FRIABLE
11–32 2.5Y 5/3 LIGHT OLIVE BROWN, LOAMY SAND WITH REDOX. FEATURES PRESENT, GRANULAR, FRIABLE
32–45 5Y 5/2 OLIVE GRAY, STRATIFIED VERY FINE SAND AND SILT WITH REDOX. FEATURES PRESENT, MASSIVE, FRIABLE
45–62 10YR 6/2 LIGHT BROWNISH GRAY, SAND WITH REDOX. FEATURES PRESENT, GRANULAR, FRIABLE
E.S.H.W.T. @ 11"
RESTRICTIVE LAYER @ NONE
GROUND WATER @ 25"
TERMINATED @ 72"
REFUSAL @ NONE
PERC RATE : 20 MIN/INCH

**TEST PIT #7**
0–11 10YR 3/2 VERY DARK GRAYISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
11–32 2.5Y 5/3 LIGHT OLIVE BROWN, LOAMY SAND WITH REDOX. FEATURES PRESENT, GRANULAR, FRIABLE3
32–45 5Y 5/2 OLIVE GRAY, STRATIFIED VERY FINE SAND AND SILT WITH REDOX. FEATURES PRESENT, MASSIVE, FRIABLE
45–62 10YR 6/2 LIGHT BROWNISH GRAY, SAND WITH REDOX. FEATURES PRESENT, GRANULAR, FRIABLE
E.S.H.W.T. @ 11"
RESTRICTIVE LAYER @ NONE
GROUND WATER @ 25"
TERMINATED @ 62"
REFUSAL @ NONE
PERC RATE : 20 MIN/INCH

**TEST PIT #8**
0–14 10YR 3/2 VERY DARK GRAYISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
14–20 10YR 5/6 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
20–26 10YR 5/4 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE
26–75 10YR 6/2 LIGHT BROWNISH GRAY, SAND WITH REDOX. FEATURES PRESENT, MASSIVE, FRIABLE
E.S.H.W.T. @ 26"
RESTRICTIVE LAYER @ N/A
GROUND WATER @ 60"
TERMINATED @ 75"
REFUSAL @ NONE
PERC RATE : 4 MIN/INCH

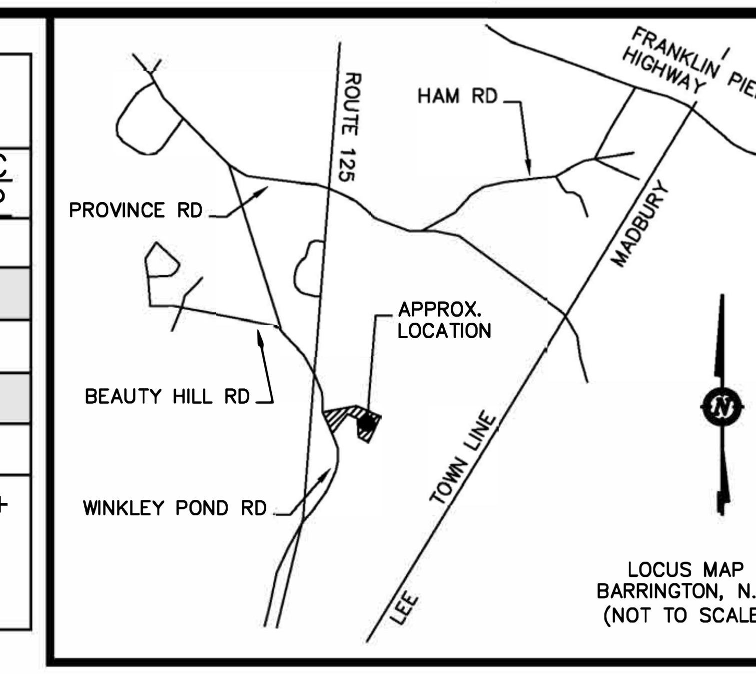



## SITE SPECIFIC SOILS LEGEND

| SYMBOL | SLOPES | SOIL TAXONOMIC NAME | HYDROLOGIC SOIL GROUP |
|---|---|---|---|
| #15/VP | A | SCARBORO | D |
| #34/P | A | WAREHAM | C |
| #313 | A,B,C,D | DEERFIELD | B |
| #400 | B,C,D | UDORTHENTS (dbabd) | B |
| #915 | B | DEERFIELD VARIANT | C |

SLOPE: A = 0–3% B = 3–8% C = 8–15% D = 15–25% E = 25–50% F = 50%+

DENOMINATOR: /VP = VERY POORLY DRAINED /PD = POORLY DRAINED /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED



LOCUS MAP
BARRINGTON, N.H.
(NOT TO SCALE)

### NOTES:

1.) OWNER: HAMBONE LLC
242 CENTRAL AVE
DOVER, NH 03820

2.) TAX MAP: TAX MAP 253, LOT 14

3.) LOT AREA: 586,793 Sq. Ft., 13.47 Ac.
330,912 Sq.Ft., 7.60 Ac., TOTAL UPLAND

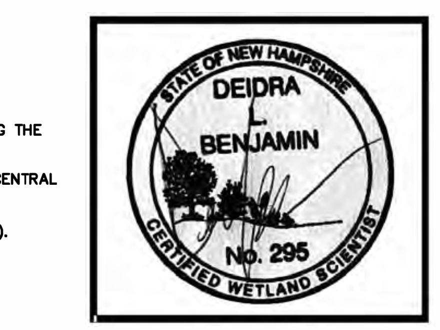
4.) S.C.R.D. BOOK 4976, PAGE 1023

5.) THE INTENT OF THIS PLAN IS TO SHOW THE EXISTING SOILS CONDITIONS OF TAX MAP 253, LOT 14 AS OF THE DATE OF THE SURVEY.

### POORLY DRAINED WETLAND DELINEATION NOTE

WETLANDS WERE DELINEATED BY DEIDRA BENJAMIN. IN JUNE 2022 AND AUGUST 2023 UTILIZING THE FOLLOWING STANDARDS:

1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).



DEIDRA BENJAMIN, CWS #295

### VERY POORLY DRAINED WETLAND DELINEATION NOTE:

WETLANDS WERE DELINEATED BY JOHN P. HAYES, CWS, IN THE SUMMER OF 2022 USING THE FOLLOWING CRITERIA:

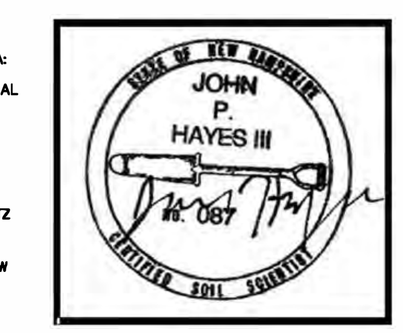
1. USACE. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION. VERSION 2.0. U.S. ARMY ENGINEER RESEARCH AND DEVELOPMENT CENTER. 2012. VICKSBURG, MS.

2. USACE. CORPS OF ENGINEERS WETLANDS DELINEATION MANUAL. ENVIRONMENTAL LABORATORY. 1987. VICKSBURG, MS.

3. UNITED STATES DEPARTMENT OF AGRICULTURE, NATURAL RESOURCES CONSERVATION SERVICE. 2018. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, VERSION 8.2. L.M. VASILAS, G.W. HURT, AND J.F. BERKOWITZ (EDS.). USDA, NRCS, IN COOPERATION WITH THE NATIONAL TECHNICAL COMMITTEE FOR HYDRIC SOILS.

4. NEW ENGLAND HYDRIC SOIL TECHNICAL COMMITTEE. FIELD INDICATORS FOR IDENTIFYING HYDRIC SOILS IN NEW ENGLAND. VERSION 4. NEW ENGLAND INTERSTATE WATER POLLUTION CONTROL COMMISSION. 2019. LOWELL, MA.

5. U.S. ARMY CORPS OF ENGINEERS 2019. NATIONAL WETLAND PLANT LIST, VERSION 3.3. HTTP://WETLAND-PLANTS.USACE.ARMY.MIL/



JOHN P. HAYES, III CSS #87

JOHN P. HAYES III, CWS #18

### LEGEND:

- IRON BOUND/IRON ROD (FND)
- IRON PIPE (FND)
- UTILITY POLE
- TEST PIT
- OVERHEAD UTILITIES LINE
- EXISTING CONTOUR MINOR
- EXISTING CONTOUR MAJOR
- SOIL LINE
- LIMIT OF SOIL SURVEY
- WdA — SOIL SERIES
- S.C.R.D. — STRAFFORD COUNTY REGISTRY OF DEEDS
- TYP. — TYPICAL
- FND — FOUND

### GRAPHIC SCALE

30 0 15 30 60 120
( IN FEET )
1 inch = 30 ft.

FOR TOWN APPROVAL PURPOSES :

THE SITE REVIEW REGULATIONS OF THE TOWN OF BARRINGTON ARE A PART OF THIS PLAN, AND APPROVAL OF THIS PLAN IS CONTINGENT UPON COMPLETION OF ALL REQUIREMENTS OF SAID SITE REVIEW REGULATIONS, EXCEPTING ONLY MODIFICATIONS MADE IN WRITING BY THE BOARD AND ATTACHED HERETO.

| REVISION | DATE | DESCRIPTION |
|---|---|---|
| | | |

SITE SPECIFIC SOILS MAP
LAND OF
HAMBONE LLC
49 WINKLEY POND ROAD
BARRINGTON, N.H.
*TAX MAP 253, LOT 14*

BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863

SCALE : 1 IN. EQUALS 30 FT.
DATE : JULY 16, 2023
FILE NO. : DB 2021-163

STATE OF NEW HAMPSHIRE
KENNETH A. BERRY
No. 805
LICENSED LAND SURVEYOR
SIGNATURE

**BERRY SURVEYING & ENGINEERING**
335 Second Crown Point Road
Barrington, NH 03825
Phone: (603) 332-2863
Fax: (603) 335-4623
www.BerrySurveying.Com

# Stormwater System Management:

# Inspection and Maintenance Manual

## 49 Winkley Pond Road
## Barrington, NH
## Tax Map 253, Lot 14

Prepared for

Hambone, LLC
242 Central Ave
Dover, NH 03820

Prepared By

Berry Surveying & Engineering
335 Second Crown Point Road
Barrington, NH 03825
603-332-2863

File Number
DB2021-163

August 16, 2023

# Table of Contents

## Introduction

The Best Management Practices (BMP) described in this manual are specified in more detail within the plan set giving design details and specifications. The New Hampshire Stormwater Manual, Volume 2, Post-Construction Best Management Practices Selection & Design (December 2008, NHDES & US EPA) is included by reference to this manual. Additional details, construction specifications, and example drawings are provided within this reference. (http://des.nh.gov/organization/divisions/water/stormwater/)

The BMP's are covered below in the general order in which the storm water flows. Each BMP has a description and maintenance consideration listed. A Check List table is proved after the narrative to summarize the maintenance responsibilities and schedule. A Log Form is also provided for the owners use.

For details regarding the design of the Storm Water System see also Drainage Analysis & Sediment and Erosion Control Plan also published by Berry Surveying & Engineering originally dated August 16, 2023, as revised. See also plan set completed for Hambone, LLC. originally dated August 16, 2023, as revised.

Robert Baldwin, Managing Member, is responsible for the Stormwater System Operation and Maintenance. A significant step in this responsibility is the Inspection and Maintenance of each component of the system. Ongoing, semi-annual, and annual inspection and maintenance requirement are documented below and must be taken seriously. Failure of any component of the system can result in surface water run-off ponding and/or freezing in the roadway and parking lots, leaving the developed site untreated, and/or causing violations to issued permits. The owner must maintain, and have available, plans of the Stormwater System in order properly inspect and maintain the system. (Reduced copies attached.) The Managing Member, Robert Baldwin, as the owner / operator, is responsible to ensure that any subsequent owner, Homeowners Association, or subcontractor has copies of the Log Form and Annual Report records and fully understands the responsibilities of this plan. The grantor owner will ensure this document is provided to the grantee owner by duplicating the Ownership Responsibility Sheet which is found toward the back of this document, which will be maintained with the Inspection & Maintenance Logs, provided to the Town of Barrington, Planning Department, with the Annual Report.

The owner of Tax Map 253, Lot 14, Hambone, LLC, is proposing the development of 7 townhouses. There will be an Infiltration Basin and a Rain Garden to manage and treat the surface water runoff.

The following drainage features will all require periodic inspections and maintenance based on this manual in addition to deep sump catch basins throughout:

Catch Basins (Ponds #C01-#C05)

Drain Manhole (Pond #D01)

Conveyance Swales and Roadside Ditches

Sediment Forebay (Pond #102)

Rain Garden #101 – P-101 w/ RipRap Inlet Protection, Outlet Structure, and Spillway.

Infiltration Basin #102 – P-102 w/ Sediment Forebay & RipRap Outlet

Outlet Protection and Level Spreader

Mulch Berm Buffer Protection (Permanent Perimeter Control)

## Deep Sump Catch Basin / Drain Manhole

Description: A deep sump catch basin consists of a manhole-type structure with an inlet grate, an outlet pipe connected to the piped drainage system, and a sump with a depth several times the diameter of the outlet pipe. The inlet grate is located at the surface, and is sometimes combined with a vertical inlet integrated with a street or parking area curb. The sump's purpose is to capture coarse sediments and debris from the runoff intercepted by the structure. The outlet pipe can be fitted with a "hood" consisting of a cast metal or formed plastic fitting, designed to prevent floating materials from exiting the structure. Deep sump catch basins used as pretreatment are most effective if sited "off-line" since flow-through basins are more susceptible to sediment re-suspension. All pretreatment deep sump catch basins will have an outlet pipe hood which extends one-foot below the outlet invert and will include a hood vent. During construction the catch basins will be protected by inlet protection per the approved construction plans. Hoods are to be installed during initial construction. See SWM Volume 2, 4-4.5 Pre-treatment Practices, 5. Pre-treatment Swales, page 144.

Maintenance Considerations:

Catch basins may require frequent maintenance. Depending on location, this may require several cleanings of the sumps each year. At a minimum, it is recommended that catch basins be inspected at least twice annually, once following snow-melt and once following leaf drop, and cleaned as indicated by inspection. Sediment should be removed when it approaches half the sump depth. If floating hydrocarbons are observed during an inspection, the material should be removed immediately by skimming, absorbent materials, or other method and disposed in conformance with applicable state and federal regulations. Cleaning may require Vacuum-truck instead of "clam-shell" to avoid damage to hood. Damaged hoods should be replaced when noted by inspection.

## Conveyance Swale

Description: Conveyance swales are stabilized channels designed to convey runoff at non-erosive velocities. They may be stabilized using vegetation, riprap, or a combination, or with an alternative lining designed to accommodate design flows while protecting the integrity of the sides and bottom of the channel. Conveyance channels may provide incidental water quality benefits, but are not specifically designed to provide treatment. Conveyance swales are not considered a Treatment or Pretreatment Practice under the AoT regulations, unless they are also designed to meet the requirements of an acceptable Treatment/Pretreatment Practice as described elsewhere in this Chapter. See SWM Volume 2, 4-6.3 Conveyance Practices, Conveyance Swale, page 166.

Maintenance Considerations: Grassed channels should be inspected periodically (at least annually) for sediment accumulation, erosion, and condition of surface lining (vegetation or riprap). Repairs, including stone or vegetation replacement, should be made based on this inspection. Remove sediment and debris annually, or more frequently as warranted by inspection. Mow vegetated channels based on frequency specified by design. Mowing at least once per year is required to control establishment of woody vegetation. It is recommended to cut grass no shorter than 4 inches.

## Sediment Forebay

Description: A sediment forebay is an impoundment, basin, or other storage structure designed to dissipate the energy of incoming runoff and allow for initial settling of coarse sediments. Forebays are used for pretreatment of runoff prior to discharge into the primary water quality treatment BMP. In some cases, forebays may be constructed as separate structures but often, they are integrated into the design of larger stormwater management structures. See SWM Volume 2, 4-4.1 Pre-treatment Practices, Sediment Forebay, page 140.

Maintenance Considerations: Forebays help reduce the sediment load to downstream BMPs, and will therefore require more frequent cleaning. Inspect at least annually; Conduct periodic mowing of embankments (generally two times per year) to control growth of woody vegetation on embankments; Remove debris from outlet structures at least once annually; Remove and dispose of accumulated sediment based on inspection; Install and maintain a staff gage or other measuring device, to indicate depth of sediment accumulation and level at which clean-out is required.

## Bio-Retention System (Rain-Garden)

Description: A bioretention system (sometimes referred to as a “rain garden”) is a type of filtration BMP designed to collect and filter moderate amounts of stormwater runoff using conditioned planting soil beds, gravel beds and vegetation within shallow depressions. The bioretention system may be designed with an underdrain, to collect treated water and convey it to discharge, or it may be designed to infiltrate the treated water directly to the subsoil. Bioretention cells are capable of reducing sediment, nutrients, oil and grease, and trace metals. Bioretention systems should be sited in close proximity to the origin of the stormwater runoff to be treated. The major difference between bioretention systems and other filtration systems is the use of vegetation. A typical surface sand filter is designed to be maintained with no vegetation, whereas a bioretention cell is planted with a variety of shrubs and perennials whose roots assist with pollutant uptake. The use of vegetation allows these systems to blend in with other landscaping features. See SWM Volume 2, 4-3.4c, Treatment Practices, Bio-Retention System, page 110.

Construction Considerations: After the stone and bio-media has been installed, Filtrexx Silt Soxx or approved equal, will be installed at the toe of slope intersection between the berm and bio-media and will remain until the slopes of the berm are stable.

Maintenance Considerations: Systems should be inspected at least twice annually, and following any rainfall event exceeding 2.5 inches in a 24 hour period, with maintenance or rehabilitation conducted as warranted by such inspection. Pretreatment measures should be inspected at least twice annually, and cleaned of accumulated sediment as warranted by inspection, but no less than once annually. Trash and debris should be removed at each inspection. At least once annually, system should be inspected for drawdown time. If bioretention system does not drain within 72-hours following a rainfall event, then a qualified professional should assess the condition of the facility to determine measures required to restore filtration function or infiltration function (as applicable), including but not limited to removal of accumulated sediments or reconstruction of the filter media. Vegetation should be inspected at least annually, and maintained in healthy condition, including pruning, removal and replacement of dead or diseased vegetation, and removal of invasive species. The rain garden is equipped with an underdrain and end cap assembly which will need to be routinely inspected for obstructions.

## In-Ground Infiltration Basin

Description: Infiltration basins are impoundments designed to temporarily store runoff, allowing all or a portion of the water to infiltrate into the ground. An infiltration basin is designed to completely drain between storm events. An infiltration basin is specifically designed to retain and infiltrate the entire Water Quality Volume. Some infiltration basins may infiltrate additional volumes during larger storm events, but many will be designed to release stormwater exceeding the water quality volume from the larger storms. In a properly sited and designed infiltration basin, water quality treatment is provided by runoff pollutants binding to soil particles beneath the basin as water percolates into the subsurface. Biological and chemical processes occurring in the soil also contribute to the breakdown of pollutants. Infiltrated water is used by plants to support growth or it is recharged to the underlying groundwater. As with all impoundment BMPs, surface infiltration basins should be designed with an outlet structure to pass peak flows during a range of storm events, as well as with an emergency spillway to pass peak flows around the embankment during extreme storm events that exceed the combined infiltration capacity and outlet structure capacity of the facility. See SWM Volume 2, 4-3.3b, Treatment Practices, In-Ground Infiltration Basin, page 88.

Maintenance Considerations: Removal of debris from inlet and outlet structures. Removal of accumulated sediment. Inspection and repair of outlet structures and appurtenances. Inspection of infiltration components at least twice annually, and following any rainfall event exceeding 2.5 inches in a 24 hour period, with maintenance or rehabilitation conducted as warranted by such inspection. Inspection of pretreatment measures at least twice annually, and removal of accumulated sediment as warranted by inspection, but no less than once annually. Periodic mowing of embankments. Removal of woody vegetation from embankments. Inspection and repair of embankments and spillways. If an infiltration system does not drain within 72-hours following a rainfall event, then a qualified professional should assess the condition of the facility to determine measures required to restore infiltration function, including but not limited to removal of accumulated sediments or reconstruction of the infiltration trench.

## Stone Berm Level Spreader

Description: A stone berm level spreader is an outlet structure constructed at zero percent grade across a slope used to convert concentrated flow to "sheet flow." It disperses or "spreads" flow thinly over a receiving area, usually consisting of undisturbed, vegetated ground. The conversion of concentrated flow to shallow, sheet flow allows runoff to be discharged at non-erosive velocities onto natural ground. To stabilize the spreader outlet, a stone berm is provided to dissipate flow energy, and help disperse flows along the length of the spreader. Level spreaders are not designed to remove pollutants from stormwater; however, some suspended sediment and associated phosphorous, nitrogen, metals and hydrocarbons will settle out of the runoff through settlement, filtration, infiltration, absorption, decomposition and volatilization. See SWM Volume 2, 4-6.6 Conveyance Practices, Stone Berm Level Spreader, page 162.

Maintenance Considerations: Inspect at least once annually for accumulation of sediment and debris and for signs of erosion within approach channel, spreader channel or down-slope of the spreader. Remove debris whenever observed during inspection. Remove sediment when accumulation exceeds 25% of spreader channel depth. Mow as required by landscaping design. At a minimum, mow annually to control woody vegetation within the spreader. Snow should not be stored within or down-slope of the level spreader or its approach channel. Repair any erosion and re-grade or replace stone berm material, as warranted by inspection. Reconstruct the spreader if down-slope channelization indicates that the spreader is not level or that discharge has become concentrated, and corrections cannot be made through minor re-grading.

## Perimeter Control (Silt Fence / SiltSoxx / Erosion Control Mix Berm)

The plan set demonstrates the location of perimeter sediment control. The Erosion and Sediment Control Details, Sheet E-101, has the specifications for installation and maintenance of the silt fence, Filtrexx mulch filled SiltSoxx (or approved equal), and Erosion Control Mix Berm. There are locations on the site, for example bio-media rain garden protection, where SiltSoxx protection is specified. An area of permanent perimeter control is shown by the well house for wetland buffer protection from steeper slopes.

## Control of Invasive Plants

During maintenance activities, check for the presence of invasive plants and remove in a safe manner as described on the following pages. They should be controlled as described on the following pages.

Invasive plants are introduced, alien, or non-native plants, which have been moved by people from their native habitat to a new area. Some exotic plants are imported for human use such as landscaping, erosion control, or food crops. They also can arrive as "hitchhikers" among shipments of other plants, seeds, packing materials, or fresh produce. Some exotic plants become invasive and cause harm by:

- becoming weedy and overgrown;
- killing established shade trees;
- obstructing pipes and drainage systems;
- forming dense beds in water;
- lowering water levels in lakes, streams, and wetlands;
- destroying natural communities;
- promoting erosion on stream banks and hillsides; and
- resisting control except by hazardous chemical.

## Snow Removal & Winter Maintenance

Description: Drainage and stormwater systems need to be maintained during the winter months so that surface water runoff from a rain storm does not become a impounding and icing problem. Catch basins must remain viable and where sheet flow is a design factor, the edge of pavement and should need to be maintained so that runoff can leave the pavement area. Sand and salt should be used at the rate that prevents sedimentation problems or excess salt deposited but yet enough to allow for protection for pedestrians and vehicles.

Maintenance Considerations: Catch basins are required to be kept viable by removing snow that is block surface water runoff from entering the structure. The edge of pavement where surface water sheet flow is designed to leave the paved area, the edge of pavement and shoulder need to be plowed to allow runoff to leave the pavement. Snow is to piled in designated areas and removed from the site when the on-site storage locations have been exceeded. At the end of the winter season, sediment is to be swept from the paved surfaces and removed from the drainage system. (Sumps if provided, sediment forebays, swale lines.) (See catch basin and drainage pipe maintenance.) NHDES offers training (Green SnowPro Certification) for contractors and owners. https://www.des.nh.gov/land/roads/road-salt-reduction/green-snowpro-certification Please find attached NHDES Green SnoPro Utilization Chart which is required to be used.

## Annual Report

Description: The owner is responsible to keep an **I & M Activity Log** that documents inspection, maintenance and repairs to the storm water management system, and a **Deicing Log** to track the amount and type of deicing material applied to the site. The original owner is responsible to ensure that any subsequent owner (s) have copies of the Stormwater System Operation: Inspection & Maintenance Manual, copies of past logs and check lists. This includes any owner association for potential condominium conversion of the property. The Annual Report will be prepared and submitted to the Town of Barrington, Planning Department with copies of both logs and check lists no later than December 15th of each year and made available to NHDES upon request. Upon an ownership change, the Annual Report will include the Transfer of Ownership Responsibility Forms duplicated from the form found below.

The plans that accompany this manual include a plan sheet, “Inspection & Maintenance Plan” and copies of the Stormwater Treatment Design Sheets. The owner will also maintain a complete set of the approved original design plans.

Respectfully
BERRY SURVEYING & ENGINEERING

Kenneth A. Berry, PE, LLS
CPSWQ, CPESC, CESSWI
Principal, VP – Technical Operations

Kevin R. Poulin, PE
Design Engineer

Christopher R. Berry, SIT
Principal - President

## STORMWATER SYSTEM OPERATIONS: INSPECTION & MAINTENANCE MANUAL

### Inspection & Maintenance Manual Checklist

49 Winkley Pond Road, Barrington, NH, Tax Map 253, Lot 14
Hambone, LLC
242 Central Ave
Dover, NH 03820

| ☑ | Date | BMP / System | Minimum Inspection Frequency | Minimum Inspection Requirements | Maintenance / Cleanout Threshold |
|---|---|---|---|---|---|
| | | Pavement Sweeping | Three Times Per Year | Clean Pavement | Pavement areas will be swept and sedimentation removed so the surface is clean |
| | | | | | |
| | | Litter/Trash Removal | Routinely | Inspect dumpsters, outdoor waste receptacles area, and yard areas. | Parcel will be free of litter/trash. |
| | | | | | |
| | | Deicing Agents | N/A | N/A | Use salt as the primary agent for roadway safety during winter. |
| | | | | | |
| | | Invasive Species | Two times per year. | Inspect for Invasive Species | Remove and dispose invasive species. |
| | | **Closed Drainage System:** | | | |
| | | Drainage Pipes | 1 time per 2 years | Check for sediment accumulation & clogging. | Less than 2" sediment depth |
| | | | | | |
| | | Drop Inlets & Catch Basins | 2 times per year | Check for sediment accumulation & clogging. | Any accumulated Sediment or debris. |

| ☑ | Date | BMP / System | Minimum Inspection Frequency | Minimum Inspection Requirements | Maintenance / Cleanout Threshold |
|---|---|---|---|---|---|
| | | Rain Garden/ Infiltration Pond | 2 times per year | Check for sediment and debris accumulation buildup. | Remove sediment & debris when required. Remove Invasive Species |
| | | | | | |
| | | Rain Garden/ Infiltration Pond | Annually | Drain completely with 72 hours | Evaluate the surface of the practice for sedimentation and clogging. Remove clogging and restore the pond surface to original conditions. |
| | | | | | |
| | | Mulch Berm Buffer Protection | 2 times per year / as needed | Check berm for breaks | Repair berm as needed / ongoing |
| | | | | | |
| | | Riprap Outlet Protection | Annually | Check for sediment buildup and structure damage. | Remove excess sediment and repair damage. |
| | | | | | |
| | | Winter Maintenance | Ongoing | Remove snow as directed. | Ongoing |
| | | | | | |
| | | Post Winter Maintenance | Annually | Remove excess sand, gross solids, and repair vegetation and plantings | Parcel will be free of excess sand, litter/trash. |
| | | | | | |
| | | Annual Report | 1 time per year | Submit Annual Report to Barrington Planning Dept. and kept on file by the owner. | Report to be submitted on or before December 15th each year. |

Inspection Check List: Page 3

The following drainage features will all require periodic inspections and maintenance based on this manual in addition to deep sump catch basins throughout:

Catch Basins (Ponds #C01-#C05)

Drain Manhole (Pond #D01)

Conveyance Swales and Roadside Ditches

Sediment Forebay (Pond #102)

Rain Garden #101 – P-101 w/ RipRap Inlet Protection, Outlet Structure, and Spillway.

Infiltration Basin #102 – P-102 w/ Sediment Forebay & RipRap Outlet

Outlet Protection and Level Spreader

Mulch Berm Buffer Protection (Permanent Perimeter Control)

## STORMWATER SYSTEM OPERATIONS: INSPECTION & MAINTENANCE MANUAL

### Inspection & Maintenance Manual Log Form

49 Winkley Pond Road, Barrington, NH, Tax Map 253, Lot 14
Hambone, LLC
242 Central Ave
Dover, NH 03820

| BMP / System | Date Inspected | Inspector | Cleaning/Repair (List Items & Comments) | Repair Date | Performed By: |
|---|---|---|---|---|---|
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See also attached Checklist for Inspection of Gravel Wetland

**STORMWATER SYSTEM OPERATIONS: INSPECTION & MAINTENANCE MANUAL**

## Deicing Log Form

49 Winkley Pond Road, Barrington, NH, Tax Map 253, Lot 14
Hambone, LLC
242 Central Ave
Dover, NH 03820

| Date | Amount Applied | Performed By: | Date | Amount Applied | Performed By: |
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## STORMWATER SYSTEM OPERATION & MAINTENANCE PLAN CERTIFICATION

| Owner | Responsibility |
|---|---|
| Name: Hambone, LLC<br>Robert Baldwin, Managing Member<br>Address: 242 Central Ave<br>Dover, NH 03820<br>Telephone: 1-603-986-2373<br>E-mail: robert@centralfallsrealty.com.com | The owner is responsible for the conduct of all construction activities, and ultimate compliance with all the provisions of the Stormwater System Operation & Maintenance Plan and the implementation of the Inspection and Maintenance Manual. |
| | |

49 Winkley Pond Road, Barrington, NH, Tax Map 253, Lot 14

## OWNER CERTIFICATION

I certify under penalty of law that this document and all attachments were prepared under my direction and supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Signed: ___________________________________ Date: _______________________

Printed Name:

Representing:


***NOTES:***

1.) OWNER: HAMBONE LLC
242 CENTRAL AVE
DOVER, NH 03820

2.) TAX MAP: TAX MAP 253, LOT 14

3.) LOT AREA: 586,793 Sq. Ft., 13.47 Ac.
330,912 Sq.Ft., 7.60 Ac., TOTAL UPLAND

4.) S.C.R.D. BOOK 4976, PAGE 1023

5.) THE INTENT OF THIS PLAN IS TO DEMONSTRATE THE DRAINAGE INFRASTRUCTURE THAT REQUIRES PERIODIC INSPECTION AND MAINTENANCE. IT IS TO ACCOMPANY A DOCUMENT ENTITLED "STORMWATER SYSTEM MANAGEMENT: INSPECTION AND MAINTENANCE MANUAL" PUBLISHED BY BERRY SURVEYING & ENGINEERING ON THE SAME DATE.

6.) 11x17" PLANS ARE TWICE THE PUBLISHED SCALE.

| REVISION | DATE | DESCRIPTION |
|---|---|---|
| | | |

*LEGEND:*

PROPOSED DRAIN MANHOLE W/ STRUCTURE
PROPOSED CATCH BASIN W/ STRUCTURE
PROPOSED STORMWATER BMP OUTLET STRUCTURE
POORLY DRAINED JURISDICTIONAL WETLAND
50' WETLAND BUFFER
CONTOUR MINOR, EXISTING
CONTOUR MAJOR, EXISTING
CONTOUR MINOR, PROPOSED
CONTOUR MAJOR, PROPOSED
EXISTING DRAINAGE LINE
PROPOSED DRAINAGE LINE
RIP RAP
STORMWATER BEST MANAGEMENT PRACTICE (BMP)

GRAPHIC SCALE

20 0 10 20 40 80

( IN FEET )
1 inch = 20 ft.

INSPECTION & MAINTENANCE PLAN
LAND OF
HAMBONE LLC
49 WINKLEY POND ROAD
BARRINGTON, N.H.
***TAX MAP 253, LOT 14***

BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863

SCALE : 1 IN. EQUALS 20 FT.
DATE : JULY 16, 2023
FILE NO. : DB 2021-163

STATE OF NEW HAMPSHIRE
KENNETH A. BERRY
No. 14243
LICENSED
PROFESSIONAL ENGINEER

## Welcome to New Hampshire's Watershed Report Cards built from the 2020/2022, 305(b)/303(d)

***Each Watershed Report Card covers a single 12-digit Hydrologic Unit Code (HUC12), on average a 34 square mile area. Each Watershed Report Card has three components;***

1. REPORT CARD - A one page card that summarizes the overall use support for Aquatic Life Integrity, Primary Contact (i.e. Swimming), and Secondary Contact (i.e. Boating) Designated Uses on every Assessment Unit ID (AUID) within the HUC12.
2. HUC 12 MAP - A map of the watershed with abbreviated labels for each AUID within the HUC12.
3. ASSESSMENT DETAILS - Anywhere from one to forty pages with the detailed assessment information for each and every AUID in the Report Card and Map.

### *How are the Surface Water Quality Assessment determinations made?*

All readily available data with reliable Quality Assurance/Quality Control is used in the biennial surface water quality assessments. For a full understanding of how the Surface Water Quality Standards (Env-Wq 1700) are translated into surface water quality assessments we urge the reader to review the 2020/2022 Consolidated Assessment and Listing Methodology (CALM).

### *Where can I find more advanced mapping resources?*

GIS files are available by assessment cycle at the NHDES FTP site.

### *I'd like to see the more raw water quality data?*

The web mapping tool allows you to download the data used in the assessment of the primary contact and aquatic life designated uses by clicking on the "Data Access Waterbody Data (Aquatic Life and Swimming Uses)" link for any assessment unit.

### *How are assessments coded in the report card?*

Assessment outcomes are displayed on a color scale as well as an alpha numeric scale that provides additional distinctions for the designated use and parameter level assessments as outlined in the table below.

| | | **Severe**<br>Not Supporting, Severe | **Poor**<br>Not Supporting, Marginal | **Likely Bad**<br>Insufficient Information – Potentially Not Supporting | **No Data**<br>No Data | **Likely Good**<br>Insufficient Information – Potentially Full Supporting | **Marginal**<br>Full Support, Marginal | **Good**<br>Full Support, Good |
|---|---|---|---|---|---|---|---|---|
| **CATEGORY** | **Description** | | | | | | | |
| Category 2 | Meets standards | | | | | | 2-M or 2-OBS | 2-G |
| Category 3 | Insufficient Information | | | 3-PNS | 3-ND | 3-PAS | | |
| Category 4 | Does not Meet Standards; | | | | | | | |
| 4A | TMDL* Completed | 4A-P | 4A-M or 4A-T | | | | | |
| 4B | Other enforceable measure will correct the issue. | 4B-P | 4B-M or 4B-T | | | | | |
| 4C | Non-pollutant (i.e. exotic weeds) | 4C-P | 4C-M | | | | | |
| Category 5 | TMDL* Needed | 5-P | 5-M or 5-T | | | | | |

* TMDL stands for Total Maximum Daily Load studies

# Watershed 305(b) Assessment Summary Report:

## Assessment Cycle: 2020/2022

HUC 12: 010600030903

HUC 12 Name: Bellamy River

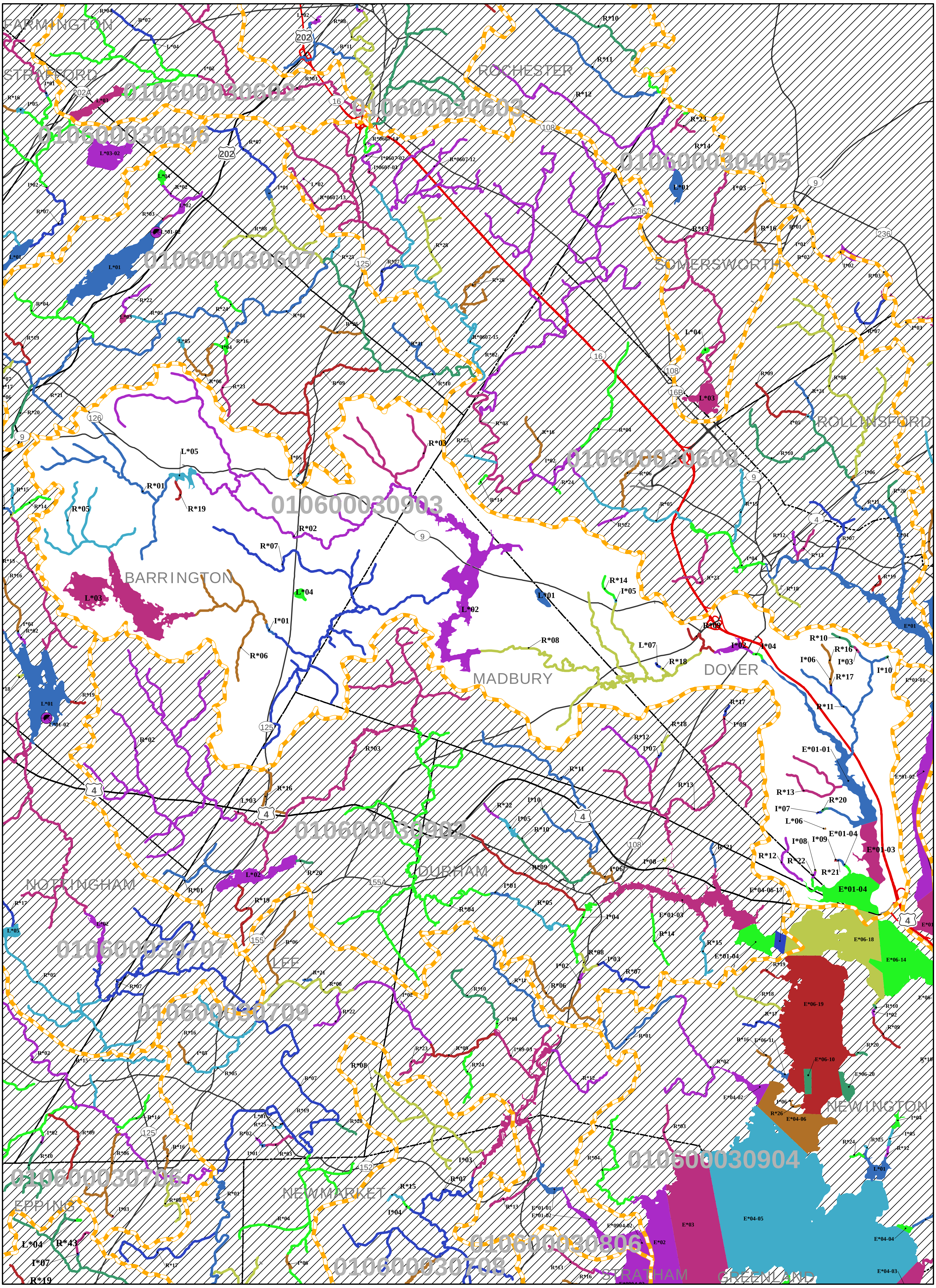
(Locator map on next page only applies to this HUC12)

| | |
|---|---|
| Good | Meets water quality standards/thresholds by a relatively large margin. |
| Marginal | Meets water quality standards/thresholds but only marginally. |
| Likely Good | Limited data available, however, the data that is available suggests that the parameter is Potentially Attaining Standards (PAS). |
| No Current Data | Insufficient information to make an assessment decision. |
| Likely Bad | Limited data available, however, the data that is available suggests that the parameter is Potentially Not Supporting (PNS) water quality standards. |
| Poor | Not meeting water quality standards/thresholds. The impairment is marginal. |
| Severe | Not meeting water quality standards/thresholds. The impairment is more severe and causes poor water quality. |

| Assessment Unit ID | Map Label | Assessment Unit Name | Aquatic Life | Fish Consump. | Swimming | Boating |
|---|---|---|---|---|---|---|
| NHEST600030903-01-01 | E*01-01 | Bellamy River North | | 5-M | 2-G | 2-G |
| NHEST600030903-01-03 | E*01-03 | Bellamy River South Clement Point | 5-P | 5-M | 2-G | 2-G |
| NHEST600030903-01-04 | E*01-04 | Bellamy River South | 5-P | 5-M | 2-G | 2-G |
| NHIMP600030903-01 | I*01 | Bellamy River | 3-ND | 4A-M | 3-ND | 3-ND |
| NHIMP600030903-02 | I*02 | Bellamy River - Sawyers Mill Dam Pond | 5-M | 4A-M | 5-M | 3-ND |
| NHIMP600030903-03 | I*03 | Canney Brook - Wildlife Pond | 3-ND | 4A-M | 3-ND | 3-ND |
| NHIMP600030903-04 | I*04 | Bellamy River Iv Dam | 3-ND | 4A-M | 3-ND | 3-ND |
| NHIMP600030903-05 | I*05 | Knox Marsh Brook | 3-ND | 4A-M | 3-ND | 3-ND |
| NHIMP600030903-06 | I*06 | Unnamed Brook - Thornwood Commons Pond | 3-ND | 4A-M | 3-ND | 3-ND |
| NHIMP600030903-07 | I*07 | Unnamed Brook - Bellamy River Wildlife Pond | 3-ND | 4A-M | 3-ND | 3-ND |
| NHIMP600030903-08 | I*08 | Unnamed Brook - Farm Pond | 3-ND | 4A-M | 3-ND | 3-ND |
| NHIMP600030903-09 | I*09 | Unnamed Brook - Webster Brook Dam | 3-ND | 4A-M | 3-ND | 3-ND |

| | | | | | | |
|---|---|---|---|---|---|---|
| NHIMP600030903-10 | I*10 | Unnamed Brook - Farm Pond | 3-ND | 4A-M | 3-ND | 3-ND |
| NHLAK600030903-01 | L*01 | Barbadoes Pond | 3-ND | 4A-M | 3-ND | 3-ND |
| NHLAK600030903-02 | L*02 | Bellamy Reservoir | 5-M | 4A-M | 3-ND | 3-ND |
| NHLAK600030903-03 | L*03 | Swains Lake | 5-P | 4A-M | 3-PAS | 3-ND |
| NHLAK600030903-04 | L*04 | Winkley Pond | 5-P | 4A-M | 3-ND | 3-ND |
| NHLAK600030903-05 | L*05 | Branch Mallego Brook Pond | 3-ND | 4A-M | 3-ND | 3-ND |
| NHLAK600030903-06 | L*06 | Farm Pond | 3-ND | 4A-M | 3-ND | 3-ND |
| NHLAK600030903-07 | L*07 | Unnamed Pond | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-01 | R*01 | Madla Brook | 5-M | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-02 | R*02 | Mallego Brook | 5-P | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-03 | R*03 | Calef Brook | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-05 | R*05 | Unnamed Brook - To Swains Lake | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-06 | R*06 | Bellamy River - Unnamed Brook | 5-M | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-07 | R*07 | Bellamy River | 5-P | 4A-M | 4A-P | 4A-P |
| NHRIV600030903-08 | R*08 | Bellamy River - Kelly Brook - Knox Marsh Brook | 5-P | 4A-M | 4A-P | 3-PAS |
| NHRIV600030903-09 | R*09 | Bellamy River - Unnamed Brook | 5-M | 4A-M | 4A-P | 3-ND |
| NHRIV600030903-10 | R*10 | Canney Brook | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-11 | R*11 | Varney Brook - Canney Brook | 3-ND | 4A-M | 4A-P | 4A-M |
| NHRIV600030903-12 | R*12 | Unnamed Brook - To Bellamy River Royalls Cove | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-13 | R*13 | Garrison Brook | 3-ND | 4A-M | 4A-P | 3-ND |
| NHRIV600030903-14 | R*14 | Knox Marsh Brook | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-16 | R*16 | Unnamed Brook | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-17 | R*17 | Varney Brook | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-18 | R*18 | Unnamed Brook | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-19 | R*19 | Unnamed Brook | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-20 | R*20 | Unnamed Brook | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-21 | R*21 | Unnamed Brook | 3-ND | 4A-M | 3-ND | 3-ND |
| NHRIV600030903-22 | R*22 | Unnamed Brook | 3-ND | 4A-M | 3-ND | 3-ND |

AUIDs For HUC12: 010600030903 - Bellamy River




HUC12 Boundaries

Town Boundaries

**Major Roads**

Interstate Highway

US Highway

State Highway

**Assessment Unit Coloring AUs Ending with:**

0 =
1 =
2 =
3 =
4 =
5 =
6 =
7 =
8 =
9 =

N W E S

Abbrv. Label: L* 03

HUC 12: 010 700060201

AUID = NH L AK700060201 - 03

Assessment Unit IDs are derived from the HUC12 they reside within. The labels have been shortened on this map for presentation purposes. Example: the Label "L*03" in HUC12 = 010700060201 represents AUID = "NHLAK700060201-03" In rare cases where an AUID extends beyond the boundary of a single HUC12, additional portions of the end of the HUC 12 number have also been replaced.

0 0.8 1.6 2.4 3.2 Miles

Scale:1:78,820

S:\WD-Watershed\WQ_Planning\305b_303d\2020\Report_Cards\HUC12_maps

**Assessment Unit ID:** NHIMP600030903-01
**Assessment Unit Name:** Bellamy River
**Town(s) Primary Town is Listed First:** Barrington

**Size:** 2.70 ACRES
Assessment Unit Category: 3-ND
**Beach:** N

**2020/2022, 305(b)/303(d) - All Reviewed Parameters by Assessment Unit**

| Designated Use Description | Desig. Use Category | Parameter Name | Parameter Threatened (Y/N) | Last Sample | Last Exceed | Parameter Category | TMDL Priority |
|---|---|---|---|---|---|---|---|
| Aquatic Life Integrity | 3-ND | Chlorophyll-a | N | N/A | NLV | 3-ND | |
| | | Dissolved oxygen saturation | N | | | 3-ND | |
| | | Oxygen, Dissolved | N | | | 3-ND | |
| | | pH | N | | | 3-ND | |
| Fish Consumption | 4A-M | MERCURY - FISH CONSUMPTION ADVISORY | N | | | 4A-M | |
| Potential Drinking Water Supply | 2-G | | | | | | |
| Primary Contact Recreation | 3-ND | Escherichia coli | N | | | 3-ND | |
| Secondary Contact Recreation | 3-ND | Escherichia coli | N | | | 3-ND | |
| Wildlife | 3-ND | | | | | | |

| Good | Marginal | Likely Good | No Current Data | Likely Bad | Poor | Severe |
|---|---|---|---|---|---|---|
| Meets water quality standards/thresholds by a relatively large margin. | Meets water quality standards/thresholds but only marginally. | Limited data available. The data that is available suggests that the parameter is Potentially Attaining Standards (PAS) | Insufficient information to make an assessment decision. | Limited data available The data that is available suggests that the parameter is Potentially Not Supporting (PNS) water quality standards. | Not meeting water quality standards/thresholds. The impairment is marginal. | Not meeting water quality standards/thresholds The impairment is more severe and causes poor water quality. |

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 2018 | NHIMP600030902-04 | OYSTER RIVER - MILL POND DAM | DURHAM | 24 | ACRES | Primary Contact Recreatior | Escherichia coli | 4A-P | 9/21/2010 | NEW HAMPSHIRE STATEWIDE E | 39272 | Non-ORW |
| 2018 | NHIMP600030902-06 | BEARDS CREEK | DURHAM | 16 | ACRES | Aquatic Life Integrity | Dissolved oxygen saturation | 5-M | | | | Non-ORW |
| 2018 | NHIMP600030902-06 | BEARDS CREEK | DURHAM | 16 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-M | | | | Non-ORW |
| 2018 | NHIMP600030902-06 | BEARDS CREEK | DURHAM | 16 | ACRES | Primary Contact Recreatior | Escherichia coli | 4A-M | 9/21/2010 | NEW HAMPSHIRE STATEWIDE E | 39272 | Non-ORW |
| 2018 | NHIMP600030903-02 | BELLAMY RIVER - SAWYERS MILL DAM POI | DOVER | 20.717 | ACRES | Aquatic Life Integrity | pH | 5-M | | | | Non-ORW |
| 2018 | NHIMP600030903-02 | BELLAMY RIVER - SAWYERS MILL DAM POI | DOVER | 20.717 | ACRES | Primary Contact Recreatior | Chlorophyll-a | 5-M | | | | Non-ORW |
| 2018 | NHIMP600030903-02 | BELLAMY RIVER - SAWYERS MILL DAM POI | DOVER | 20.717 | ACRES | Primary Contact Recreatior | Escherichia coli | 4A-P | 9/21/2010 | NEW HAMPSHIRE STATEWIDE E | 39272 | Non-ORW |
| 2018 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | 1.377 | ACRES | Aquatic Life Integrity | Arsenic | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | 1.377 | ACRES | Aquatic Life Integrity | Barium | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | 1.377 | ACRES | Aquatic Life Integrity | Benzo(a)pyrene (PAHs) | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | 1.377 | ACRES | Aquatic Life Integrity | Benzo[b]fluoranthene | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | 1.377 | ACRES | Aquatic Life Integrity | Benzo[k]fluoranthene | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | 1.377 | ACRES | Aquatic Life Integrity | DDE | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | 1.377 | ACRES | Aquatic Life Integrity | Indeno[1,2,3-cd]pyrene | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | 1.377 | ACRES | Aquatic Life Integrity | Nickel | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | 1.377 | ACRES | Aquatic Life Integrity | Zinc | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031004-04 | SECORD POND DAM | SEABROOK | 2.5 | ACRES | Aquatic Life Integrity | pH | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031004-04 | SECORD POND DAM | SEABROOK | 2.5 | ACRES | Aquatic Life Integrity | Sedimentation/Siltation | 4C-P | | | | Non-ORW |
| 2018 | NHIMP600031004-05 | CAINS BROOK | SEABROOK | 2.4 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-P | | | | Non-ORW |
| 2018 | NHIMP600031004-05 | CAINS BROOK | SEABROOK | 2.4 | ACRES | Aquatic Life Integrity | pH | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031004-06 | CAINS BROOK - NOYES POND | SEABROOK | 0.9 | ACRES | Aquatic Life Integrity | Chloride | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031004-06 | CAINS BROOK - NOYES POND | SEABROOK | 0.9 | ACRES | Aquatic Life Integrity | Dissolved oxygen saturation | 5-P | | | | Non-ORW |
| 2018 | NHIMP600031004-06 | CAINS BROOK - NOYES POND | SEABROOK | 0.9 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-P | | | | Non-ORW |
| 2018 | NHIMP600031004-06 | CAINS BROOK - NOYES POND | SEABROOK | 0.9 | ACRES | Aquatic Life Integrity | pH | 5-M | | | | Non-ORW |
| 2018 | NHIMP600031004-06 | CAINS BROOK - NOYES POND | SEABROOK | 0.9 | ACRES | Primary Contact Recreatior | Escherichia coli | 4A-M | 8/29/2011 | 58 NH BACTERIA IMPAIRED WA | 40662 | Non-ORW |
| 2018 | NHIMP700010104-01 | LOON POND BROOK - LOON RESERVOIR | LINCOLN | 0.15 | ACRES | | | | | | | ORW |
| 2018 | NHIMP700010201-01 | BOYCE BROOK - BOYCE BROOK DAM | LINCOLN | 0.25 | ACRES | | | | | | | ORW |
| 2018 | NHIMP700010201-04 | UNNAMED BROOK - HIGHWAY DAM | FRANCONIA | 2.415 | ACRES | | | | | | | ORW |
| 2018 | NHIMP700010201-05 | SHADOW LAKE | LINCOLN | 3.091 | ACRES | | | | | | | Review OneStop GIS |
| 2018 | NHIMP700010202-01 | GORDON POND | WOODSTOCK | 1 | ACRES | | | | | | | ORW |
| 2018 | NHIMP700010203-01 | BEAVER BROOK | WOODSTOCK | 0.679 | ACRES | | | | | | | Review OneStop GIS |
| 2018 | NHIMP700010206-01 | DEER RUN POND DAM | CAMPTON | 2.4 | ACRES | | | | | | | ORW |
| 2018 | NHIMP700010302-01 | BLACK BROOK - WEEKS CROSSING POND | WARREN | 8.61 | ACRES | | | | | | | ORW |
| 2018 | NHIMP700010302-03 | ORE HILL MINE POND | WARREN | 1.22 | ACRES | Aquatic Life Integrity | Aluminum | 5-M | | | | ORW |
| 2018 | NHIMP700010302-03 | ORE HILL MINE POND | WARREN | 1.22 | ACRES | Aquatic Life Integrity | Lead | 5-P | | | | ORW |
| 2018 | NHIMP700010302-03 | ORE HILL MINE POND | WARREN | 1.22 | ACRES | Aquatic Life Integrity | pH | 5-P | | | | ORW |
| 2018 | NHIMP700010302-03 | ORE HILL MINE POND | WARREN | 1.22 | ACRES | Aquatic Life Integrity | Zinc | 5-P | | | | ORW |
| 2018 | NHIMP700010401-01-01 | SNOWS BROOK | WATERVILLE VALLEY | 4.361 | ACRES | | | | | | | ORW |
| 2018 | NHIMP700010401-01-02 | SNOWS BROOK - CORCORAN POND TOWN | WATERVILLE VALLEY | 1.38 | ACRES | Primary Contact Recreatior | Escherichia coli | 4A-M | 9/21/2010 | NEW HAMPSHIRE STATEWIDE E | 39276 | ORW |
| 2018 | NHIMP700010401-03 | UNNAMED BROOK - LOCKE 1 DAM | CAMPTON | 1.363 | ACRES | | | | | | | ORW |
| 2018 | NHIMP700010401-04 | CHICKENBORO BROOK RESERVOIR | CAMPTON | 3.877 | ACRES | | | | | | | ORW |
| 2018 | NHIMP700010801-08 | PEMIGEWASSET RIVER - AYERS ISLAND DA | NEW HAMPTON, BRISTOL | 500 | ACRES | Aquatic Life Integrity | Non-Native Aquatic Plants | 4C-P | | | | Non-ORW |
| 2018 | NHIMP700010801-08 | PEMIGEWASSET RIVER - AYERS ISLAND DA | NEW HAMPTON, BRISTOL | 500 | ACRES | Aquatic Life Integrity | pH | 5-P | | | | Non-ORW |
| 2018 | NHIMP700010803-02 | FRANKLIN FALLS FLOOD CTRL - PEMIGEWA | FRANKLIN, HILL, SANBORNTON | 440 | ACRES | Aquatic Life Integrity | Non-Native Aquatic Plants | 4C-M | | | | Non-ORW |
| 2018 | NHIMP700010804-03 | SUCKER BROOK-SUCKER BROOK I DAM | ANDOVER | 0.15 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-M | | | | Non-ORW |
| 2018 | NHIMP700010804-03 | SUCKER BROOK-SUCKER BROOK I DAM | ANDOVER | 0.15 | ACRES | Aquatic Life Integrity | pH | 5-M | | | | Non-ORW |
| 2018 | NHIMP700010804-08 | CHANCE POND BROOK - WEBSTER LAKE D/ | FRANKLIN | 12.3 | ACRES | Aquatic Life Integrity | Non-Native Aquatic Plants | 4C-M | | | | Non-ORW |
| 2018 | NHIMP700020102-01-01 | JONES DAM POND | NEW DURHAM | 56.558 | ACRES | Aquatic Life Integrity | Non-Native Aquatic Plants | 4C-M | | | | Non-ORW |
| 2018 | NHIMP700020102-01-01 | JONES DAM POND | NEW DURHAM | 56.558 | ACRES | Primary Contact Recreatior | Cyanobacteria hepatotoxic microcystins | 5-M | | | | Non-ORW |
| 2018 | NHIMP700020102-01-02 | MARSH POND | NEW DURHAM, ALTON | 58.208 | ACRES | Primary Contact Recreatior | Cyanobacteria hepatotoxic microcystins | 5-M | | | | Non-ORW |
| 2018 | NHIMP700020102-02 | MERRYMEETING RIVER - ALTON POWER D. | ALTON, NEW DURHAM | 719 | ACRES | Aquatic Life Integrity | pH | 5-M | | | | Non-ORW |
| 2018 | NHIMP700020203-01 | KNOWLES POND - TR WILLIAMS BROOK | NORTHFIELD | 54.931 | ACRES | Aquatic Life Integrity | Dissolved oxygen saturation | 5-M | | | | Non-ORW |
| 2018 | NHIMP700020203-01 | KNOWLES POND - TR WILLIAMS BROOK | NORTHFIELD | 54.931 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-P | | | | Non-ORW |
| 2018 | NHIMP700020203-01 | KNOWLES POND - TR WILLIAMS BROOK | NORTHFIELD | 54.931 | ACRES | Aquatic Life Integrity | pH | 4A-M | 9/24/2004 | KNOWLES POND | 11506 | Non-ORW |
| 2018 | NHIMP700020203-07 | WINNIPESAUKEE RIVER - FRANKLIN FALLS I | FRANKLIN | 1.5 | ACRES | Primary Contact Recreatior | Escherichia coli | 4B-M | | | | Non-ORW |
| 2018 | NHIMP700030101-02 | CONTOOCOOK RIVER DAM | JAFFREY | 5 | ACRES | Aquatic Life Integrity | Dissolved oxygen saturation | 5-P | | | | Non-ORW |
| 2018 | NHIMP700030101-02 | CONTOOCOOK RIVER DAM | JAFFREY | 5 | ACRES | Aquatic Life Integrity | Non-Native Aquatic Plants | 4C-P | | | | Non-ORW |
| 2018 | NHIMP700030101-02 | CONTOOCOOK RIVER DAM | JAFFREY | 5 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-P | | | | Non-ORW |
| 2018 | NHIMP700030101-03 | CONTOOCOOK RIVER | JAFFREY | 0.5 | ACRES | Aquatic Life Integrity | Dissolved oxygen saturation | 5-M | | | | Non-ORW |
| 2018 | NHIMP700030101-03 | CONTOOCOOK RIVER | JAFFREY | 0.5 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-M | | | | Non-ORW |
| 2018 | NHIMP700030101-03 | CONTOOCOOK RIVER | JAFFREY | 0.5 | ACRES | Aquatic Life Integrity | pH | 5-P | | | | Non-ORW |
| 2018 | NHIMP700030104-04 | CONTOOCOOK RIVER - NOONE MILL POND | PETERBOROUGH | 17.561 | ACRES | Aquatic Life Integrity | pH | 5-M | | | | Non-ORW |
| 2018 | NHIMP700030104-08 | CONTOOCOOK RIVER - TRANSCRIPT PRINT | PETERBOROUGH | 2.5 | ACRES | Aquatic Life Integrity | pH | 5-M | | | | Non-ORW |
| 2018 | NHIMP700030108-02 | CONTOOCOOK RIVER - PIERCE POWER DAI | BENNINGTON | 3.5 | ACRES | Aquatic Life Integrity | pH | 5-M | | | | Non-ORW |
| 2018 | NHIMP700030202-03 | NORTH BRANCH - WILLIAMS DAM | STODDARD | 55.437 | ACRES | Aquatic Life Integrity | pH | 5-P | | | | Non-ORW |
| 2018 | NHIMP700030204-05-01 | BEARDS BROOK - EAST WASHINGTON DAM | WASHINGTON | 3.502 | ACRES | Aquatic Life Integrity | pH | 5-M | | | | Non-ORW |
| 2018 | NHIMP700030204-05-01 | BEARDS BROOK - EAST WASHINGTON DAM | WASHINGTON | 3.502 | ACRES | Primary Contact Recreatior | Chlorophyll-a | 5-P | | | | Non-ORW |
| 2018 | NHIMP700030204-05-02 | BEARDS BROOK - MILL POND TOWN BEACI | WASHINGTON | 1.38 | ACRES | Primary Contact Recreatior | Escherichia coli | 4A-P | 12/13/2006 | MILL POND TOWN BEACH | 31735 | Non-ORW |
| 2018 | NHIMP700030304-04-02 | SILVER BROOK - SILVER LAKE RESERVOIR B | WARNER | 1.38 | ACRES | Primary Contact Recreatior | Escherichia coli | 4A-P | 8/29/2011 | 58 NH BACTERIA IMPAIRED WA | 40666 | Non-ORW |
| 2018 | NHIMP700030402-04 | BLACKWATER RIVER | NEW LONDON | 2 | ACRES | Aquatic Life Integrity | pH | 5-M | | | | Non-ORW |
| 2018 | NHIMP700030503-01-01 | HOPKINTON DIKE ELM BROOK | HOPKINTON | 213.8 | ACRES | Aquatic Life Integrity | Non-Native Aquatic Plants | 4C-P | | | | Non-ORW |
| 2018 | NHIMP700030503-01-01 | HOPKINTON DIKE ELM BROOK | HOPKINTON | 213.8 | ACRES | Primary Contact Recreatior | Cyanobacteria hepatotoxic microcystins | 5-M | | | | Non-ORW |
| 2018 | NHIMP700030503-01-02 | STATE PARK BEACH ON ELM BROOK | HOPKINTON | 1.38 | ACRES | Primary Contact Recreatior | Cyanobacteria hepatotoxic microcystins | 5-M | | | | Non-ORW |
| 2018 | NHIMP700030503-01-02 | STATE PARK BEACH ON ELM BROOK | HOPKINTON | 1.38 | ACRES | Primary Contact Recreatior | Escherichia coli | 4A-P | 9/21/2010 | NEW HAMPSHIRE STATEWIDE E | 39275 | Non-ORW |

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 2020 | NHEST600031004-09-06 | HAMPTON/SEABROOK HARBOR - HAMPTON HARBOR | HAMPTON | Yes | 0.000 | SQUARE | Shellfish Consumption | MERCURY - FISH CONSUMPTION ADVISORY | 5-M | LOW | Y | | |
| 2020 | NHEST600031004-09-06 | HAMPTON/SEABROOK HARBOR - HAMPTON HARBOR | HAMPTON | Yes | 0.000 | SQUARE | Shellfish Consumption | PCBS - FISH CONSUMPTION ADVISORY | 5-M | LOW | Y | | |
| 2020 | NHEST600031004-09-07 | FISH COOP 150 FT SZ | SEABROOK | Yes | 0.006 | SQUARE | Fish Consumption | MERCURY - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-07 | FISH COOP 150 FT SZ | SEABROOK | Yes | 0.006 | SQUARE | Fish Consumption | PCBS - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-07 | FISH COOP 150 FT SZ | SEABROOK | Yes | 0.006 | SQUARE | Shellfish Consumption | DIOXIN - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-07 | FISH COOP 150 FT SZ | SEABROOK | Yes | 0.006 | SQUARE | Shellfish Consumption | MERCURY - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-07 | FISH COOP 150 FT SZ | SEABROOK | Yes | 0.006 | SQUARE | Shellfish Consumption | PCBS - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-08 | HAMPTON RIVER MARINA SZ | HAMPTON | Yes | 0.146 | SQUARE | Fish Consumption | MERCURY - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-08 | HAMPTON RIVER MARINA SZ | HAMPTON | Yes | 0.146 | SQUARE | Fish Consumption | PCBS - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-08 | HAMPTON RIVER MARINA SZ | HAMPTON | Yes | 0.146 | SQUARE | Shellfish Consumption | DIOXIN - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-08 | HAMPTON RIVER MARINA SZ | HAMPTON | Yes | 0.146 | SQUARE | Shellfish Consumption | MERCURY - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-08 | HAMPTON RIVER MARINA SZ | HAMPTON | Yes | 0.146 | SQUARE | Shellfish Consumption | PCBS - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-09 | HAMPTON/SEABROOK HARBOR | SEABROOK, HAMPTON, HAMPTON FALLS | Yes | 0.615 | SQUARE MILES | Aquatic Life Integrity | Aluminum | 5-M | LOW | N | 2006 | 2006 |
| 2020 | NHEST600031004-09-09 | HAMPTON/SEABROOK HARBOR | SEABROOK, HAMPTON, HAMPTON FALLS | Yes | 0.615 | SQUARE MILES | Aquatic Life Integrity | DDD | 5-M | LOW | N | 2006 | 2004 |
| 2020 | NHEST600031004-09-09 | HAMPTON/SEABROOK HARBOR | SEABROOK, HAMPTON, HAMPTON FALLS | Yes | 0.615 | SQUARE MILES | Aquatic Life Integrity | Dieldrin | 5-M | LOW | N | 2006 | 2004 |
| 2020 | NHEST600031004-09-09 | HAMPTON/SEABROOK HARBOR | SEABROOK, HAMPTON, HAMPTON FALLS | Yes | 0.615 | SQUARE MILES | Aquatic Life Integrity | Lindane | 5-M | LOW | N | 2006 | 2004 |
| 2020 | NHEST600031004-09-09 | HAMPTON/SEABROOK HARBOR | SEABROOK, HAMPTON, HAMPTON FALLS | Yes | 0.615 | SQUARE MILES | Aquatic Life Integrity | trans-Nonachlor | 5-M | LOW | N | 2006 | N/A |
| 2020 | NHEST600031004-09-09 | HAMPTON/SEABROOK HARBOR | SEABROOK, HAMPTON, HAMPTON FALLS | Yes | 0.615 | SQUARE MILES | Fish Consumption | MERCURY - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-09 | HAMPTON/SEABROOK HARBOR | SEABROOK, HAMPTON, HAMPTON FALLS | Yes | 0.615 | SQUARE MILES | Fish Consumption | PCBS - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-09 | HAMPTON/SEABROOK HARBOR | SEABROOK, HAMPTON, HAMPTON FALLS | Yes | 0.615 | SQUARE MILES | Shellfish Consumption | DIOXIN - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-09 | HAMPTON/SEABROOK HARBOR | SEABROOK, HAMPTON, HAMPTON FALLS | Yes | 0.615 | SQUARE MILES | Shellfish Consumption | MERCURY - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-09-09 | HAMPTON/SEABROOK HARBOR | SEABROOK, HAMPTON, HAMPTON FALLS | Yes | 0.615 | SQUARE MILES | Shellfish Consumption | PCBS - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-10 | LITTLE RIVER | NORTH HAMPTON, HAMPTON | Yes | 0.011 | SQUARE | Fish Consumption | MERCURY - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-10 | LITTLE RIVER | NORTH HAMPTON, HAMPTON | Yes | 0.011 | SQUARE | Fish Consumption | PCBS - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-10 | LITTLE RIVER | NORTH HAMPTON, HAMPTON | Yes | 0.011 | SQUARE | Shellfish Consumption | DIOXIN - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-10 | LITTLE RIVER | NORTH HAMPTON, HAMPTON | Yes | 0.011 | SQUARE | Shellfish Consumption | MERCURY - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHEST600031004-10 | LITTLE RIVER | NORTH HAMPTON, HAMPTON | Yes | 0.011 | SQUARE | Shellfish Consumption | PCBS - FISH CONSUMPTION ADVISORY | 5-M | LOW | N | | |
| 2020 | NHIMP400010605-01 | ANDROSCOGGIN RIVER - D. C. POWER DAM | BERLIN | | 100.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2018 | 2018 |
| 2020 | NHIMP400020103-01 | ANDROSCOGGIN RIVER - REFLECTION POND | SHELBURNE | | 56.219 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2013 | 2011 |
| 2020 | NHIMP600020105-04 | GOODRICH FALLS DAM-ELLIS RIVER | BARTLETT | | 3.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2011 | 2011 |
| 2020 | NHIMP600020901-03 | COLD BROOK - MILL BROOK | FREEDOM | | 2.000 | ACRES | Aquatic Life Integrity | Dissolved oxygen saturation | 5-P | LOW | N | 2008 | N/A |
| 2020 | NHIMP600020901-03 | COLD BROOK - MILL BROOK | FREEDOM | | 2.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2008 | 2008 |
| 2020 | NHIMP600030405-03 | SALMON FALLS RIVER - GREAT FALLS UPPER DAM | SOMERSWORTH | Yes | 50.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2018 | 2018 |
| 2020 | NHIMP600030405-04 | SALMON FALLS RIVER - BAXTER MILL DAM POND | ROCHESTER | Yes | 157.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2016 | 2014 |
| 2020 | NHIMP600030406-03 | SALMON FALLS RIVER - ROLLINSFORD DAM | ROLLINSFORD, SOMERSWORTH | Yes | 57.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2018 | 2016 |
| 2020 | NHIMP600030406-04 | SALMON FALLS RIVER - SOUTH BERWICK DAM | ROLLINSFORD | Yes | 58.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2018 | 2016 |
| 2020 | NHIMP600030406-04 | SALMON FALLS RIVER - SOUTH BERWICK DAM | ROLLINSFORD | Yes | 58.000 | ACRES | Primary Contact Recreation | Chlorophyll-a | 5-M | LOW | N | 2018 | 2016 |
| 2020 | NHIMP600030603-01 | COCHECO RIVER - CITY DAM 1 | ROCHESTER | Yes | 50.000 | ACRES | Aquatic Life Integrity | Dissolved oxygen saturation | 5-M | LOW | N | 2019 | 2002 |
| 2020 | NHIMP600030603-01 | COCHECO RIVER - CITY DAM 1 | ROCHESTER | Yes | 50.000 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-M | LOW | N | 2019 | 2007 |
| 2020 | NHIMP600030603-01 | COCHECO RIVER - CITY DAM 1 | ROCHESTER | Yes | 50.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2019 | 2019 |
| 2020 | NHIMP600030603-02 | COCHECO RIVER - HATFIELD DAM | ROCHESTER | Yes | 1.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2010 | 2010 |
| 2020 | NHIMP600030607-02 | COCHECO RIVER - GONIC DAM POND | ROCHESTER | Yes | 18.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2019 | 2019 |
| 2020 | NHIMP600030608-02 | COCHECO RIVER - WATSON WALDRON DAM | DOVER | Yes | 54.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2016 | 2016 |
| 2020 | NHIMP600030608-04 | COCHECO RIVER - CENTRAL AVE DAM | DOVER | Yes | 20.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2018 | 2016 |
| 2020 | NHIMP600030701-01 | LAMPREY RIVER | DEERFIELD | | 40.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2017 | 2017 |
| 2020 | NHIMP600030708-03 | PISCASSIC RIVER | NEWMARKET | Yes | 4.000 | ACRES | Aquatic Life Integrity | Dissolved oxygen saturation | 5-P | LOW | N | 2017 | 2010 |
| 2020 | NHIMP600030708-03 | PISCASSIC RIVER | NEWMARKET | Yes | 4.000 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-P | LOW | N | 2017 | 2017 |
| 2020 | NHIMP600030708-03 | PISCASSIC RIVER | NEWMARKET | Yes | 4.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2017 | 2017 |
| 2020 | NHIMP600030709-02 | LAMPREY RIVER - WISWALL DAM | DURHAM, LEE | | 30.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2019 | 2019 |
| 2020 | NHIMP600030709-03 | LAMPREY RIVER - MACALLEN DAM | DURHAM, NEWMARKET | Yes | 120.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2019 | 2019 |
| 2020 | NHIMP600030803-03 | EXETER RIVER | FREMONT, BRENTWOOD | Yes | 24.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2019 | 2018 |
| 2020 | NHIMP600030901-02 | WINNICUT RIVER DAM POND | GREENLAND | Yes | 1.000 | ACRES | Aquatic Life Integrity | Dissolved oxygen saturation | 5-P | LOW | N | 2018 | 2018 |
| 2020 | NHIMP600030901-02 | WINNICUT RIVER DAM POND | GREENLAND | Yes | 1.000 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-P | LOW | N | 2018 | 2018 |
| 2020 | NHIMP600030901-02 | WINNICUT RIVER DAM POND | GREENLAND | Yes | 1.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2018 | 2018 |
| 2020 | NHIMP600030902-04 | OYSTER RIVER - MILL POND DAM | DURHAM | Yes | 24.000 | ACRES | Aquatic Life Integrity | Dissolved oxygen saturation | 5-M | LOW | N | 2019 | 2017 |
| 2020 | NHIMP600030902-04 | OYSTER RIVER - MILL POND DAM | DURHAM | Yes | 24.000 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-P | LOW | N | 2019 | 2019 |
| 2020 | NHIMP600030902-04 | OYSTER RIVER - MILL POND DAM | DURHAM | Yes | 24.000 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2019 | 2018 |
| 2020 | NHIMP600030902-04 | OYSTER RIVER - MILL POND DAM | DURHAM | Yes | 24.000 | ACRES | Primary Contact Recreation | Chlorophyll-a | 5-M | LOW | N | 2007 | 2007 |
| 2020 | NHIMP600030902-06 | BEARDS CREEK | DURHAM | Yes | 16.000 | ACRES | Aquatic Life Integrity | Dissolved oxygen saturation | 5-M | LOW | N | 2016 | 2005 |
| 2020 | NHIMP600030902-06 | BEARDS CREEK | DURHAM | Yes | 16.000 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-M | LOW | N | 2016 | 2007 |
| 2020 | NHIMP600030903-02 | BELLAMY RIVER - SAWYERS MILL DAM POND | DOVER | Yes | 20.717 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2019 | 2018 |
| 2020 | NHIMP600030903-02 | BELLAMY RIVER - SAWYERS MILL DAM POND | DOVER | Yes | 20.717 | ACRES | Primary Contact Recreation | Chlorophyll-a | 5-M | LOW | N | 2007 | 2006 |
| 2020 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | | 1.377 | ACRES | Aquatic Life Integrity | Arsenic | 5-M | LOW | N | 2006 | 2006 |
| 2020 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | | 1.377 | ACRES | Aquatic Life Integrity | Barium | 5-M | LOW | N | 2006 | 2006 |
| 2020 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | | 1.377 | ACRES | Aquatic Life Integrity | Benzo(a)pyrene (PAHs) | 5-M | LOW | N | 2006 | 2006 |
| 2020 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | | 1.377 | ACRES | Aquatic Life Integrity | Benzo[b]fluoranthene | 5-M | LOW | N | 2006 | 2006 |
| 2020 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | | 1.377 | ACRES | Aquatic Life Integrity | Benzo[k]fluoranthene | 5-M | LOW | N | 2006 | 2006 |
| 2020 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | | 1.377 | ACRES | Aquatic Life Integrity | DDE | 5-M | LOW | N | 2006 | 2006 |
| 2020 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | | 1.377 | ACRES | Aquatic Life Integrity | Indeno[1,2,3-cd]pyrene | 5-M | LOW | N | 2006 | 2006 |
| 2020 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | | 1.377 | ACRES | Aquatic Life Integrity | Nickel | 5-M | LOW | N | 2006 | 2006 |
| 2020 | NHIMP600031003-19 | RICE DAM POND - ON TAYLOR RIVER | HAMPTON FALLS, HAMPTON | | 1.377 | ACRES | Aquatic Life Integrity | Zinc | 5-M | LOW | N | 2006 | 2006 |
| 2020 | NHIMP600031004-04 | SECORD POND DAM | SEABROOK | Yes | 2.500 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2009 | 2008 |
| 2020 | NHIMP600031004-05 | CAINS BROOK | SEABROOK | Yes | 2.400 | ACRES | Aquatic Life Integrity | Oxygen, Dissolved | 5-P | LOW | N | 2009 | 2009 |
| 2020 | NHIMP600031004-05 | CAINS BROOK | SEABROOK | Yes | 2.400 | ACRES | Aquatic Life Integrity | pH | 5-M | LOW | N | 2009 | 2008 |

# ***Control of Invasive Plants***

**New Hampshire**
**Department of Agriculture,**
**Markets & Food**
***Douglas Cygan***
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This guide lists garden plants and weeds which are already causing significant changes to natural areas in the Mid-Atlantic. **Measures for controlling each species are indicated by number, e.g., (3), in the text with a full explanation at the end of this article.** Click on the word Control: to jump to that section. Then click your "back" button to return to the text. Following each section suggested alternative plants are given. These alternatives are native plants, well adapted and needing little care, attractive to birds and butterflies, and an important part of the food web for our indigenous species.

## INVASIVE TREES

**NORWAY MAPLE** (*Acer platanoides*) has large leaves similar to sugar maple. To easily confirm that the plant is Norway maple, break off a leaf and if it's truly Norway maple it will exude milky white sap. Fall foliage is yellow. (Exception: cultivars such as 'Crimson King,' which have red leaves in spring or summer, may have red autumn leaves.) The leaves turn color late, usually in late October after native trees have dropped their foliage. This tree suppresses growth of grass, garden plants, and forest understory beneath it, at least as far as the drip-line. Its wind-borne seeds can germinate and grow in deep shade. The presence of young Norway maples in our woodlands is increasing.

*Control:* (1); (7), (8), (9), or (10); (11) in mid-October to early November, before the leaves turn color.

**TREE OF HEAVEN** (*Ailanthus altissima*), is incredibly tough and can grow in the poorest conditions. It produces huge quantities of wind-borne seeds, grows rapidly, and secretes a toxin that kills other plants. Its long compound leaves, with 11-25 lance-shaped leaflets, smell like peanut butter or burnt coffee when crushed. Once established, this tree cannot be removed by mechanical means alone.

*Control:* (1) - seedlings only. Herbicide - use Garlon 3a (9) with no more than a 1" gap between cuts, or (10); plus (11) on re-growth. Or paint bottom 12" of bark with Garlon 4 Ultra (in February or March to protect surrounding plants). USE MAXIMUM STRENGTH SPECIFIED ON LABEL for all herbicide applications on Ailanthus. Glyphosate is not effective against Ailanthus.

## INVASIVE SHRUBS

**AUTUMN OLIVE** (*Eleagnus umbellata*): Formerly recommended for erosion control and wildlife value, these have proved highly invasive and diminish the overall quality of wildlife habitat.

*Control:* (1) - up to 4" diameter trunks; (7) or (10) or bury stump. Do not mow.

**MULTIFLORA ROSE** (*Rosa multiflora*), formerly recommended for erosion control, hedges, and wildlife habitat, becomes a huge shrub that chokes out all other vegetation and is too dense for many species of birds to nest in, though a few favor it. In shade, it grows up trees like a vine. It is covered with white flowers in June. (Our native roses have fewer flowers, mostly pink.) Distinguish multiflora by its size, and by the presence of very hard, curved thorns, and a fringed edge to the leaf stalk.

*Control:* (1) - pull seedlings, dig out larger plants at least 6" from the crown and 6" down; (4) on extensive infestations; (10) or (11). It may remain green in winter, so herbicide may *applied when other plants are dormant. For foliar application, mix Rodeo with extra sticker-spreader, or use Roundup Sure Shot Foam on small plants.*

**BUSH HONEYSUCKLES** (*Lonicera spp.*), including Belle, Amur, Morrow's, and Tatarian honeysuckle. (In our region, assume that any honeysuckle is exotic unless it is a scarlet-flowered vine). Bush honeysuckles create denser shade than native shrubs, reducing plant diversity and eliminating nest sites for many forest interior species.
*Control*: (2) on ornamentals; (1); on shady sites only, brush cut in early spring and again in early fall (3); (4) during the growing season; (7); or (10) late in the growing season.

**BLUNT-LEAVED PRIVET** (*Ligustrum* obtusifolium). *Control*: (1); (7) or (10); or trim off all flowers. Do not cut back or mow.

**BURNING BUSH, WINGED EUONYMUS** (*Euonymus alatus*), identified by wide, corky wings on the branches.
*Control*: (1); (7) or (10); or trim off all flowers.

**JAPANESE BARBERRY** (*Berberis thunbergii*), and all cultivars and varieties.
*Control*: (1); (7) or (10); or trim off all flowers.

## INVASIVE WOODY VINES

All of these vines shade out the shrubs and young trees of the forest understory, eventually killing them, and changing the open structure of the forest into a dense tangle. DO NOT PLANT NEXT TO OPEN SPACE.

**JAPANESE HONEYSUCKLE** (*Lonicera japonica*), including Hall's honeysuckle, has gold-and-white flowers with a heavenly scent and sweet nectar in June. This is probably the familiar honeysuckle of your childhood. It is a rampant grower that spirals around trees, often strangling them.
*Control*: (1); (3); (10); (11) in fall or early spring when native vegetation is dormant. Plan to re-treat repeatedly.

**ORIENTAL BITTERSWEET** (*Celastrus orbiculatus*) has almost completely displaced American bittersweet (*C. scandens*). The Asian plant has its flowers and bright orange seed capsules in clusters all along the stem, while the native species bears them only at the branch tips.
*Control*: (1); keep ornamental plants cut back, remove all fruits as soon as they open, and bag or burn fruits; to eradicate use Garlon 3a (10).

**JAPANESE KNOTWEED, MEXICAN BAMBOO** (*Polygonum cuspidatum*) can grow in shade. The stems have knotty joints, reminiscent of bamboo. It grows 6-10' tall and has large pointed oval or triangular leaves.
*Control*: Cut at least 3 times each growing season and/or treat with Rodeo (10) or (11). In gardens, heavy mulch or dense shade may kill it.

## INVASIVE HERBACEOUS PLANTS

**GARLIC MUSTARD** (*Alliaria petiolata*, *A. officinalis*), a white-flowered biennial with rough, scalloped leaves (kidney-, heart- or arrow-shaped), recognizable by the smell of garlic and taste of mustard when its leaves are crushed. (The odor fades by fall.)
*Control*: Pull before it flowers in spring (1), removing crown and roots. Tamp down soil afterwards. Once it has flowered, cut (2), being careful not to scatter seed, then bag and burn or send to the landfill. (11) may be appropriate in some settings.

**JAPANESE STILT GRASS** (*Microstegium vimineum*) can be identified by its lime-green color and a line of silvery hairs down the middle of the 2-3" long blade. It tolerates sun or dense shade and quickly invades areas left bare or disturbed by tilling or flooding. An annual grass, it builds up a large seed bank in the soil.

*Control:* Easily pulled in early to mid-summer (1) - be sure to pull before it goes to seed. If seeds have formed, bag and burn or send to landfill. Mowing weekly or when it has just begun to flower may prevent it from setting seed (3). Use glyphosate (11) or herbicidal soap (less effective) on large infestations. Follow up with (5) in spring.

**MILE-A-MINUTE VINE, DEVIL'S TAIL TEARTHUMB** (*Polygonum perfoliatum*), a rapidly growing annual vine with triangular leaves, barbed stems, and turquoise berries in August which are spread by birds. It quickly covers and shades out herbaceous plants.
*Control*: same as for stilt grass.

**SPOTTED KNAPWEED** (*Centaurea maculosa*), a biennial with thistle-like flowers.
*Control:* Do NOT pull (1) unless the plant is young and the ground is very soft - the tap root will break off and produce several new plants. Wear sturdy gloves. (2); (6); (10) or (11).

## CONTROL MEASURES

(1) PULL seedlings and small or shallow-rooted plants when soil is moist. Dig out larger plants, including the root systems. Use a forked spade or weed wrench for trees or shrubs.
(2) DEADHEAD to prevent spread of seeds of invasive plants. Cut off seeds or fruits before they ripen. Bag, and burn or send to a landfill.
(3) MOW or CUTTING at least 4 times a season to deplete plants' store of nutrients and carbohydrates, reduce seed formation, and kill or minimize spread of plants. If necessary, repeat each year.
(4) CONTROLLED BURNING during the spring, repeated over several years, allows native vegetation to compete more effectively with the invasive species. This requires a permit. Spot treatment with glyphosate in late fall can be used to make this method more effective.
(5) Use a CORN-BASED PRE-EMERGENCE HERBICIDE on annual weeds. This product is also an organic fertilizer, i.e., it can stimulate growth of existing plants, including weeds, so it is appropriate for lawns and gardens but may not be appropriate in woodlands.
(6) In lawns, SPOT TREAT with BROAD-LEAF WEEDKILLER. Good lawn-care practices (test soil; use lime and fertilizer only when soil test shows a need; mow high and frequently; leave clippings on lawn) reduce weed infestations.
(7) CUT DOWN the tree. Grind out the stump, or clip off re-growth.
(8) GIRDLE tree: cut through the bark and growing layer (cambium) all around the trunk, about 6" above the ground. Girdling is most effective in spring when the sap is rising, and from middle to late summer when the tree is sending down food to the roots. Clip off sucker sprouts.
(9) FRILL: Using a machete, hatchet or similar device, hack scars (several holes in larger trees) downward into the cambium layer, and squirt in glyphosate (or triclopyr if recommended in text above). Follow label directions for Injection and Frill Applications. This is most effective from middle to late summer. Clip off any sucker sprouts or treat with glyphosate.
(10) CUT STEM / CUT STUMP WITH GLYPHOSATE (or triclopyr if specified above). Follow label directions for Cut Stump Application. Clip off sucker sprouts or paint with glyphosate. See Note on Herbicides.
(11) FOLIAR SPRAY WITH GLYPHOSATE herbicide (see Note on Herbicides). Use a backpack or garden sprayer or mist blower, following label directions. Avoid overspray and/or dripping onto non-target plants, because glyphosate kills most plants except moss. If it rolls off waxy or grass-like foliage, use additional sticker-spreader. Deciduous trees, shrubs, and perennials move nutrients down to the roots in late summer. Glyphosate is particularly effective at this time and when plants have just gone out of flowering. Several invasive species retain their foliage after native plants have lost theirs, and resume growth earlier in spring than most natives. This allows you to treat them without harming the natives. However, the plant must be actively growing for the herbicide to work. Retreatments may be necessary the following year if suckering occurs or the plant hasn't been entirely killed.

NOTE ON HERBICIDES: It is highly recommended that small populations try to be controlled using non-chemical methods wherever feasible. However, for large infestations, and for a few plants specified above, herbicide use is essential. Apply herbicides carefully to avoid non-target plants, glyphosate is the least environmentally damaging herbicide in most cases. Add food coloring for visibility, and a soap-based sticker such as Cide-Kick. Glyphosate is ineffective on some plants; for these, triclopyr (Garlon) may be indicated. When using herbicides, read the entire label and observe all precautions listed, including proper disposal. If in doubt, call your local Cooperative Extension Service.

# Infiltration Feasibility Report

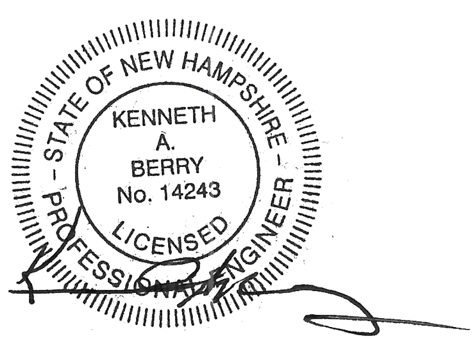
## 49 Winkley Pond Road
## Barrington, NH
## Tax Map 253, Lot 14

Prepared for

Hambone, LLC
242 Central Ave
Dover, NH 03820

Prepared By

Berry Surveying & Engineering
335 Second Crown Point Road
Barrington, NH  03825
603-332-2863




File Number
DB2021-163

August 16, 2023

# Table of Contents

## 1.0 Location of Practices:

The project proposes one location of infiltration for ground water recharge as well as channel flow protection purposes via Infiltration Basin #102.

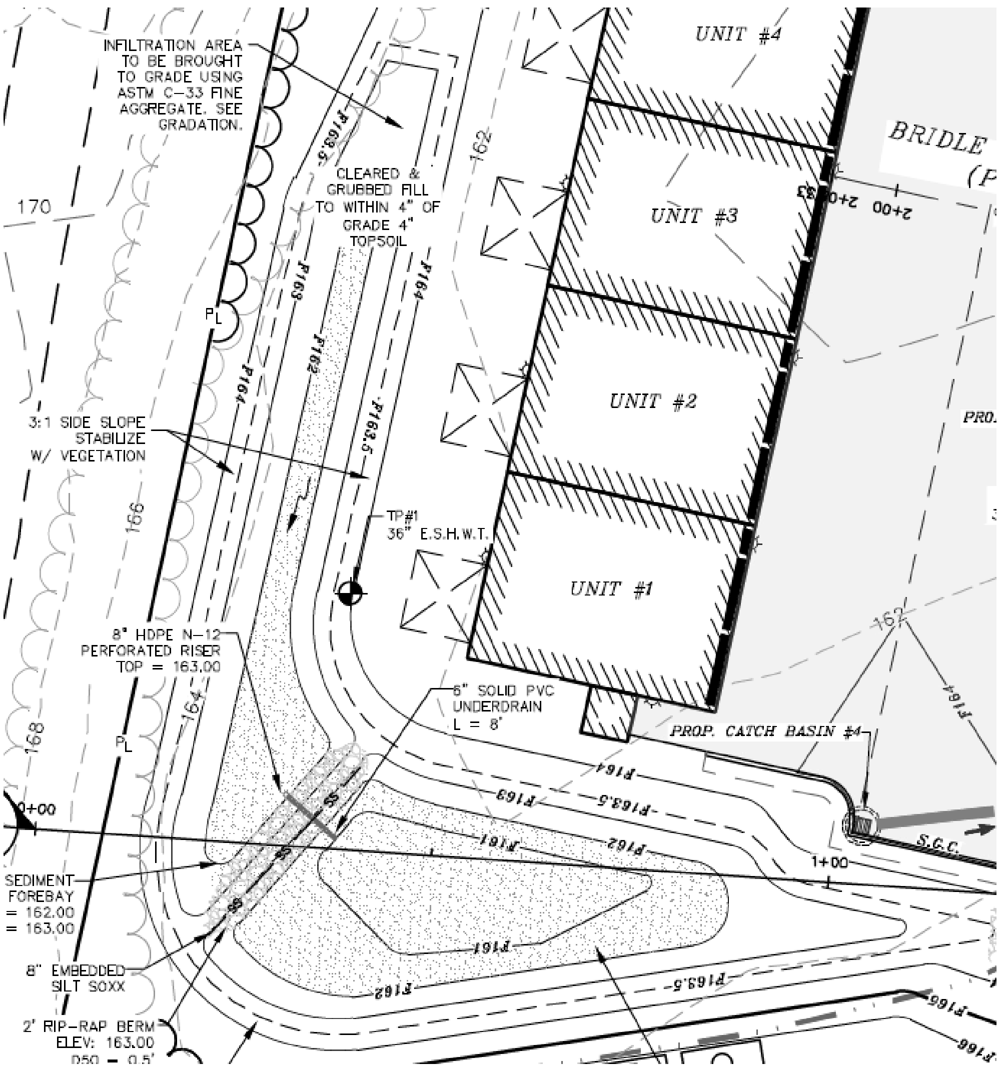
Infiltration Basin #102 (POND 102) – This infiltration basin is on the northeasterly corner of the row of townhouses at the end of the proposed shared driveway. Runoff is collected in a sediment forebay where pre-treatment occurs, before being infiltrated into the ground. This practice infiltrates runoff from residential buildings, grassed area, and collects runoff from uphill of the area of construction.

## 2.0 Existing Topography at the Location of the Practice

Infiltration Basin #102 (POND #102) – The existing topography within the area is at a 3-8% slope. The area is currently a grassed yard that has been mowed over the years.

## 3.0 Test Pit Locations

**Infiltration Basin #102 (POND 102)** – The practice has a surface area of 459 SF at the lowest point. The practice is located over test pit #1. See test pit profiles below. See test pit locations on Sheet P-102, Proposed Infiltration Basin #102 Detail Plan. The test holes were completed in February 2022, (See Site Specific Soil Map Report by John P Hayes III). The soil in the vicinity of this practice is Deerfield (313B), considered to be HSG B soil where the most restrictive published Ksat is 6 inches per hour. This practice was designed using 3 in. / hr.



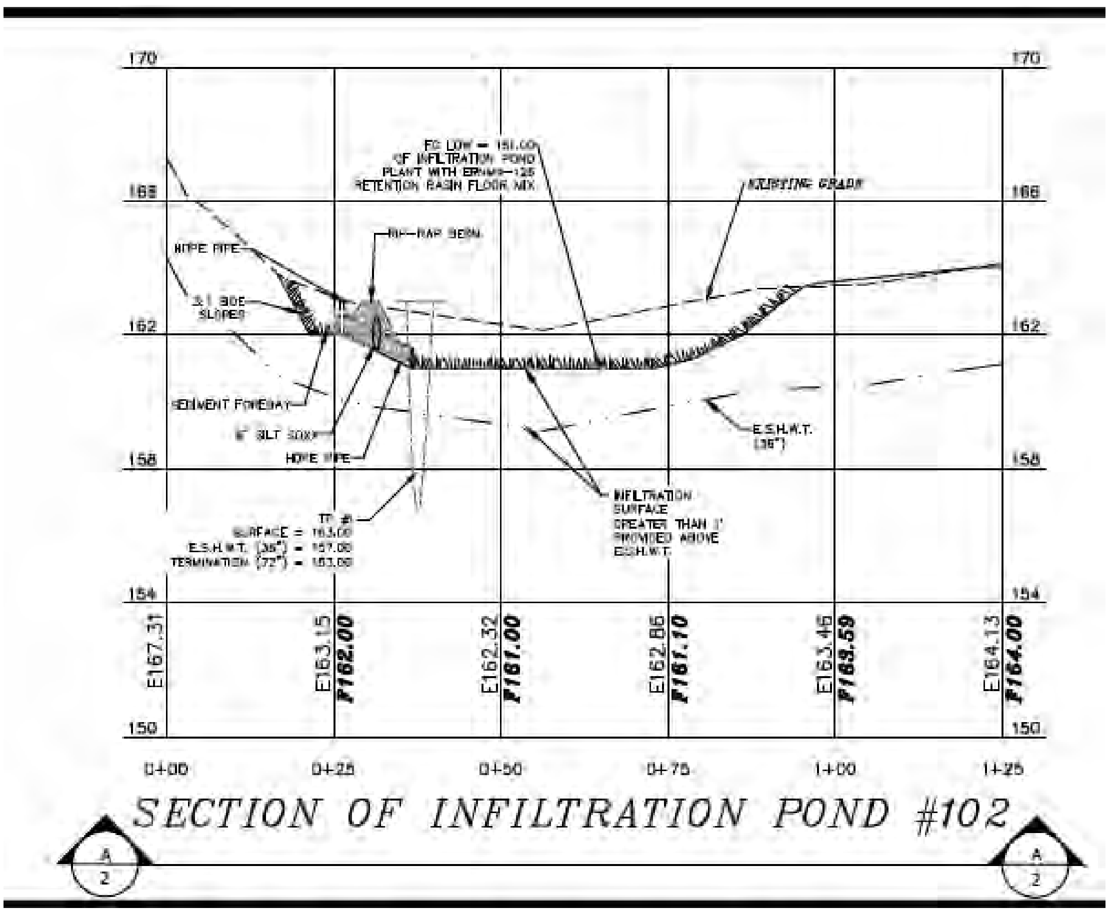

Infiltration Basin #102 (POND 102) – (Reference Sheet P-102)

## 4.0 Seasonal High Water Table (SHWT) and Bedrock Elevations

| | | |
|---|---|---|
| TP#103: | Existing Surface Elevation of TP = | 163.00’ |
| | SHWT = 36 Inches | 160.00’ |
| | Bedrock > 72 Inches | 157.00’ |
| | Ground Water = 50 Inches | 158.83 |
| | Deepest Elevation of TP = | 157.00’ |

Infiltration Basin #102 (Pond 102): Inv. Open Water Storage 161.00’

See cross section below.



## 5.0 Profile descriptions

The following test pit data was collected, see profile below.

TEST PIT #1

0-10” 10YR 3/2 VERY DARK GRAYISH BROWN, LOAMY SAND, GRANULAR, FRIABLE

10-13” 7.5YR 6/1 GRAY, LOAMY SAND, GRANULAR, FRIABLE

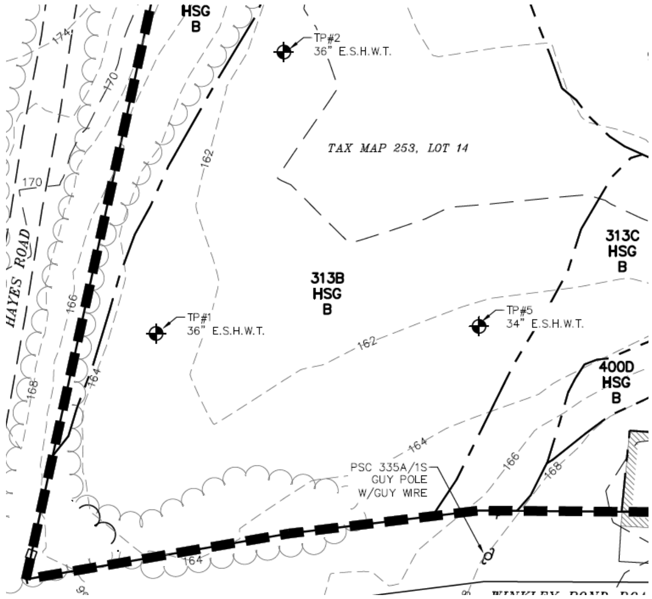
13-18” 5YR 3/3 DARK REDDISH BROWN, LOAMY SAND, GRANULAR, FRIABLE

18-36” 10YR 5/4 YELLOWISH BROWN, LOAMY SAND, GRANULAR, FRIABLE

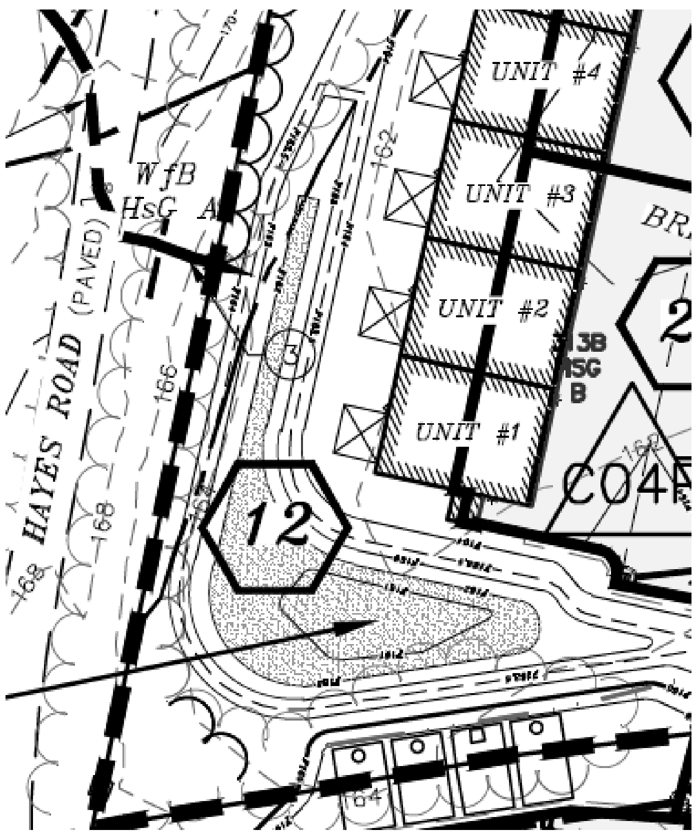
36-72” 10YR 6/2 LIGHT BROWNISH GRAY, FINE SAND WITH REDOX. FEATURES PRESENT, GRANULAR, FRIABLE

E.S.H.W.T. @ 36"
RESTRICTIVE LAYER @ NONE
GROUND WATER @ 50"
TERMINATED @ 72"
REFUSAL @ NONE

# 6.0 Soil Plan in the Area of the Constructed Practice




Infiltration Basin #102 (Pond #102) is located over Deerfield soil. See Test Pit #1.




Infiltration Basin #102 (Pond #102)

## 7.0 Summary of Infiltration Rate

Infiltration Basin #102 is located in Deerfield (313B), considered to be HSG B, soil area as mapped by Site Specific Soil Survey by John P. Hayes III, CSS, with a documented Ksat of 6 inches per hour. The design exfiltration rate for the infiltration basin is 3 inches per hour.

Amoozemeter testing was not conducted on site and the alternate method of using the USDA / NRCS published values was employed. Reference is made to K Sat Values for New Hampshire Soils (Including Hydrologic and DES Soil Lot Sizing Groups, sponsored by the Society of Soil Scientists of Norther New England, Publication #5 dated September 2009.

Respectfully submitted:

BERRY SURVEYING & ENGINEERING

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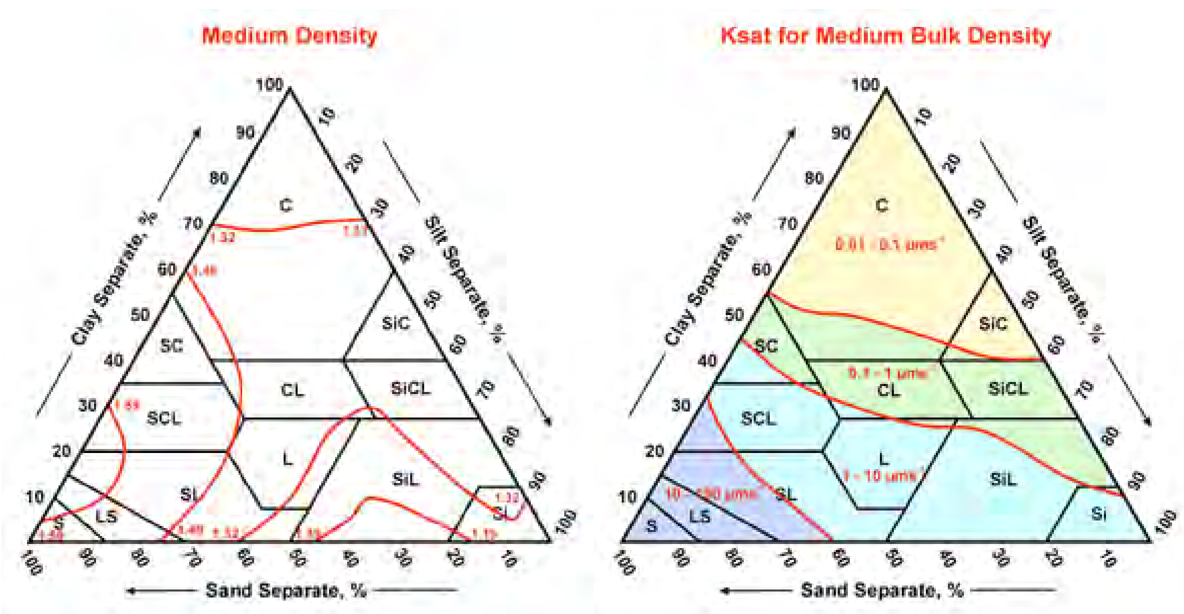
CPSWQ, CPESC, CESSWI
Principal, VP – Technical Operations

# K$_{sat}$ VALUES
## FOR
# NEW HAMPSHIRE SOILS
### (Including Hydrologic and DES Soil Lot Sizing Groups)




**From: Guide for Estimating Ksat from Soil Properties** (**Exhibit 618-9**). (http://soils.usda.gov/technical/handbook/contents/part618ex.html)

**Sponsored by the Society of Soil Scientists of Northern New England**
**SSSNNE Special Publication No. 5**
**September, 2009**

# $K_{sat}$ VALUES
# FOR
# NEW HAMPSHIRE SOILS

## ABOUT THE SOCIETY OF SOIL SCIENTISTS OF NORTHERN NEW ENGLAND

The Society of Soil Scientists of Northern New England (SSSNNE) is a non-profit professional organization of soil scientists, both in the private and public sectors, which is dedicated to the advancement of soil science. The Society fosters the profession of soil classification, mapping and interpretation, and encourages the dissemination of information concerning soil science. With the intent of contributing to the general human welfare, the Society seeks to educate the public on the wise use of soils and the associated natural resources.

## INTRODUCTION

The publication "$K_{sat}$ Values for New Hampshire Soils" is designed to assist soil scientists, engineers, and other professionals by assembling tables of existing data for all soil series currently on the state soil legend with regard to $K_{sat}$ values and hydrologic groupings (Hyd.Grp.). The need for this information has become more important since the adoption by the New Hampshire Department of Environmental Services of the revised Alteration of Terrain rules for stormwater management.  Additional information has been provided for each soil series with regard to landform, temperature regime (Temp.), soil textures, NHDES Soil Lot Size Groupings (Group), whether the soil is a Spodosol (Spodosol?) and other information which will be valuable to a variety of soil information users.

The data for each soil series has been sorted 3 ways for ease of searching:

Table A-Sorted by Numerical Legend
Table B-Sorted by Soil Series Name
Table C-Sorted by NHDES Soil Group for Establishing Lot Size

The report represents cumulative efforts by private soil scientists and NHDES staff with assistance from the USDA Natural Resource Conservation Service.

Comments or inquires on the information in this publication may be directed to the Board of Directors at the following address:

**Society of Soil Scientists**
**of Northern New England**
**PO Box 76**
**Durham, NH  03824**

## SATURATED HYDRAULIC CONDUCTIVITY ($K_{SAT}$)

$K_{sat}$ refers to the ease with which pores in a saturated soil transmit water. The estimates presented here are expressed in terms of inches per hour (NRCS official data presents $K_{sat}$ in both micrometers per second and inches per hour). $K_{sat}$ values are based on soil characteristics observed in the field, particularly structure, consistence, porosity, and texture. (USDA NRCS, Web Soil Survey)

Saturated flow occurs when the soil water pressure is positive; that is, when the soil matric potential is zero (satiated wet condition). In most soils this situation takes place when about 95 percent of the total pore space is filled with water. The remaining 5 percent is filled with entrapped air. Saturated hydraulic conductivity cannot be used to describe water movement under unsaturated conditions. (Soil Survey Manual, 1993)

It is commonly known that soil features (and thus data) for a certain soil series name may be slightly different from one county soil survey to the next and the range in characteristics (via the Typical Pedon) may be slightly different. For example – a Marlow soil (series) in Carroll County may have a higher sand content in its B horizon as opposed to a Marlow soil (series) in Coos County; resulting in a slightly different Ksat range for the B horizon.

The $K_{sat}$ data for this publication was obtained from the USDA-NRCS Soil Data Mart using the Typical Pedon from the county that best reflected the soil and/or had the most acres of that soil. This data is presented in B and C horizons only as it is assumed that the topsoil (A or $A_p$ horizon) will be removed in typical construction practices.

References:

Web Soil Survey. *Soil Survey Staff, Natural Resources Conservation Service, United States Department of Agriculture. Web Soil Survey. Available online at http://websoilsurvey.nrcs.usda.gov/.*

Soil Data Mart. *http://soildatamart.nrcs.usda.gov/*.

Soil Survey Manual. *Soil Survey Division Staff. 1993. Soil survey manual. Soil Conservation Service. U.S. Department of Agriculture Handbook 18.*

**HYDROLOGIC SOIL GROUPS**

Hydrologic group is a group of soils having the same runoff potential under similar storm and cover conditions.

Hydrologic groups are used in equations that estimate runoff from rainfall. These estimates are needed for solving hydrologic problems that arise in planning stormwater management, watershed protection, and flood-prevention projects and for planning or designing structures for the use, control, and disposal of water.

Classifications assigned to soils were based on the use of rainfall-runoff data from small watersheds and infiltrometer plots. From these data, relationships between soil properties and hydrologic groups were established. Assignment of soils to hydrologic groups is based on the relationship between soil properties and hydrologic groups. Wetness characteristics, permeability after prolonged wetting, and depth to very slowly permeable layers are properties that assist in estimating hydrologic groups. Minimum annual steady ponded infiltration rate for a bare ground surface determines the hydrologic soil groups.

Soil properties that influence runoff potential are those that influence the minimum rate of infiltration for a bare soil after prolonged wetting and when not frozen. These properties are depth to a seasonally high water table, intake rate and permeability after prolonged wetting, and depth to a very slowly permeable layer. (The influence of ground cover is treated independently, not in hydrologic soil groups.).

The soils in the United States are placed into four groups, A, B, C, and D, and three dual classes, *A/D, B/D,* and *C/D.* In the definitions of the classes, infiltration rate is the rate at which water enters the soil at the surface and is controlled by the surface conditions. Transmission rate is the rate at which water moves in the soil and is controlled by soil properties. Definitions of the classes are as follows:

**Group A-** Saturated hydraulic conductivity is very high or in the upper half of high and internal free water occurrence is very deep. Soils in this group have low runoff potential when thoroughly wet. Water is transmitted freely through the soil. Group A soils typically have less than 10 percent clay and more than 90 percent sand or gravel and have gravel or sand textures. Some soils having loamy sand, sandy loam, loam or silt loam textures may be placed in this group if they are well aggregated, of low bulk density, or contain greater than 35 percent rock fragments. The limits on the diagnostic physical characteristics of group A are as follows. The saturated hydraulic conductivity of all soil layers exceeds 40.0 micrometers per second (5.67 inches per hour). The depth to any water impermeable layer is greater than 50 centimeters [20 inches]. The depth to the water table is greater than 60 centimeters [24 inches]. Soils that are deeper than 100 centimeters [40 inches] to a water impermeable layer are in group A if the saturated hydraulic conductivity of all soil layers within 100 centimeters [40 inches] of the surface exceeds 10 micrometers per second (1.42 inches per hour).

**Group B-** Saturated hydraulic conductivity is in the lower half of high or in the upper half of moderately high and free water occurrence is deep or very deep. Soils in this group have moderately low runoff potential when thoroughly wet. Water transmission through the soil is unimpeded. Group B soils typically have between 10 percent and 20 percent clay and 50 percent to 90 percent sand and have loamy sand or sandy loam textures. Some soils having loam, silt loam, silt, or sandy clay loam textures may be placed in this group if they are well aggregated, of low bulk density, or contain greater than 35 percent rock fragments. The limits on the diagnostic physical characteristics of group B are as follows. The saturated hydraulic conductivity in the least transmissive layer between the surface and 50 centimeters [20 inches] ranges from 10.0 micrometers per second (1.42 inches per hour) to 40.0 micrometers per second (5.67 inches per hour). The depth to any water impermeable layer is greater than 50 centimeters [20 inches]. The depth to the water table is greater than 60 centimeters [24 inches]. Soils that are deeper than 100 centimeters [40 inches] to a water impermeable layer or water table are in group B if the saturated hydraulic conductivity of all soil layers within 100 centimeters [40 inches] of the surface exceeds 4.0 micrometers per second (0.57 inches per hour) but is less than 10.0 micrometers per second (1.42 inches per hour).

**Group C-** Saturated hydraulic conductivity is in the lower half of moderately high or in the upper half of moderately low and internal free water occurrence is deeper than shallow. Soils in this group have moderately high runoff potential when thoroughly wet. Water transmission through the soil is somewhat restricted. Group C soils typically have between 20 percent and 40 percent clay and less than 50 percent sand and have loam, silt loam, sandy clay loam, clay loam, and silty clay loam textures. Some soils having clay, silty clay, or sandy clay textures may be placed in this group if they are well aggregated, of low bulk density, or contain greater than 35 percent rock fragments. The limits on the diagnostic physical characteristics of group C are as follows. The saturated hydraulic conductivity in the least transmissive layer between the surface and 50 centimeters [20 inches] is between 1.0 micrometers per second (0.14 inches per hour) and 10.0 micrometers per second (1.42 inches per hour). The depth to any water impermeable layer is greater than 50 centimeters [20 inches]. The depth to the water table is greater than 60 centimeters [24 inches]. Soils that are deeper than 100 centimeters [40 inches] to a restriction or water table are in group C if the saturated hydraulic conductivity of all soil layers within 100 centimeters [40 inches] of the surface exceeds 0.40 micrometers per second (0.06 inches per hour) but is less than 4.0 micrometers per second (0.57 inches per hour). .

**Group D-** Saturated hydraulic conductivity is below the upper half of moderately low, and/or internal free water occurrence is shallow or very shallow and transitory through permanent. Soils in this group have high runoff potential when thoroughly wet. Water movement through the soil is restricted or very restricted. Group D soils typically have greater than 40 percent clay, less than 50 percent sand, and have clayey textures. In some areas, they also have high shrink-swell potential. All soils with a depth to a water impermeable layer less than 50 centimeters [20 inches] and all soils with a water table within 60 centimeters [24 inches] of the surface are in this group, although some may have a dual classification, as described in the next section, if they can be adequately drained. The limits on the physical diagnostic characteristics of group D are as follows. For soils with a water impermeable layer at a depth between 50 centimeters and 100 centimeters [20 and 40 inches], the saturated hydraulic conductivity in the least transmissive soil layer is less than or equal to 1.0 micrometers per second (0.14 inches per hour). For soils that are deeper than 100 centimeters [40 inches] to a restriction or water table, the saturated hydraulic conductivity of all soil layers within 100 centimeters [40 inches] of the surface is less than or equal to 0.40 micrometers per second (0.06 inches per hour).

**Dual hydrologic soil groups**-Certain wet soils are placed in group D based solely on the presence of a water table within 60 centimeters [24 inches] of the surface even though the saturated hydraulic conductivity may be favorable for water transmission. If these soils can be adequately drained, then they are assigned to dual hydrologic soil groups *(A/D, B/D,* and *C/D)* based on their saturated hydraulic conductivity and the water table depth when drained. The first letter applies to the drained condition and the second to the undrained condition. For the purpose of hydrologic soil group, adequately drained means that the seasonal high water table is kept at least 60 centimeters [24 inches] below the surface in a soil where it would be higher in a natural state.

References:

National Engineering Handbook, Natural Resource Conservation Service, U.S. Department of Agriculture.

Soil Data Mart. *http://soildatamart.nrcs.usda.gov/*.

Soil Survey Manual. *Soil Survey Division Staff. 1993. Soil survey manual. Natural Resources Conservation Service. U.S. Department of Agriculture Handbook 18.*

# TABLE A

# NUMERICAL LEGEND

| Soil Series | legend number | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Group | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Occum | 1 | 0.6 | 2.0 | 6.00 | 20.0 | B | 2 | Flood Plain (Bottom Land) | mesic | loamy | no | loamy over loamy sand |
| Suncook | 2 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Flood Plain (Bottomland) | mesic | sandy | no | occasionally flooded |
| Lim | 3 | 0.6 | 2.0 | 6.00 | 20.0 | C | 5 | Flood Plain (Bottom Land) | mesic | loamy | no | |
| Pootatuck | 4 | 0.6 | 6.0 | 6.00 | 20.0 | B | 3 | Flood Plain (Bottom Land) | mesic | loamy | no | single grain in C |
| Rippowam | 5 | 0.6 | 6.0 | 6.00 | 20.0 | C | 5 | Flood Plain (Bottom Land) | mesic | loamy | no | |
| Saco | 6 | 0.6 | 2.0 | 6.00 | 20.0 | D | 6 | Flood Plain (Bottom Land) | mesic | silty | no | strata |
| Hadley | 8 | 0.6 | 2.0 | 0.60 | 6.0 | B | 2 | Flood Plain (Bottom Land) | mesic | silty | no | strata of fine sand |
| Winooski | 9 | 0.6 | 6.0 | 0.60 | 6.0 | B | | Flood Plain (Bottom Land) | mesic | silty over loamy | no | |
| Merrimac | 10 | 2.0 | 20.0 | 6.00 | 20.0 | A | 1 | Outwash and Stream Terraces | mesic | gravelly sand | no | loamy cap |
| Gloucester | 11 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Sandy Till | mesic | sandy-skeletal | no | loamy cap |
| Hinckley | 12 | 6.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | mesic | sandy-skeletal | no | |
| Sheepscot | 14 | 6.0 | 20.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | gravelly coarse sand |
| Searsport | 15 | 6.0 | 20.0 | 6.00 | 20.0 | D | 6 | Outwash and Stream Terraces | frigid | sandy | no | organic over sand |
| Saugatuck | 16 | 0.06 | 0.2 | 6.00 | 20.0 | C | 5 | Outwash and Stream Terraces | mesic | sandy | yes | ortstein |
| Colton, gravelly | 21 | 6.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | gravelly surface |
| Colton | 22 | 6.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | |
| Masardis | 23 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | slate, loamy cap |
| Agawam | 24 | 6.0 | 20.0 | 20.00 | 100.0 | B | 2 | Outwash and Stream Terraces | mesic | loamy over sandy | no | loamy over sand/gravel |
| Windsor | 26 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Outwash and Stream Terraces | mesic | sandy | no | |
| Groveton | 27 | 0.6 | 2.0 | 0.60 | 6.0 | B | 2 | Outwash and Stream Terraces | frigid | loamy | yes | loamy over sandy |
| Madawaska | 28 | 0.6 | 2.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | frigid | loamy over sandy | yes | sandy or sandy-skeletal |
| Woodbridge | 29 | 0.6 | 2.0 | 0.00 | 0.6 | C | 3 | Firm, platy, loamy till | mesic | loamy | no | sandy loam in Cd |
| Unadilla | 30 | 0.6 | 2.0 | 2.00 | 20.0 | B | 2 | Terraces and glacial lake plains | mesic | silty | no | silty over gravelly |
| Hartland | 31 | 0.6 | 2.0 | 0.20 | 2.0 | B | 2 | Terraces and glacial lake plains | mesic | silty | no | very fine sandy loam |
| Boxford | 32 | 0.1 | 0.2 | 0.00 | 0.2 | C | 3 | Silt and Clay Deposits | mesic | fine | no | silty clay loam |
| Scitico | 33 | 0.0 | 0.2 | 0.00 | 0.2 | C | 5 | Silt and Clay Deposits | mesic | fine | no | |
| Wareham | 34 | 6.0 | 20.0 | 6.00 | 20.0 | C | 5 | Outwash and Stream Terraces | mesic | sandy | no | |
| Champlain | 35 | 6.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | frigid | gravelly sand | no | |
| Adams | 36 | 6.0 | 20.0 | 20.00 | 99.0 | A | 1 | Outwash and Stream Terraces | frigid | sandy | yes | |
| Melrose | 37 | 2.0 | 6.0 | 0.00 | 0.2 | C | 3 | Sandy/loamy over silt/clay | frigid | loamy over clayey | no | silty clay loam in C |
| Eldridge | 38 | 6.0 | 20.0 | 0.06 | 0.6 | C | 3 | Sandy/loamy over silt/clay | mesic | sandy over loamy | no | |
| Millis | 39 | | | | | C | 3 | Firm, platy, sandy till | frigid | loamy | yes | loamy sand in Cd |
| Canton | 42 | 2.0 | 6.0 | 6.00 | 20.0 | B | 2 | Loose till, sandy textures | mesic | loamy over sandy | no | loamy over loamy sand |
| Montauk | 44 | 0.6 | 6.0 | 0.06 | 0.6 | C | 3 | Firm, platy, sandy till | mesic | loamy | no | loamy sand in Cd |
| Henniker | 46 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, sandy till | frigid | loamy | no | loamy sand in Cd |
| Madawaska, aquentic | 48 | 0.6 | 2.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | frigid | loamy over sandy | yes | sandy or sandy-skeletal |
| Whitman | 49 | 0.0 | 0.2 | 0.00 | 0.2 | D | 6 | Firm, platy, loamy till | mesic | loamy | no | mucky loam |
| Hermon | 55 | 2.0 | 20.0 | 6.00 | 20.0 | A | 1 | Sandy Till | frigid | sandy-skeletal | yes | loamy cap |
| Becket | 56 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, sandy till | frigid | loamy | yes | gravelly sandy loam in Cd |
| Waumbeck | 58 | 2.0 | 20.0 | 6.00 | 20.0 | B | 3 | Loose till, sandy textures | frigid | sandy-skeletal | yes | very cobbly loamy sand |
| Charlton | 62 | 0.6 | 6.0 | 0.60 | 6.0 | B | 2 | Loose till, loamy textures | mesic | loamy | no | fine sandy loam |
| Paxton | 66 | 0.6 | 2.0 | 0.00 | 0.2 | C | 3 | Firm, platy, loamy till | mesic | loamy | no | |
| Sutton | 68 | 0.6 | 6.0 | 0.60 | 6.0 | B | 3 | Loose till, loamy textures | mesic | loamy | no | |
| Berkshire | 72 | 0.6 | 6.0 | 0.60 | 6.0 | B | 2 | Loose till, loamy textures | frigid | loamy | yes | fine sandy loam |
| Marlow | 76 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | yes | fine sandy loam in Cd |
| Peru | 78 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | yes | |
| Thorndike | 84 | 0.6 | 2.0 | 0.60 | 2.0 | C/D | 4 | Friable till, silty, schist & phyllite | frigid | loamy-skeletal | yes | less than 20 in. deep |
| Hollis | 86 | 0.6 | 6.0 | 0.60 | 6.0 | C/D | 4 | Loose till, bedrock | mesic | loamy | no | less than 20 in. deep |
| Winnecook | 88 | 0.6 | 2.0 | 0.60 | 2.0 | C | 4 | Friable till, silty, schist & phyllite | frigid | loamy-skeletal | yes | 20 to 40 in. deep |
| Chatfield | 89 | 0.6 | 6.0 | 0.60 | 6.0 | B | 4 | Loose till, bedrock | mesic | loamy | no | 20 to 40 in. deep |
| Hogback | 91 | 2.0 | 6.0 | 2.00 | 6.0 | C | 4 | Loose till, bedrock | frigid | loamy | yes | less than 20 in. deep |
| Lyman | 92 | 2.0 | 6.0 | 2.00 | 6.0 | A/D | 4 | Loose till, bedrock | frigid | loamy | yes | less than 20 in. deep |
| Woodstock | 93 | 2.0 | 6.0 | 2.00 | 6.0 | C/D | 4 | Loose till, bedrock | frigid | loamy | no | less than 20 in. deep |
| Rawsonville | 98 | 0.6 | 6.0 | 0.60 | 6.0 | C | 4 | Loose till, bedrock | frigid | loamy | yes | 20 to 40 in. deep |
| Tunbridge | 99 | 0.6 | 6.0 | 0.60 | 6.0 | C | 4 | Loose till, bedrock | frigid | loamy | yes | 20 to 40 in. deep |

| Soil Series | legend number | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Group | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Ondawa | 101 | 0.6 | 6.0 | 6.00 | 20.0 | B | 2 | Flood Plain (Bottom Land) | frigid | loamy | no | loamy over loamy sand |
| Sunday | 102 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Flood Plain (Bottomland) | frigid | sandy | no | occasionally flooded |
| Winooski | 103 | 0.6 | 6.0 | 0.60 | 6.0 | B | 3 | Flood Plain (Bottom Land) | mesic | silty | no | very fine sandy loam |
| Podunk | 104 | 0.6 | 6.0 | 6.00 | 20.0 | B | 3 | Flood Plain (Bottom Land) | frigid | loamy | no | loamy to coarse sand in C |
| Rumney | 105 | 0.6 | 6.0 | 6.00 | 20.0 | C | 5 | Flood Plain (Bottom Land) | frigid | loamy | no | |
| Hadley | 108 | 0.6 | 2.0 | 0.60 | 6.0 | B | 2 | Flood Plain (Bottom Land) | mesic | silty | no | strata of fine sand, occ flooded |
| Limerick | 109 | 0.6 | 2.0 | 0.60 | 2.0 | C | 5 | Flood Plain (Bottom Land) | mesic | silty | no | |
| Scarboro | 115 | 6.0 | 20.0 | 6.00 | 20.0 | D | 6 | Outwash and Stream Terraces | mesic | sandy | no | organic over sand, non stony |
| Finch | 116 | | | | | C | 3 | Outwash and Stream Terraces | frigid | sandy | yes | cemented (ortstein) |
| Sudbury | 118 | 2.0 | 6.0 | 2.00 | 20.0 | B | 3 | Outwash and Stream Terraces | mesic | sandy | no | loam over gravelly sand |
| Telos | 123 | 0.6 | 2.0 | 0.02 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | channery silt loam in Cd |
| Chesuncook | 126 | 0.6 | 2.0 | 0.02 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | channery silt loam in Cd |
| Allagash | 127 | 0.6 | 2.0 | 6.00 | 20.0 | B | 2 | Outwash and Stream Terraces | frigid | loamy over sandy | yes | loamy over sandy |
| Elliottsville | 128 | 0.6 | 2.0 | 0.60 | 2.0 | B | 4 | Friable till, silty, schist & phyllite | frigid | loamy | yes | 20 to 40 in. deep |
| Hitchcock | 130 | 0.6 | 2.0 | 0.06 | 0.6 | B | 3 | Terraces and glacial lake plains | mesic | silty | no | silt loam to silt in C |
| Burnham | 131 | 0.2 | 6.0 | 0.02 | 0.2 | D | 6 | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | organic over silt |
| Dartmouth | 132 | 0.6 | 2.0 | 0.06 | 0.6 | B | 3 | Terraces and glacial lake plains | mesic | silty | no | thin strata silty clay loam |
| Monson | 133 | 0.6 | 2.0 | 0.60 | 2.0 | D | 4 | Friable till, silty, schist & phyllite | frigid | loamy | yes | less than 20 in. deep |
| Maybid | 134 | 0.0 | 0.2 | 0.00 | 0.2 | D | 6 | Silt and Clay Deposits | mesic | fine | no | silt over clay |
| Shapleigh | 136 | | | | | C/D | 4 | Sandy Till | mesic | sandy | yes | less than 20 in. deep |
| Monadnock | 142 | 0.6 | 2.0 | 2.00 | 6.0 | B | 2 | Loose till, sandy textures | frigid | loamy over sandy, sandy-skeletal | yes | gravelly loamy sand in C |
| Acton | 146 | 2.0 | 20.0 | 2.00 | 20.0 | B | 3 | Loose till, sandy textures | mesic | sandy-skeletal | no | cobbly loamy sand |
| Vassalboro | 150 | | | | | D | 6 | Organic Materials - Freshwater | frigid | peat | no | deep organic |
| Success | 154 | 2.0 | 6.0 | 6.00 | 20.0 | A | 1 | Sandy Till | frigid | sandy-skeletal | yes | cemented |
| Canterbury | 166 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | no | loam in Cd |
| Sunapee | 168 | 0.6 | 2.0 | 0.60 | 6.0 | B | 3 | Loose till, loamy textures | frigid | loamy | yes | |
| Waskish | 195 | | | | | D | 6 | Organic Materials - Freshwater | frigid | peat | no | deep organic |
| Ondawa | 201 | 0.6 | 6.0 | 6.00 | 20.0 | B | 2 | Flood Plain (Bottom Land) | frigid | loamy | no | occ flood, loamy over l. sand |
| Sunday | 202 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Flood Plain (Bottomland) | frigid | sandy | no | frequently flooded |
| Fryeburg | 208 | 0.6 | 2.0 | 2.00 | 6.0 | B | 2 | Flood Plain (Bottom Land) | frigid | silty | no | very fine sandy loam |
| Charles | 209 | 0.6 | 100.0 | 0.60 | 100.0 | C | 5 | Flood Plain (Bottom Land) | frigid | silty | no | |
| Warwick | 210 | 2.0 | 6.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | mesic | loamy-skeletal | no | loamy over slate gravel |
| Naumburg | 214 | 6.0 | 20.0 | 6.00 | 20.0 | C | 5 | Outwash and Stream Terraces | frigid | sandy | yes | |
| Boscawen | 220 | 6.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | frigid | sandy-skeletal | no | loamy cap |
| Bemis | 224 | 0.6 | 0.2 | 0.00 | 0.2 | C | 5 | Firm, platy, loamy till | cryic | loamy | no | |
| Bice | 226 | 0.6 | 6.0 | 0.60 | 6.0 | B | 2 | Loose till, loamy textures | frigid | loamy | no | sandy loam |
| Lanesboro | 228 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | channery silt loam in Cd |
| Poocham | 230 | 0.6 | 2.0 | 0.20 | 2.0 | B | 3 | Terraces and glacial lake plains | mesic | silty | no | silt loam in C |
| Buxton | 232 | 0.1 | 0.6 | 0.00 | 0.2 | C | 3 | Silt and Clay Deposits | frigid | fine | no | silty clay |
| Scantic | 233 | 0.0 | 0.2 | 0.00 | 0.2 | D | 5 | Silt and Clay Deposits | frigid | fine | no | |
| Biddeford | 234 | 0.0 | 0.2 | 0.00 | 0.2 | D | 6 | Silt and Clay Deposits | frigid | fine | no | organic over clay |
| Buckland | 237 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, loamy till | frigid | loamy | no | loam in Cd |
| Elmridge | 238 | 2.0 | 6.0 | 0.00 | 0.2 | C | 3 | Sandy/loamy over silt/clay | mesic | loamy over clayey | no | |
| Brayton | 240 | 0.6 | 2.0 | 0.06 | 0.6 | C | 5 | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | |
| Lyme | 246 | 0.6 | 6.0 | 0.60 | 6.0 | C | 5 | Loose till, sandy textures | frigid | loamy | no | |
| Millsite | 251 | 0.6 | 6.0 | 0.60 | 6.0 | C | 4 | Loose till, bedrock | frigid | loamy | no | 20 to 40 in. deep |
| Macomber | 252 | 0.6 | 2.0 | 0.60 | 2.0 | C | 4 | Friable till, silty, schist & phyllite | frigid | loamy-skeletal | yes | 20 to 40 in. deep |
| Lombard | 259 | 0.6 | 6.0 | 2.00 | 20.0 | C/D | 2 | Weathered bedrock, phyllite | frigid | loamy | no | very channery |
| Sunapee var | 269 | 0.6 | 2.0 | 0.60 | 6.0 | B | 3 | Loose till, loamy textures | frigid | loamy | yes | frigid dystrudept |
| Chatfield Var. | 289 | 0.6 | 6.0 | 0.60 | 6.0 | B | 3 | Loose till, bedrock | mesic | loamy | no | mwd to swpd |
| Greenwood | 295 | | | | | A/D | 6 | Organic Materials - Freshwater | frigid | hemic | no | deep organic |
| Catden | 296 | | | | | A/D | 6 | Organic Materials - Freshwater | mesic | sapric | no | deep organic |
| Lovewell | 307 | 0.6 | 2.0 | 0.60 | 2.0 | B | 3 | Flood Plain (Bottom Land) | frigid | silty | no | very fine sandy loam |
| Quonset | 310 | 2.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | mesic | sandy-skeletal | no | shale |
| Deerfield | 313 | 6.0 | 20.0 | 20.00 | 100.0 | B | 3 | Outwash and Stream Terraces | mesic | sandy | no | single grain in C |

| Soil Series | legend number | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Group | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Pipestone | 314 | | | | | B | 5 | Outwash and Stream Terraces | mesic | sandy | yes | |
| Mashpee | 315 | 6.0 | 20.0 | 6.00 | 20.0 | B | 5 | Outwash and Stream Terraces | mesic | sandy | yes | |
| Bernardston | 330 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | mesic | loamy | no | channery silt loam in Cd |
| Roundabout | 333 | 0.2 | 2.0 | 0.06 | 0.6 | C | 5 | Terraces and glacial lake plains | frigid | silty | no | silt loam in the C |
| Pittstown | 334 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | mesic | loamy | no | channery silt loam in Cd |
| Elmwood | 338 | 2.0 | 6.0 | 0.00 | 0.2 | C | 3 | Sandy/loamy over silt/clay | frigid | loamy over clayey | no | |
| Stissing | 340 | 0.6 | 2.0 | 0.06 | 0.2 | C | 5 | Firm, platy, silty till, schist & phyllite | mesic | loamy | no | |
| Cardigan | 357 | 0.6 | 2.0 | 0.60 | 2.0 | B | 4 | Friable till, silty, schist & phyllite | mesic | loamy | no | 20 to 40 in. deep |
| Kearsarge | 359 | 0.6 | 2.0 | 0.60 | 2.0 | B | 4 | Friable till, silty, schist & phyllite | mesic | loamy | no | less than 20 in. deep |
| Dutchess | 366 | 0.6 | 2.0 | 0.60 | 2.0 | B | 2 | Friable till, silty, schist & phyllite | mesic | loamy | no | very channery |
| Dixfield | 378 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | yes | fine sandy loam in Cd |
| Timakwa | 393 | | | 6.00 | 100.0 | D | 6 | Organic Materials - Freshwater | mesic | sandy or sandy-skeletal | no | organic over sand |
| Chocorua | 395 | | | 6.00 | 20.0 | D | 6 | Organic Materials - Freshwater | frigid | sandy or sandy-skeletal | no | organic over sand |
| Ipswich | 397 | | | | | D | 6 | Tidal Flat | mesic | hemic/sapric | no | deep organic |
| Suncook | 402 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Flood Plain (Bottomland) | mesic | sandy | no | frequent flooding |
| Metallak | 404 | 6.0 | 100.0 | 6.00 | 100.0 | B | 3 | Flood Plain (Bottom Land) | frigid | loamy over sandy | no | sandy or sandy-skeletal |
| Medomak | 406 | 0.6 | 2.0 | 0.60 | 2.0 | D | 6 | Flood Plain (Bottom Land) | frigid | silty | no | organic over silt |
| Haven | 410 | 0.6 | 2.0 | 20.00 | 100.0 | B | 2 | Outwash and Stream Terraces | mesic | loamy over sandy | no | loamy over sand/gravel |
| Duane | 413 | 6.0 | 20.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | cemented (ortstein) |
| Moosilauke | 414 | 6.0 | 20.0 | 6.00 | 20.0 | C | 5 | Loose till, sandy textures | frigid | sandy | no | |
| Grange | 433 | 0.6 | 2.0 | 0.60 | 2.0 | C | 5 | Outwash and Stream Terraces | frigid | co. loamy over sandy (skeletal) | no | |
| Swanton | 438 | 2.0 | 6.0 | 0.00 | 0.2 | C | 5 | Sandy/loamy over silt/clay | frigid | co. loamy over clayey | no | |
| Shaker | 439 | 2.0 | 6.0 | 0.00 | 0.2 | C | 5 | Sandy/loamy over silt/clay | mesic | co. loamy over clayey | no | |
| Chichester | 442 | 0.6 | 2.0 | 2.00 | 6.0 | B | | Loose till, sandy textures | frigid | loamy over sandy | no | loamy over loamy sand |
| Newfields | 444 | 0.6 | 2.0 | 0.60 | 2.0 | B | 3 | Loose till, sandy textures | mesic | loamy over sandy | no | sandy or sandy-skeletal |
| Scituate | 448 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, sandy till | mesic | loamy | no | loamy sand in Cd |
| Metacomet | 458 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, sandy till | frigid | loamy | no | loamy sand in Cd |
| Pennichuck | 460 | 0.6 | 2.0 | 0.60 | 2.0 | B | 4 | Friable till, silty, schist & phyllite | mesic | loamy-skeletal | no | 20 to 40 in. deep |
| Gilmanton | 478 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | no | fine sandy loam in Cd |
| Ossipee | 495 | | | 0.20 | 2.0 | D | 6 | Organic Materials - Freshwater | frigid | loamy | no | organic over loam |
| Natchaug | 496 | | | 0.20 | 2.0 | D | 6 | Organic Materials - Freshwater | mesic | loamy | no | organic over loam |
| Pawcatuck | 497 | | | 20.00 | 100.0 | D | 6 | Tidal Flat | mesic | sandy or sandy-skeletal | no | organic over sand |
| Abenaki | 501 | 0.6 | 2.0 | 6.00 | 99.0 | B | 2 | Outwash and Stream Terraces | frigid | loamy over sandy-skeletal | no | loamy over gravelly |
| Cohas | 505 | 0.6 | 2.0 | 0.60 | 100.0 | C | 5 | Flood Plain (Bottom Land) | frigid | co. loamy over sandy (skeletal) | no | |
| Hoosic | 510 | 2.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | mesic | sandy-skeletal | no | slate, loamy cap |
| Ninigret | 513 | 0.6 | 6.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | mesic | loamy over sandy | no | sandy or sandy-skeletal |
| Leicester | 514 | 0.6 | 6.0 | 0.60 | 20.0 | C | 5 | Loose till, loamy textures | mesic | loamy | no | |
| Au Gres | 516 | | | | | B | 5 | Outwash and Stream Terraces | frigid | sandy | yes | single grain, loose |
| Machias | 520 | 2.0 | 6.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | frigid | sandy or sandy-skeletal | yes | strata sand/gravel in C |
| Stetson | 523 | 0.6 | 6.0 | 6.00 | 20.0 | B | 2 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | loamy over gravelly |
| Caesar | 526 | 20.0 | 100.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | mesic | coarse sand | no | |
| Scio | 531 | 0.6 | 2.0 | 0.60 | 2.0 | B | 3 | Terraces and glacial lake plains | mesic | silty | no | gravelly sand in 2C |
| Belgrade | 532 | 0.6 | 2.0 | 0.06 | 2.0 | B | 3 | Terraces and glacial lake plains | mesic | silty | no | strata of fine sand |
| Raynham | 533 | 0.2 | 2.0 | 0.06 | 0.2 | C | 5 | Terraces and glacial lake plains | mesic | silty | no | |
| Binghamville | 534 | 0.2 | 2.0 | 0.06 | 0.2 | D | 5 | Terraces and glacial lake plains | mesic | silty | no | |
| Suffield | 536 | 0.6 | 2.0 | 0.00 | 0.2 | C | 3 | Sandy/loamy over silt/clay | mesic | silty over clayey | no | deep to clay C |
| Squamscott | 538 | 6.0 | 20.0 | 0.06 | 0.6 | C | 5 | Sandy/loamy over silt/clay | mesic | sandy over loamy | yes | |
| Raypol | 540 | 0.6 | 2.0 | 6.00 | 100.0 | D | 5 | Outwash and Stream Terraces | mesic | co. loamy over sandy (skeletal) | no | |
| Walpole | 546 | 2.0 | 6.0 | 6.00 | 20.0 | C | 5 | Outwash and Stream Terraces | mesic | sandy | no | |
| Peacham | 549 | 0.6 | 2.0 | 0.00 | 0.2 | D | 6 | Firm, platy, silty till, schist & phylitte | frigid | loamy | no | organic over loam |
| Skerry | 558 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, sandy till | frigid | loamy | yes | loamy sand in Cd |
| Plaisted | 563 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | channery silt loam in Cd |
| Howland | 566 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | silt loam, platy in Cd |
| Monarda | 569 | 0.2 | 2.0 | 0.02 | 0.2 | D | 5 | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | |
| Bangor | 572 | 0.6 | 2.0 | 0.60 | 2.0 | B | 2 | Friable till, silty, schist & phyllite | frigid | loamy | yes | silt loam |

| Soil Series | legend number | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Group | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Dixmont | 578 | 0.6 | 2.0 | 0.60 | 2.0 | C | 3 | Friable till, silty, schist & phyllite | frigid | loamy | yes | silt loam, platy in C |
| Cabot | 589 | 0.6 | 2.0 | 0.06 | 0.2 | D | 5 | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | |
| Westbrook | 597 | | | 0.00 | 2.0 | D | 6 | Tidal Flat | mesic | loamy | no | organic over loam |
| Mundal | 610 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | yes | gravelly sandy loam in Cd |
| Croghan | 613 | 20.0 | 100.0 | 20.00 | 100.0 | B | 3 | Outwash and Stream Terraces | frigid | sandy | yes | single grain in C |
| Kinsman | 614 | 6.0 | 20.0 | 6.00 | 20.0 | C | 5 | Outwash and Stream Terraces | frigid | sandy | yes | |
| Salmon | 630 | 0.6 | 2.0 | 0.60 | 2.0 | B | 2 | Terraces and glacial lake plains | frigid | silty | yes | very fine sandy loam |
| Nicholville | 632 | 0.6 | 2.0 | 0.60 | 2.0 | C | 3 | Terraces and glacial lake plains | frigid | silty | yes | very fine sandy loam |
| Pemi | 633 | 0.6 | 2.0 | 0.06 | 0.6 | C | 5 | Terraces and glacial lake plains | frigid | silty | no | |
| Pillsbury | 646 | 0.6 | 2.0 | 0.06 | 0.2 | C | 5 | Firm, platy, loamy till | frigid | silty | no | |
| Ridgebury | 656 | 0.6 | 6.0 | 0.00 | 0.2 | C | 5 | Firm, platy, loamy till | mesic | loamy | no | |
| Canaan | 663 | 2.0 | 20.0 | 2.00 | 20.0 | C | 4 | Weathered Bedrock Till | frigid | loamy-skeletal | yes | less than 20 in. deep |
| Redstone | 665 | 2.0 | 6.0 | 6.00 | 20.0 | A | 1 | Weathered Bedrock Till | frigid | fragmental | yes | loamy cap |
| Sisk | 667 | 0.6 | 2.0 | 0.00 | 0.6 | C | 3 | Firm, platy, loamy till | cryic | loamy | yes | sandy loam in Cd |
| Surplus | 669 | 0.6 | 2.0 | 0.00 | 0.6 | C | 3 | Firm, platy, loamy till | cryic | loamy | yes | mwd, sandy loam in Cd |
| Glebe | 671 | 2.0 | 6.0 | 2.00 | 6.0 | C | 4 | Loose till, bedrock | cryic | loamy | yes | 20 to 40 in. deep |
| Saddleback | 673 | 0.6 | 2.0 | 0.60 | 2.0 | C/D | 4 | Loose till, bedrock | cryic | loamy | yes | less than 20 in. deep |
| Ricker | 674 | 2.0 | 6.0 | 2.00 | 6.0 | A | 4 | Organic over bedrock (up to 4" of mineral) | cryic | fibric to hemic | no | well drained, less than 20 in. deep |
| Houghtonville | 795 | 0.6 | 6.0 | 0.60 | 6.0 | B | 2 | Loose till, loamy textures | frigid | loamy | yes | cobbly fine sandy loam |
| Matunuck | 797 | | | 20.00 | 100.0 | D | 6 | Tidal Flat | mesic | sandy | no | organic over sand |
| Meadowsedge | 894 | | | | | D | 6 | Organic Materials - Freshwater | frigid | peat | no | deep organic |
| Bucksport | 895 | | | | | D | 6 | Organic Materials - Freshwater | frigid | sapric | no | deep organic |
| Colonel | 927 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | yes | loam in Cd |
| Pondicherry | 992 | | | 6.00 | 20.0 | D | 6 | Organic Materials - Freshwater | frigid | sandy or sandy-skeletal | no | organic over sand |
| Wonsqueak | 995 | | | 0.20 | 2.0 | D | 6 | Organic Materials - Freshwater | frigid | loamy | no | organic over loam |
| Glover | NA | 0.6 | 2.0 | 0.60 | 2 | D | 4 | Friable till, silty, schist & phyllite | frigid | loamy | no | less than 20 in. deep |

| | |
|---|---|
| (shaded) | no longer recognized |
| (stippled) | organic materials |

# TABLE B

# SOIL SERIES

| Soil Series | legend number | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Group | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Abenaki | 501 | 0.6 | 2.0 | 6.00 | 99.0 | B | 2 | Outwash and Stream Terraces | frigid | loamy over sandy-skeletal | no | loamy over gravelly |
| Acton | 146 | 2.0 | 20.0 | 2.00 | 20.0 | B | 3 | Loose till, sandy textures | mesic | sandy-skeletal | no | cobbly loamy sand |
| Adams | 36 | 6.0 | 20.0 | 20.00 | 99.0 | A | 1 | Outwash and Stream Terraces | frigid | sandy | yes | |
| Agawam | 24 | 6.0 | 20.0 | 20.00 | 100.0 | B | 2 | Outwash and Stream Terraces | mesic | loamy over sandy | no | loamy over sand/gravel |
| Allagash | 127 | 0.6 | 2.0 | 6.00 | 20.0 | B | 2 | Outwash and Stream Terraces | frigid | loamy over sandy | yes | loamy over sandy |
| Au Gres | 516 | | | | | B | 5 | Outwash and Stream Terraces | frigid | sandy | yes | single grain, loose |
| Bangor | 572 | 0.6 | 2.0 | 0.60 | 2.0 | B | 2 | Friable till, silty, schist & phyllite | frigid | loamy | yes | silt loam |
| Becket | 56 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, sandy till | frigid | loamy | yes | gravelly sandy loam in Cd |
| Belgrade | 532 | 0.6 | 2.0 | 0.06 | 2.0 | B | 3 | Terraces and glacial lake plains | mesic | silty | no | strata of fine sand |
| Bemis | 224 | 0.6 | 0.2 | 0.00 | 0.2 | C | 5 | Firm, platy, loamy till | cryic | loamy | no | |
| Berkshire | 72 | 0.6 | 6.0 | 0.60 | 6.0 | B | 2 | Loose till, loamy textures | frigid | loamy | yes | fine sandy loam |
| Bernardston | 330 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | mesic | loamy | no | channery silt loam in Cd |
| Bice | 226 | 0.6 | 6.0 | 0.60 | 6.0 | B | 2 | Loose till, loamy textures | frigid | loamy | no | sandy loam |
| Biddeford | 234 | 0.0 | 0.2 | 0.00 | 0.2 | D | 6 | Silt and Clay Deposits | frigid | fine | no | organic over clay |
| Binghamville | 534 | 0.2 | 2.0 | 0.06 | 0.2 | D | 5 | Terraces and glacial lake plains | mesic | silty | no | |
| Boscawen | 220 | 6.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | frigid | sandy-skeletal | no | loamy cap |
| Boxford | 32 | 0.1 | 0.2 | 0.00 | 0.2 | C | 3 | Silt and Clay Deposits | mesic | fine | no | silty clay loam |
| Brayton | 240 | 0.6 | 2.0 | 0.06 | 0.6 | C | 5 | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | |
| Buckland | 237 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, loamy till | frigid | loamy | no | loam in Cd |
| Bucksport | 895 | | | | | D | 6 | Organic Materials - Freshwater | frigid | sapric | no | deep organic |
| Burnham | 131 | 0.2 | 6.0 | 0.02 | 0.2 | D | 6 | Firm, platy, silty till, schist & phylite | frigid | loamy | no | organic over silt |
| Buxton | 232 | 0.1 | 0.6 | 0.00 | 0.2 | C | 3 | Silt and Clay Deposits | frigid | fine | no | silty clay |
| Cabot | 589 | 0.6 | 2.0 | 0.06 | 0.2 | D | 5 | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | |
| Caesar | 526 | 20.0 | 100.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | mesic | coarse sand | no | |
| Canaan | 663 | 2.0 | 20.0 | 2.00 | 20.0 | C | 4 | Weathered Bedrock Till | frigid | loamy-skeletal | yes | less than 20 in. deep |
| Canterbury | 166 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | no | loam in Cd |
| Canton | 42 | 2.0 | 6.0 | 6.00 | 20.0 | B | 2 | Loose till, sandy textures | mesic | loamy over sandy | no | loamy over loamy sand |
| Cardigan | 357 | 0.6 | 2.0 | 0.60 | 2.0 | B | 4 | Friable till, silty, schist & phyllite | mesic | loamy | no | 20 to 40 in. deep |
| Catden | 296 | | | | | A/D | 6 | Organic Materials - Freshwater | mesic | sapric | no | deep organic |
| Champlain | 35 | 6.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | frigid | gravelly sand | no | |
| Charles | 209 | 0.6 | 100.0 | 0.60 | 100.0 | C | 5 | Flood Plain (Bottom Land) | frigid | silty | no | |
| Charlton | 62 | 0.6 | 6.0 | 0.60 | 6.0 | B | 2 | Loose till, loamy textures | mesic | loamy | no | fine sandy loam |
| Chatfield | 89 | 0.6 | 6.0 | 0.60 | 6.0 | B | 4 | Loose till, bedrock | mesic | loamy | no | 20 to 40 in. deep |
| Chatfield Var. | 289 | 0.6 | 6.0 | 0.60 | 6.0 | B | 3 | Loose till, bedrock | mesic | loamy | no | mwd to swpd |
| Chesuncook | 126 | 0.6 | 2.0 | 0.02 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | channery silt loam in Cd |
| Chichester | 442 | 0.6 | 2.0 | 2.00 | 6.0 | B | | Loose till, sandy textures | frigid | loamy over sandy | no | loamy over loamy sand |
| Chocorua | 395 | | | 6.00 | 20.0 | D | 6 | Organic Materials - Freshwater | frigid | sandy or sandy-skeletal | no | organic over sand |
| Cohas | 505 | 0.6 | 2.0 | 0.60 | 100.0 | C | 5 | Flood Plain (Bottom Land) | frigid | co. loamy over sandy (skeletal) | no | |
| Colonel | 927 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | yes | loam in Cd |
| Colton | 22 | 6.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | |
| Colton, gravelly | 21 | 6.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | gravelly surface |
| Croghan | 613 | 20.0 | 100.0 | 20.00 | 100.0 | B | 3 | Outwash and Stream Terraces | frigid | sandy | yes | single grain in C |
| Dartmouth | 132 | 0.6 | 2.0 | 0.06 | 0.6 | B | 3 | Terraces and glacial lake plains | mesic | silty | no | thin strata silty clay loam |
| Deerfield | 313 | 6.0 | 20.0 | 20.00 | 100.0 | B | 3 | Outwash and Stream Terraces | mesic | sandy | no | single grain in C |
| Dixfield | 378 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | yes | fine sandy loam in Cd |
| Dixmont | 578 | 0.6 | 2.0 | 0.60 | 2.0 | C | 3 | Friable till, silty, schist & phyllite | frigid | loamy | yes | silt loam, platy in C |
| Duane | 413 | 6.0 | 20.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | cemented (ortstein) |
| Dutchess | 366 | 0.6 | 2.0 | 0.60 | 2.0 | B | 2 | Friable till, silty, schist & phyllite | mesic | loamy | no | very channery |
| Eldridge | 38 | 6.0 | 20.0 | 0.06 | 0.6 | C | 3 | Sandy/loamy over silt/clay | mesic | sandy over loamy | no | |
| Elliottsville | 128 | 0.6 | 2.0 | 0.60 | 2.0 | B | 4 | Friable till, silty, schist & phyllite | frigid | loamy | yes | 20 to 40 in. deep |
| Elmridge | 238 | 2.0 | 6.0 | 0.00 | 0.2 | C | 3 | Sandy/loamy over silt/clay | mesic | loamy over clayey | no | |
| Elmwood | 338 | 2.0 | 6.0 | 0.00 | 0.2 | C | 3 | Sandy/loamy over silt/clay | frigid | loamy over clayey | no | |
| Finch | 116 | | | | | C | 3 | Outwash and Stream Terraces | frigid | sandy | yes | cemented (ortstein) |

| Soil Series | legend number | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Group | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Fryeburg | 208 | 0.6 | 2.0 | 2.00 | 6.0 | B | 2 | Flood Plain (Bottom Land) | frigid | silty | no | very fine sandy loam |
| Gilmanton | 478 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | no | fine sandy loam in Cd |
| Glebe | 671 | 2.0 | 6.0 | 2.00 | 6.0 | C | 4 | Loose till, bedrock | cryic | loamy | yes | 20 to 40 in. deep |
| Gloucester | 11 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Sandy Till | mesic | sandy-skeletal | no | loamy cap |
| Glover | NA | 0.6 | 2.0 | 0.60 | 2 | D | 4 | Friable till, silty, schist & phyllite | frigid | loamy | no | less than 20 in. deep |
| Grange | 433 | 0.6 | 2.0 | 0.60 | 2.0 | C | 5 | Outwash and Stream Terraces | frigid | co. loamy over sandy (skeletal) | no | |
| Greenwood | 295 | | | | | A/D | 6 | Organic Materials - Freshwater | frigid | hemic | no | deep organic |
| Groveton | 27 | 0.6 | 2.0 | 0.60 | 6.0 | B | 2 | Outwash and Stream Terraces | frigid | loamy | yes | loamy over sandy |
| Hadley | 8 | 0.6 | 2.0 | 0.60 | 6.0 | B | 2 | Flood Plain (Bottom Land) | mesic | silty | no | strata of fine sand |
| Hadley | 108 | 0.6 | 2.0 | 0.60 | 6.0 | B | 2 | Flood Plain (Bottom Land) | mesic | silty | no | strata of fine sand, occ flooded |
| Hartland | 31 | 0.6 | 2.0 | 0.20 | 2.0 | B | 2 | Terraces and glacial lake plains | mesic | silty | no | very fine sandy loam |
| Haven | 410 | 0.6 | 2.0 | 20.00 | 100.0 | B | 2 | Outwash and Stream Terraces | mesic | loamy over sandy | no | loamy over sand/gravel |
| Henniker | 46 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, sandy till | frigid | loamy | no | loamy sand in Cd |
| Hermon | 55 | 2.0 | 20.0 | 6.00 | 20.0 | A | 1 | Sandy Till | frigid | sandy-skeletal | yes | loamy cap |
| Hinckley | 12 | 6.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | mesic | sandy-skeletal | no | |
| Hitchcock | 130 | 0.6 | 2.0 | 0.06 | 0.6 | B | 3 | Terraces and glacial lake plains | mesic | silty | no | silt loam to silt in C |
| Hogback | 91 | 2.0 | 6.0 | 2.00 | 6.0 | C | 4 | Loose till, bedrock | frigid | loamy | yes | less than 20 in. deep |
| Hollis | 86 | 0.6 | 6.0 | 0.60 | 6.0 | C/D | 4 | Loose till, bedrock | mesic | loamy | no | less than 20 in. deep |
| Hoosic | 510 | 2.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | mesic | sandy-skeletal | no | slate, loamy cap |
| Houghtonville | 795 | 0.6 | 6.0 | 0.60 | 6.0 | B | 2 | Loose till, loamy textures | frigid | loamy | yes | cobbly fine sandy loam |
| Howland | 566 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | silt loam, platy in Cd |
| Ipswich | 397 | | | | | D | 6 | Tidal Flat | mesic | hemic/sapric | no | deep organic |
| Kearsarge | 359 | 0.6 | 2.0 | 0.60 | 2.0 | B | 4 | Friable till, silty, schist & phyllite | mesic | loamy | no | less than 20 in. deep |
| Kinsman | 614 | 6.0 | 20.0 | 6.00 | 20.0 | C | 5 | Outwash and Stream Terraces | frigid | sandy | yes | |
| Lanesboro | 228 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | channery silt loam in Cd |
| Leicester | 514 | 0.6 | 6.0 | 0.60 | 20.0 | C | 5 | Loose till, loamy textures | mesic | loamy | no | |
| Lim | 3 | 0.6 | 2.0 | 6.00 | 20.0 | C | 5 | Flood Plain (Bottom Land) | mesic | loamy | no | |
| Limerick | 109 | 0.6 | 2.0 | 0.60 | 2.0 | C | 5 | Flood Plain (Bottom Land) | mesic | silty | no | |
| Lombard | 259 | 0.6 | 6.0 | 2.00 | 20.0 | C/D | 2 | Weathered bedrock, phyllite | frigid | loamy | no | very channery |
| Lovewell | 307 | 0.6 | 2.0 | 0.60 | 2.0 | B | 3 | Flood Plain (Bottom Land) | frigid | silty | no | very fine sandy loam |
| Lyman | 92 | 2.0 | 6.0 | 2.00 | 6.0 | A/D | 4 | Loose till, bedrock | frigid | loamy | yes | less than 20 in. deep |
| Lyme | 246 | 0.6 | 6.0 | 0.60 | 6.0 | C | 5 | Loose till, sandy textures | frigid | loamy | no | |
| Machias | 520 | 2.0 | 6.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | frigid | sandy or sandy-skeletal | yes | strata sand/gravel in C |
| Macomber | 252 | 0.6 | 2.0 | 0.60 | 2.0 | C | 4 | Friable till, silty, schist & phyllite | frigid | loamy-skeletal | yes | 20 to 40 in. deep |
| Madawaska | 28 | 0.6 | 2.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | frigid | loamy over sandy | yes | sandy or sandy-skeletal |
| ladawaska, aquer | 48 | 0.6 | 2.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | frigid | loamy over sandy | yes | sandy or sandy-skeletal |
| Marlow | 76 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | yes | fine sandy loam in Cd |
| Masardis | 23 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | slate, loamy cap |
| Mashpee | 315 | 6.0 | 20.0 | 6.00 | 20.0 | B | 5 | Outwash and Stream Terraces | mesic | sandy | yes | |
| Matunuck | 797 | | | 20.00 | 100.0 | D | 6 | Tidal Flat | mesic | sandy | no | organic over sand |
| Maybid | 134 | 0.0 | 0.2 | 0.00 | 0.2 | D | 6 | Silt and Clay Deposits | mesic | fine | no | silt over clay |
| Meadowsedge | 894 | | | | | D | 6 | Organic Materials - Freshwater | frigid | peat | no | deep organic |
| Medomak | 406 | 0.6 | 2.0 | 0.60 | 2.0 | D | 6 | Flood Plain (Bottom Land) | frigid | silty | no | organic over silt |
| Melrose | 37 | 2.0 | 6.0 | 0.00 | 0.2 | C | 3 | Sandy/loamy over silt/clay | frigid | loamy over clayey | no | silty clay loam in C |
| Merrimac | 10 | 2.0 | 20.0 | 6.00 | 20.0 | A | 1 | Outwash and Stream Terraces | mesic | gravelly sand | no | loamy cap |
| Metacomet | 458 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, sandy till | frigid | loamy | no | loamy sand in Cd |
| Metallak | 404 | 6.0 | 100.0 | 6.00 | 100.0 | B | 3 | Flood Plain (Bottom Land) | frigid | loamy over sandy | no | sandy or sandy-skeletal |
| Millis | 39 | | | | | C | 3 | Firm, platy, sandy till | frigid | loamy | yes | loamy sand in Cd |
| Millsite | 251 | 0.6 | 6.0 | 0.60 | 6.0 | C | 4 | Loose till, bedrock | frigid | loamy | no | 20 to 40 in. deep |
| Monadnock | 142 | 0.6 | 2.0 | 2.00 | 6.0 | B | 2 | Loose till, sandy textures | frigid | bamy over sandy, sandy-skeleta | yes | gravelly loamy sand in C |
| Monarda | 569 | 0.2 | 2.0 | 0.02 | 0.2 | D | 5 | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | |
| Monson | 133 | 0.6 | 2.0 | 0.60 | 2.0 | D | 4 | Friable till, silty, schist & phyllite | frigid | loamy | yes | less than 20 in. deep |
| Montauk | 44 | 0.6 | 6.0 | 0.06 | 0.6 | C | 3 | Firm, platy, sandy till | mesic | loamy | no | loamy sand in Cd |
| Moosilauke | 414 | 6.0 | 20.0 | 6.00 | 20.0 | C | 5 | Loose till, sandy textures | frigid | sandy | no | |

| Soil Series | legend number | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Group | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Mundal | 610 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | yes | gravelly sandy loam in Cd |
| Natchaug | 496 | | | 0.20 | 2.0 | D | 6 | Organic Materials - Freshwater | mesic | loamy | no | organic over loam |
| Naumburg | 214 | 6.0 | 20.0 | 6.00 | 20.0 | C | 5 | Outwash and Stream Terraces | frigid | sandy | yes | |
| Newfields | 444 | 0.6 | 2.0 | 0.60 | 2.0 | B | 3 | Loose till, sandy textures | mesic | loamy over sandy | no | sandy or sandy-skeletal |
| Nicholville | 632 | 0.6 | 2.0 | 0.60 | 2.0 | C | 3 | Terraces and glacial lake plains | frigid | silty | yes | very fine sandy loam |
| Ninigret | 513 | 0.6 | 6.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | mesic | loamy over sandy | no | sandy or sandy-skeletal |
| Occum | 1 | 0.6 | 2.0 | 6.00 | 20.0 | B | 2 | Flood Plain (Bottom Land) | mesic | loamy | no | loamy over loamy sand |
| Ondawa | 101 | 0.6 | 6.0 | 6.00 | 20.0 | B | 2 | Flood Plain (Bottom Land) | frigid | loamy | no | loamy over loamy sand |
| Ondawa | 201 | 0.6 | 6.0 | 6.00 | 20.0 | B | 2 | Flood Plain (Bottom Land) | frigid | loamy | no | occ flood, loamy over l. sand |
| Ossipee | 495 | | | 0.20 | 2.0 | D | 6 | Organic Materials - Freshwater | frigid | loamy | no | organic over loam |
| Pawcatuck | 497 | | | 20.00 | 100.0 | D | 6 | Tidal Flat | mesic | sandy or sandy-skeletal | no | organic over sand |
| Paxton | 66 | 0.6 | 2.0 | 0.00 | 0.2 | C | 3 | Firm, platy, loamy till | mesic | loamy | no | |
| Peacham | 549 | 0.6 | 2.0 | 0.00 | 0.2 | D | 6 | Firm, platy, silty till, schist & phylitte | frigid | loamy | no | organic over loam |
| Pemi | 633 | 0.6 | 2.0 | 0.06 | 0.6 | C | 5 | Terraces and glacial lake plains | frigid | silty | no | |
| Pennichuck | 460 | 0.6 | 2.0 | 0.60 | 2.0 | B | 4 | Friable till, silty, schist & phyllite | mesic | loamy-skeletal | no | 20 to 40 in. deep |
| Peru | 78 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, loamy till | frigid | loamy | yes | |
| Pillsbury | 646 | 0.6 | 2.0 | 0.06 | 0.2 | C | 5 | Firm, platy, loamy till | frigid | silty | no | |
| Pipestone | 314 | | | | | B | 5 | Outwash and Stream Terraces | mesic | sandy | yes | |
| Pittstown | 334 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | mesic | loamy | no | channery silt loam in Cd |
| Plaisted | 563 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | channery silt loam in Cd |
| Podunk | 104 | 0.6 | 6.0 | 6.00 | 20.0 | B | 3 | Flood Plain (Bottom Land) | frigid | loamy | no | loamy to coarse sand in C |
| Pondicherry | 992 | | | 6.00 | 20.0 | D | 6 | Organic Materials - Freshwater | frigid | sandy or sandy-skeletal | no | organic over sand |
| Poocham | 230 | 0.6 | 2.0 | 0.20 | 2.0 | B | 3 | Terraces and glacial lake plains | mesic | silty | no | silt loam in C |
| Pootatuck | 4 | 0.6 | 6.0 | 6.00 | 20.0 | B | 3 | Flood Plain (Bottom Land) | mesic | loamy | no | single grain in C |
| Quonset | 310 | 2.0 | 20.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | mesic | sandy-skeletal | no | shale |
| Rawsonville | 98 | 0.6 | 6.0 | 0.60 | 6.0 | C | 4 | Loose till, bedrock | frigid | loamy | yes | 20 to 40 in. deep |
| Raynham | 533 | 0.2 | 2.0 | 0.06 | 0.2 | C | 5 | Terraces and glacial lake plains | mesic | silty | no | |
| Raypol | 540 | 0.6 | 2.0 | 6.00 | 100.0 | D | 5 | Outwash and Stream Terraces | mesic | co. loamy over sandy (skeletal) | no | |
| Redstone | 665 | 2.0 | 6.0 | 6.00 | 20.0 | A | 1 | Weathered Bedrock Till | frigid | fragmental | yes | loamy cap |
| Ricker | 674 | 2.0 | 6.0 | 2.00 | 6.0 | A | 4 | rganic over bedrock (up to 4" of minera | cryic | fibric to hemic | no | well drained, less than 20 in. deep |
| Ridgebury | 656 | 0.6 | 6.0 | 0.00 | 0.2 | C | 5 | Firm, platy, loamy till | mesic | loamy | no | |
| Rippowam | 5 | 0.6 | 6.0 | 6.00 | 20.0 | C | 5 | Flood Plain (Bottom Land) | mesic | loamy | no | |
| Roundabout | 333 | 0.2 | 2.0 | 0.06 | 0.6 | C | 5 | Terraces and glacial lake plains | frigid | silty | no | silt loam in the C |
| Rumney | 105 | 0.6 | 6.0 | 6.00 | 20.0 | C | 5 | Flood Plain (Bottom Land) | frigid | loamy | no | |
| Saco | 6 | 0.6 | 2.0 | 6.00 | 20.0 | D | 6 | Flood Plain (Bottom Land) | mesic | silty | no | strata |
| Saddleback | 673 | 0.6 | 2.0 | 0.60 | 2.0 | C/D | 4 | Loose till, bedrock | cryic | loamy | yes | less than 20 in. deep |
| Salmon | 630 | 0.6 | 2.0 | 0.60 | 2.0 | B | 2 | Terraces and glacial lake plains | frigid | silty | yes | very fine sandy loam |
| Saugatuck | 16 | 0.06 | 0.2 | 6.00 | 20.0 | C | 5 | Outwash and Stream Terraces | mesic | sandy | yes | ortstein |
| Scantic | 233 | 0.0 | 0.2 | 0.00 | 0.2 | D | 5 | Silt and Clay Deposits | frigid | fine | no | |
| Scarboro | 115 | 6.0 | 20.0 | 6.00 | 20.0 | D | 6 | Outwash and Stream Terraces | mesic | sandy | no | organic over sand, non stony |
| Scio | 531 | 0.6 | 2.0 | 0.60 | 2.0 | B | 3 | Terraces and glacial lake plains | mesic | silty | no | gravelly sand in 2C |
| Scitico | 33 | 0.0 | 0.2 | 0.00 | 0.2 | C | 5 | Silt and Clay Deposits | mesic | fine | no | |
| Scituate | 448 | 0.6 | 2.0 | 0.06 | 0.2 | C | 3 | Firm, platy, sandy till | mesic | loamy | no | loamy sand in Cd |
| Searsport | 15 | 6.0 | 20.0 | 6.00 | 20.0 | D | 6 | Outwash and Stream Terraces | frigid | sandy | no | organic over sand |
| Shaker | 439 | 2.0 | 6.0 | 0.00 | 0.2 | C | 5 | Sandy/loamy over silt/clay | mesic | co. loamy over clayey | no | |
| Shapleigh | 136 | | | | | C/D | 4 | Sandy Till | mesic | sandy | yes | less than 20 in. deep |
| Sheepscot | 14 | 6.0 | 20.0 | 6.00 | 20.0 | B | 3 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | gravelly coarse sand |
| Sisk | 667 | 0.6 | 2.0 | 0.00 | 0.6 | C | 3 | Firm, platy, loamy till | cryic | loamy | yes | sandy loam in Cd |
| Skerry | 558 | 0.6 | 2.0 | 0.06 | 0.6 | C | 3 | Firm, platy, sandy till | frigid | loamy | yes | loamy sand in Cd |
| Squamscott | 538 | 6.0 | 20.0 | 0.06 | 0.6 | C | 5 | Sandy/loamy over silt/clay | mesic | sandy over loamy | yes | |
| Stetson | 523 | 0.6 | 6.0 | 6.00 | 20.0 | B | 2 | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | loamy over gravelly |
| Stissing | 340 | 0.6 | 2.0 | 0.06 | 0.2 | C | 5 | Firm, platy, silty till, schist & phyllite | mesic | loamy | no | |
| Success | 154 | 2.0 | 6.0 | 6.00 | 20.0 | A | 1 | Sandy Till | frigid | sandy-skeletal | yes | cemented |
| Sudbury | 118 | 2.0 | 6.0 | 2.00 | 20.0 | B | 3 | Outwash and Stream Terraces | mesic | sandy | no | loam over gravelly sand |

| Soil Series | legend number | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Group | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Suffield | 536 | 0.6 | 2.0 | 0.00 | 0.2 | C | 3 | Sandy/loamy over silt/clay | mesic | silty over clayey | no | deep to clay C |
| Sunapee | 168 | 0.6 | 2.0 | 0.60 | 6.0 | B | 3 | Loose till, loamy textures | frigid | loamy | yes | |
| Sunapee var | 269 | 0.6 | 2.0 | 0.60 | 6.0 | B | 3 | Loose till, loamy textures | frigid | loamy | yes | frigid dystrudept |
| Suncook | 2 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Flood Plain (Bottomland) | mesic | sandy | no | occasionally flooded |
| Suncook | 402 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Flood Plain (Bottomland) | mesic | sandy | no | frequent flooding |
| Sunday | 102 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Flood Plain (Bottomland) | frigid | sandy | no | occasionally flooded |
| Sunday | 202 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Flood Plain (Bottomland) | frigid | sandy | no | frequently flooded |
| Surplus | 669 | 0.6 | 2.0 | 0.00 | 0.6 | C | 3 | Firm, platy, loamy till | cryic | loamy | yes | mwd, sandy loam in Cd |
| Sutton | 68 | 0.6 | 6.0 | 0.60 | 6.0 | B | 3 | Loose till, loamy textures | mesic | loamy | no | |
| Swanton | 438 | 2.0 | 6.0 | 0.00 | 0.2 | C | 5 | Sandy/loamy over silt/clay | frigid | co. loamy over clayey | no | |
| Telos | 123 | 0.6 | 2.0 | 0.02 | 0.2 | C | 3 | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | channery silt loam in Cd |
| Thorndike | 84 | 0.6 | 2.0 | 0.60 | 2.0 | C/D | 4 | Friable till, silty, schist & phyllite | frigid | loamy-skeletal | yes | less than 20 in. deep |
| Timakwa | 393 | | | 6.00 | 100.0 | D | 6 | Organic Materials - Freshwater | mesic | sandy or sandy-skeletal | no | organic over sand |
| Tunbridge | 99 | 0.6 | 6.0 | 0.60 | 6.0 | C | 4 | Loose till, bedrock | frigid | loamy | yes | 20 to 40 in. deep |
| Unadilla | 30 | 0.6 | 2.0 | 2.00 | 20.0 | B | 2 | Terraces and glacial lake plains | mesic | silty | no | silty over gravelly |
| Vassalboro | 150 | | | | | D | 6 | Organic Materials - Freshwater | frigid | peat | no | deep organic |
| Walpole | 546 | 2.0 | 6.0 | 6.00 | 20.0 | C | 5 | Outwash and Stream Terraces | mesic | sandy | no | |
| Wareham | 34 | 6.0 | 20.0 | 6.00 | 20.0 | C | 5 | Outwash and Stream Terraces | mesic | sandy | no | |
| Warwick | 210 | 2.0 | 6.0 | 20.00 | 100.0 | A | 1 | Outwash and Stream Terraces | mesic | loamy-skeletal | no | loamy over slate gravel |
| Waskish | 195 | | | | | D | 6 | Organic Materials - Freshwater | frigid | peat | no | deep organic |
| Waumbeck | 58 | 2.0 | 20.0 | 6.00 | 20.0 | B | 3 | Loose till, sandy textures | frigid | sandy-skeletal | yes | very cobbly loamy sand |
| Westbrook | 597 | | | 0.00 | 2.0 | D | 6 | Tidal Flat | mesic | loamy | no | organic over loam |
| Whitman | 49 | 0.0 | 0.2 | 0.00 | 0.2 | D | 6 | Firm, platy, loamy till | mesic | loamy | no | mucky loam |
| Windsor | 26 | 6.0 | 20.0 | 6.00 | 20.0 | A | 1 | Outwash and Stream Terraces | mesic | sandy | no | |
| Winnecook | 88 | 0.6 | 2.0 | 0.60 | 2.0 | C | 4 | Friable till, silty, schist & phyllite | frigid | loamy-skeletal | yes | 20 to 40 in. deep |
| Winooski | 9 | 0.6 | 6.0 | 0.60 | 6.0 | B | | Flood Plain (Bottom Land) | mesic | silty over loamy | no | |
| Winooski | 103 | 0.6 | 6.0 | 0.60 | 6.0 | B | 3 | Flood Plain (Bottom Land) | mesic | silty | no | very fine sandy loam |
| Wonsqueak | 995 | | | 0.20 | 2.0 | D | 6 | Organic Materials - Freshwater | frigid | loamy | no | organic over loam |
| Woodbridge | 29 | 0.6 | 2.0 | 0.00 | 0.6 | C | 3 | Firm, platy, loamy till | mesic | loamy | no | sandy loam in Cd |
| Woodstock | 93 | 2.0 | 6.0 | 2.00 | 6.0 | C/D | 4 | Loose till, bedrock | frigid | loamy | no | less than 20 in. deep |

no longer recognized
organic materials

# TABLE C

# NHDES SOIL GROUPINGS

| Soil Series | number | NHDES Soil Group | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | | | | | |
| Adams | 36 | 1 | 6.0 | 20.0 | 20.00 | 99.0 | A | Outwash and Stream Terraces | frigid | sandy | yes | |
| Boscawen | 220 | 1 | 6.0 | 20.0 | 20.00 | 100.0 | A | Outwash and Stream Terraces | frigid | sandy-skeletal | no | loamy cap |
| Caesar | 526 | 1 | 20.0 | 100.0 | 20.00 | 100.0 | A | Outwash and Stream Terraces | mesic | coarse sand | no | |
| Champlain | 35 | 1 | 6.0 | 20.0 | 20.00 | 100.0 | A | Outwash and Stream Terraces | frigid | gravelly sand | no | |
| Colton | 22 | 1 | 6.0 | 20.0 | 20.00 | 100.0 | A | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | |
| Colton, gravelly | 21 | 1 | 6.0 | 20.0 | 20.00 | 100.0 | A | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | gravelly surface |
| Gloucester | 11 | 1 | 6.0 | 20.0 | 6.00 | 20.0 | A | Sandy Till | mesic | sandy-skeletal | no | loamy cap |
| Hermon | 55 | 1 | 2.0 | 20.0 | 6.00 | 20.0 | A | Sandy Till | frigid | sandy-skeletal | yes | loamy cap |
| Hinckley | 12 | 1 | 6.0 | 20.0 | 20.00 | 100.0 | A | Outwash and Stream Terraces | mesic | sandy-skeletal | no | |
| Hoosic | 510 | 1 | 2.0 | 20.0 | 20.00 | 100.0 | A | Outwash and Stream Terraces | mesic | sandy-skeletal | no | slate, loamy cap |
| Masardis | 23 | 1 | 6.0 | 20.0 | 6.00 | 20.0 | A | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | slate, loamy cap |
| Merrimac | 10 | 1 | 2.0 | 20.0 | 6.00 | 20.0 | A | Outwash and Stream Terraces | mesic | gravelly sand | no | loamy cap |
| Quonset | 310 | 1 | 2.0 | 20.0 | 20.00 | 100.0 | A | Outwash and Stream Terraces | mesic | sandy-skeletal | no | shale |
| Redstone | 665 | 1 | 2.0 | 6.0 | 6.00 | 20.0 | A | Weathered Bedrock Till | frigid | fragmental | yes | loamy cap |
| Success | 154 | 1 | 2.0 | 6.0 | 6.00 | 20.0 | A | Sandy Till | frigid | sandy-skeletal | yes | cemented |
| Suncook | 2 | 1 | 6.0 | 20.0 | 6.00 | 20.0 | A | Flood Plain (Bottomland) | mesic | sandy | no | occasionally flooded |
| Suncook | 402 | 1 | 6.0 | 20.0 | 6.00 | 20.0 | A | Flood Plain (Bottomland) | mesic | sandy | no | frequent flooding |
| Sunday | 102 | 1 | 6.0 | 20.0 | 6.00 | 20.0 | A | Flood Plain (Bottomland) | frigid | sandy | no | occasionally flooded |
| Sunday | 202 | 1 | 6.0 | 20.0 | 6.00 | 20.0 | A | Flood Plain (Bottomland) | frigid | sandy | no | frequently flooded |
| Warwick | 210 | 1 | 2.0 | 6.0 | 20.00 | 100.0 | A | Outwash and Stream Terraces | mesic | loamy-skeletal | no | loamy over slate gravel |
| Windsor | 26 | 1 | 6.0 | 20.0 | 6.00 | 20.0 | A | Outwash and Stream Terraces | mesic | sandy | no | |
| | | | | | | | | | | | | |
| Abenaki | 501 | 2 | 0.6 | 2.0 | 6.00 | 99.0 | B | Outwash and Stream Terraces | frigid | loamy over sandy-skeletal | no | loamy over gravelly |
| Agawam | 24 | 2 | 6.0 | 20.0 | 20.00 | 100.0 | B | Outwash and Stream Terraces | mesic | loamy over sandy | no | loamy over sand/gravel |
| Allagash | 127 | 2 | 0.6 | 2.0 | 6.00 | 20.0 | B | Outwash and Stream Terraces | frigid | loamy over sandy | yes | loamy over sandy |
| Bangor | 572 | 2 | 0.6 | 2.0 | 0.60 | 2.0 | B | Friable till, silty, schist & phyllite | frigid | loamy | yes | silt loam |
| Berkshire | 72 | 2 | 0.6 | 6.0 | 0.60 | 6.0 | B | Loose till, loamy textures | frigid | loamy | yes | fine sandy loam |
| Bice | 226 | 2 | 0.6 | 6.0 | 0.60 | 6.0 | B | Loose till, loamy textures | frigid | loamy | no | sandy loam |
| Canton | 42 | 2 | 2.0 | 6.0 | 6.00 | 20.0 | B | Loose till, sandy textures | mesic | loamy over sandy | no | loamy over loamy sand |
| Charlton | 62 | 2 | 0.6 | 6.0 | 0.60 | 6.0 | B | Loose till, loamy textures | mesic | loamy | no | fine sandy loam |
| Dutchess | 366 | 2 | 0.6 | 2.0 | 0.60 | 2.0 | B | Friable till, silty, schist & phyllite | mesic | loamy | no | very channery |
| Fryeburg | 208 | 2 | 0.6 | 2.0 | 2.00 | 6.0 | B | Flood Plain (Bottom Land) | frigid | silty | no | very fine sandy loam |
| Groveton | 27 | 2 | 0.6 | 2.0 | 0.60 | 6.0 | B | Outwash and Stream Terraces | frigid | loamy | yes | loamy over sandy |
| Hadley | 8 | 2 | 0.6 | 2.0 | 0.60 | 6.0 | B | Flood Plain (Bottom Land) | mesic | silty | no | strata of fine sand |
| Hadley | 108 | 2 | 0.6 | 2.0 | 0.60 | 6.0 | B | Flood Plain (Bottom Land) | mesic | silty | no | strata of fine sand, occ flooded |
| Hartland | 31 | 2 | 0.6 | 2.0 | 0.20 | 2.0 | B | Terraces and glacial lake plains | mesic | silty | no | very fine sandy loam |
| Haven | 410 | 2 | 0.6 | 2.0 | 20.00 | 100.0 | B | Outwash and Stream Terraces | mesic | loamy over sandy | no | loamy over sand/gravel |
| Houghtonville | 795 | 2 | 0.6 | 6.0 | 0.60 | 6.0 | B | Loose till, loamy textures | frigid | loamy | yes | cobbly fine sandy loam |
| Lombard | 259 | 2 | 0.6 | 6.0 | 2.00 | 20.0 | C/D | Weathered bedrock, phyllite | frigid | loamy | no | very channery |
| Monadnock | 142 | 2 | 0.6 | 2.0 | 2.00 | 6.0 | B | Loose till, sandy textures | frigid | oamy over sandy, sandy-skeleta | yes | gravelly loamy sand in C |
| Occum | 1 | 2 | 0.6 | 2.0 | 6.00 | 20.0 | B | Flood Plain (Bottom Land) | mesic | loamy | no | loamy over loamy sand |
| Ondawa | 101 | 2 | 0.6 | 6.0 | 6.00 | 20.0 | B | Flood Plain (Bottom Land) | frigid | loamy | no | loamy over loamy sand |
| Ondawa | 201 | 2 | 0.6 | 6.0 | 6.00 | 20.0 | B | Flood Plain (Bottom Land) | frigid | loamy | no | occ flood, loamy over l. sand |
| Salmon | 630 | 2 | 0.6 | 2.0 | 0.60 | 2.0 | B | Terraces and glacial lake plains | frigid | silty | yes | very fine sandy loam |
| Stetson | 523 | 2 | 0.6 | 6.0 | 6.00 | 20.0 | B | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | loamy over gravelly |
| Unadilla | 30 | 2 | 0.6 | 2.0 | 2.00 | 20.0 | B | Terraces and glacial lake plains | mesic | silty | no | silty over gravelly |
| Chichester | 442 | 2 | 0.6 | 2.0 | 2.00 | 6.0 | B | Loose till, sandy textures | frigid | loamy over sandy | no | loamy over loamy sand |
| | | | | | | | | | | | | |
| Acton | 146 | 3 | 2.0 | 20.0 | 2.00 | 20.0 | B | Loose till, sandy textures | mesic | sandy-skeletal | no | cobbly loamy sand |
| Becket | 56 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, sandy till | frigid | loamy | yes | gravelly sandy loam in Cd |
| Belgrade | 532 | 3 | 0.6 | 2.0 | 0.06 | 2.0 | B | Terraces and glacial lake plains | mesic | silty | no | strata of fine sand |
| Bernardston | 330 | 3 | 0.6 | 2.0 | 0.06 | 0.2 | C | Firm, platy, silty till, schist & phyllite | mesic | loamy | no | channery silt loam in Cd |
| Boxford | 32 | 3 | 0.1 | 0.2 | 0.00 | 0.2 | C | Silt and Clay Deposits | mesic | fine | no | silty clay loam |

| Soil Series | number | NHDES Soil Group | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Buckland | 237 | 3 | 0.6 | 2.0 | 0.06 | 0.2 | C | Firm, platy, loamy till | frigid | loamy | no | loam in Cd |
| Buxton | 232 | 3 | 0.1 | 0.6 | 0.00 | 0.2 | C | Silt and Clay Deposits | frigid | fine | no | silty clay |
| Canterbury | 166 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, loamy till | frigid | loamy | no | loam in Cd |
| Chatfield Var. | 289 | 3 | 0.6 | 6.0 | 0.60 | 6.0 | B | Loose till, bedrock | mesic | loamy | no | mwd to swpd |
| Chesuncook | 126 | 3 | 0.6 | 2.0 | 0.02 | 0.2 | C | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | channery silt loam in Cd |
| Colonel | 927 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, loamy till | frigid | loamy | yes | loam in Cd |
| Croghan | 613 | 3 | 20.0 | 100.0 | 20.00 | 100.0 | B | Outwash and Stream Terraces | frigid | sandy | yes | single grain in C |
| Dartmouth | 132 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | B | Terraces and glacial lake plains | mesic | silty | no | thin strata silty clay loam |
| Deerfield | 313 | 3 | 6.0 | 20.0 | 20.00 | 100.0 | B | Outwash and Stream Terraces | mesic | sandy | no | single grain in C |
| Dixfield | 378 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, loamy till | frigid | loamy | yes | fine sandy loam in Cd |
| Dixmont | 578 | 3 | 0.6 | 2.0 | 0.60 | 2.0 | C | Friable till, silty, schist & phyllite | frigid | loamy | yes | silt loam, platy in C |
| Duane | 413 | 3 | 6.0 | 20.0 | 6.00 | 20.0 | B | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | cemented (ortstein) |
| Eldridge | 38 | 3 | 6.0 | 20.0 | 0.06 | 0.6 | C | Sandy/loamy over silt/clay | mesic | sandy over loamy | no | |
| Elmridge | 238 | 3 | 2.0 | 6.0 | 0.00 | 0.2 | C | Sandy/loamy over silt/clay | mesic | loamy over clayey | no | |
| Elmwood | 338 | 3 | 2.0 | 6.0 | 0.00 | 0.2 | C | Sandy/loamy over silt/clay | frigid | loamy over clayey | no | |
| Finch | 116 | 3 | | | | | C | Outwash and Stream Terraces | frigid | sandy | yes | cemented (ortstein) |
| Gilmanton | 478 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, loamy till | frigid | loamy | no | fine sandy loam in Cd |
| Henniker | 46 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, sandy till | frigid | loamy | no | loamy sand in Cd |
| Hitchcock | 130 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | B | Terraces and glacial lake plains | mesic | silty | no | silt loam to silt in C |
| Howland | 566 | 3 | 0.6 | 2.0 | 0.06 | 0.2 | C | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | silt loam, platy in Cd |
| Lanesboro | 228 | 3 | 0.6 | 2.0 | 0.06 | 0.2 | C | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | channery silt loam in Cd |
| Lovewell | 307 | 3 | 0.6 | 2.0 | 0.60 | 2.0 | B | Flood Plain (Bottom Land) | frigid | silty | no | very fine sandy loam |
| Machias | 520 | 3 | 2.0 | 6.0 | 6.00 | 20.0 | B | Outwash and Stream Terraces | frigid | sandy or sandy-skeletal | yes | strata sand/gravel in C |
| Madawaska | 28 | 3 | 0.6 | 2.0 | 6.00 | 20.0 | B | Outwash and Stream Terraces | frigid | loamy over sandy | yes | sandy or sandy-skeletal |
| ladawaska, aquer | 48 | 3 | 0.6 | 2.0 | 6.00 | 20.0 | B | Outwash and Stream Terraces | frigid | loamy over sandy | yes | sandy or sandy-skeletal |
| Marlow | 76 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, loamy till | frigid | loamy | yes | fine sandy loam in Cd |
| Melrose | 37 | 3 | 2.0 | 6.0 | 0.00 | 0.2 | C | Sandy/loamy over silt/clay | frigid | loamy over clayey | no | silty clay loam in C |
| Metacomet | 458 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, sandy till | frigid | loamy | no | loamy sand in Cd |
| Metallak | 404 | 3 | 6.0 | 100.0 | 6.00 | 100.0 | B | Flood Plain (Bottom Land) | frigid | loamy over sandy | no | sandy or sandy-skeletal |
| Millis | 39 | 3 | | | | | C | Firm, platy, sandy till | frigid | loamy | yes | loamy sand in Cd |
| Montauk | 44 | 3 | 0.6 | 6.0 | 0.06 | 0.6 | C | Firm, platy, sandy till | mesic | loamy | no | loamy sand in Cd |
| Mundal | 610 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, loamy till | frigid | loamy | yes | gravelly sandy loam in Cd |
| Newfields | 444 | 3 | 0.6 | 2.0 | 0.60 | 2.0 | B | Loose till, sandy textures | mesic | loamy over sandy | no | sandy or sandy-skeletal |
| Nicholville | 632 | 3 | 0.6 | 2.0 | 0.60 | 2.0 | C | Terraces and glacial lake plains | frigid | silty | yes | very fine sandy loam |
| Ninigret | 513 | 3 | 0.6 | 6.0 | 6.00 | 20.0 | B | Outwash and Stream Terraces | mesic | loamy over sandy | no | sandy or sandy-skeletal |
| Paxton | 66 | 3 | 0.6 | 2.0 | 0.00 | 0.2 | C | Firm, platy, loamy till | mesic | loamy | no | |
| Peru | 78 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, loamy till | frigid | loamy | yes | |
| Pittstown | 334 | 3 | 0.6 | 2.0 | 0.06 | 0.2 | C | Firm, platy, silty till, schist & phyllite | mesic | loamy | no | channery silt loam in Cd |
| Plaisted | 563 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | channery silt loam in Cd |
| Podunk | 104 | 3 | 0.6 | 6.0 | 6.00 | 20.0 | B | Flood Plain (Bottom Land) | frigid | loamy | no | loamy to coarse sand in C |
| Poocham | 230 | 3 | 0.6 | 2.0 | 0.20 | 2.0 | B | Terraces and glacial lake plains | mesic | silty | no | silt loam in C |
| Pootatuck | 4 | 3 | 0.6 | 6.0 | 6.00 | 20.0 | B | Flood Plain (Bottom Land) | mesic | loamy | no | single grain in C |
| Scio | 531 | 3 | 0.6 | 2.0 | 0.60 | 2.0 | B | Terraces and glacial lake plains | mesic | silty | no | gravelly sand in 2C |
| Scituate | 448 | 3 | 0.6 | 2.0 | 0.06 | 0.2 | C | Firm, platy, sandy till | mesic | loamy | no | loamy sand in Cd |
| Sheepscot | 14 | 3 | 6.0 | 20.0 | 6.00 | 20.0 | B | Outwash and Stream Terraces | frigid | sandy-skeletal | yes | gravelly coarse sand |
| Sisk | 667 | 3 | 0.6 | 2.0 | 0.00 | 0.6 | C | Firm, platy, loamy till | cryic | loamy | yes | sandy loam in Cd |
| Skerry | 558 | 3 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, sandy till | frigid | loamy | yes | loamy sand in Cd |
| Sudbury | 118 | 3 | 2.0 | 6.0 | 2.00 | 20.0 | B | Outwash and Stream Terraces | mesic | sandy | no | loam over gravelly sand |
| Suffield | 536 | 3 | 0.6 | 2.0 | 0.00 | 0.2 | C | Sandy/loamy over silt/clay | mesic | silty over clayey | no | deep to clay C |
| Sunapee | 168 | 3 | 0.6 | 2.0 | 0.60 | 6.0 | B | Loose till, loamy textures | frigid | loamy | yes | |
| Sunapee var | 269 | 3 | 0.6 | 2.0 | 0.60 | 6.0 | B | Loose till, loamy textures | frigid | loamy | yes | frigid dystrudept |
| Surplus | 669 | 3 | 0.6 | 2.0 | 0.00 | 0.6 | C | Firm, platy, loamy till | cryic | loamy | yes | mwd, sandy loam in Cd |
| Sutton | 68 | 3 | 0.6 | 6.0 | 0.60 | 6.0 | B | Loose till, loamy textures | mesic | loamy | no | |
| Telos | 123 | 3 | 0.6 | 2.0 | 0.02 | 0.2 | C | Firm, platy, silty till, schist & phyllite | frigid | loamy | yes | channery silt loam in Cd |

| Soil Series | number | NHDES Soil Group | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Waumbeck | 58 | 3 | 2.0 | 20.0 | 6.00 | 20.0 | B | Loose till, sandy textures | frigid | sandy-skeletal | yes | very cobbly loamy sand |
| Winooski | 103 | 3 | 0.6 | 6.0 | 0.60 | 6.0 | B | Flood Plain (Bottom Land) | mesic | silty | no | very fine sandy loam |
| Woodbridge | 29 | 3 | 0.6 | 2.0 | 0.00 | 0.6 | C | Firm, platy, loamy till | mesic | loamy | no | sandy loam in Cd |
| Winooski | 9 | 3 | 0.6 | 6.0 | 0.60 | 6.0 | B | Flood Plain (Bottom Land) | mesic | silty over loamy | no | |
| | | | | | | | | | | | | |
| Canaan | 663 | 4 | 2.0 | 20.0 | 2.00 | 20.0 | C | Weathered Bedrock Till | frigid | loamy-skeletal | yes | less than 20 in. deep |
| Cardigan | 357 | 4 | 0.6 | 2.0 | 0.60 | 2.0 | B | Friable till, silty, schist & phyllite | mesic | loamy | no | 20 to 40 in. deep |
| Chatfield | 89 | 4 | 0.6 | 6.0 | 0.60 | 6.0 | B | Loose till, bedrock | mesic | loamy | no | 20 to 40 in. deep |
| Elliottsville | 128 | 4 | 0.6 | 2.0 | 0.60 | 2.0 | B | Friable till, silty, schist & phyllite | frigid | loamy | yes | 20 to 40 in. deep |
| Glebe | 671 | 4 | 2.0 | 6.0 | 2.00 | 6.0 | C | Loose till, bedrock | cryic | loamy | yes | 20 to 40 in. deep |
| Glover | NA | 4 | 0.6 | 2.0 | 0.60 | 2 | D | Friable till, silty, schist & phyllite | frigid | loamy | no | less than 20 in. deep |
| Hogback | 91 | 4 | 2.0 | 6.0 | 2.00 | 6.0 | C | Loose till, bedrock | frigid | loamy | yes | less than 20 in. deep |
| Hollis | 86 | 4 | 0.6 | 6.0 | 0.60 | 6.0 | C/D | Loose till, bedrock | mesic | loamy | no | less than 20 in. deep |
| Kearsarge | 359 | 4 | 0.6 | 2.0 | 0.60 | 2.0 | B | Friable till, silty, schist & phyllite | mesic | loamy | no | less than 20 in. deep |
| Lyman | 92 | 4 | 2.0 | 6.0 | 2.00 | 6.0 | A/D | Loose till, bedrock | frigid | loamy | yes | less than 20 in. deep |
| Macomber | 252 | 4 | 0.6 | 2.0 | 0.60 | 2.0 | C | Friable till, silty, schist & phyllite | frigid | loamy-skeletal | yes | 20 to 40 in. deep |
| Millsite | 251 | 4 | 0.6 | 6.0 | 0.60 | 6.0 | C | Loose till, bedrock | frigid | loamy | no | 20 to 40 in. deep |
| Monson | 133 | 4 | 0.6 | 2.0 | 0.60 | 2.0 | D | Friable till, silty, schist & phyllite | frigid | loamy | yes | less than 20 in. deep |
| Pennichuck | 460 | 4 | 0.6 | 2.0 | 0.60 | 2.0 | B | Friable till, silty, schist & phyllite | mesic | loamy-skeletal | no | 20 to 40 in. deep |
| Rawsonville | 98 | 4 | 0.6 | 6.0 | 0.60 | 6.0 | C | Loose till, bedrock | frigid | loamy | yes | 20 to 40 in. deep |
| Ricker | 674 | 4 | 2.0 | 6.0 | 2.00 | 6.0 | A | rganic over bedrock (up to 4" of minera | cryic | fibric to hemic | no | well drained, less than 20 in. deep |
| Saddleback | 673 | 4 | 0.6 | 2.0 | 0.60 | 2.0 | C/D | Loose till, bedrock | cryic | loamy | yes | less than 20 in. deep |
| Shapleigh | 136 | 4 | | | | | C/D | Sandy Till | mesic | sandy | yes | less than 20 in. deep |
| Thorndike | 84 | 4 | 0.6 | 2.0 | 0.60 | 2.0 | C/D | Friable till, silty, schist & phyllite | frigid | loamy-skeletal | yes | less than 20 in. deep |
| Tunbridge | 99 | 4 | 0.6 | 6.0 | 0.60 | 6.0 | C | Loose till, bedrock | frigid | loamy | yes | 20 to 40 in. deep |
| Winnecook | 88 | 4 | 0.6 | 2.0 | 0.60 | 2.0 | C | Friable till, silty, schist & phyllite | frigid | loamy-skeletal | yes | 20 to 40 in. deep |
| Woodstock | 93 | 4 | 2.0 | 6.0 | 2.00 | 6.0 | C/D | Loose till, bedrock | frigid | loamy | no | less than 20 in. deep |
| | | | | | | | | | | | | |
| Au Gres | 516 | 5 | | | | | B | Outwash and Stream Terraces | frigid | sandy | yes | single grain, loose |
| Bemis | 224 | 5 | 0.6 | 0.2 | 0.00 | 0.2 | C | Firm, platy, loamy till | cryic | loamy | no | |
| Binghamville | 534 | 5 | 0.2 | 2.0 | 0.06 | 0.2 | D | Terraces and glacial lake plains | mesic | silty | no | |
| Brayton | 240 | 5 | 0.6 | 2.0 | 0.06 | 0.6 | C | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | |
| Cabot | 589 | 5 | 0.6 | 2.0 | 0.06 | 0.2 | D | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | |
| Charles | 209 | 5 | 0.6 | 100.0 | 0.60 | 100.0 | C | Flood Plain (Bottom Land) | frigid | silty | no | |
| Cohas | 505 | 5 | 0.6 | 2.0 | 0.60 | 100.0 | C | Flood Plain (Bottom Land) | frigid | co. loamy over sandy (skeletal) | no | |
| Grange | 433 | 5 | 0.6 | 2.0 | 0.60 | 2.0 | C | Outwash and Stream Terraces | frigid | co. loamy over sandy (skeletal) | no | |
| Kinsman | 614 | 5 | 6.0 | 20.0 | 6.00 | 20.0 | C | Outwash and Stream Terraces | frigid | sandy | yes | |
| Leicester | 514 | 5 | 0.6 | 6.0 | 0.60 | 20.0 | C | Loose till, loamy textures | mesic | loamy | no | |
| Lim | 3 | 5 | 0.6 | 2.0 | 6.00 | 20.0 | C | Flood Plain (Bottom Land) | mesic | loamy | no | |
| Limerick | 109 | 5 | 0.6 | 2.0 | 0.60 | 2.0 | C | Flood Plain (Bottom Land) | mesic | silty | no | |
| Lyme | 246 | 5 | 0.6 | 6.0 | 0.60 | 6.0 | C | Loose till, sandy textures | frigid | loamy | no | |
| Mashpee | 315 | 5 | 6.0 | 20.0 | 6.00 | 20.0 | B | Outwash and Stream Terraces | mesic | sandy | yes | |
| Monarda | 569 | 5 | 0.2 | 2.0 | 0.02 | 0.2 | D | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | |
| Moosilauke | 414 | 5 | 6.0 | 20.0 | 6.00 | 20.0 | C | Loose till, sandy textures | frigid | sandy | no | |
| Naumburg | 214 | 5 | 6.0 | 20.0 | 6.00 | 20.0 | C | Outwash and Stream Terraces | frigid | sandy | yes | |
| Pemi | 633 | 5 | 0.6 | 2.0 | 0.06 | 0.6 | C | Terraces and glacial lake plains | frigid | silty | no | |
| Pillsbury | 646 | 5 | 0.6 | 2.0 | 0.06 | 0.2 | C | Firm, platy, loamy till | frigid | silty | no | |
| Pipestone | 314 | 5 | | | | | B | Outwash and Stream Terraces | mesic | sandy | yes | |
| Raynham | 533 | 5 | 0.2 | 2.0 | 0.06 | 0.2 | C | Terraces and glacial lake plains | mesic | silty | no | |
| Raypol | 540 | 5 | 0.6 | 2.0 | 6.00 | 100.0 | D | Outwash and Stream Terraces | mesic | co. loamy over sandy (skeletal) | no | |
| Ridgebury | 656 | 5 | 0.6 | 6.0 | 0.00 | 0.2 | C | Firm, platy, loamy till | mesic | loamy | no | |
| Rippowam | 5 | 5 | 0.6 | 6.0 | 6.00 | 20.0 | C | Flood Plain (Bottom Land) | mesic | loamy | no | |
| Roundabout | 333 | 5 | 0.2 | 2.0 | 0.06 | 0.6 | C | Terraces and glacial lake plains | frigid | silty | no | silt loam in the C |
| Rumney | 105 | 5 | 0.6 | 6.0 | 6.00 | 20.0 | C | Flood Plain (Bottom Land) | frigid | loamy | no | |

| Soil Series | number | NHDES Soil Group | Ksat low - B in/hr | Ksat high - B in/hr | Ksat low - C in/hr | Ksat high - C in/hr | Hyd. Grp. | Land Form | Temp. | Soil Textures | Spodosol ? | Other |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Saugatuck | 16 | 5 | 0.06 | 0.2 | 6.00 | 20.0 | C | Outwash and Stream Terraces | mesic | sandy | yes | ortstein |
| Scantic | 233 | 5 | 0.0 | 0.2 | 0.00 | 0.2 | D | Silt and Clay Deposits | frigid | fine | no | |
| Scitico | 33 | 5 | 0.0 | 0.2 | 0.00 | 0.2 | C | Silt and Clay Deposits | mesic | fine | no | |
| Shaker | 439 | 5 | 2.0 | 6.0 | 0.00 | 0.2 | C | Sandy/loamy over silt/clay | mesic | co. loamy over clayey | no | |
| Squamscott | 538 | 5 | 6.0 | 20.0 | 0.06 | 0.6 | C | Sandy/loamy over silt/clay | mesic | sandy over loamy | yes | |
| Stissing | 340 | 5 | 0.6 | 2.0 | 0.06 | 0.2 | C | Firm, platy, silty till, schist & phyllite | mesic | loamy | no | |
| Swanton | 438 | 5 | 2.0 | 6.0 | 0.00 | 0.2 | C | Sandy/loamy over silt/clay | frigid | co. loamy over clayey | no | |
| Walpole | 546 | 5 | 2.0 | 6.0 | 6.00 | 20.0 | C | Outwash and Stream Terraces | mesic | sandy | no | |
| Wareham | 34 | 5 | 6.0 | 20.0 | 6.00 | 20.0 | C | Outwash and Stream Terraces | mesic | sandy | no | |
| | | | | | | | | | | | | |
| Biddeford | 234 | 6 | 0.0 | 0.2 | 0.00 | 0.2 | D | Silt and Clay Deposits | frigid | fine | no | organic over clay |
| Bucksport | 895 | 6 | | | | | D | Organic Materials - Freshwater | frigid | sapric | no | deep organic |
| Burnham | 131 | 6 | 0.2 | 6.0 | 0.02 | 0.2 | D | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | organic over silt |
| Catden | 296 | 6 | | | | | A/D | Organic Materials - Freshwater | mesic | sapric | no | deep organic |
| Chocorua | 395 | 6 | | | 6.00 | 20.0 | D | Organic Materials - Freshwater | frigid | sandy or sandy-skeletal | no | organic over sand |
| Greenwood | 295 | 6 | | | | | A/D | Organic Materials - Freshwater | frigid | hemic | no | deep organic |
| Ipswich | 397 | 6 | | | | | D | Tidal Flat | mesic | hemic/sapric | no | deep organic |
| Matunuck | 797 | 6 | | | 20.00 | 100.0 | D | Tidal Flat | mesic | sandy | no | organic over sand |
| Maybid | 134 | 6 | 0.0 | 0.2 | 0.00 | 0.2 | D | Silt and Clay Deposits | mesic | fine | no | silt over clay |
| Meadowsedge | 894 | 6 | | | | | D | Organic Materials - Freshwater | frigid | peat | no | deep organic |
| Medomak | 406 | 6 | 0.6 | 2.0 | 0.60 | 2.0 | D | Flood Plain (Bottom Land) | frigid | silty | no | organic over silt |
| Natchaug | 496 | 6 | | | 0.20 | 2.0 | D | Organic Materials - Freshwater | mesic | loamy | no | organic over loam |
| Ossipee | 495 | 6 | | | 0.20 | 2.0 | D | Organic Materials - Freshwater | frigid | loamy | no | organic over loam |
| Pawcatuck | 497 | 6 | | | 20.00 | 100.0 | D | Tidal Flat | mesic | sandy or sandy-skeletal | no | organic over sand |
| Peacham | 549 | 6 | 0.6 | 2.0 | 0.00 | 0.2 | D | Firm, platy, silty till, schist & phyllite | frigid | loamy | no | organic over loam |
| Pondicherry | 992 | 6 | | | 6.00 | 20.0 | D | Organic Materials - Freshwater | frigid | sandy or sandy-skeletal | no | organic over sand |
| Saco | 6 | 6 | 0.6 | 2.0 | 6.00 | 20.0 | D | Flood Plain (Bottom Land) | mesic | silty | no | strata |
| Scarboro | 115 | 6 | 6.0 | 20.0 | 6.00 | 20.0 | D | Outwash and Stream Terraces | mesic | sandy | no | organic over sand, non stony |
| Searsport | 15 | 6 | 6.0 | 20.0 | 6.00 | 20.0 | D | Outwash and Stream Terraces | frigid | sandy | no | organic over sand |
| Timakwa | 393 | 6 | | | 6.00 | 100.0 | D | Organic Materials - Freshwater | mesic | sandy or sandy-skeletal | no | organic over sand |
| Vassalboro | 150 | 6 | | | | | D | Organic Materials - Freshwater | frigid | peat | no | deep organic |
| Waskish | 195 | 6 | | | | | D | Organic Materials - Freshwater | frigid | peat | no | deep organic |
| Westbrook | 597 | 6 | | | 0.00 | 2.0 | D | Tidal Flat | mesic | loamy | no | organic over loam |
| Whitman | 49 | 6 | 0.0 | 0.2 | 0.00 | 0.2 | D | Firm, platy, loamy till | mesic | loamy | no | mucky loam |
| Wonsqueak | 995 | 6 | | | 0.20 | 2.0 | D | Organic Materials - Freshwater | frigid | loamy | no | organic over loam |
| | | | | | | | | | | | | |

no longer recognized — organic materials — denotes break betweenSoil Group

# ORDER FORM

## Ksat VALUES
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## NEW HAMPSHIRE SOILS
**(Including Hydrologic and Soil Lot Sizing Groups)**

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Quantity of Publications_____ @ $8.00 = Total Order: $_________

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Enclose check or money order for the full amount payable to:

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**PO Box 76**
**Durham, NH 03824**

Please allow 4 weeks for delivery.

# SWPPP Cut Sheet:

# Filtrexx® Sediment Control

*Sediment & Perimeter Control Technology*

## PURPOSE & DESCRIPTION

Filtrexx® Sediment control is a three-dimensional tubular sediment control and storm water runoff filtration device typically used for **perimeter control** of sediment and other soluble pollutants (such as phosphorus and petroleum hydrocarbons), on and around construction activities.

## APPLICATION

Filtrexx® Sediment control is to be installed down slope of any disturbed area requiring erosion and sediment control and filtration of soluble pollutants from runoff. Sediment control is effective when installed perpendicular to sheet or low concentrated flow. Acceptable applications include:

- Site perimeters
- Above and below disturbed areas subject to sheet runoff, interrill and rill erosion
- Above and below exposed and erodable slopes
- Around area drains or inlets located in a 'sump'
- On compacted soils where trenching of silt fence is difficult or impossible
- Around sensitive trees where trenching of silt fence is not beneficial for tree survival or may unnecessarily disturb established vegetation.
- On frozen ground where trenching of silt fence is impossible.
- On paved surfaces where trenching of silt fence is impossible.

## INSTALLATION

1. Sediment control used for perimeter control of sediment and soluble pollutants in storm runoff shall meet Filtrexx® Soxx™ Material Specifications and use Certified Filtrexx® FilterMedia™.
2. Contractor is required to be Filtrexx® Certified™, or use pre-filled Filtrexx® Sediment control products manufactured by a Filtrexx® Certified Manufacturer™ as determined by Filtrexx® International, LLC (440-926-2607 or visit www.filtrexx.com). Certification shall be considered current if appropriate identification is shown during time of bid or at time of application. Look for the Filtrexx® Certified™ Seal.
3. Sediment control will be placed at locations indicated on plans as directed by the Engineer.
4. Sediment control should be installed parallel to the base of the slope or other disturbed area. In extreme conditions (i.e., 2:1 slopes), a second Sediment control shall be constructed at the top of the slope.
5. Effective Soxx™ height in the field should be as follows: 8" Diameter Sediment control = 6.5" high, 12" Diameter Sediment control = 9.5" high, 18" Diameter SiltSoxx™ = 14.5" high, 24" Diameter Sediment control = 19" high.
6. Stakes shall be installed through the middle of the Sediment control on 10 ft (3m) centers, using 2 in (50mm) by 2 in (50mm) by 3 ft (1m) hard wood stakes. In the event staking is not possible, i.e., when Sediment control is used on pavement, heavy concrete blocks shall be used behind the Sediment control to help stabilize during rainfall/runoff events.
7. Staking depth for sand and silt loam soils shall be 12 in (300mm), and 8 in (200mm) for clay soils.
8. Loose compost may be backfilled along the upslope side of the Sediment control, filling the seam between the soil surface and the device, improving filtration and sediment retention.
9. If the Sediment control is to be left as a permanent filter or part of the natural landscape, it may be seeded at time of installation for

establishment of permanent vegetation. The Engineer will specify seed requirements.

10. Filtrexx® Sediment control is not to be used in perennial, ephemeral, or intermittent streams.

See design drawing schematic for correct Filtrexx® Sediment control installation (Figure 1.1).

## INSPECTION AND MAINTENANCE

Routine inspection should be conducted within 24 hrs of a runoff event or as designated by the regulating authority. Sediment control should be regularly inspected to make sure they maintain their shape and are producing adequate hydraulic flow-through. If ponding becomes excessive, additional Sediment control may be required to reduce effective slope length or sediment removal may be necessary. Sediment control shall be inspected until area above has been permanently stabilized and construction activity has ceased

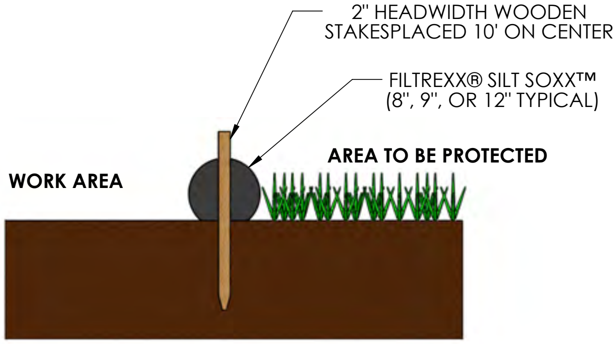
1. The Contractor shall maintain the Sediment control in a functional condition at all times and it shall be routinely inspected.
2. If the Sediment control has been damaged, it shall be repaired, or replaced if beyond repair.
3. The Contractor shall remove sediment at the base of the upslope side of the Sediment control when accumulation has reached 1/2 of the effective height of the Sediment control, or as directed by the Engineer. Alternatively, a new Sediment control can be placed on top of and slightly behind the original one creating more sediment storage capacity without soil disturbance.
4. Sediment control shall be maintained until disturbed area above the device has been permanently stabilized and construction activity has ceased.
5. The FilterMedia™ will be dispersed on site once disturbed area has been permanently stabilized, construction activity has ceased, or as determined by the Engineer.
6. For long-term sediment and pollution control applications, Sediment control can be seeded at the time of installation to create a vegetative filtering system for prolonged and increased filtration of sediment and soluble pollutants (contained vegetative filter strip). The appropriate seed mix shall be determined by the Engineer.

| Slope Percent | Maximum Slope Length Above Sediment Control in Feet (meters)* | | | | |
|---|---|---|---|---|---|
| | 8 in (200 mm) Sediment control | 12 in (300 mm) Sediment control | 18 in (450 mm) Sediment control | 24 in (600mm) Sediment control | 32 in (800mm) Sediment control |
| | 6.5 in (160 mm)** | 9.5 in (240 mm) ** | 14.5 in (360 mm) ** | 19 in (480 mm) ** | 26 in (650 mm) ** |
| 2 (or less) | 600 (180) | 750 (225) | 1000 (300) | 1300 (400) | 1650 (500) |
| 5 | 400 (120) | 500 (150) | 550 (165) | 650 (200) | 750 (225) |
| 10 | 200 (60) | 250 (75) | 300 (90) | 400 (120) | 500 (150) |
| 15 | 140 (40) | 170 (50) | 200 (60) | 325 (100) | 450 (140) |
| 20 | 100 (30) | 125 (38) | 140 (42) | 260 (80) | 400 (120) |
| 25 | 80 (24) | 100 (30) | 110 (33) | 200 (60) | 275 (85) |
| 30 | 60 (18) | 75 (23) | 90 (27) | 130 (40) | 200 (60) |
| 35 | 60 (18) | 75 (23) | 80 (24) | 115 (35) | 150 (45) |
| 40 | 60 (18) | 75 (23) | 80 (24) | 100 (30) | 125 (38) |
| 45 | 40 (12) | 50 (15) | 60 (18) | 80 (24) | 100 (30) |
| 50 | 40 (12) | 50 (15) | 55 (17) | 65 (20) | 75 (23) |

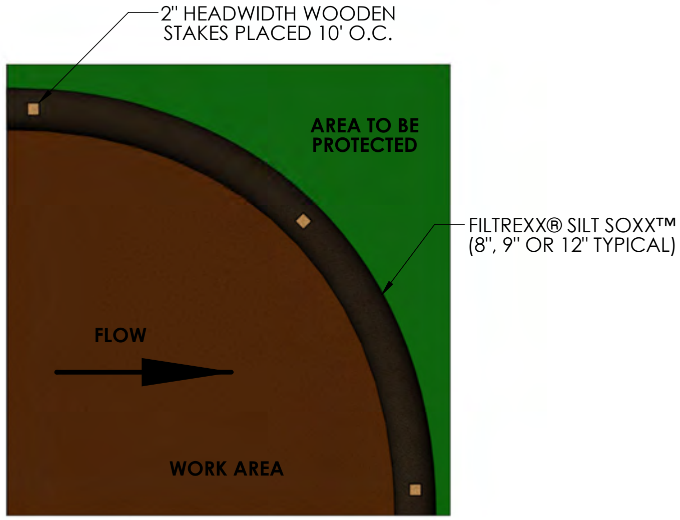
* Based on a failure point of 36 in (0.9 m) super silt fence (wire reinforced) at 1000 ft (303 m) of slope, watershed width equivalent to receiving length of sediment control device, 1 in/ 24 hr (25 mm/24 hr) rain event.

** Effective height of Sediment control after installation and with constant head from runoff as determined by Ohio State University.

## FILTREXX® SILT SOXX™

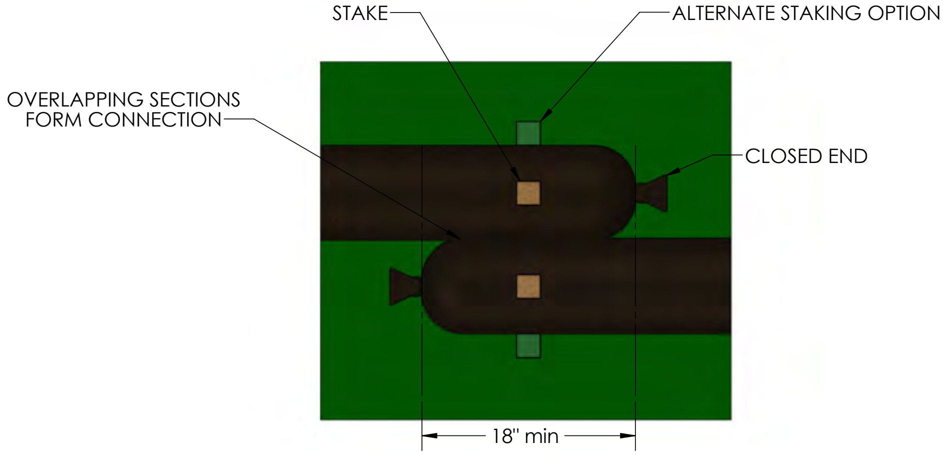



SECTION VIEW

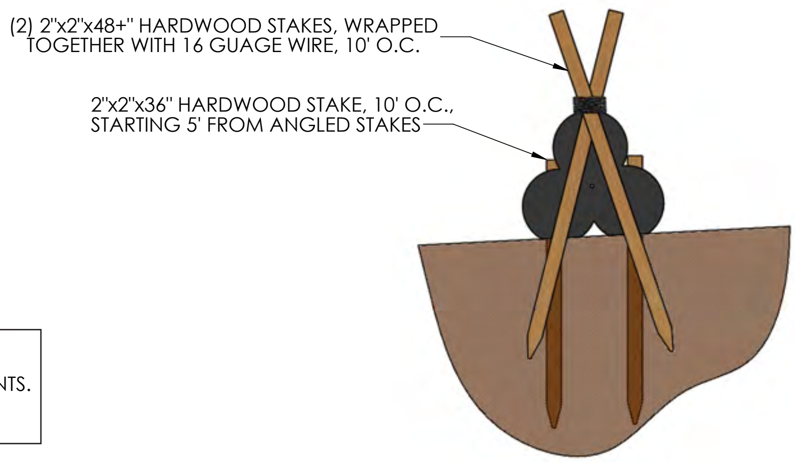



TOP VIEW

## COMPOST SOCK CONNECTION/ATTACHMENT DETAIL




## FILTREXX® PYRAMID STAKING DETAIL




NOTES:
1. ALL MATERIAL TO MEET FILTREXX® SPECIFICATIONS.
2. SILT SOXX™ FILL TO MEET APPLICATION REQUIREMENTS.
3. COMPOST MATERIAL TO BE DISPERSED ON SITE, AS DETERMINED BY ENGINEER.

# SWPPP Cut Sheet:

# Filtrexx® Inlet Protection

*Sediment & Perimeter Control Technology*

## PURPOSE & DESCRIPTION

Filtrexx® Inlet protection is a three-dimensional tubular sediment control and storm water runoff filtration device typically used for storm drain **inlet protection** of sediment and soluble pollutants (such as phosphorus and petroleum hydrocarbons) on and around construction activities.

## APPLICATION

**Drain inlets** are located in areas that receive runoff from surrounding lands, often exposed and disturbed soils, and are located at a low point, or in a sump. Inlet protection used around drain inlets (or *Drain* Inlet protection) should completely enclose the circumference of the drain and where possible should not be placed on a grade or slope. Inlet protection used around drain inlets should never be the only form of site sediment control and should be accompanied by erosion control/slope stabilization practices, such as Slope protection or rolled erosion control blankets (RECB). Inlet protection should never be placed where they divert runoff flow from the drain inlet, or on top of the inlet, which can cause flooding. Under high runoff and sediment loading conditions placement of 1-2 in (25-50 mm) diameter rock (AASHTO #2) may be placed around the outer circumference of the Inlet protection up to ½ the height of the Inlet protection. This will slow runoff velocity as it contacts the Inlet protection and will reduce sediment build-up and clogging of the Inlet protection.

**Curb inlets** are generally located on paved surfaces and are designed to rapidly drain storm runoff from roadways to prevent flooding that poses a hazard to vehicular traffic. Inlet protection devices should be placed in a manner which intercepts runoff prior to entering the inlet, but does not block or divert runoff from the inlet. To prevent diversion of runoff, Inlet protection used around curbs (or *Curb* Inlet protection) should be used in low points, or sumps, and minor slopes or grades. Inlet protection should never be placed in or on the curb inlet drain, or placed in a manner than obstructs vehicular traffic. Inlet protection height should be at least 1 in (25 mm) lower than top of curb inlet to allow for overflow into the drain and not over the curb. Maximum sediment removal efficiency occurs when minor ponding exists behind Inlet protection but should never lead to flooding.

**Curb sediment containment systems** are used to reduce the sediment and pollutant load flowing to a curb inlet. They are generally placed on paved surfaces perpendicular to runoff flow and should be lower than the height of the curb. Curb sediment containment systems should never cause flooding or placed where they are a hazard to vehicular traffic. Inlet protection used for curb sediment containment (or *Curb Sediment Containment* Inlet protection) can be placed on a grade but should never be placed directly upslope from curb inlet where it may inadvertently divert runoff from entering curb inlet.

## INSTALLATION

1. Inlet protection used for inlet protection to reduce sediment and soluble pollutants entering storm drains shall meet Filtrexx® FilterSoxx™ Material Specifications and use Certified Filtrexx® FilterMedia™.
2. Contractor is required to be a Filtrexx® Certified™ Installer as determined by Filtrexx® International, LLC (440-926-2607 or visit web site at Filtrexx.com). Certification shall be considered current if appropriate identification is shown during time of bid or at time of application (current list of installers can be found at www.filtrexx.com). Look for the Filtrexx® Certified™ Installer Seal.

3. Filtrexx® Inlet protection shall be placed at locations indicated on plans as directed by the Engineer. Inlet protection should be installed in a pattern that allows complete protection of the inlet area.
4. Installation of curb Inlet protection will ensure a minimal overlap of at least 1 ft (300mm) on either side of the opening being protected. The Inlet protection will be anchored to the soil behind the curb using staples, stakes or other devices capable of holding the Inlet protection in place.
5. Standard Inlet protection for curb inlet protection and curb sediment containment will use 8 in (200mm) diameter Inlet protection, and drain inlets on soil will use 12 in (300mm) or 18 in (450mm) diameter Inlet protection. In severe flow situations, larger Inlet protection may be specified by the Engineer. During curb installation, Inlet protection shall be compacted to be slightly shorter than curb height.
6. If Inlet protection becomes clogged with debris and sediment, they shall be maintained so as to assure proper drainage and water flow into the storm drain. In severe storm events, overflow of the Inlet protection may be acceptable in order to keep the area from flooding.
7. Curb and drain Inlet protection shall be positioned so as to provide a permeable physical barrier to the drain itself, allowing sediment to collect on the outside of the Inlet protection.
8. For drains and inlets that have only curb cuts, without street grates, a spacer is required in order to keep the Inlet protection away from the drain opening. This spacer should be a hog wire screen bent to overlap the grate opening and keep the sock from falling into the opening. Use at least one spacer for every 4 ft (1.2m) of curb drain opening. The wire grid also prevents other floatable waste from passing over the Inlet protection.
9. Stakes shall be installed through the middle of the drain Inlet protection on 5 ft (1.5m) centers, using 2 in (50mm) x 2 in (50mm) x 3 ft (1m) wood stakes.
10. Staking depth for sand and silt loam soils shall be 12 in (300mm), and 8 in (200mm) for clay soils.

### INSPECTION AND MAINTENANCE

Routine inspection should be conducted within 24 hrs of a runoff event or as designated by the regulating authority. Inlet protection should be regularly inspected to make sure they maintain their shape and are producing adequate hydraulic flow-through. If ponding becomes excessive, additional Inlet protection may be required or sediment removal may be necessary. Inlet protection shall be inspected until contributing drainage area has been permanently stabilized and construction activity has ceased

1. The Contractor shall maintain the Inlet protection in a functional condition at all times and it shall be routinely inspected.
2. If the Inlet protection has been damaged, it shall be repaired, or replaced if beyond repair.
3. The Contractor shall remove sediment at the base of the upslope side of the Inlet protection when accumulation has reached 1/2 of the effective height of the Inlet protection, or as directed by the Engineer. Alternatively, for drain Inlet protection a new Soxx™ may be placed on top of the original increasing the sediment storage capacity without soil disturbance.
4. Inlet protection shall be maintained until disturbed area above or around the device has been permanently stabilized and construction activity has ceased.
5. Regular maintenance includes lifting the Inlet protection and cleaning around and under them as sediment collects.
6. The FilterMedia™ will be removed from paved areas or dispersed on site soil or behind curb once disturbed area has been permanently stabilized, construction activity has ceased, or as determined by the Engineer.

**Table 2.4** Spacing for Curb Sediment Containment Systems.

| Grade (%) | Spacing (ft) | Spacing (mm) |
|---|---|---|
| 0.5 | 100 | 30 |
| 1.0 | 50 | 15 |
| 2.0 | 25 | 8 |
| 3.0 | 16 | 5 |
| 4.0 | 13 | 4 |
| 5.0 | 10 | 3 |

Source: Fifield, 2001.

**Figure 2.1.** Engineering Design Drawing for Curb and Drain Inlet Protection

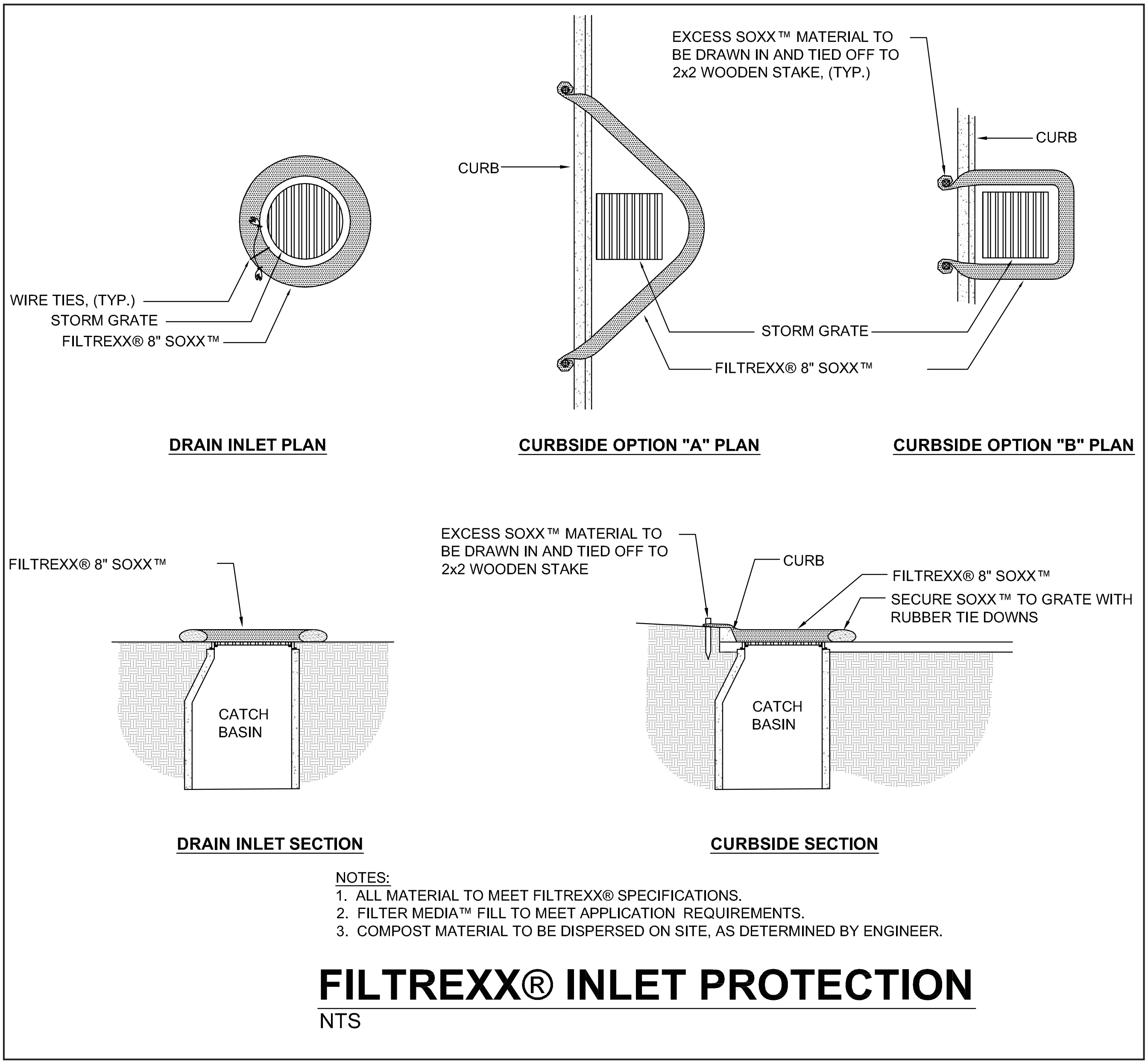
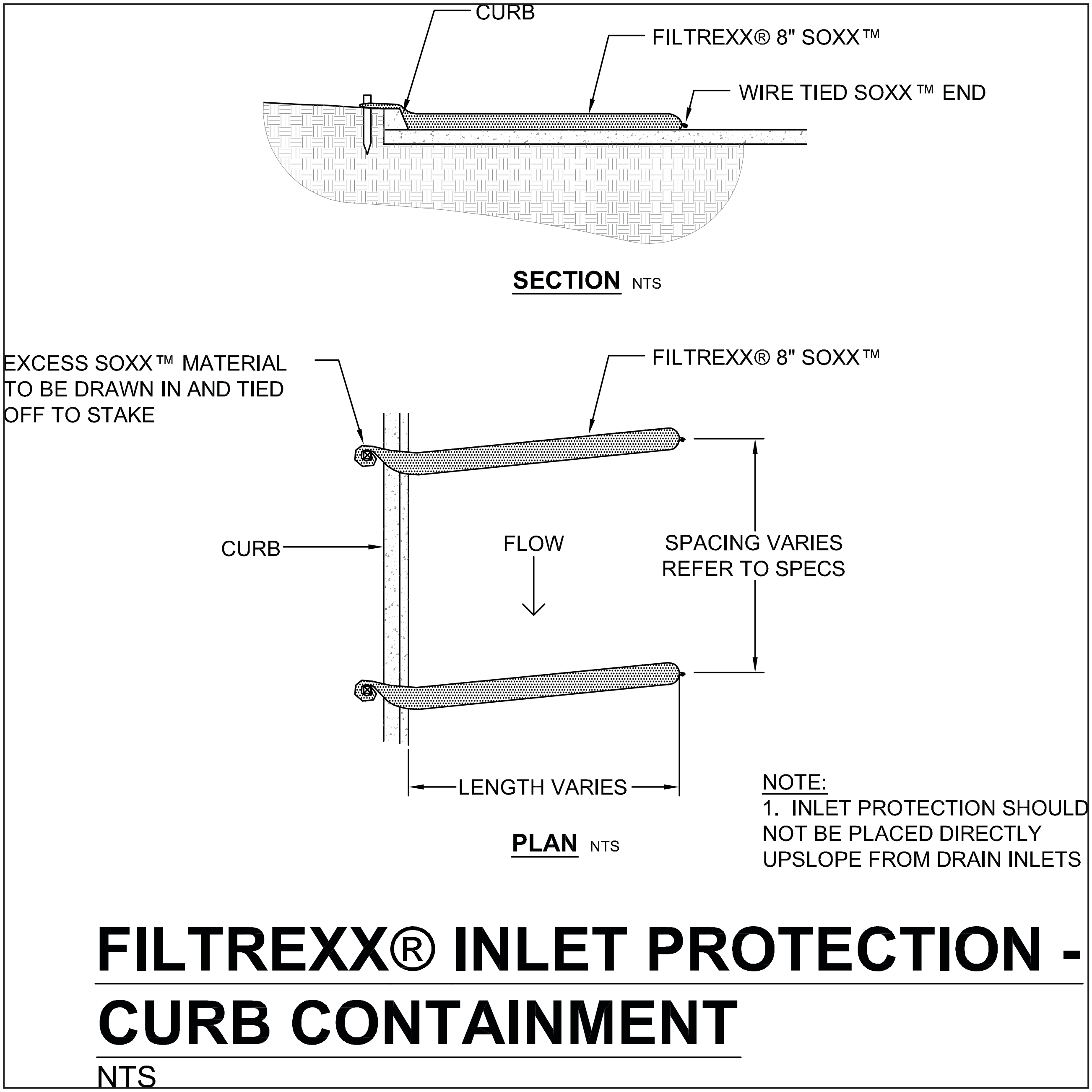


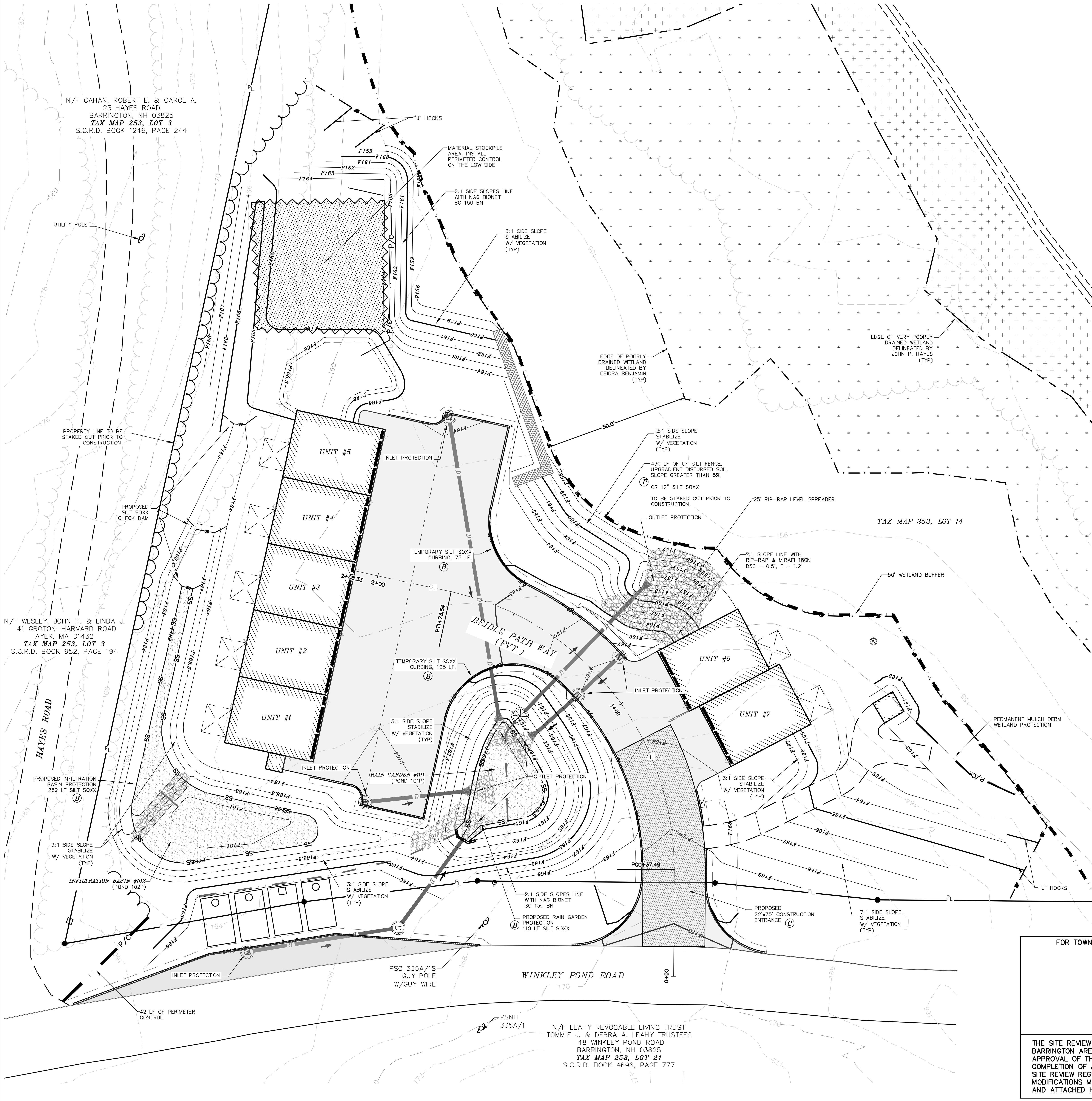
**Figure 2.2.** Engineering Design Drawing for Curb Sediment Containment Inlet Protection



| Pavement Temp. (°F) and Trend ( ↑ ↓ ) | Weather Condition | Maintenance Actions | Application Rate (lbs/per 1000 sq.ft.) | | | |
|---|---|---|---|---|---|---|
| | | | Salt Prewetted/Pretreated with salt brine | Salt Prewetted/Pretreated with other blends | Dry salt | Winter sand |
| >30 ↑ | Snow | Plow, treat intersections only | | | | Not recommended |
| | Frz. Rain | Apply chemical | | | | Not recommended |
| 30 ↓ | Snow | Plow and apply chemical | | | | Not recommended |
| | Frz. Rain | Apply chemical | | | | Not recommended |
| 25 - 30 ↑ | Snow | Plow and apply chemical | | | | Not recommended |
| | Frz. Rain | Apply chemical | | | | Not recommended |
| 25 - 30 ↓ | Snow | Plow and apply chemical | | | | Not recommended |
| | Frz. Rain | Apply chemical | | | | 3.25 |
| 20 - 25 ↑ | Snow or frz. Rain | Plow and Apply chemical | | | | 3.25 for frz. Rain |
| 20 - 25 ↓ | Snow | Plow and apply chemical | | | | Not recommended |
| | Frz. Rain | Apply chemical | | | | 3.25 |
| 15 - 20 ↑ | Snow | Plow and apply chemical | | | | Not recommended |
| | Frz. Rain | Apply chemical | | | | 3.25 |
| 15 - 20 ↓ | Snow or Frz. Rain | Plow and apply chemical | | | | 3.25 for frz. Rain |
| 0 to 15 ↑↓ | Snow | Plow, treat with blends, sand hazardous areas | Not recommended | | Not recommended | 5.0 and spot-treat as needed |
| < 0 | Snow | Plow, treat with blends, sand hazardous areas | Not recommended | | Not recommended | 5.0 and spot-treat as needed |

**Table 19. Application Rates for Deicing**

These rates & table format are based on road application guidelines (Mn Snow & Ice Control Field Handbook, Manual 2005-1). Develop your own application rates by adjusting your current rates incrementally downward toward these guidelines. Where temperature categories overlap, select the rate most applicable to your situation.




## EROSION AND SEDIMENT CONTROL NOTES:

1.) OWNER: HAMBONE LLC
242 CENTRAL AVEUNE
DOVER, NH 03820

2.) APPLICANT: HAMBONE LLC
242 CENTRAL AVEUNE
DOVER, NH 03820

3.) LOT AREA: 586,793 Sq. Ft., 13.47 Ac.
330,912 Sq.Ft., 7.60 Ac., TOTAL UPLAND

4.) S.C.R.D. BOOK 4976, PAGE 1023

5.) EROSION AND SEDIMENT CONTROL INSPECTIONS TO BE CONDUCTED ONCE PER EVERY SEVEN DAYS AND AT AN INCREASED FREQUENCY INCLUDING WITHIN 24-HOURS OF A 0.25 INCH RAIN EVENT. INSPECTIONS TO BE CONDUCTED BY A "QUALIFIED PERSON" AS DEFINED BY EPA CGP 4.1.1 AND INSPECTION REPORTS SUBMITTED TO THE TOWN OF BARRINGTON, PLANNING DEPARTMENT WITHIN 24 HOURS IN ACCORDANCE WITH CGP 4.1.7 AND MAINTAINED BY THE OWNER FOR A PERIOD OF THREE YEARS AFTER THE PROJECT IS COMPLETED.

6.) PER EPA CGP 2.1.2.2 (INSTALL PERIMETER CONTROL), "YOU MUST INSTALL SEDIMENT CONTROLS ALONG THOSE PERIMETER AREAS OF YOUR SITE THAT WILL RECEIVE STORMWATER FROM EARTH DISTURBING ACTIVITIES." AS A RESULT OF SWPPP INSPECTIONS, THE CONTRACTOR MAY HAVE TO EXPAND PERIMETER CONTROLS TO MEET THIS REQUIREMENT. THE E&SC PLAN IS INITIAL GUIDANCE AS TO THE ANTICIPATED REQUIREMENTS AND IT THE CONTRACTORS RESPONSIBILITY TO ENSURE THAT STORMWATER VIOLATION DO NOT OCCUR

7.) CONTRACTOR IS REQUIRED TO HAVE A CONSTRUCTION ENTRANCE.

8.) CONTRACTOR IS RESPONSIBLE FOR SWEEPING THE DRIVEWAY TO ENSURE THAT NO SEDIMENT IS BEING TRACKED ONTO WINKLEY POND ROAD.

9.) CONTRACTOR IS RESPONSIBLE FOR CLEANING AND MAINTAINING THE INLET PROTECTION ONCE INSTALLED.

10.) FUGITIVE DUST IS TO BE CONTROLLED THROUGHOUT THE CONSTRUCTION PROCESS IN ACCORDANCE WITH ENV-A 1000.

11.) CONTRACTOR IS TO MEET THE REQUIREMENTS SPECIFIED IN RSA 430:51-57 AND AGR 3800, RELATING TO INVASIVE SPECIES.

12.) CONTRACTOR IS RESPONSIBLE FOR PROTECTING THE WATER QUALITY FROM ANY RUN OFF DURING THE CONSTRUCTION PROCESS, IN ACCORDANCE WITH ENV-WQ 1507, IN ORDER TO PREVENT VIOLATIONS OF THE STORM WATER QUALITY STANDARDS.

13.) CONTRACTOR CAN USE SILT FENCE, SILT SOXX OR MULCH BERM FOR PERIMETER CONTROL. SPECIFIC PRACTICES MAY BE SPECIFIED, SEE PLAN. SILT FENCE OR SILT SOXX REQUIRED WHEN UPGRADIENT DISTURBED SOIL IS GREATER THAN 5%. MULCH BERM CAN BE USED WHEN THE UPGRADIENT DISTURBED SOIL IS 5% OR LESS.

**STABILIZATION NOTE:**
SEE NOTE #6, SHEET E-102, DETAIL E-18
SIDE SLOPES ARE TO BE STABILIZED WITHIN THREE WORKING DAY UPON COMPLETION OF FINAL GRADE.

## LEGEND:

- STONE BOUND ~FND~
- UTILITY POLE/GUY WIRE
- TEST PIT
- TEMPORARY BENCHMARK (T.B.M.)
- DETAIL SHEET / DETAIL
- STREAM
- POORLY DRAINED JURISDICTIONAL WETLAND
- VERY POORLY DRAINED JURISDICTIONAL WETLAND
- WETLAND BUFFER
- CONTOUR MINOR, EXISTING
- CONTOUR MAJOR, EXISTING
- CONTOUR MINOR, PROPOSED
- CONTOUR MAJOR, PROPOSED
- BUILDING SETBACK LINE
- WELL RADIUS
- TREELINE
- ROAD CENTERLINE
- SHOULDER
- PAVEMENT SEAM
- DRAIN CULVERT W/ FLARED END SECTION (F.E.S.)
- UNDERDRAIN
- GUARD RAIL
- RIP RAP
- STORMWATER BEST MANAGEMENT PRACTICE (BMP)
- DRAIN MANHOLE W/STRUCTURE
- CATCH BASIN W/ STRUCTURE
- STORMWATER BMP OUTLET STRUCTURE
- SILT FENCE / EROSION MIX BERM
- FILTREXX 8" - 12" SILT SOXX AS SPECIFIED
- PERIMETER CONTROL
- CONSTRUCTION FENCE
- (B) STORMWATER BMP PROTECTION
- (P) PERIMETER CONTROL
- (C) RESIDENTIAL/ROADWAY CONSTRUCTION

**GRAPHIC SCALE**

20 0 10 20 40 80
( IN FEET )
1 inch = 20 ft.

**SOILS & DEWATERING:**

| | | |
|---|---|---|
| 313 | DEERFIELD | LOAMY SAND K= 0.17 |
| 400 | UDORTHENTS (DEERFIELD DERIVED) | LOAMY SAND K= 0.17 |
| 915 | DEERFIELD VARIANT | LOAMY SAND K= 0.17 |

SEE SITE SPECIFIC SOILS MAP (SSSM)
SEE WEBSOIL USDA-NRCS
ERODIBILITY FACTOR - K, CPESC MANUAL, ENVIROCERT INTERNATIONAL INC. & ROCKINGHAM COUNTY SOIL SURVEY, ROCKWEB SOIL ATTRIBUTES.

CONTRACTOR TO BE AWARE OF THE SOIL PROFILES AND ENSURE THAT PROPER EROSION PREVENTION AND SEDIMENT CONTROL MEASURES ARE TAKEN AT ALL TIMES. ANY DEWATERING REQUIREMENTS IN NEW HAMPSHIRE REQUIRE SPECIAL PROVISIONS IN ACCORDANCE WITH THE "CLARIFICATION OF SECTION 9.1.2 (STATE OF NEW HAMPSHIRE CONDITIONS) AND OTHER NH SPECIFIC INFORMATION FOR THE U.S. EPA 2012 NPDES CONSTRUCTION GENERAL PERMIT (CGP)" DATED MAY 3, 2012 INCLUDED IN THE SWPPP.

COVER MANAGEMENT DURING CONSTRUCTION FOR EXPOSED SOIL WILL INCLUDE HAY / STRAW APPLIED AT A RATE OF 2.0 TONS PER ACRE, TEMPORARY SEEDING OF ANNUAL RYE GRASS, AND PERMANENT SEEDING AT THE EARLIES OPPORTUNITY. SEE ADDITIONAL REQUIREMENT FOR STABILIZATION ON THE EROSION AND SEDIMENT CONTROL DETAIL SHEETS, E-101 AND E-102.

THE CONSTRUCTION SCHEDULE WILL BE MANAGED SO THAT ALL STORMWATER STRUCTURES WILL BE BUILT AND STABILIZED PRIOR TO RECEIVING SURFACE WATER RUNOFF. CONTRACTOR TO BE RESPONSIBLE FOR ALL DIVERSIONS DURING CONSTRUCTION AND FOR INTERIM SEDIMENT AND EROSION CONTROL MEASURES.

FOR TOWN APPROVAL PURPOSES :

THE SITE REVIEW REGULATIONS OF THE TOWN OF BARRINGTON ARE A PART OF THIS PLAN, AND APPROVAL OF THIS PLAN IS CONTINGENT UPON COMPLETION OF ALL REQUIREMENTS OF SAID SITE REVIEW REGULATIONS, EXCEPTING ONLY MODIFICATIONS MADE IN WRITING BY THE BOARD AND ATTACHED HERETO.

| REVISION | DATE | DESCRIPTION |
|---|---|---|
| | | |

EROSION AND SEDIMENT CONTROL PLAN
LAND OF
HAMBONE LLC
49 WINKLEY POND ROAD
BARRINGTON, N.H.
*TAX MAP 253, LOT 14*

BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863

SCALE : 1 IN. EQUALS 20 FT.
DATE : AUGUST 16, 2023
FILE NO. : DB 2021-163

STATE OF NEW HAMPSHIRE
KENNETH A. BERRY
No. 14243
LICENSED PROFESSIONAL ENGINEER