

**DRAINAGE ANALYSIS
&
EROSION AND SEDIMENT
CONTROL PLAN**

**The Village at Barrington Square
Tax Map 235, Lot 1-1 & Lot 3**

Prepared for:

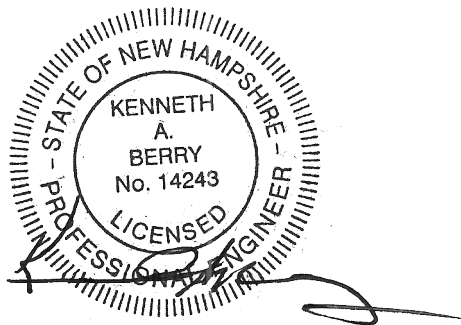
**Dove Development Group, LLC
242 Central Avenue
Dover, NH 03820**

Land of

Dove Development Group LLC

Prepared by:

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335 Second Crown Point Road
Barrington, NH 03825**



Project Number:
DB 2020-097

June 14, 2021

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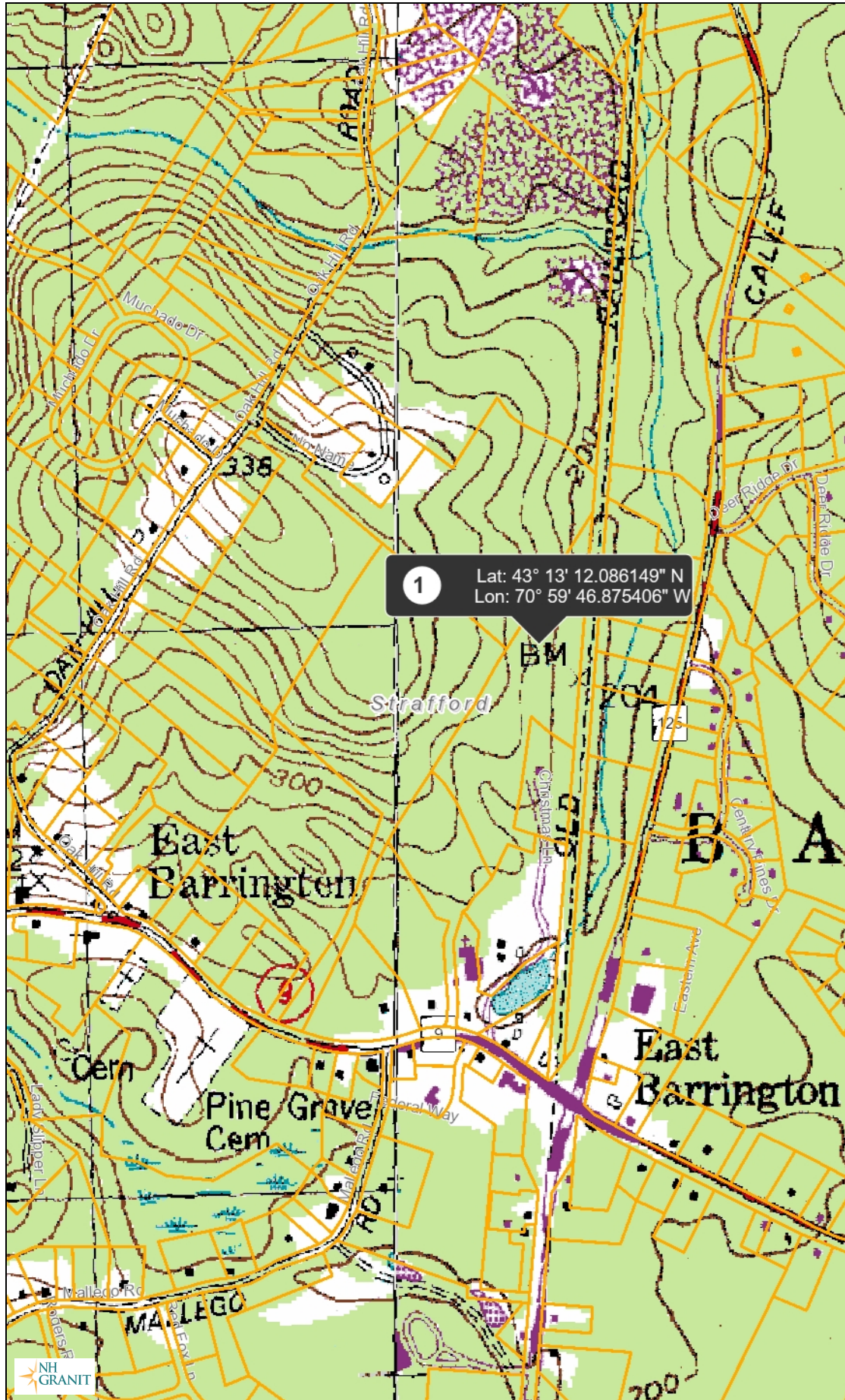
25 Yr.-24 Hr. Full Summary
2 Yr.-24 Hr. Node Listing
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Map by NH GRANIT



1 Lat: 43° 13' 12.086149" N
Lon: 70° 59' 46.875406" W

Legend

- Polygons
- State
- County
- City/Town

Map Scale

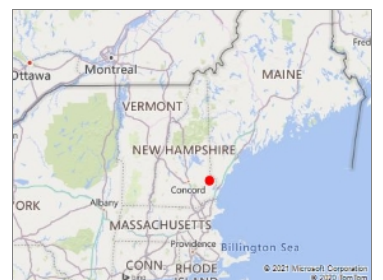
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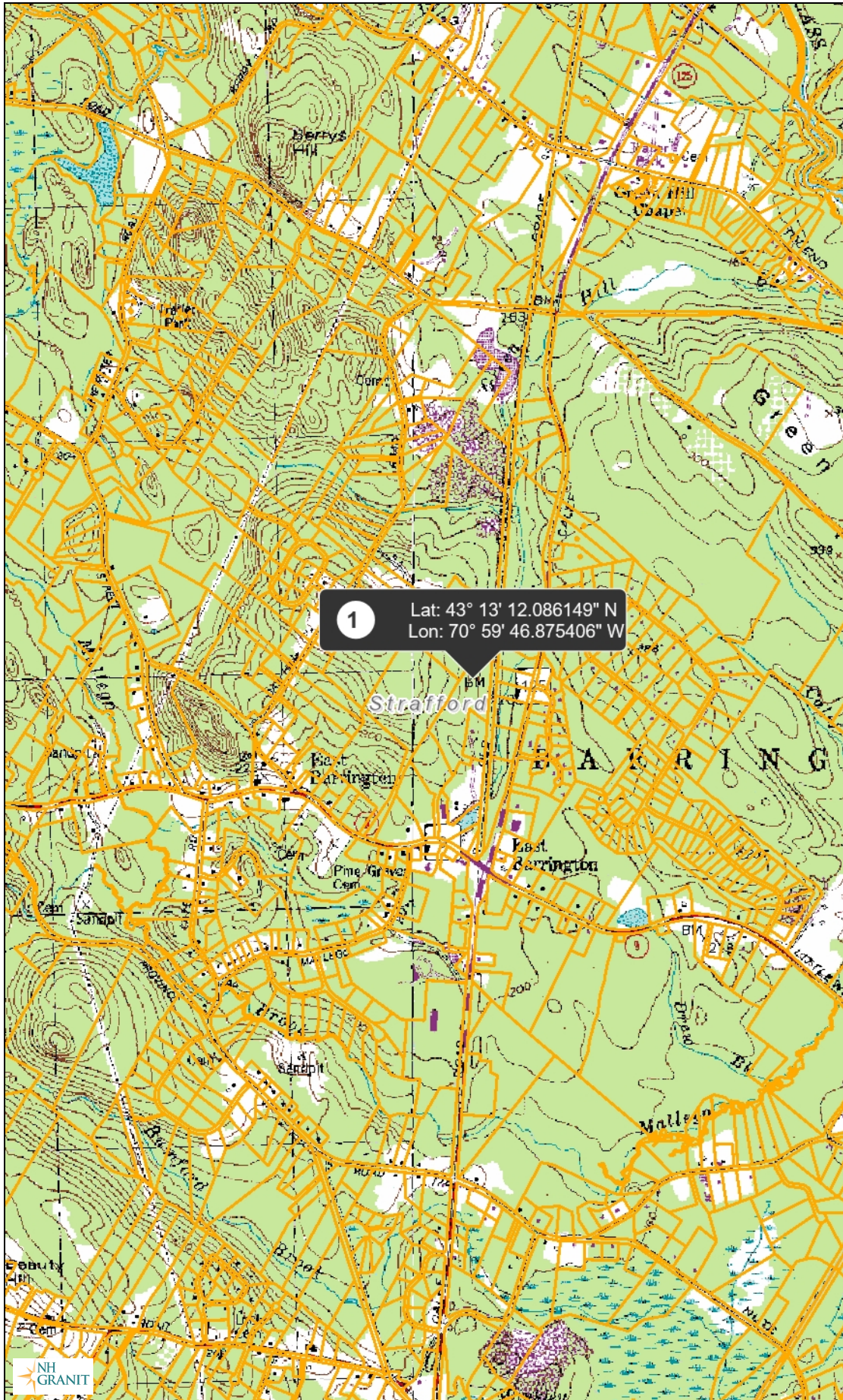
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Notes



Map by NH GRANIT



Legend

- Polygons
- State
- County
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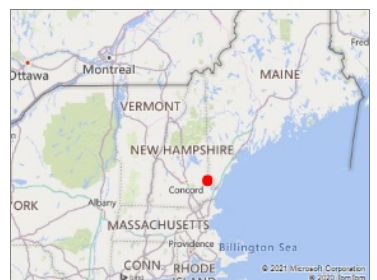
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Notes



DESIGN METHOD OBJECTIVES

The owners of Tax Map 235, Lot 1 John and Linda Svenson, in conjunction with the land owners of Tax Map 239, Lot 2, 1962 Real Estate LLC, proposed to construct an access road to the rear section of the Christmas Dove parking Lot. The applicants have received a variance from the Barrington Zoning Board which contemplates a residential subdivision beyond the Christmas Dove. The owners have re-developed Christmas Lane (now Community Way) to provide proper access to the Christmas Dove and the land owned by 1962 Real Estate LLC. A portion of the project is conceptual in nature at this time and contains the future branch location of Holy Rosary Credit Union. The project plans call out areas that have been constructed on that project site so as to ensure the proper drainage design is implemented as part of this project path.

The current owners of Tax Map 235, Lot 1-1 and Lot 3, Dove Development Group, LLC. are proposing to develop the land behind the Christmas Dove to include a mixed use building as well as 25 residential units. This development would include the construction of two roads including two cul-de-sac's as well as the associated parking area required for the mixed use building.

A Pre-Existing and Proposed Conditions analysis was conducted for the purpose of estimating the peak rate of stormwater run-off and to subsequently design adequate mitigation of drainage. There are five existing discharge points analyzed on the project site, noted as Final Reaches #100, #200, #300, #400, and #800. Final Reaches #100, #200, #300, and #400 are all different cross culverts along the Svenson driveway and edge of the existing trail that runs alongside a portion of the parcel. Final Reach #800 is the existing pond located on the Svenson property. Designing two watershed models we have compared the differences in these rates of peak run-off and surface water volume. Sheets W-1 outline the characteristics of the site in its existing or pre-construction conditions. The second analysis displays the proposed (post-construction) conditions (See Sheets W-2). The analysis was conducted using data for the 2 Yr – 24 Hr (3.08”), 10 Yr – 24 Hr (4.64”), 25 Yr -24 Hr (5.86”), 50 Yr – 24 Hr (7.00”), and 100 YR-24 Hr (8.37”) storm events. Storm event analysis was accomplished using the USDA SCS TR-20 method within the HydroCAD Stormwater Modeling System environment and rainfall quantities are based on the Extreme Precipitation Table for this location from the Northeast Regional Climate Center / Cornell University (<http://precip.eas.cornell.edu>), (Attached in Appendix 3).

1.0 Pre-Existing Analysis:

Reference: W-1 Sheets - Existing Conditions Watershed Plan (Enclosed)
Sheet 2 Existing Conditions Plan

The Existing parcels consists of a vacant land which are 7.42 acres and 17.07 acres being Tax Map 235 Lots 1-1 and Lot 3. These two parcels will be merged in the process of development.

During the spring and summer of 2019 Community Way, then Christmas Lane, was reconstructed based on a Site Plan Review entitled Christmas Lane Reconstruction for 1962 Real Estate, LLC and John & Linda Svenson, Franklin Pierce Highway, Barrington, NH, as revised through October 28, 2018. This site plan was reviewed and approved by the Town of Barrington and peer reviewed by their engineering consultant. After the construction of the infrastructure, John & Linda Svenson sold the two locus parcels to the applicant, Dove Development Group, LLC.

For the completion of this application, due to the size and requirement that the design be approved by NHDES Alteration of Terrain Bureau, and the look back period of this bureau being ten years, the comparative analysis was conducted as a Pre-existing Analysis. The original topography from the site in 2018 was utilized for the Pre-Existing Analysis and the As-Built Grades imported into the Proposed Conditions Analysis for the current application.

In addition to the locus parcels, there is a substantial off-site component where surface water runoff runs across the locus parcel(s) and through the infrastructure constructed as stated above.

Existing Topography was derived from the Existing Conditions Survey conducted for the locus parcels and for land owned by 1962 Real Estate, LLC from previous work, to include test holes previously conducted. Off-site topography was determined by USGS Contours and by Google Tin. On-site soils and wetlands were mapped by John P. Hayes, III, CSS, CWS and off-site soils were evaluated by USDA / NRCS Websoil. A large component of the off-site soils are Hollis – Charlton Very Rocky soil which has a Hydrological Soil Group rating of D – A. Where test pits could not confirm depth to ledge, this soils group was considered to be 50% HSG D and 50% A. The site specific soils survey was limited in extent to the two parcels owned by the Dove Development Group, LLC.

The parcels of land total 24.49 acres and the analysis involves 79.08 acres of land. The runoff is all part of the Greenhill Brook watershed and flows north roughly parallel with the abutting privately owned rail road grade. The original analysis completed for 1962 Real Estate, LLC and the Svenson's culminated with Final Reach #800 at a box culvert under the R.R. grade. Final Reach #100 is an existing culvert under a private driveway on land of Garth & Elizabeth Svenson. Final Reach #200 is a point on the driveway know to seasonally flood but no culvert currently exists. Final Reaches #300 and #400 are existing box culverts under the R.R. Grade.

Final Reach #800:

There are eleven subcatchments that contribute runoff to Final Reach #800. Final Reach #800 is the inlet to the pond which is located on Svenson land and is labeled on the Watershed Sheets as "Svenson Pond". The subcatchments are divided by the various inlet sumps, catch basis, and driveway cross culverts. The pond is not evaluated nor is all of the land directly abutting the pond.

Final Reach #100:

One subcatchment (Subcatchment #16) contributes runoff to a 12" CMP cross culvert (Pond #16) under the existing driveway which provides access to Kimberly B. and Rondi M. Boyer over land of Garth and Elizabeth Svenson.

Final Reach #200:

One Subcatchment (Subcatchment #17) contributes runoff to a point in the above referenced driveway where it is known there is seasonal / periodic flooding. (Pond #17)

Final Reach #300:

One Subcatchment (Subcatchment #18) contributes runoff to an existing box culvert under the rail road grade. (Pond #18)

Final Reach #400:

One Subcatchment (Subcatchment #19) contributes runoff to a third box culvert under the rail road grade. (Pond #19)

2.0 Proposed Analysis:

Reference: W-2 Sheets - Proposed Conditions Watershed Plan (Enclosed)
Proposed Site Plan
Proposed Grading & Drainage Overview Plan
Plan and Profile Sheets

The 2019 construction consists of re-construction a roadway to the Town of Barrington Standards for approximately 550 linear feet. Through its development proper access is provided to the 1962 Real Estate LLC lot. As noted above, a future branch for Holy Rosary Credit Union is contemplated at this location. As such, this site has been conceptually designed with an adequate grading plan which includes the installation of rain garden #101 to handle and treat the flow from the future bank as well as the revised Christmas Lane. (Infrastructure that is now built.)

The four following paragraphs represent construction that is now built. There are two infiltration features on this project site, on land of 1962 Real Estate, as well as a cross culvert, which was constructed as part of the conceptual site plan for a branch bank location. These areas are Subcatchments 13S, 14S, 15S and are routed to Pond 101P for treatment. The infiltration features are modeled as Ponds 13P & 14P. These ponds provide the adequate separation to the seasonal high water table (3') to provide treatment through the infiltrating process. Pond 101P is routed to the new cross culvert discussed below, 2P.

The runoff from the abutting property to the west, and limit of the Greenland Brook Watershed bisects the 1962 Real Estate Property. The crossing is proposed as an 18" HDPE N-12 culvert which is oversized hydraulically. Though this area isn't a wetland, it provides a connection to a downstream wetlands, and in keeping with best management practices for migration, we have opted to oversize the device. This device is modeled as Pond 21P and receives flow from the modified Subcatchments 2S & 3S. Flow from this crossing is routed to the downstream driveway crossing and then to the Svenson Pond.

There is a sidewalk constructed on the eastern side of the roadway with a 6" vertical granite curb. This curb and gutter system is routed to a series of basins along the roadway. These basins also provide for better drainage practices within the existing Christmas Dove project site. 15" HDPE N-12 pipe was chosen to flow from one basin to another so as to provide adequate capacity for future connections. Applicants moving forward would be expected to adequately mitigate flows and volumes prior to entering this closed system. These areas are modeled as Subcatchments 1S, 6S, 4S and 12S, and are routed to the respective ponds modeled as Pond 10P, 13P, 40P and 12P.

The closed systems and the Dove project site are routed to rain garden #102. This rain garden provides full treatment of the revised roadway as well as the existing project site which was untreated in the existing condition. Subcatchment 5S also contributes flow to this pond (102P). The pond is then routed to the existing driveway cross culvert, draining to Final Reach 800, inlet to Svenson Pond. The pond is not included in the analysis nor all of the land directly adjacent to the pond.

The proposed analysis is evaluated at the same five locations as the existing analysis.

Final Reach #800: (2019 Christmas Lane Construction)

Flow areas to this final reach remain the same, with a minor increase in the total watershed area curve number. This increase in the curve number is offset by the installation of the Low Impact Development rain gardens #101 & 102, as well as the two infiltration areas. This mitigation allows for the peak rates from this site to be reduced to the inlet to Svenson Pond with the minor exception of the 10 Yr – 24 Hr. peak rate of 0.2 CFS to a permanent pond which discharges to a permanent stream. The volume conforms to the channel protection standards.

In addition to the infrastructure from the Christmas Lane, now Community Way, the discharge from Subsurface Gravel Wetland #103 is intercepted at a culvert entrance prior to existing Catch basin #10 (Pond #10). The network hydraulically upslope of the gravel wetland routes runoff from a part of the mixed-use building for treatment. A small section of the proposed roadway extension is also intercepted by proposed catch basin #30 and existing catch basin #10. The constructed infrastructure is represented best on Sheet 10 of 14 and the proposed infrastructure is on Sheet 11 of 14.

Final Reach #100:

The components of the project that contribute runoff to this final reach include the northern portion of the mixed-use building, the back half of seven residential units, collection system, and subsurface gravel wetlands (SGW) #104 and #105. The infrastructure collecting the runoff consists of nine catch basins (Ponds C31, C32, C35, C36, C37, C38, C39, C40, & C43) and one drain manhole (Pond D2). From the level spreader it travels overland in the natural course (Reach 65) to the existing CMP Culvert. (Pond 16) The Subcatchment associated include nine from the catch basins, two associated with the SGW (Pond #64 & #65), and one associated with the pond around the level spreader. (Subcatchment & Pond #51) This portion of the design is best represented on Sheet 11 of 14

Final Reach #200:

The components of the project that contribute runoff to this final reach include the balance of the residential units, collection system, and Rain Gardens #106, #107, #108, & #109. The infrastructure collecting the runoff consists of five catch basins (Ponds C41, C42, C44, C45, & C46), two drain manholes (Pond D3 & D4), two culvert sumps (Pond 47 & 48), one of which is the inside of the cul-de-sac and the other collecting runoff from off-site a subcatchment. The subcatchments associated include the five catch basins, four rain gardens, drainage sumps which includes Subcatchment #47 from primarily off-site. This portion of the design is best represented on Sheet 12 of 14.

Final Reach #300:

The components of the project that contribute runoff to this final reach include the access road to the wells, the pump house, and detention infrastructure. In addition to Detention Pond #110, there are two culverts (Pond #52 and #53) where the well access road crosses a jurisdictional wetland in two places because of branching in the wetlands.

Final Reach #400:

Subcatchment is altered in shape due to the placement of the well field and required fill. There is no additional alteration to this subcatchment or final reach.

Summary:

The peak rates of run off from the analyzed areas are reduced at the 2,10, 25, 50, 100 Yr. 24Hr. storm events. Volumes are reduced during the 2, 10, 25 Yr. 24Hr. storm events with minor increases at the 50 and 100 Yr. 24Hr. storm events.

Stormwater Treatment:

Surface water runoff from the development area is being treated by bio-detention rain gardens which are low impact development methods (LID) Storm flow is to sheet off from the proposed paved areas into pre-treatment forebay cells prior to entering either the pre-treatment bio cell or rain gardens; and treated by Subsurface Gravel Wetlands, also a LID method. Water Quality Volume calculations based on the Alteration of Terrain model are included along with Pond Storage Tables are included in Appendix 3 for all seven modeled rain gardens and two Subsurface Gravel Wetlands. This LID design allows for full treatment while maintaining flows and volumes.

The receiving waters for the project are known as Svenson Pond locally but as Unnamed Brook – Fire Pond (NHIMP600030607-05) which discharges into Green Hill Brook (NHRIV600030607-09). The pond is impaired by Mercury, as is the assumption with all New Hampshire waters, and covered by the NE Regional Mercury TMDL #33883. The brook is also impaired by pH which does not have a TMDL, is considered low priority and not considered an Outstanding Resource Water. Due to the lack of sediment or turbidity as an impairment, the pond and brook are considered Tier 2 Waters by NHDES and construction will be subject to E&SC inspections at an increased frequency, i.e. once every seven days and after a rain event of 0.25 inches or more.

Infiltration Practices:

Infiltration takes place in Ponds 13P, 14P & 107P. These ponds contain deep sands and provide for over 3' of separation between the seasonal high water table and the top of in grassed infiltration practice. The lowest rate provided by the NRCS was multiplied by 0.5 pursuant to the Alteration of Terrain rules and a rate of 0.71 was applied to the model.

Please see attached Infiltration Feasibility Study for further detail.

3.0 FULL COMPARATIVE ANALYSIS 06-25-21

<u>ANALYSIS</u>	<u>COMPONENT</u>	<u>PEAK RATE DISCHARGE (Cubic Feet / Second)</u>			
		2 Yr.	10 Yr.	25 Yr.	50 Yr.
Final Reach #800	Existing	2.35	4.92	11.40	18.46
	Proposed	0.90	5.10	10.74	16.06
Final Reach #100	Existing	0.17	1.74	2.49	6.51
	Proposed	0.07	0.46	1.42	2.29
Final Reach #200	Existing	0.30	3.90	8.23	13.07
	Proposed	0.38	2.22	4.15	7.18
Final Reach #300	Existing	0.98	5.45	10.52	15.97
	Proposed	0.92	5.24	10.19	15.45
Final Reach #400	Existing	0.61	4.74	9.97	15.83
	Proposed	0.61	4.74	9.97	15.83

<u>ANALYSIS</u>	<u>COMPONENT</u>	<u>VOLUME (ACRE FEET)</u>			
		2 Yr.	10 Yr.	25 Yr.	50 Yr.
Final Reach #800	Existing	0.427	1.617	3.023	4.625
	Proposed	0.468	1.695	3.095	4.689
Final Reach #100	Existing	0.081	0.365	0.685	1.040
	Proposed	0.067	0.312	0.541	0.810
Final Reach #200	Existing	0.130	0.657	1.232	1.861
	Proposed	0.171	0.812	1.378	2.054
Final Reach #300	Existing	0.243	0.826	1.433	2.085
	Proposed	0.287	0.981	1.651	2.393
Final Reach #400	Existing	0.247	0.978	1.776	2.649
	Proposed	0.247	0.978	1.776	2.649

4.0 EROSION & SEDIMENT CONTROL PLANS BEST MANAGEMENT PRACTICES (BMP's)

Reference: Proposed Site Plan and Grading Plan
Erosion & Sediment Control Plan
Erosion & Sediment Control Details, E-101 & E-102

The proposed site development is protected from erosion and the abutting properties are protected from sediment by the use of Best Management Practices as outlined in the New Hampshire Stormwater Manual, Volume 2, Post-Construction Best Management Practices Selection & Design (December 2008, NHDES & US EPA). Any area disturbed by construction will be re-stabilized within 30 days and abutting properties will not be adversely affected by this development. All swales and drainage structures will be constructed and stabilized prior to having run-off directed to them. Reference is also made to the Stormwater System Operation and Maintenance Plan / Inspection & Maintenance Manual which has been written specifically for this project and available to the owner.

Silt Fence / Perimeter Control

The plan set demonstrates the location of silt fence for sediment control. The Erosion and Sediment Control Details, Sheet E-101, has the specifications for installation and maintenance of the silt fence. Silt fence is rated to be effective for 100 linear feet of fence to capture runoff from one-quarter acre or basically 100 feet of land area sloping toward the fence. Filtrexx silt soxx have a variable area and depth, see Filtrexx supporting documents. The NHDES Stormwater Manual requires that the maximum spacing for support stakes is six-feet.

Filtrexx Silt Soxx, or approve equal, has been specified in numerous locations within the plan set and silt fence is not a substitution for silt soxx. Multiple sizes of this product have been specified for use.

EPA CGP 2012: "You must install sediment control along those perimeter areas of your site that will receive stormwater from earth disturbing activity."

In accordance with EPA CGP 2.1.2.1, Provide Natural Buffers or Equivalent Sediment Controls, and CGP Appendix G, Table G-3, and Table G-7, slopes between 3% and 6% with soils that are Fine Sandy Loams, there is a High Risk Factor and it is required to Double Perimeter Control and 7-Day Site Stabilization.

Erosion Control Mix Berm

As an alternative to the Silt Fence, an Erosion Control Mix Berm can be utilized as a perimeter control. The specifications can be found on Sheet E-101, Detail E6.

Bioretention System (Rain Garden)

Description: Rain Gardens, or bioretention areas are located close to the source of runoff. They are intended to integrate with the site landscaping and become an aesthetically attractive opportunity to provide highly effective stormwater treatment. The rain gardens associated with this proposed development contribute toward recharge of surface water run-off into the ground. It is important that sediment be removed from run-off prior to discharge into the bioretention area to preserve the mulch and soil mix ratio. During construction it is important that the ground surface not be exposed to traffic or construction equipment to preserve the infiltration capabilities of the existing soil. Construction specifications are included in the plan set and New Hampshire Stormwater Manual, Volume 2, 4-3 Treatment Practices, 4c Bioretention System.

Construction Considerations:

After the stone and bio-media has been installed, Filtrexx Silt Soxx or approved equal, will be installed at the toe of slope intersection between the berm and bio-media and will remain until the slopes of the berm are stable.

See the Stormwater Management Inspection and Maintenance Manual for more details.

Subsurface Gravel Wetland

Description: A Gravel Wetland (NHDES SWM 4-3 Treatment Practice 2D) or Subsurface Gravel Wetland consists of a forebay and multiple flow-through treatment cells. During smaller rain events, the surface water runoff is intended to pass from the forebay, into the gravel media through perforated pipes and structures where it passes through an anaerobic environment where the Water Quality Volume will have 24-72 hours of contact time. The forebay is required to contain 10% of the WQV and each of the two cell must contain 45% of the WQV. During larger storm events, the system works as a detention pond. The design of a Subsurface Gravel Wetland will be constructed in accordance with the most current version of the Design Specifications provided by the UNH Stormwater Center and SWM Volume 2, Section 4-3 Treatment Practices, 2d Gravel Wetlands.

See the Stormwater Management Inspection and Maintenance Manual for more details

Rip Rap Outlet Protection, Level Spreaders, & Emergency Spillways

Description: Outlet Protection consists of a riprap apron or preformed scour hole that is designed to provide velocity reduction of the surface water run-off that is leaving a culvert. The design is dependent on the culvert size, soil conditions, velocity, and quantity of the run-off. There are to be no bend or curves at the intersection of the conduit and apron. Level spreaders are intended to provide a level lip where surface water runoff is allowed to continue downhill closer to sheet flow. The level lip is to be

constructed as level as possible for the entire length. Emergency Spillways are rip rap reinforced outlets near the top of the berm that allow runoff to leave a practice during periods of very high flow. Ref.: NHDES SWM Volume 2, Section 4-6 Conveyance Practices, 6. Outlet Protection and 1. Detention Ponds, Note 3, Page 158.

Maintenance Considerations: The riprap outlet protection will be inspected annually for damage, which must be corrected immediately. Any sediment buildup will be removed and disposed of correctly. Sediment and subsequent vegetation will build up in the Level Spreader. This material will be cleaned out along with any gross solids and disposed of properly. (See invasive species below) Any rip rap that has been displaced from the original construction will be repaired, especially recreating the level lip.

Description: Infiltration Basins and the Infiltration component of some Rain Gardens, are constructed ponds that are intended to detain surface water runoff and during the detention to infiltrate runoff into the ground. Detention Ponds are also constructed ponds with the purpose of detaining runoff but not necessarily for infiltration purposes. During construction it is important that the ground surface not be exposed to traffic or construction equipment to preserve the infiltration capabilities of the existing soil. Construction specifications are included in the plan set and New Hampshire Stormwater Manual, Volume 2, 4-3 Treatment Practices, 3B, In-ground Infiltration Basin and Section 4-6, Conveyance Practices, 2. Detention Basins.

Maintenance Considerations:

Infiltration Basins and Detention Ponds should be inspected at least twice annually and following any rainfall event exceeding 0.25 inches in a twenty-four hour period. Maintenance rehabilitation will be conducted as warranted by each inspection. Trash and debris will be removed at each inspection.

On an annual basis the infiltration capabilities need to be confirmed by evaluation the drawdown time. If the infiltration system does not drain within 72-hours following a rainfall event, a qualified professional will assess the condition of the basin to determine measures required to restore the infiltration function. This is normally the direct result of sediment accumulation which will be removed to restore the filter media ratio.

Also on an annual basis the vegetation should be inspected to ensure healthy condition. Invasive species need to be removed along with dead or diseased vegetation.

Rolled Erosion Control Blanket

Description: Rolled Erosion Control Blankets, such as American Excelsior Company Curlex II, Curlex III, (or equal) or turf reinforcement such as North American Green V-Max C-350 (or equal) consist of interlocking fiber mesh, bio-degradable or permanent,

used to stabilize sloping earth while vegetation is being established. The product comes in rolls that are laid out over the earth, normally over-lapped, and secured to the soil by the use of anchors or staples. The RECB may be anchored in the earth at the top of the slope to prevent wash-out. Construction specifications are included in the plan set and New Hampshire Stormwater Manual, Volume 3, 4-1 Erosion Control Practices, Temporary Erosion Control Blanket

Construction Considerations: It is recommended that the blanket be installed in the same direction as the water flow or perpendicular to the slope. The manufacturer will recommend the amount of over-lap from one row to the next and on longer slopes between sections. Care must be taken that the RECB is laid directly on the earth / topsoil and that any existing vegetation not cause tenting as this will cause an issue with the blanket not staying in place. The staples or stakes are to be placed according to the manufacturer based on the slope of the receiving soil and forces that may be encountered. Care must be taken to utilize the correct product as specified. The choice of product are all different and in most cases are not interchangeable. NHDES or NH F&G may specify that some RECBs not be used in some applications.

Maintenance Considerations: RECBs will be inspected during the regular inspection schedule and any construction corrections made if the blanket is compromised.

Vegetated Stabilization

All areas that are disturbed during construction will be stabilized with vegetated material within 30 days of breaking ground. Construction will be managed in such a manner that erosion is prevented and that no abutter's property will be subjected to any siltation, unless otherwise permitted. All areas to be planted with grass for long-term cover will follow the specification and on Sheet E-102 using seeding mixture C, as follows:

Mixture	Pounds per Acre	Pounds per 1,000 Sq. Ft.
Tall Fescue	24	0.55
Creeping Red Fescue	24	0.55
Total	48	1.10

Conservation Mix

Mixture	Pounds per Acre	Pounds per 1,000 Sq. Ft.
Tall Fescue	15	0.35
Creeping Red Fescue	15	0.35
Annual Ryegrass	5	0.12
Perennial Ryegrass	5	0.12
Kentucky Bluegrass	15	0.35
White Clover	7	0.16
Total	62	1.45

Conservation Mix will be used to stabilize all 2:1 slopes and all land area disturbed within the wetland buffer. As the site is to be stabilized with erosion control mix as a mulch, the vegetation should be established with a high percentage of white clover for growth to be established.

Rain garden mix

The grass that is planted within a rain garden bio-filtration system within the bio-media must consist of a combination of warm season grass seed and cold season grass seed in order for the grass to start growing for stabilization and continue growing in the sandy well-drained environment. Planting specification will meet the requirements as outlined in 'Vegetation New Hampshire Sand and Gravel Pits' mix 1 (warm season grasses) (15 lbs/ac) and include annual and perennial rye grass seed (15 lbs/ac); the New England native warm season grass mix (23 lbs/ac) by New England Wetland Plants, Inc.; rain garden mix 180 (15 lbs/ac & 15 lbs/ac of rye) / rain garden grass mix 180-1 (20 lbs/ac & 10 lbs/ac of rye) by Ernst Conservation Seeds; or approved equal.

Detention Pond Mix:

The grass that is planted within a Detention Pond will be a mix designed for both inundation and dry conditions such as Ernst Seeds, Retention Basin Floor Mix ERNMX-126.

Subsurface Gravel Wetland Mix:

The grass that is planted within a Subsurface Gravel Wetland will be a diverse mix of species to provide food and cover as well as erosion control in the seasonally flooded conditions such as Ernst Seeds Seasonally Flooded Wildlife Mix ERNMX-128.

Stabilized Construction Entrance

A temporary gravel construction entrance provides an area where mud can be dislodged from tires before the vehicle leaves the construction site to reduce the amount of mud and sediment transported onto paved municipal and state roads. The stone size for the pad should be 3-inch coarse aggregate, and the pad itself constructed to a minimum length of 75' for the full width of the access road. The aggregate should be placed at least six inches thick. A plan view and profile are shown on Sheet E-102- Erosion and Sediment Control Detail Plan. Alternatives to the length and berm are demonstrated on the detail.

Environmental Dust Control

Dust will be controlled on the site by the use of multiple Best Management Practices. Mulching and temporary seeding will be the first line of protection to be utilized where problems occur. If dust problems are not solved by these applications, the use of water

and calcium chloride can be applied. Calcium chloride will be applied at a rate that will keep the surface moist but not cause pollution.

Drainage Swales / Stormwater Conveyance Channels

Drainage swales will be stabilized with vegetation for long term cover as outlined below, and on Sheet E-102 using seed mixture C. As a general rule, velocities in the swale should not exceed 3.0 feet per second for a vegetated swale although velocities as high as 4.5 FPS are allowed under certain soil conditions.

Outlet Protection

Outlet Protection consists of a riprap apron or preformed scour hole that is designed to provide velocity reduction of the surface water run-off that is leaving a culvert. The design is dependent on the culvert size, soil conditions, velocity, and quantity of the run-off. There are to be no bend or curves at the intersection of the conduit and apron. See sheet E-102 for details.

Rip Rap Level Spreader / Stone Berm Level Spreader

The purpose of the level spreader is to convert concentrated flow into sheet flow, for example from a rip rap outlet protection at the end of a culvert discharge pipe prior to discharge overland through a filter strip or buffer. Each level spreader is specifically designed based on the amount of flow and specified on the grading plan. Details for the level spreader can be found on Sheet E-102, detail E12 and page 162 in the referenced NH Stormwater Manual, Volume 2. The level spreader should be inspected after it is installed and stabilized for the deposit of sediment. Any sediment build-up will be removed and transported to a suitable location.

Stockpiled Sediment or Soil

Stockpiled materials including topsoil, excavated materials, borrow materials imported onto the site, construction aggregates, and sediment removed from temporary sediment traps will be located in designated areas at least 50 feet away from concentrated flows. All stockpiles will have erosion protection in the form of silt fence and diversion swales will be applied to protect the material and surrounding areas. Inactive stockpiles will be seeded for temporary stabilization. Erosion control measures will be inspected in accordance with the schedule for all other activities on site.

At a minimum, you must comply with following (EPA 2012 CGP Part 2.1.2.4d) "Do no hose down or sweep soil or sediment accumulated on pavement or other impervious surfaces into any stormwater conveyance (unless connected to a sediment basin, sediment trap, or similar effective control,) storm drain inlet, or surface water."

Dewatering Practices

Dewatering practices are not known to be required on this site. If during construction this becomes required, an addendum will be published specific for the requirements. As a general rule, ground water that needs to be removed from an excavation will be pumped to a sediment basin or a storm drain inlet prior to discharge from the site.

At a minimum, you must comply with following (EPA 2012 CGP Part 2.1.3.4) "With backwash water, either haul it away for disposal or return it to the beginning of the treatment process; and replace and clean the filter media used in dewatering devices when the pressure differential equals or exceeds the manufacturer's specifications."

Regarding dewatering practices in the State of New Hampshire, specifically see Construction General Permit Section 9.1.1 NHR12000 State of New Hampshire and "Clarification of Section 9.1.1 ... and other New Hampshire specific information for the U.S. EPA 2012 NPDES Construction General Permit (CGP), January 20, 2017"

Construction Sequence

1. Cut and remove trees in construction areas as directed or required.
2. Install Silt Fence and construct and/or install temporary and permanent sediment erosion and detention control facilities (Vegetated swales, level spreaders, and constructed filter strips), as required. Erosion, sediment and facilities shall be installed and stabilized prior to any earth moving operation, and prior to directing run-off to them.
3. Clear, grub, and dispose of debris in approved facilities.
4. Excavate and stockpile topsoil / loam. All disturbed areas shall be stabilized immediately after grading.
5. Construct the roadway and its associated drainage structures.
6. Begin permanent and temporary seeding and mulching. All cut and fill slopes and disturbed areas shall be seeded and mulched as required, or directed.
7. Daily, or as required, construct temporary berms, drainage ditches, sediment traps, etc. to prevent erosion on the site and prevent any siltation of abutting waters or property.
8. Inspect and maintain all erosion and sediment control measures during construction.

9. Complete permanent seeding and landscaping.
10. Remove temporary erosion control measures after seeding areas have established themselves and site improvements are complete. Smooth and re-vegetate all disturbed areas.
11. All swales and drainage structures will be constructed and stabilized prior to having run-off being directed to them.
12. Finish paving all roadways/parking.

Temporary Erosion Control Measures

1. The smallest practical area of land shall be exposed at any one time.
2. Erosion, sediment control measures shall be installed as shown on the plans and at locations as required, or directed by the engineer.
3. All disturbed areas shall be returned to original grades and elevations. Disturbed areas shall be loamed with a minimum of 4" of loam and seeded with not less than 1.10 pound of seed per 1,000 square feet (48 pounds per acre) of area.
4. Silt fences and other barriers shall be inspected periodically and after every rainstorm during the life of the project. All damaged areas shall be repaired, sediment deposits shall periodically be removed and properly disposed of.
5. After all disturbed areas have been stabilized, the temporary erosion control measures are to be removed and the area disturbed by the removal smoothed and re-vegetated.
6. Areas must be seeded and mulched within 5 days of final grading, permanently stabilized within 15 days of final grading, or temporarily stabilized within 30 days of initial disturbance of soil.

Inspection and Maintenance Schedule

Perimeter control will be inspected during and after storm events to ensure that the fence still has integrity and is not allowing sediment to pass. Depending on SWPPP criteria, all controls will be inspected once every 7 days and after storm events. Inspection reports must be submitted to Town of Barrington Planning Office. Sediment build-up in swales and level spreaders will be removed if it is deeper than six inches. See also Stormwater System Operation & Maintenance Plan and Inspection & Maintenance Manual published separately also by Berry Surveying & Engineering. See also Storm Water Pollution Prevention Plan (SWPPP) developed in accordance with EPA NPDES requirements.

Corrective Action measures will be made in accordance with SWPPP requirements and records maintained on site by the Contractor.

5.0 CONCLUSION

Peak rates of runoff are reduced in the model in the post-construction analysis / condition, as compared to the pre-construction peak rates of runoff flow at the final analysis point, with the exception noted in Final Reach 800, the permanent Svenson Pond which discharges into a stream that is perennial. The volume of runoff through the analysis conforms to the channel protection standards.

A Site Specific, Terrain Alteration Permit (RSA 485: A-17) is required for this site plan due to the area of disturbance being greater than 100,000 SF. Due to the nature of the cuts and fills associated with this proposed development, the owner is proposing to complete the project in one single phase and will have an environmental monitor responsible for weekly inspections. An EPA Notice of Intent will also be required for the construction process.

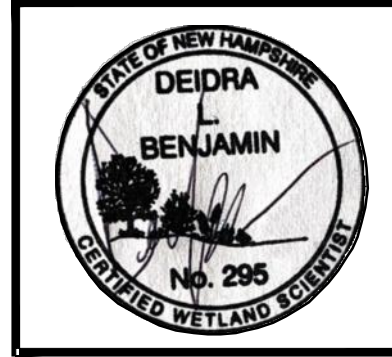
Respectfully Submitted,
BERRY SURVEYING & ENGINEERING



Christopher R. Berry, SIT 567
Principal, President



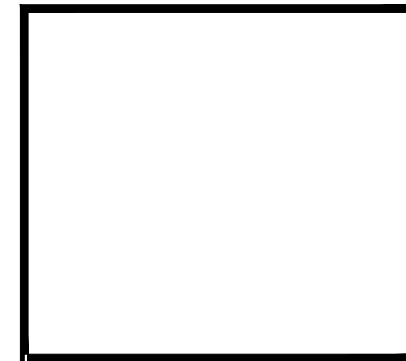
Kenneth A. Berry PE, LLS,
CPSWQ, CPESC, CESSWI
Principal, VP - Technical Operations



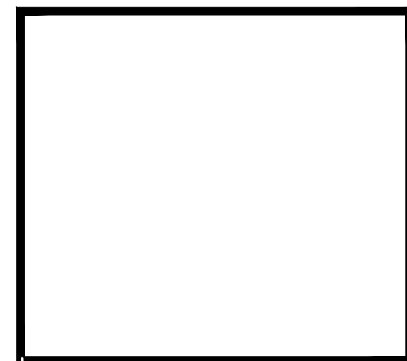
DEIDRA BENJAMIN, CWS #295

WETLAND NOTES:
WETLANDS LOCATED ON TAX MAP 235, LOT 1 & TAX MAP 239, LOT 2 WERE DELINEATED BY DEIDRA BENJAMIN, IN MAY OF 2017 AND CONFIRMED IN JUNE OF 2021 UTILIZING THE FOLLOWING STANDARDS:

1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).



JOHN P. HAYES III, CSS #87



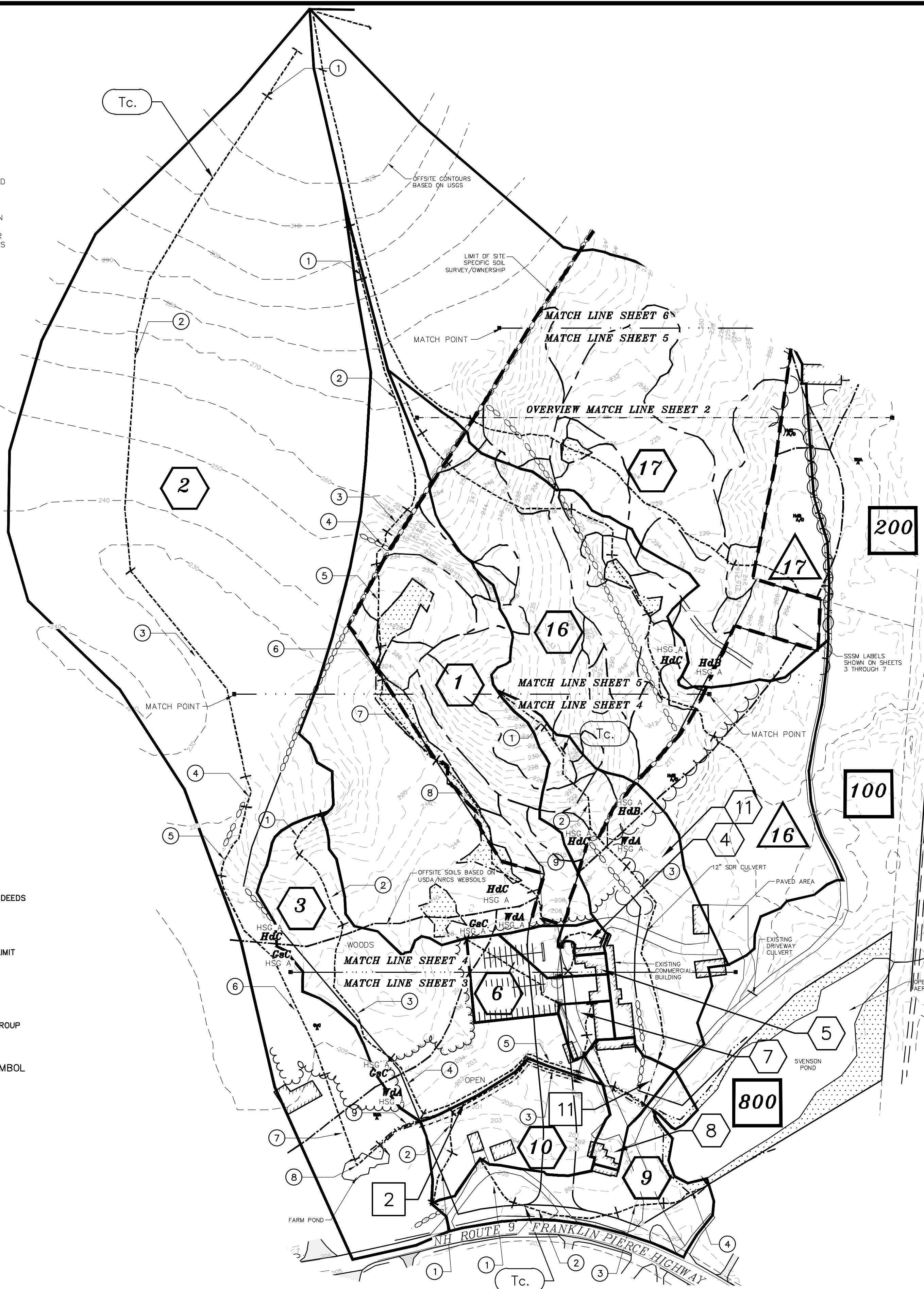
JOHN P. HAYES III, CWS #18

WETLAND NOTES:
WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:

1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

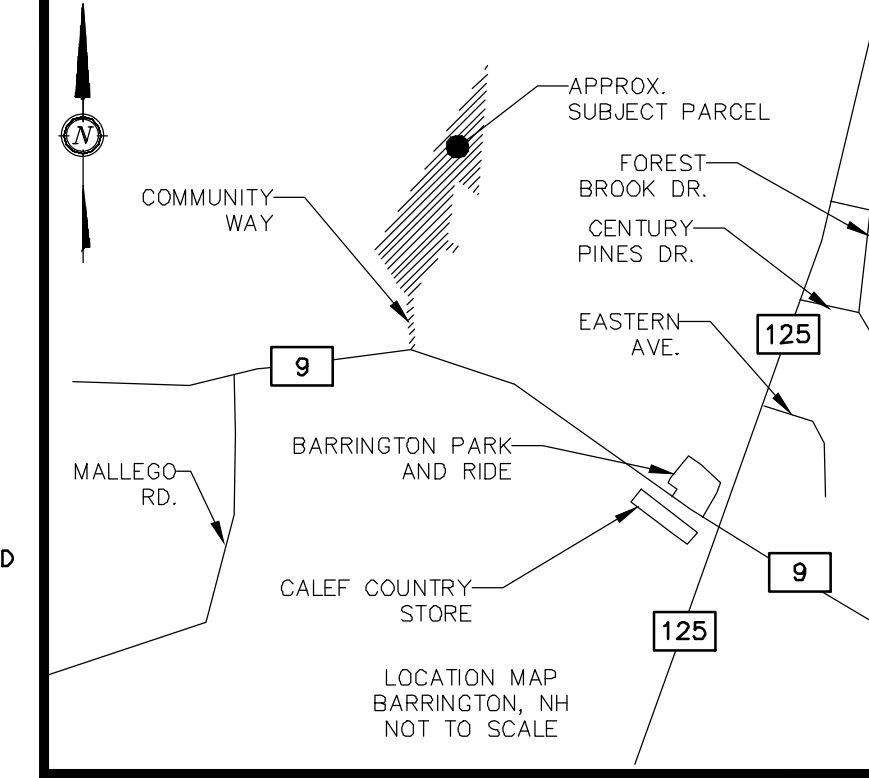
LEGEND:

- DRILL HOLE (FND)
- IRON PIPE (FND)
- IRON BOUND (FND)
- UTILITY POLE
- ⊕ WELL
- LOT LINE
- - - APPROXIMATE PROPERTY LINE
- - - EXISTING CONTOUR MINOR
- - - EXISTING CONTOUR MAJOR
- - - NRCS SOIL DELINEATION LINE
- STONE WALL
- WETLAND LINE
- 50' WETLAND BUFFER
- BUILDING SETBACK LINE
- OVERHEAD UTILITIES LINE
- STRAFFORD COUNTY REGISTRY OF DEEDS
- TYP. FND
- SITE SPECIFIC SOIL SURVEY LIMIT
- SITE SPECIFIC SOIL SURVEY SOIL LIMIT
- USDA NRCS SOILS
- LIMIT OF WATERSHEDS
- Tc PATH
- HfB/A SOIL LABEL / HYDROLOGIC SOIL GROUP
- # SUBCATCHMENT AREA SYMBOL
- # FLOW REACH SYMBOL
- # POND DEVICE SYMBOL
- Tc. Tc SEGMENT



NOTES:

- 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
B.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
- 2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
B.) TAX MAP 235, LOT 3
- 3.) LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
B.) 743,421 Sq. Ft., 17.07 Ac.
- 4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
B.) BOOK 4816, PAGE 504
- 5.) VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS.
HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
- 6.) THE INTENT OF THIS PLAN IS TO SHOW THE PRE-EXISTING CONDITIONS WATERSHEDS OF TAX MAP 235 LOT 1-1 AND TAX MAP 235 LOT 3.



SITE SPECIFIC SOILS LEGEND

SYMBOL	SOIL TAXONOMIC NAME	HYDROLOGIC SOIL GROUP
CsB	CHARLTON (VERY STONY)	B
CsC	CHARLTON (VERY STONY)	B
CsD	CHARLTON (VERY STONY)	B
CsE	CHARLTON (VERY STONY)	B
HcC	HOLLIS (VERY STONY)	C/D
HcD	HOLLIS (VERY STONY)	C/D
HcE	HOLLIS (VERY STONY)	C/D
HdD	HOLLIS CHARLTON COMPLEX (VERY STONY)	C/D
HdE	HOLLIS CHARLTON COMPLEX (VERY STONY)	C/D
LeB	LEICESTER (VERY STONY)	C
LeC	LEICESTER (VERY STONY)	C
LeD	LEICESTER (VERY STONY)	C
SuB	SUTTON	B
SuC	SUTTON	B
SuD	SUTTON	B

SLOPE: A = 0-3% B = 3-8% C = 8-15% D = 15-25% E = 25-50% F = 50%+

DENOMINATOR: /VPD = VERY POORLY DRAINED /PD = POORLY DRAINED /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED

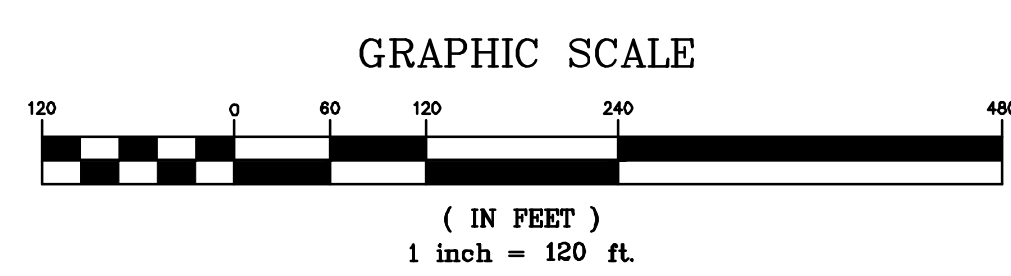
NRCS SOILS LEGEND

SYMBOL	SOIL TAXONOMIC NAME	HYDROLOGIC SOIL GROUP
HdB	HOLLIS-CHARLTON (VERY ROCKY)	A/D
HdC	HOLLIS-CHARLTON (VERY ROCKY)	A/D
Ml	MIXED ALLUVIAL LAND	D
WdA	WINDSOR	A
WdB	WINDSOR	A

SLOPE: A = 0-3% B = 3-8% C = 8-15% D = 15-25% E = 25-50% F = 50%+

DENOMINATOR: /VPD = VERY POORLY DRAINED /PD = POORLY DRAINED /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED

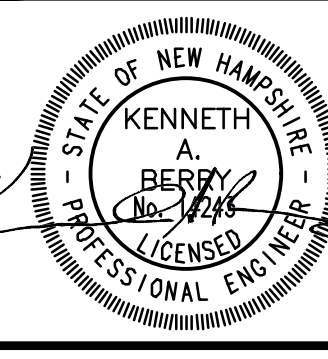
SUBCATCHMENTS 1 THROUGH 11, REACHES AND PONDS ASSOCIATED WITH FINAL REACH 800 WERE PREVIOUSLY SUBMITTED TO BARRINGTON FOR 1982 REAL ESTATE, LLC AND JOHN & LINDA SVENSON (CHRISTMAS DOVE)

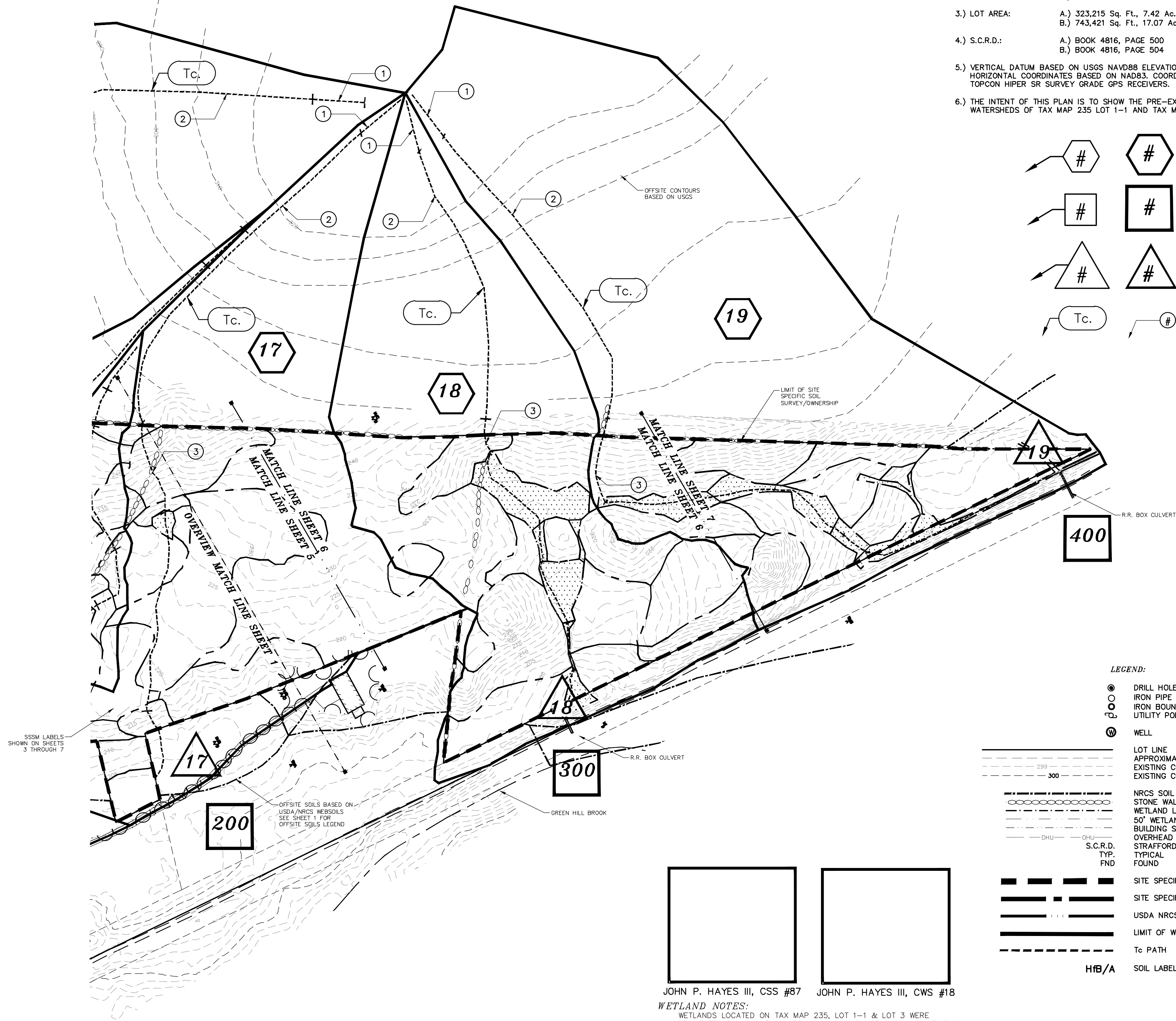
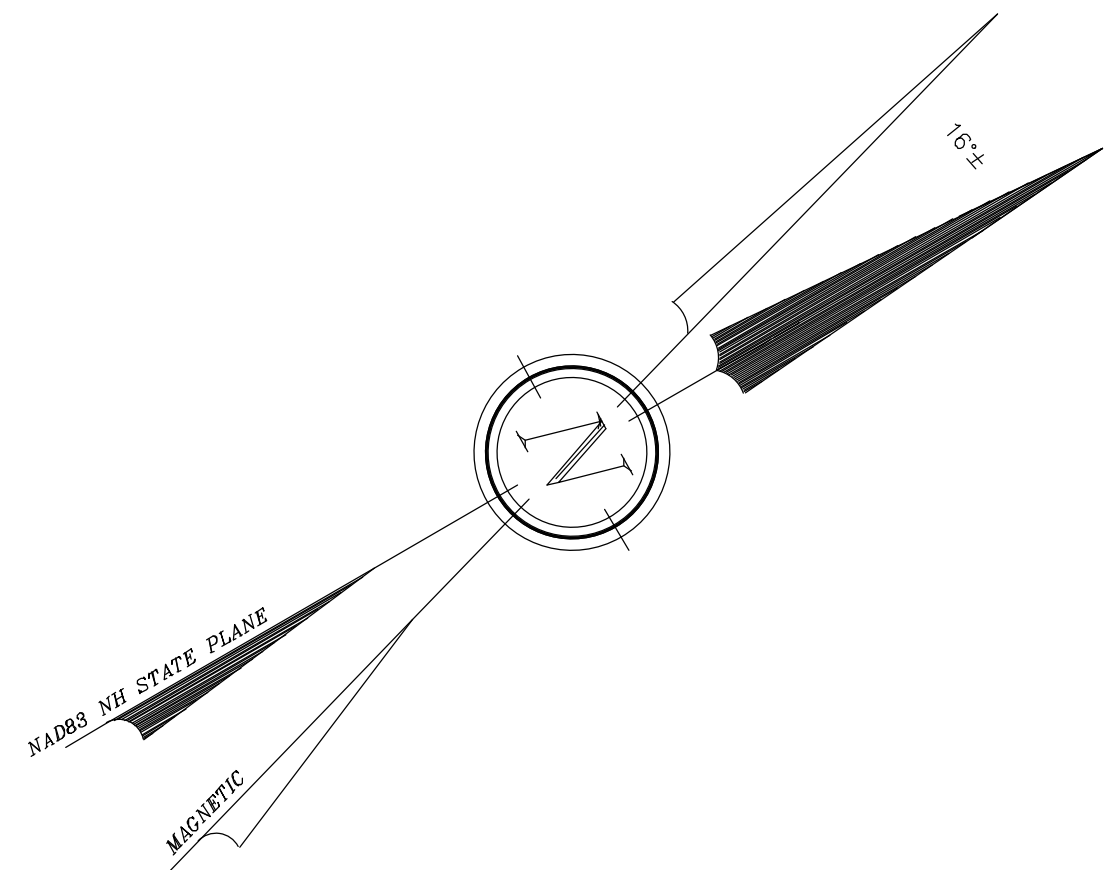
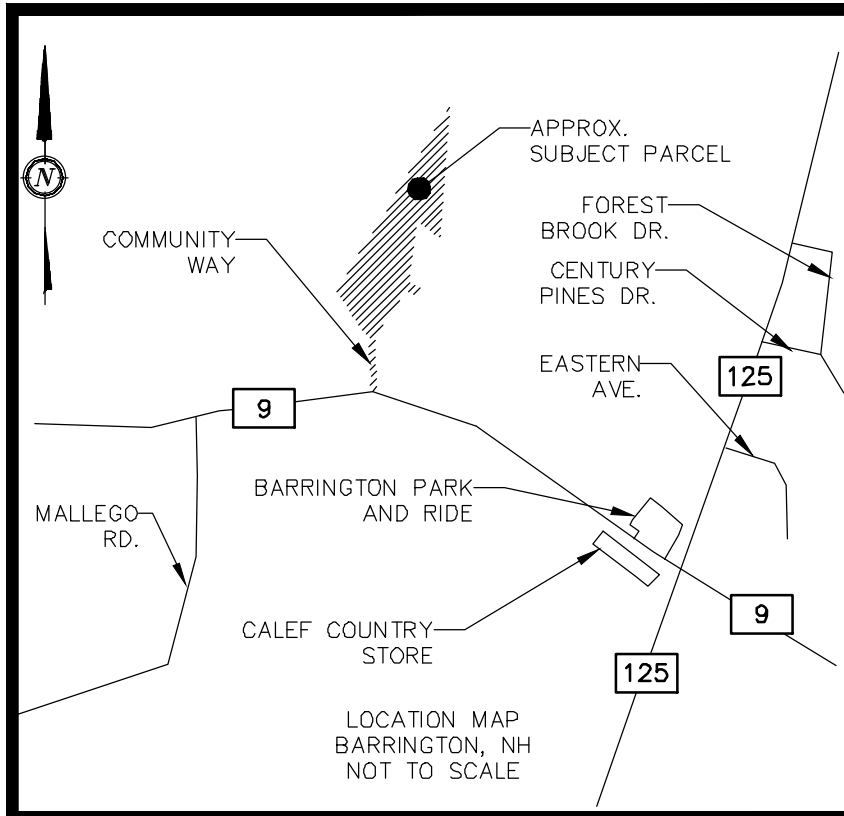


REVISION	DATE	DESCRIPTION

W-1 PRE-EXISTING CONDITIONS WATERSHED OVERVIEW PLAN
 LAND OF DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 COMMUNITY WAY
 BARRINGTON, NH
TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603)332-2863
 SCALE : 1 IN. EQUALS 120 FT.
 DATE : JUNE 14, 2021
 FILE NO. : DB 2020 - 097





SSSM LABELS
SHOWN ON SHEETS
3 THROUGH 7

OFFSITE SOILS BASED ON
USDA/NRCS WEBSOILS
SEE SHEET 1 FOR
OFFSITE SOILS LEGEND

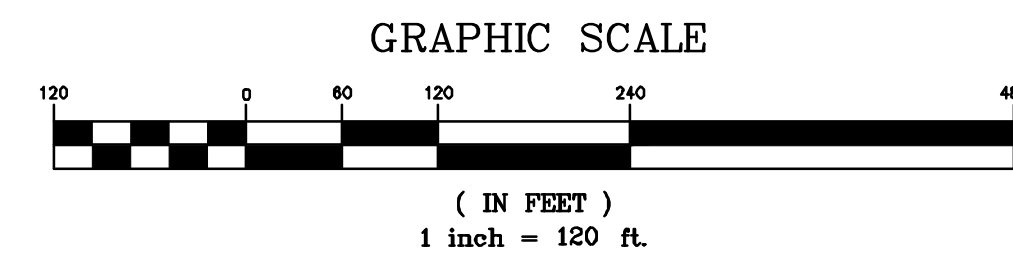
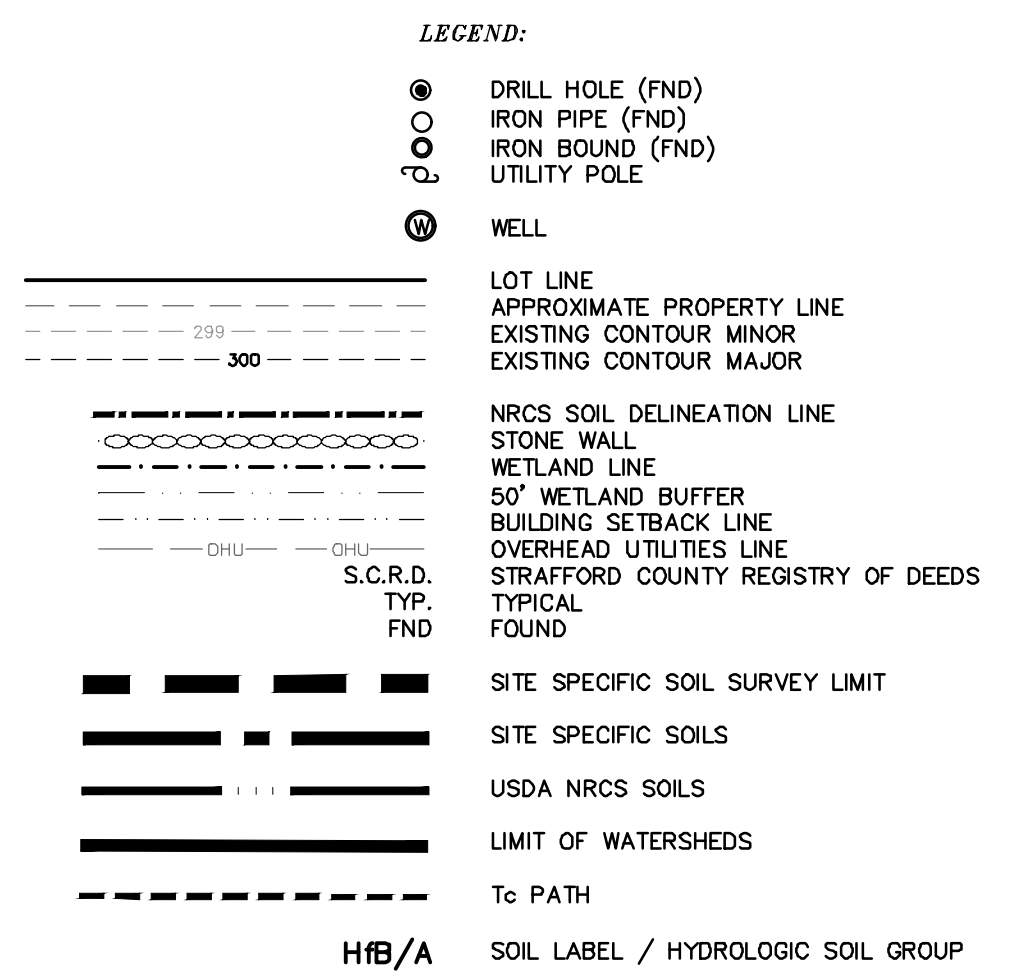
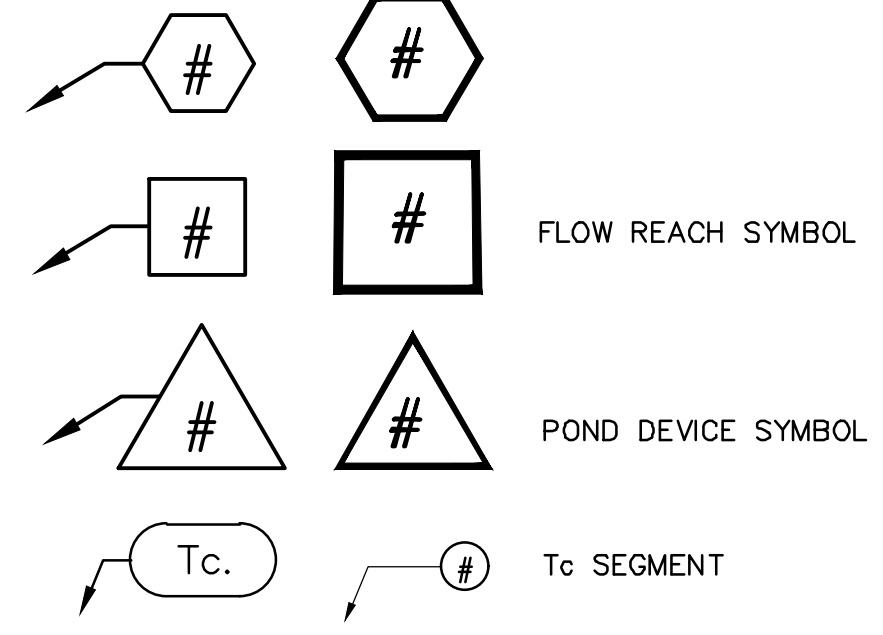
JOHN P. HAYES III, CSS #87

JOHN P. HAYES III, CWS #18

WETLAND NOTES:
WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE
DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING
THE FOLLOWING STANDARDS:

- REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
- FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
- NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

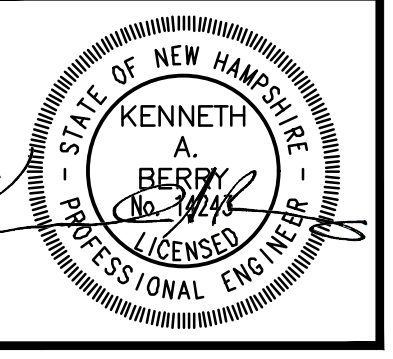
- NOTES:**
- OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
B.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
 - LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
B.) TAX MAP 235, LOT 3
 - LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
B.) 743,421 Sq. Ft., 17.07 Ac.
 - S.C.R.D.: A.) BOOK 4816, PAGE 500
B.) BOOK 4816, PAGE 504
 - VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS.
HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED USING
TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
 - THE INTENT OF THIS PLAN IS TO SHOW THE PRE-EXISTING CONDITIONS
WATERSHEDS OF TAX MAP 235 LOT 1-1 AND TAX MAP 235 LOT 3.

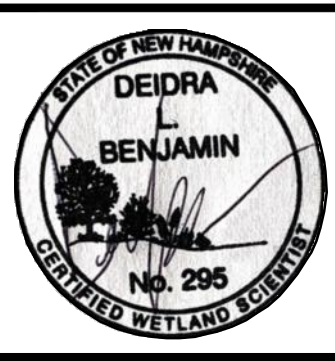


REVISION	DATE	DESCRIPTION

W-1 PRE-EXISTING CONDITIONS WATERSHED OVERVIEW PLAN
LAND OF
DOVE DEVELOPMENT GROUP, LLC
N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
COMMUNITY WAY
BARRINGTON, NH
TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863
SCALE : 1 IN. EQUALS 120 FT.
DATE : JUNE 14, 2021
FILE NO. : DB 2020 - 097





DEIDRA BENJAMIN, CWS #295

WETLAND NOTES:

WETLANDS LOCATED ON TAX MAP 235, LOT 1 & TAX MAP 239, LOT 2 WERE DELINEATED BY DEIDRA BENJAMIN, IN MAY OF 2017 AND CONFIRMED IN JUNE OF 2021 UTILIZING THE FOLLOWING STANDARDS:

1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

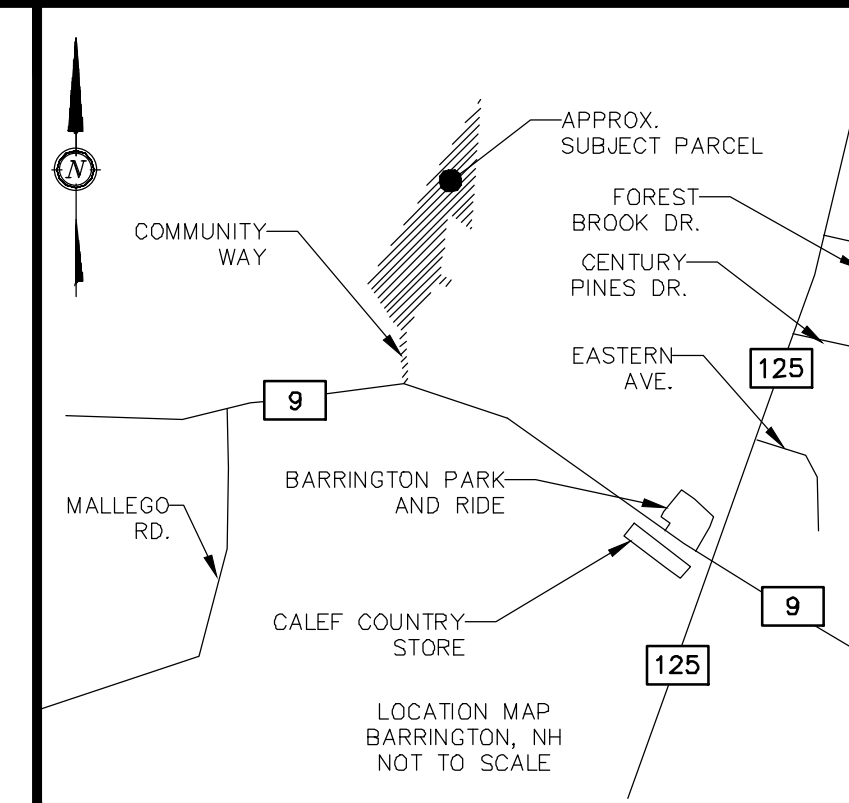
WETLAND NOTES:

WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:

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2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

JOHN P. HAYES III, CSS #87

JOHN P. HAYES III, CWS #18



NOTES:

- 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
B.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
- 2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
B.) TAX MAP 235, LOT 3
- 3.) LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
B.) 743,421 Sq. Ft., 17.07 Ac.
- 4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
B.) BOOK 4816, PAGE 504
- 5.) VERTICAL DATUM BASED ON USGS NAVD89 ELEVATIONS.
HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
- 6.) THE INTENT OF THIS PLAN IS TO SHOW THE EXISTING CONDITIONS WATERSHEDS OF TAX MAP 235 LOT 1-1 AND TAX MAP 235 LOT 3.

LEGEND:

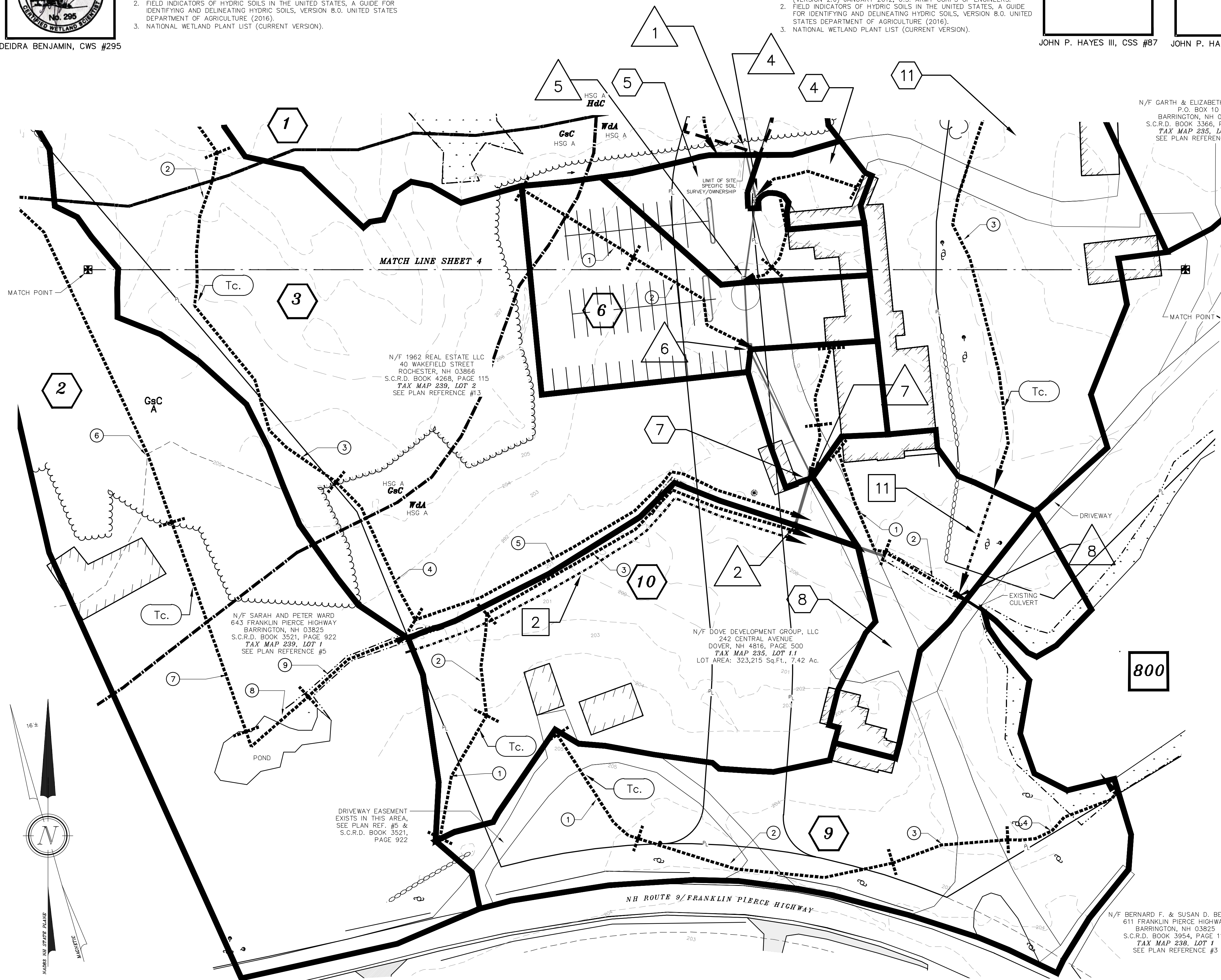
- ⊙ DRILL HOLE (FND)
- ⊖ IRON PIPE (FND)
- ⊕ IRON BOUND (FND)
- ⊗ UTILITY POLE
- ⊙ WELL
- LOT LINE
- - - APPROXIMATE PROPERTY LINE
- ⋯ EXISTING CONTOUR MINOR
- ⋯ EXISTING CONTOUR MAJOR
- NRCS SOIL DELINEATION LINE
- STONE WALL
- WETLAND LINE
- 50' WETLAND BUFFER
- BUILDING SETBACK LINE
- OVERHEAD UTILITIES LINE
- STRAFFORD COUNTY REGISTRY OF DEEDS
- S.C.R.D. TYP.
- FND
- SITE SPECIFIC SOIL SURVEY LIMIT
- SITE SPECIFIC SOIL SURVEY SOIL LIMIT
- USDA NRCS SOILS
- LIMIT OF WATERSHEDS
- Tc PATH
- H2B/A SOIL LABEL / HYDROLOGIC SOIL GROUP
- # SUBCATCHMENT AREA SYMBOL
- # FLOW REACH SYMBOL
- # POND DEVICE SYMBOL
- Tc. Tc SEGMENT

SUBCATCHMENTS 1 THROUGH 11, REACHES AND PONDS ASSOCIATED WITH FINAL REACH 800 WERE PREVIOUSLY SUBMITTED TO BARRINGTON FOR 1962 REAL ESTATE, LLC AND JOHN & LINDA SVENSON (CHRISTMAS DOVE)

GRAPHIC SCALE



(IN FEET)
1 inch = 40 ft.



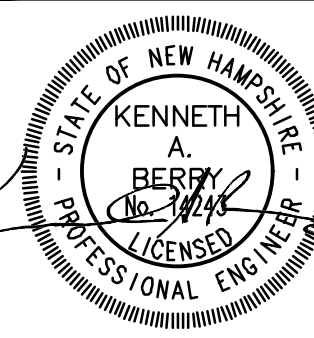
800

N/F BERNARD F. & SUSAN D. BENNETT
611 FRANKLIN PIERCE HIGHWAY
BARRINGTON, NH 03825
S.C.R.D. BOOK 3954, PAGE 119
TAX MAP 238, LOT 1
SEE PLAN REFERENCE #3

REVISION	DATE	DESCRIPTION

W-1 PRE-EXISTING WATERSHED DETAIL (SOUTH)
LAND OF
DOVE DEVELOPMENT GROUP, LLC
N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
COMMUNITY WAY
BARRINGTON, NH
TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863
SCALE : 1 IN. EQUALS 40 FT.
DATE : JUNE 14, 2021
FILE NO. : DB 2020 - 097

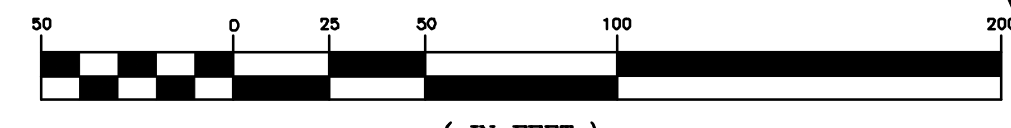


N/F DAVID R. & GLENDA J. HERDERSON
 UND INT LIV REV TRUST 1/2
 1272 WINGED FOOT LANE
 DENVER, NC 28037-6520
 S.C.R.D. BOOK 897, PAGE 121
 TAX MAP 235, LOT 1
 SEE PLAN REFERENCE #5

N/F 1962 REAL ESTATE LLC
 40 WAKEFIELD STREET
 ROCHESTER, NH 03866
 S.C.R.D. BOOK 4268, PAGE 115
 TAX MAP 239, LOT 2
 SEE PLAN REFERENCE #11 &
 #13

N/F GARTH & ELIZABETH SVENSON
 P.O. BOX 10
 BARRINGTON, NH 03825
 S.C.R.D. BOOK 3366, PAGE 451
 TAX MAP 235, LOT 2
 SEE PLAN REFERENCE #4

GRAPHIC SCALE



(IN FEET)

NOTES: 1 inch = 50 ft.

- 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 B.) DOVE DEVELOPMENT GROUP, LLC
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 DOVER, NH 03820
- 2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
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- 4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
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- 6.) THE INTENT OF THIS PLAN IS TO SHOW THE EXISTING CONDITIONS WATERSHEDS OF TAX MAP
 235 LOT 1-1 AND TAX MAP 235 LOT 3.

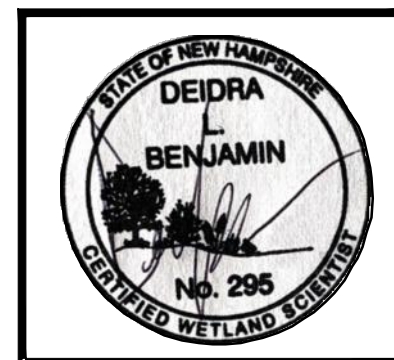
WETLAND NOTES:

- WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE
 DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING
 THE FOLLOWING STANDARDS:
1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND
 DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION,
 (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
 2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE
 FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED
 STATES DEPARTMENT OF AGRICULTURE (2016).
 3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

WETLAND NOTES:

- WETLANDS LOCATED ON TAX MAP 235, LOT 1 & TAX MAP 239, LOT 2
 WERE DELINEATED BY DEIDRA BENJAMIN, IN MAY OF 2017 AND CONFIRMED
 IN JUNE OF 2021 UTILIZING THE FOLLOWING STANDARDS:
1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND
 DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION
 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
 2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR
 IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED STATES
 DEPARTMENT OF AGRICULTURE (2016).
 3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

JOHN P. HAYES III, CSS #87
 JOHN P. HAYES III, CWS #18

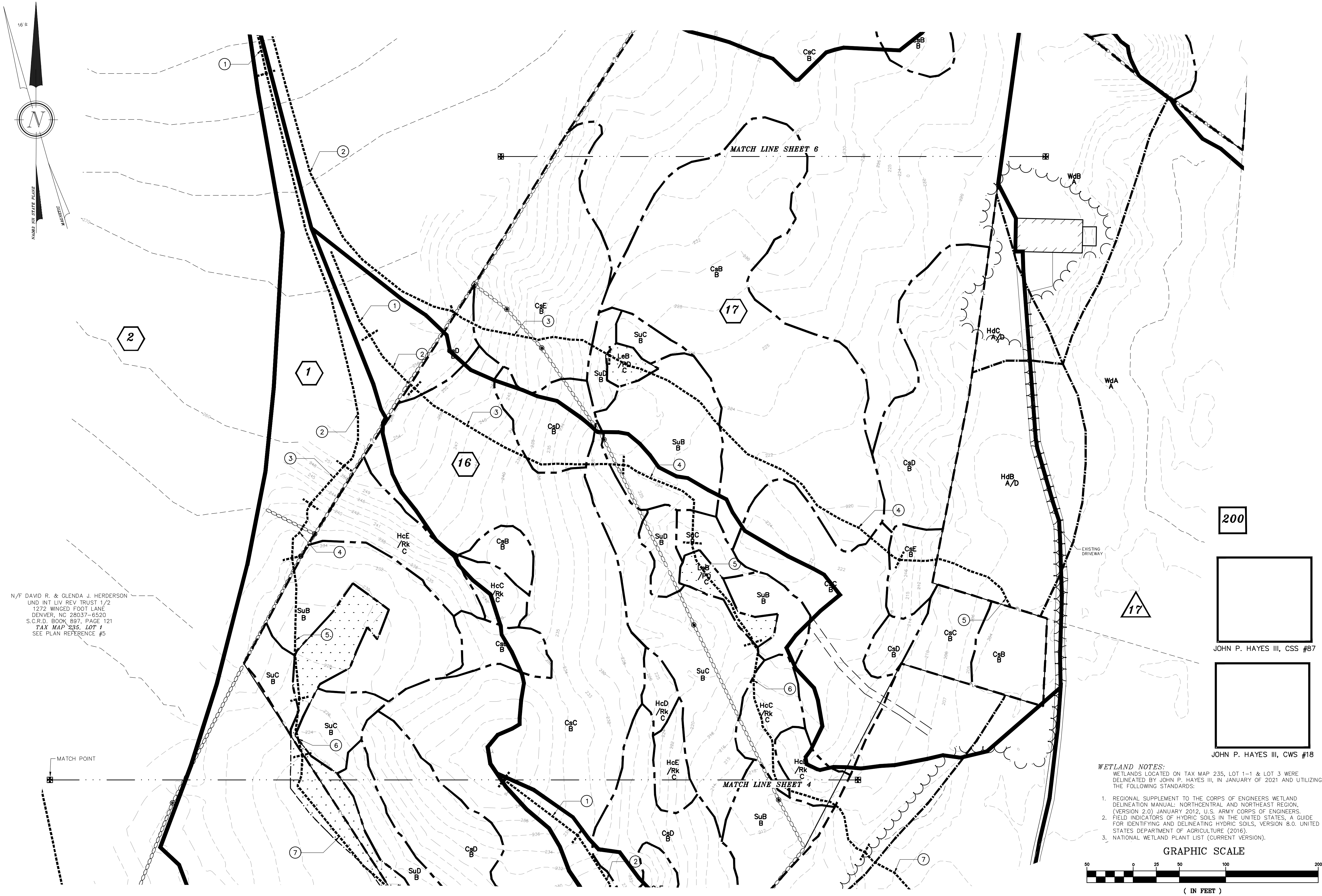


DEIDRA BENJAMIN, CWS #295

BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603)332-2863
 SCALE : 1 IN. EQUALS 50 FT.
 DATE : JUNE 14, 2021
 FILE NO. : DB 2020 - 097

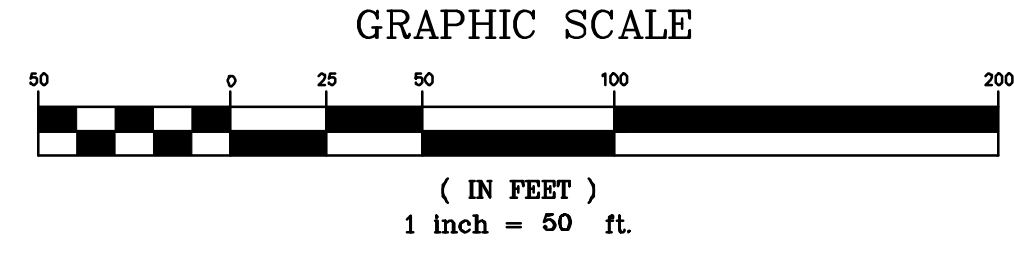
REVISION	DATE	DESCRIPTION

W-1 PRE-EXISTING WATERSHED DETAIL (MID)
 MADE UP OF
 DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 COMMUNITY WAY
 BARRINGTON, NH
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3



N/F DAVID R. & GLENDA J. HERDERSON
 UND INT LIV REV TRUST 1/2
 1272 WINGED FOOT LANE
 DENVER, CO 80037-6520
 S.C.R.D. BOOK 897, PAGE 121
 TAX MAP 235, LOT 1
 SEE PLAN REFERENCE #5

WETLAND NOTES:
 WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE
 DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING
 THE FOLLOWING STANDARDS:
 1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND
 DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION,
 (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
 2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE
 FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED
 STATES DEPARTMENT OF AGRICULTURE (2016).
 3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

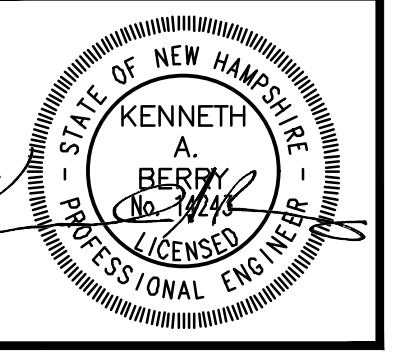


200
 17
 JOHN P. HAYES III, CSS #87
 JOHN P. HAYES III, CWS #18

REVISION	DATE	DESCRIPTION

W-1 PRE-EXISTING WATERSHED DETAIL (NORTH)
 LAND OF
 DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 COMMUNITY WAY
 BARRINGTON, NH
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603)332-2863
 SCALE : 1 IN. EQUALS 50 FT.
 DATE : JUNE 14, 2021
 FILE NO. : DB 2020 - 097



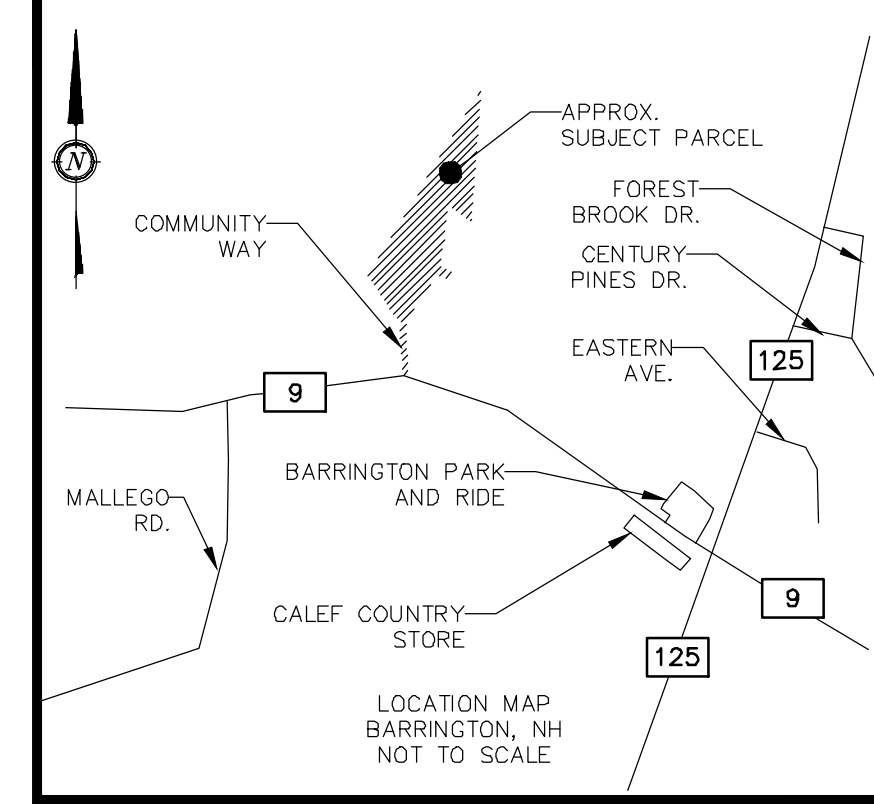
LEGEND:

- DRILL HOLE (FND)
- IRON PIPE (FND)
- IRON BOUND (FND)
- UTILITY POLE
- ⊙ WELL
- LOT LINE
- - - APPROXIMATE PROPERTY LINE
- EXISTING CONTOUR MINOR
- EXISTING CONTOUR MAJOR
- NRCS SOIL DELINEATION LINE
- STONE WALL
- WETLAND LINE
- 50' WETLAND BUFFER
- BUILDING SETBACK LINE
- OVERHEAD UTILITIES LINE
- S.C.R.D.
- TYP.
- FND
- SITE SPECIFIC SOIL SURVEY LIMIT
- SITE SPECIFIC SOIL SURVEY SOIL LIMIT
- USDA NRCS SOILS
- LIMIT OF WATERSHEDS
- Tc PATH
- HfB/A SOIL LABEL / HYDROLOGIC SOIL GROUP
- ⬠ # SUBCATCHMENT AREA SYMBOL
- ⬠ # FLOW REACH SYMBOL
- ⬠ # POND DEVICE SYMBOL
- Tc. Tc SEGMENT

N/F DAVID R. & GLENDA J. HERDERSON
 UND INT LIV REV TRUST 1/2
 1272 WINGED FOOT LANE
 DENVER, NC 28037-6520
 S.C.R.D. BOOK 897, PAGE 121
 TAX MAP 235, LOT 1
 SEE PLAN REFERENCE #5

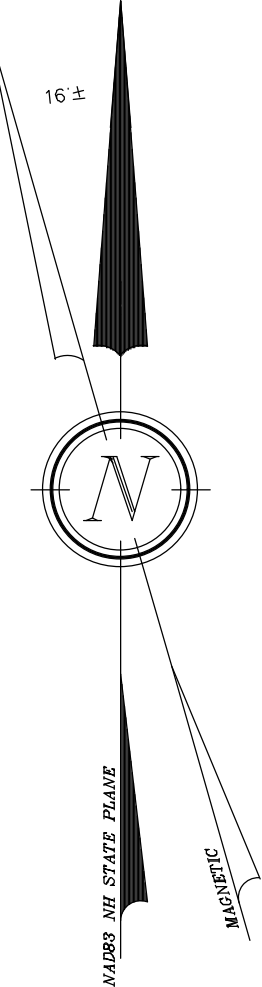
N/F KIMBERLY B & RONDI M BOYER
 P.O. BOX 387
 BARRINGTON, NH 03825-0387
 S.C.R.D. BOOK 4410, PAGE 800
 TAX MAP 235, LOT 4

N/F LINDA SVENSON
 P.O. BOX 10
 BARRINGTON, NH 03825-0010
 S.C.R.D. BOOK 4022, PAGE 576
 TAX MAP 235, LOT 3
 SEE PLAN REFERENCE #3



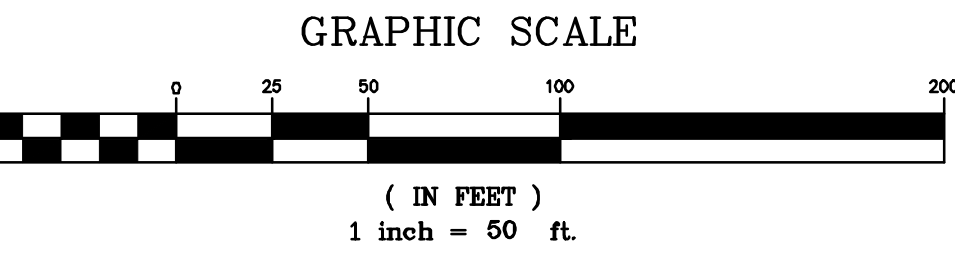
NOTES:

- 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 B.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
- 2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
 B.) TAX MAP 235, LOT 3
- 3.) LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
 B.) 743,421 Sq. Ft., 17.07 Ac.
- 4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
 B.) BOOK 4816, PAGE 504
- 5.) VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS.
 HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED
 USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
- 6.) THE INTENT OF THIS PLAN IS TO SHOW THE EXISTING CONDITIONS
 WATERSHEDS OF TAX MAP 235 LOT 1-1 AND TAX MAP 235 LOT 3.



300

JOHN P. HAYES III, CSS #87 JOHN P. HAYES III, CWS #18
WETLANDS NOTES:
 WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE
 DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING
 THE FOLLOWING STANDARDS:
 1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND
 DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION,
 (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
 2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE
 FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED
 STATES DEPARTMENT OF AGRICULTURE (2016).
 3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).



REVISION	DATE	DESCRIPTION

W-1 PRE-EXISTING WATERSHED DETAIL (NORTH)
 LAND OF
 DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 COMMUNITY WAY
 BARRINGTON, NH
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603)332-2863
 SCALE : 1 IN. EQUALS 50 FT.
 DATE : JUNE 14, 2021
 FILE NO. : DB 2020 - 097

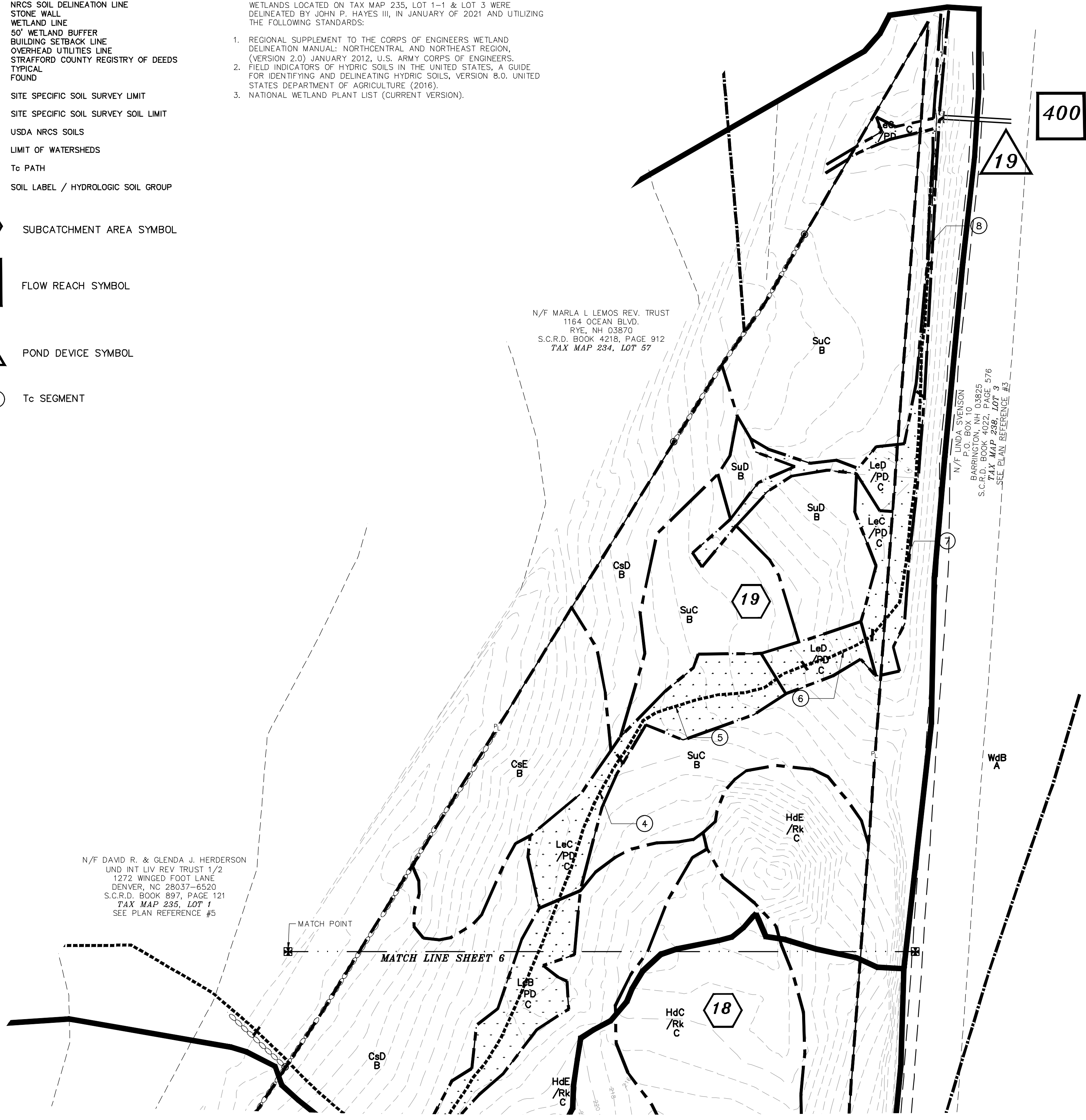
SHEET 6 OF 14

LEGEND:

- DRILL HOLE (FND)
- IRON PIPE (FND)
- IRON BOUND (FND)
- UTILITY POLE
- ⊙ WELL
- LOT LINE
- - - APPROXIMATE PROPERTY LINE
- EXISTING CONTOUR MINOR
- EXISTING CONTOUR MAJOR
- NRCS SOIL DELINEATION LINE
- STONE WALL
- WETLAND LINE
- 50' WETLAND BUFFER
- BUILDING SETBACK LINE
- OVERHEAD UTILITIES LINE
- S.C.R.D. TYP. FND
- STRAFFORD COUNTY REGISTRY OF DEEDS TYP. FND
- SITE SPECIFIC SOIL SURVEY LIMIT
- SITE SPECIFIC SOIL SURVEY SOIL LIMIT
- USDA NRCS SOILS
- LIMIT OF WATERSHEDS
- Tc PATH
- HtB/A SOIL LABEL / HYDROLOGIC SOIL GROUP
- # SUBCATCHMENT AREA SYMBOL
- # FLOW REACH SYMBOL
- # POND DEVICE SYMBOL
- Tc. Tc SEGMENT

JOHN P. HAYES III, CSS #87 JOHN P. HAYES III, CWS #18

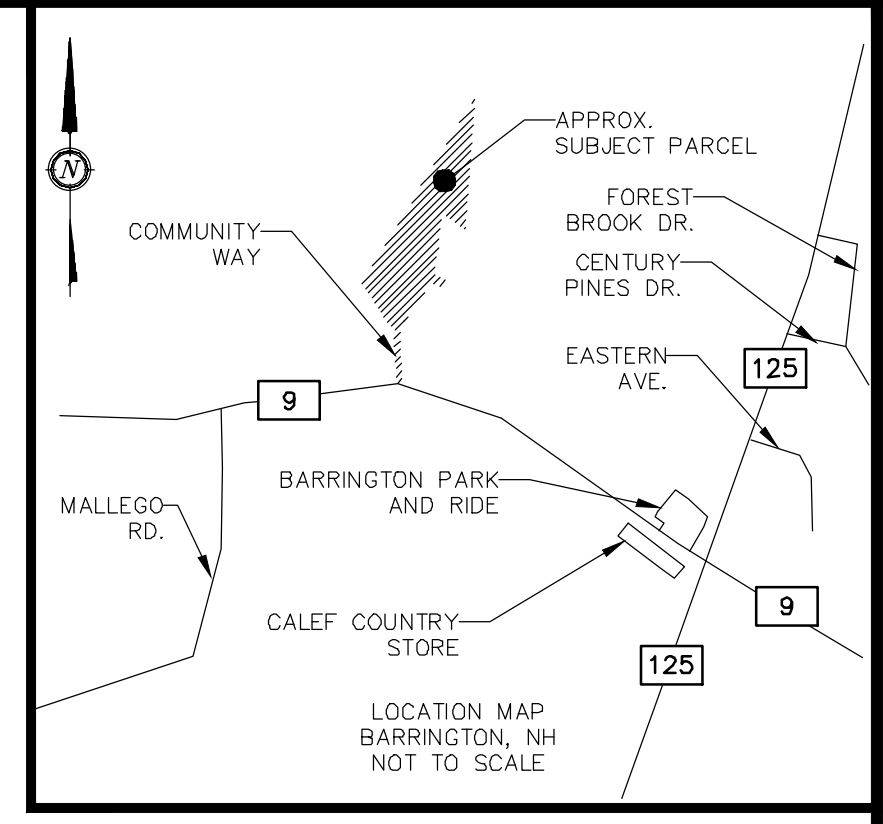
WETLAND NOTES:
 WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:
 1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
 2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
 3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).



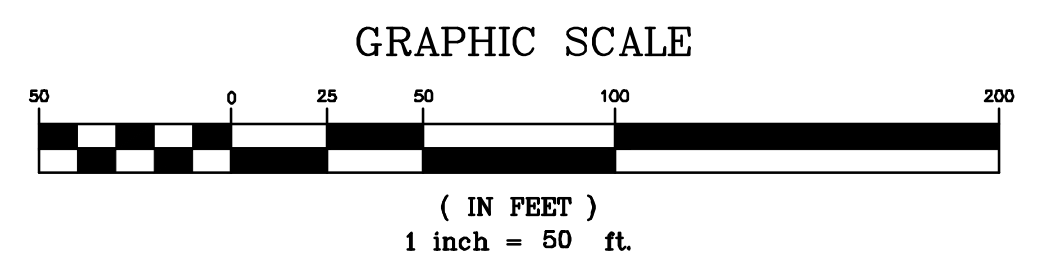
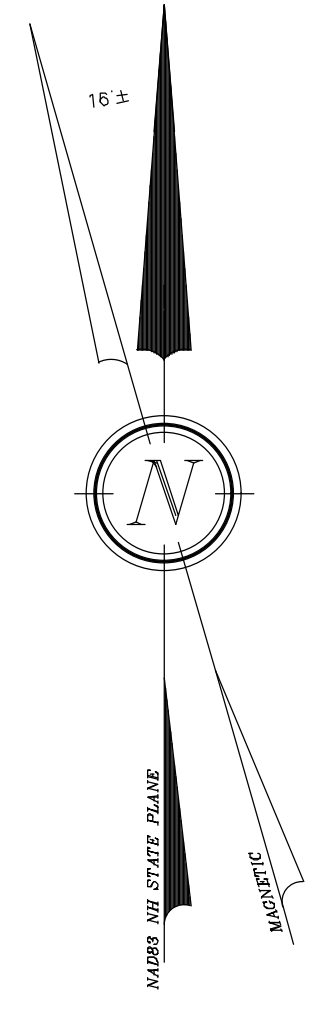
N/F DAVID R. & GLENDA J. HERDERSON
 UND INT LIV REV TRUST 1/2
 1272 WINGED FOOT LANE
 DENVER, CO 28037-6520
 S.C.R.D. BOOK 897, PAGE 121
 TAX MAP 235, LOT 1
 SEE PLAN REFERENCE #5

N/F MARLA L. LEMOS REV. TRUST
 1164 OCEAN BLVD.
 RYE, NH 03870
 S.C.R.D. BOOK 4218, PAGE 912
 TAX MAP 234, LOT 57

N/F TINA JOHNSON
 P.O. BOX 250
 BARRINGTON, NH 03825
 S.C.R.D. BOOK 4022, PAGE 576
 TAX MAP 235, LOT 3
 SEE PLAN REFERENCE #3



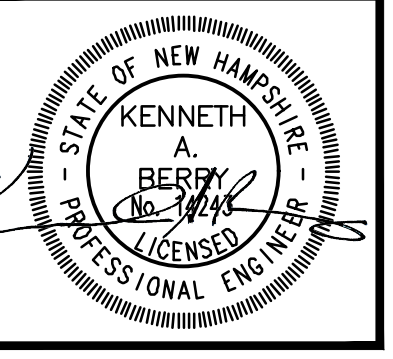
- NOTES:**
- 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 B.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 - 2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
 B.) TAX MAP 235, LOT 3
 - 3.) LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
 B.) 743,421 Sq. Ft., 17.07 Ac.
 - 4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
 B.) BOOK 4816, PAGE 504
 - 5.) VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS.
 HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
 - 6.) THE INTENT OF THIS PLAN IS TO SHOW THE EXISTING CONDITIONS WATERSHEDS OF TAX MAP 235 LOT 1-1 TAX MAP 235 LOT 3.

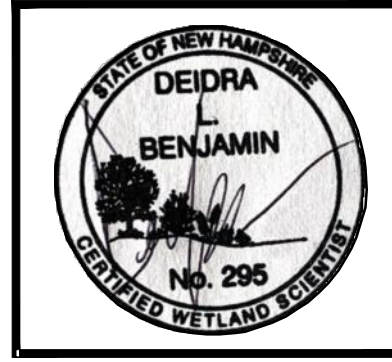


REVISION	DATE	DESCRIPTION

W-1 PRE-EXISTING WATERSHED DETAIL (NORTH)
 LAND OF
 DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 COMMUNITY WAY
 BARRINGTON, NH
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603)332-2863
 SCALE : 1 IN. EQUALS 50 FT.
 DATE : JUNE 14, 2021
 FILE NO. : DB 2020 - 097

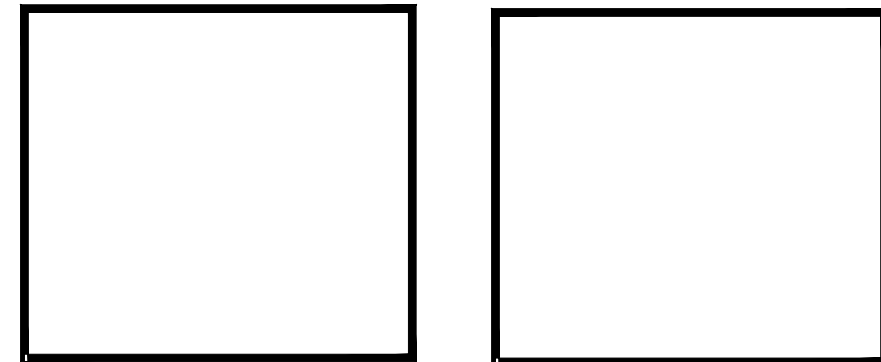




DEIDRA BENJAMIN, CWS #295

WETLAND NOTES:
WETLANDS LOCATED ON TAX MAP 235, LOT 1 & TAX MAP 239, LOT 2 WERE DELINEATED BY DEIDRA BENJAMIN, IN MAY OF 2017 AND CONFIRMED IN JUNE OF 2021 UTILIZING THE FOLLOWING STANDARDS:

1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).



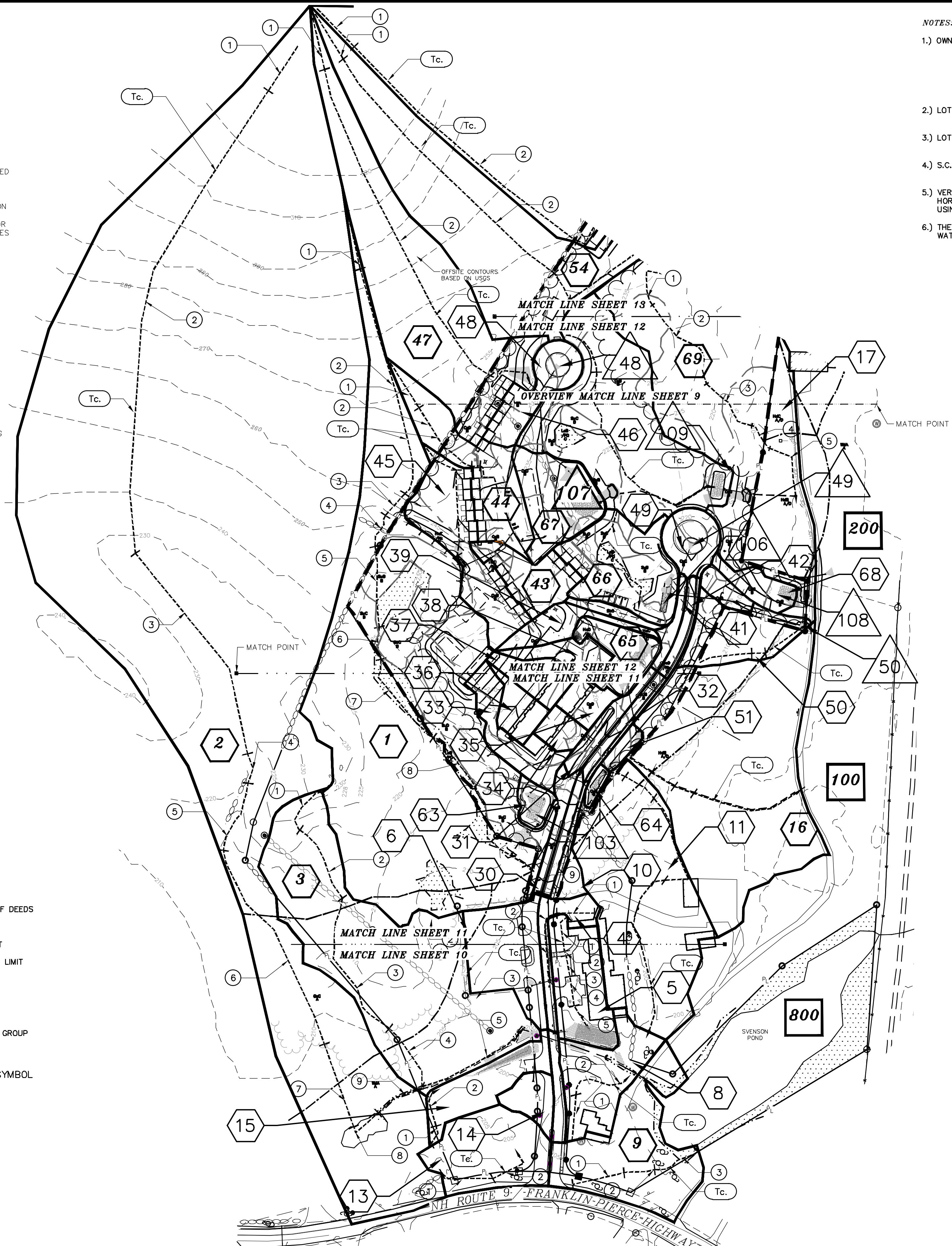
JOHN P. HAYES III, CSS #87 JOHN P. HAYES III, CWS #18

WETLAND NOTES:
WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:

1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

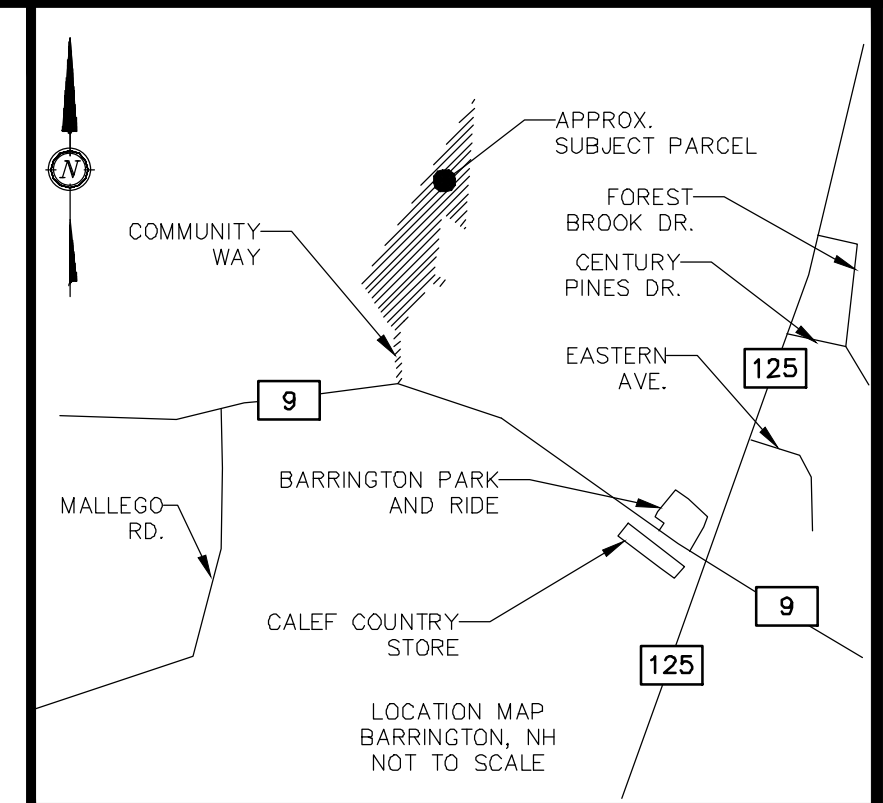
LEGEND:

- DRILL HOLE (FND)
- IRON PIPE (FND)
- IRON BOUND (FND)
- UTILITY POLE
- ⊙ WELL
- LOT LINE
- APPROXIMATE PROPERTY LINE
- EXISTING CONTOUR MINOR
- EXISTING CONTOUR MAJOR
- NRCS SOIL DELINEATION LINE
- STONE WALL
- WETLAND LINE
- 50' WETLAND BUFFER
- BUILDING SETBACK LINE
- OVERHEAD UTILITIES LINE
- STRAFFORD COUNTY REGISTRY OF DEEDS
- TYPICAL
- FND
- SITE SPECIFIC SOIL SURVEY LIMIT
- SITE SPECIFIC SOIL SURVEY SOIL LIMIT
- USDA NRCS SOILS
- LIMIT OF WATERSHEDS
- Tc PATH
- HtB/A SOIL LABEL / HYDROLOGIC SOIL GROUP
- # SUBCATCHMENT AREA SYMBOL
- # FLOW REACH SYMBOL
- # POND DEVICE SYMBOL
- Tc. Tc SEGMENT



NOTES:

- 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
B.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
- 2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
B.) TAX MAP 235, LOT 3
- 3.) LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
B.) 743,421 Sq. Ft., 17.07 Ac.
- 4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
B.) BOOK 4816, PAGE 504
- 5.) VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS.
HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
- 6.) THE INTENT OF THIS PLAN IS TO SHOW THE PROPOSED CONDITIONS WATERSHEDS OF TAX MAP 235 LOT 1-1 TAX MAP 235 LOT 3.



SITE SPECIFIC SOILS LEGEND

SYMBOL	SOIL TAXONOMIC NAME	HYDROLOGIC SOIL GROUP
CsB	CHARLTON (VERY STONY)	B
CsC	CHARLTON (VERY STONY)	B
CsD	CHARLTON (VERY STONY)	B
CsE	CHARLTON (VERY STONY)	B
HcC	HOLLIS (VERY STONY)	C/D
HcD	HOLLIS (VERY STONY)	C/D
HcE	HOLLIS (VERY STONY)	C/D
HdD	HOLLIS CHARLTON COMPLEX (VERY STONY)	C/D
HdE	HOLLIS CHARLTON COMPLEX (VERY STONY)	C/D
LeB	LEICESTER (VERY STONY)	C
LeC	LEICESTER (VERY STONY)	C
LeD	LEICESTER (VERY STONY)	C
SuB	SUTTON	B
	SUTTON	B
SuD	SUTTON	B

SLOPE: A = 0-3% B = 3-8% C = 8-15% D = 15-25% E = 25-50% F = 50%+

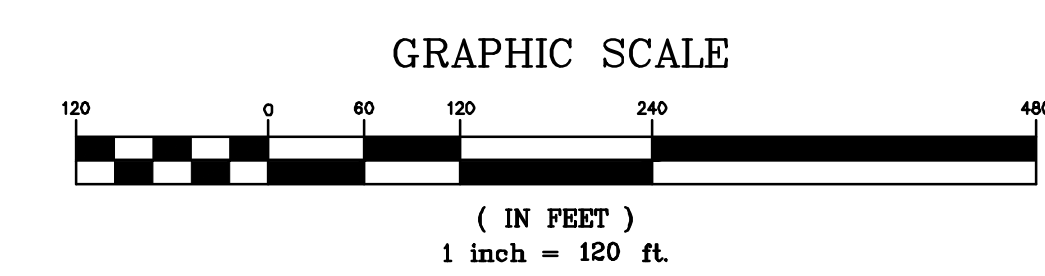
DENOMINATOR: /VPD = VERY POORLY DRAINED /PD = POORLY DRAINED /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED

NRCS SOILS LEGEND

SYMBOL	SOIL TAXONOMIC NAME	HYDROLOGIC SOIL GROUP
HdB	HOLLIS-CHARLTON (VERY ROCKY)	A/D
HdC	HOLLIS-CHARLTON (VERY ROCKY)	A/D
Ml	MIXED ALLUVIAL LAND	D
WdA	WINDSOR	A
WdB	WINDSOR	A

SLOPE: A = 0-3% B = 3-8% C = 8-15% D = 15-25% E = 25-50% F = 50%+

DENOMINATOR: /VPD = VERY POORLY DRAINED /PD = POORLY DRAINED /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED

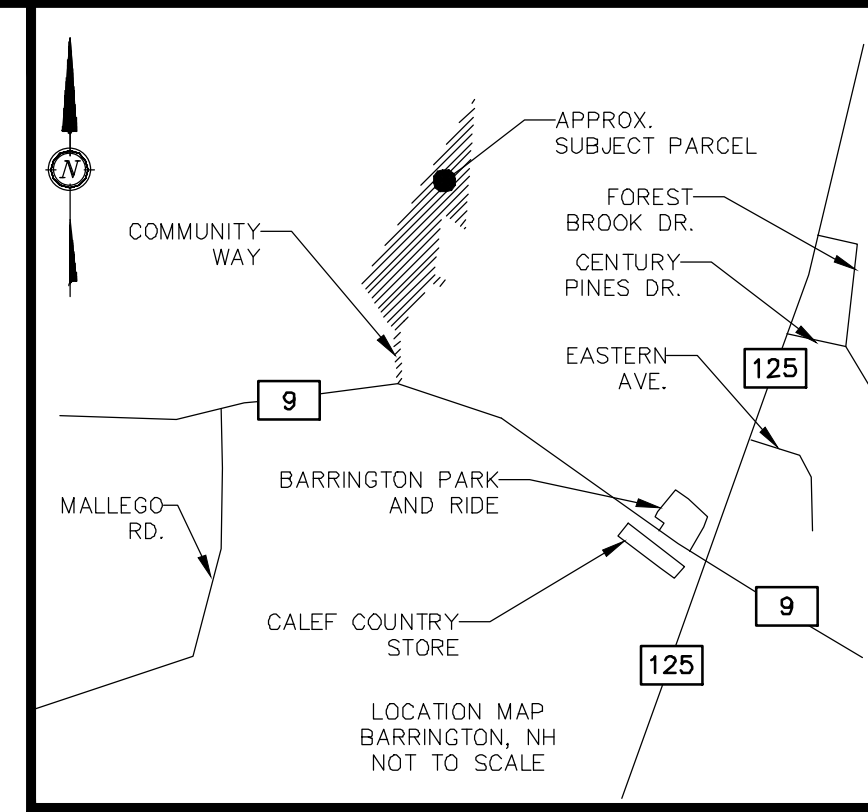
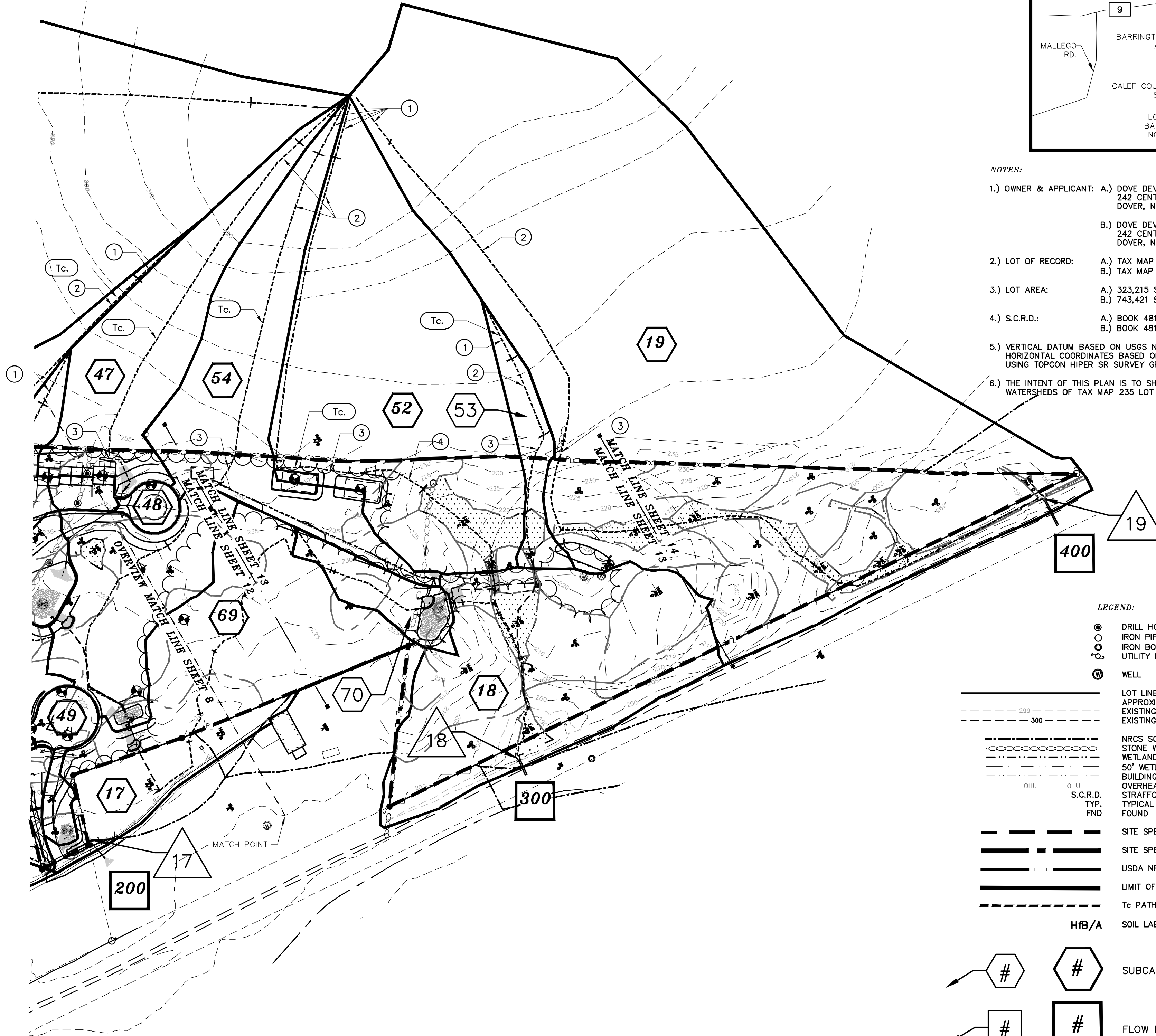
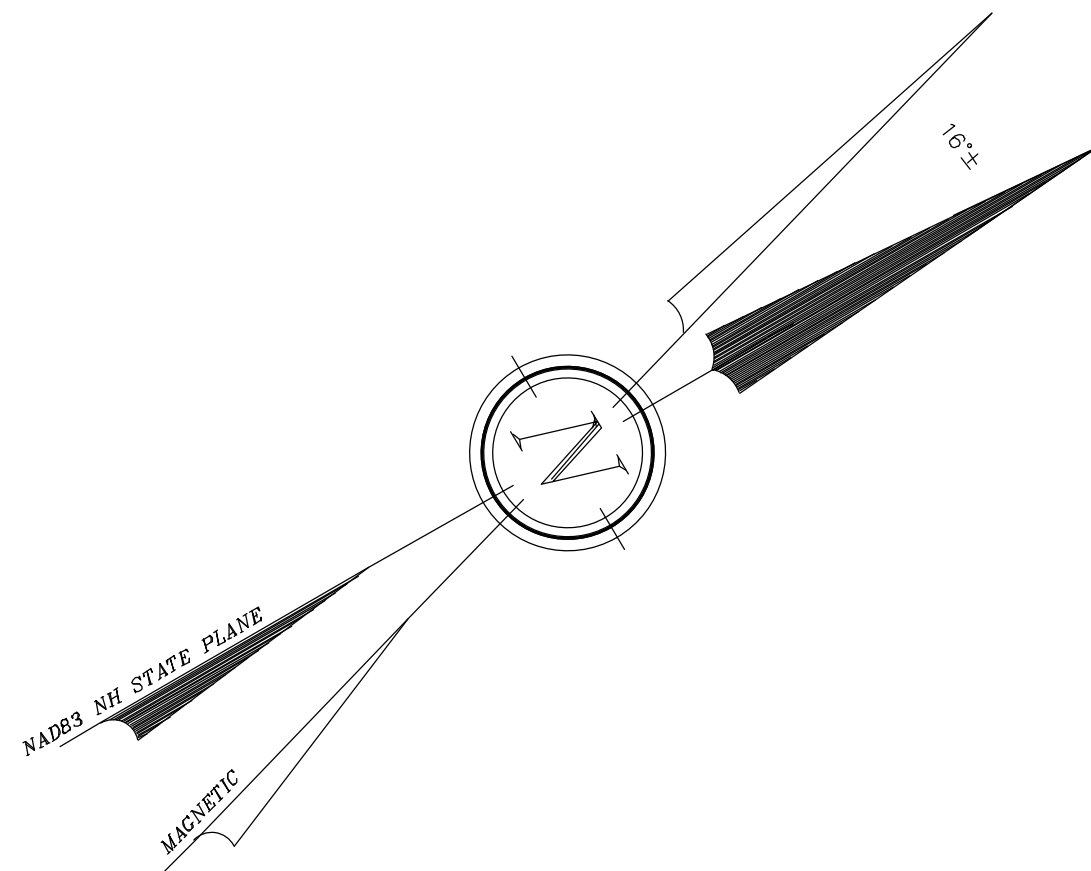


REVISION	DATE	DESCRIPTION

W-2 PROPOSED CONDITIONS WATERSHED OVERVIEW PLAN - SOUTH
LAND OF
DOVE DEVELOPMENT GROUP, LLC
N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
COMMUNITY WAY
BARRINGTON, NH
TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

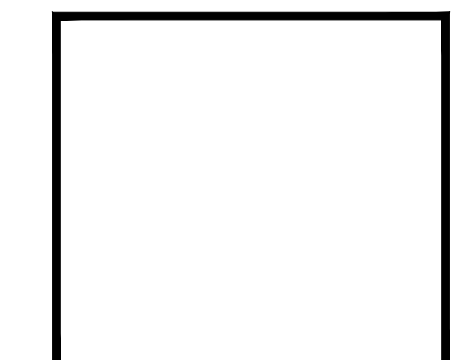
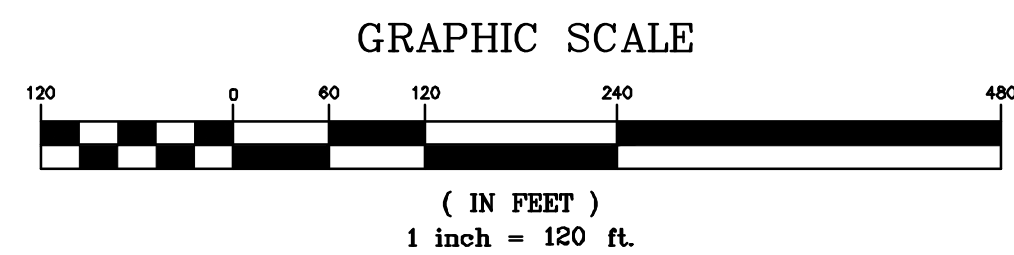
BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863
SCALE : 1 IN. EQUALS 120 FT.
DATE : JUNE 14, 2021
FILE NO. : DB 2020 - 097

SHEET 8 OF 14



- NOTES:**
- OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
B.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
 - LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
B.) TAX MAP 235, LOT 3
 - LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
B.) 743,421 Sq. Ft., 17.07 Ac.
 - S.C.R.D.: A.) BOOK 4816, PAGE 500
B.) BOOK 4816, PAGE 504
 - VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS.
HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED
USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
 - THE INTENT OF THIS PLAN IS TO SHOW THE PROPOSED CONDITIONS
WATERSHEDS OF TAX MAP 235 LOT 1-1 AND TAX MAP 235 LOT 3.

- LEGEND:**
- DRILL HOLE (FND)
 - IRON PIPE (FND)
 - IRON BOUND (FND)
 - UTILITY POLE
 - ⊙ WELL
 - LOT LINE
 - - - APPROXIMATE PROPERTY LINE
 - - - EXISTING CONTOUR MINOR
 - - - EXISTING CONTOUR MAJOR
 - NRCS SOIL DELINEATION LINE
 - STONE WALL
 - WETLAND LINE
 - 50' WETLAND BUFFER
 - BUILDING SETBACK LINE
 - OVERHEAD UTILITIES LINE
 - STRAFFORD COUNTY REGISTRY OF DEEDS
 - TYPICAL FOUND
 - SITE SPECIFIC SOIL SURVEY LIMIT
 - SITE SPECIFIC SOILS
 - USDA NRCS SOILS
 - LIMIT OF WATERSHEDS
 - - - Tc PATH
 - HtB/A SOIL LABEL / HYDROLOGIC SOIL GROUP
 - # SUBCATCHMENT AREA SYMBOL
 - # FLOW REACH SYMBOL
 - # POND DEVICE SYMBOL
 - Tc. Tc SEGMENT



JOHN P. HAYES III, CSS #87 JOHN P. HAYES III, CWS #18

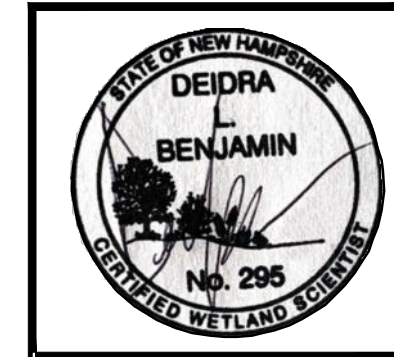
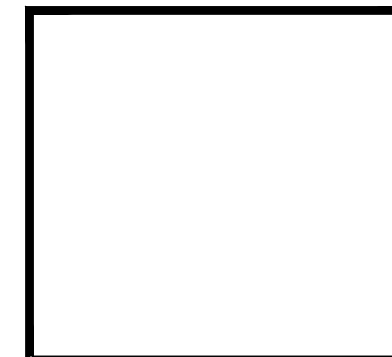
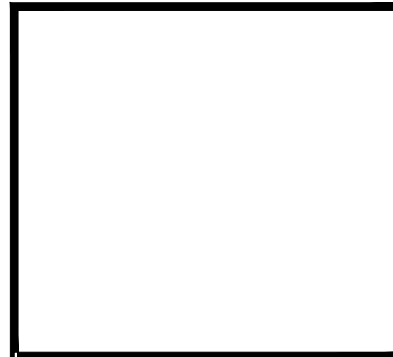
WETLAND NOTES:
WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE
DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING
THE FOLLOWING STANDARDS:

- REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND
DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION,
(VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
- FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE
FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED
STATES DEPARTMENT OF AGRICULTURE (2016).
- NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

REVISION	DATE	DESCRIPTION

W-2 PROPOSED CONDITIONS WATERSHED OVERVIEW PLAN - NORTH
LAND OF
DOVE DEVELOPMENT GROUP, LLC
N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
BARRINGTON, NH
TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863
SCALE : 1 IN. EQUALS 120 FT.
DATE : JUNE 14, 2021
FILE NO. : DB 2020 - 097



JOHN P. HAYES III, CSS #87

JOHN P. HAYES III, CWS #18

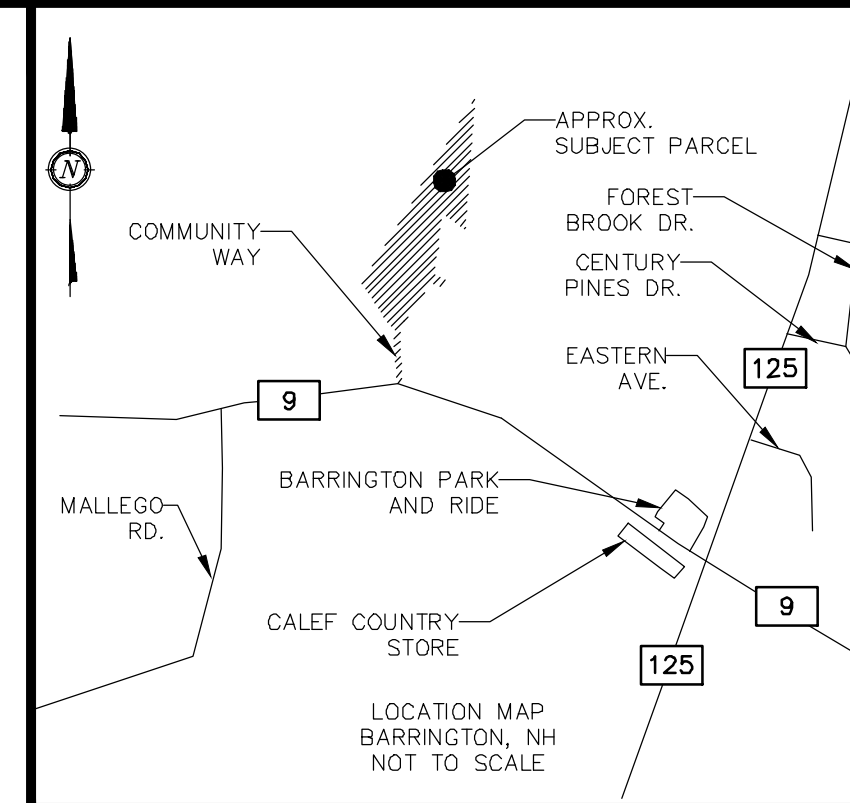
DEIDRA BENJAMIN, CWS #295

WETLAND NOTES: WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:

- 1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

WETLAND NOTES: WETLANDS LOCATED ON TAX MAP 235, LOT 1 & TAX MAP 239, LOT 2 WERE DELINEATED BY DEIDRA BENJAMIN, IN MAY OF 2017 AND CONFIRMED IN JUNE OF 2021 UTILIZING THE FOLLOWING STANDARDS:

- 1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0. UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).



- NOTES:
1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
3.) LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
5.) VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS.
6.) THE INTENT OF THIS PLAN IS TO SHOW THE PROPOSED CONDITIONS WATERSHEDS OF TAX MAP 235 LOT 1-1 AND TAX MAP 235 LOT 3.

- Legend symbols for: DRILL HOLE (FND), IRON PIPE (FND), IRON BOUND (FND), UTILITY POLE, WELL, LOT LINE, APPROXIMATE PROPERTY LINE, EXISTING CONTOUR MINOR, EXISTING CONTOUR MAJOR, NRCS SOIL DELINEATION LINE, STONE WALL, WETLAND LINE, 50' WETLAND BUFFER, BUILDING SETBACK LINE, OVERHEAD UTILITIES LINE, STRAFFORD COUNTY REGISTRY OF DEEDS, TYPICAL, FND, SITE SPECIFIC SOIL SURVEY LIMIT, USDA NRCS SOILS, LIMIT OF WATERSHEDS, Tc PATH, SOIL LABEL / HYDROLOGIC SOIL GROUP.

- Legend symbols for: SUBCATCHMENT AREA SYMBOL, FLOW REACH SYMBOL, POND DEVICE SYMBOL, Tc SEGMENT.

Subcatchments 1 through 11, reaches and ponds associated with final reach 800 were previously submitted to Barrington for 1982 Real Estate, LLC and John & Linda Svenson (Christmas Dove)

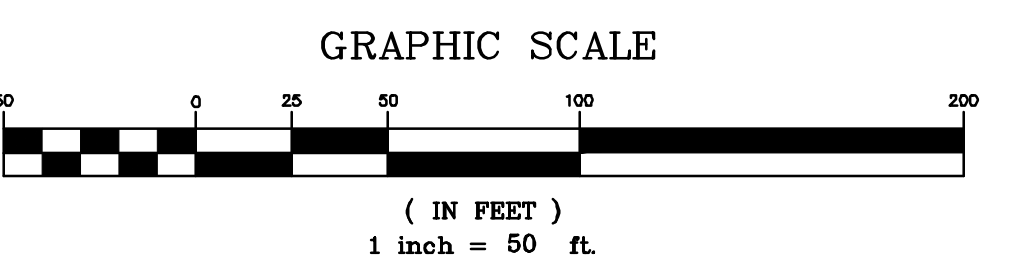
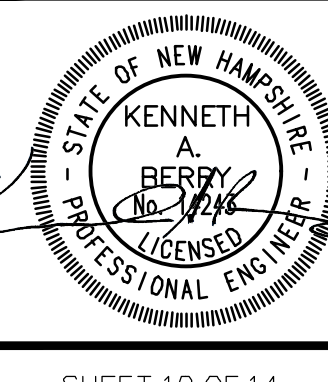
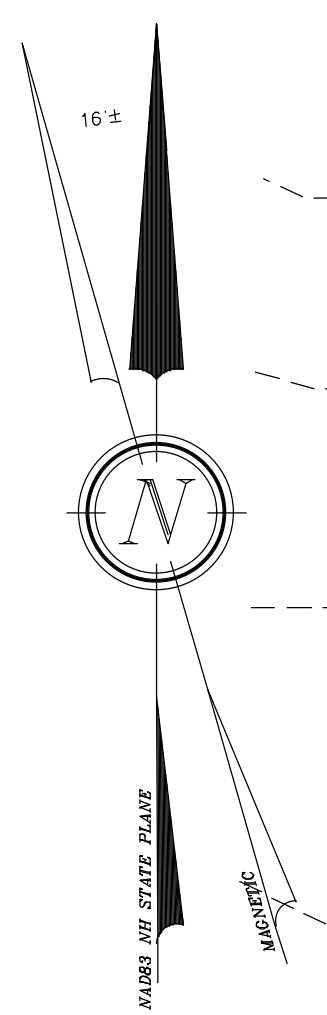


Table with 3 columns: REVISION, DATE, DESCRIPTION

W-2 PROPOSED WATERSHED DETAIL
DOVE DEVELOPMENT GROUP, LLC
N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
COMMUNITY WAY
BARRINGTON, NH
TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

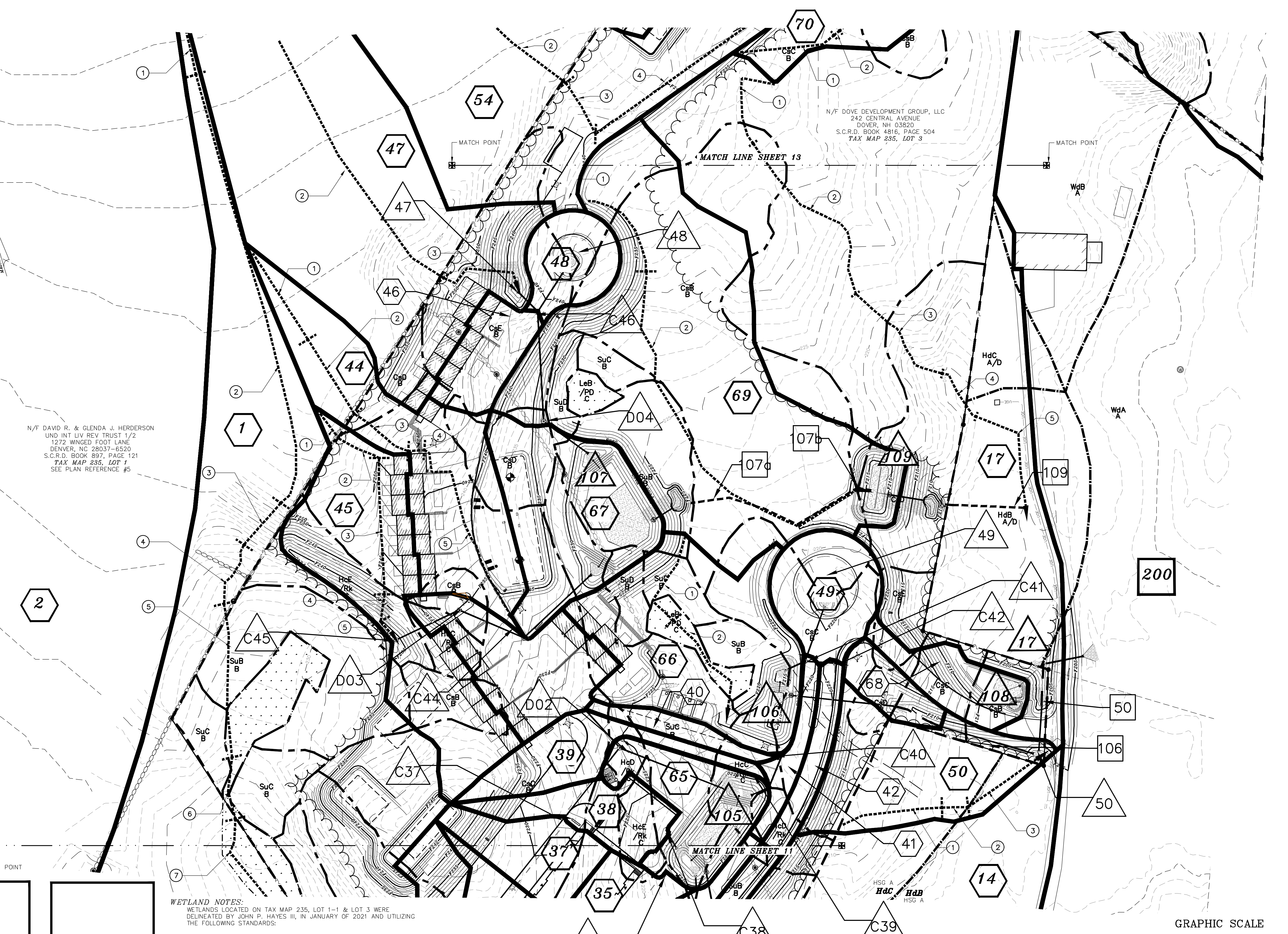
BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863
SCALE: 1 IN. EQUALS 50 FT.
DATE: JUNE 14, 2021
FILE NO.: DB 2020 - 097





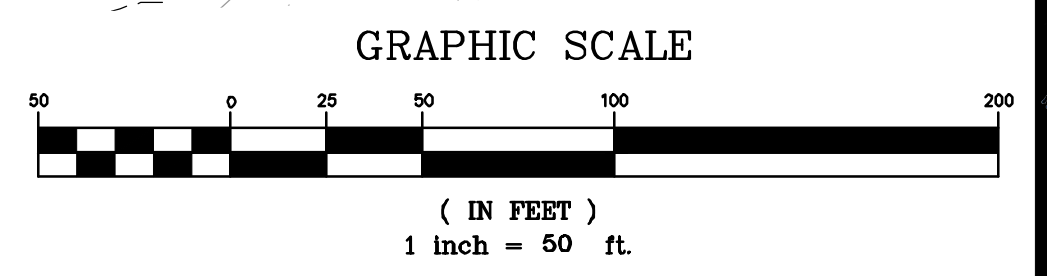
N/F DAVID R. & GLENDA J. HERDERSON
 UND INT LIV REV TRUST 1/2
 1272 WINGED FOOT LANE
 DENVER, NC 28037-6520
 S.C.R.D. BOOK 897, PAGE 121
 TAX MAP 235, LOT 1
 SEE PLAN REFERENCE #5

N/F DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVENUE
 DOVER, NH 03820
 S.C.R.D. BOOK 4816, PAGE 504
 TAX MAP 235, LOT 3



- WETLAND NOTES:**
 WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE
 DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING
 THE FOLLOWING STANDARDS:
1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
 2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 3.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
 3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

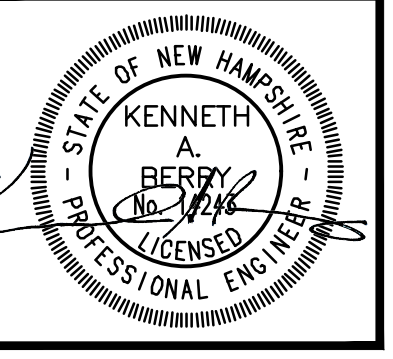
JOHN P. HAYES III, CSS #87 JOHN P. HAYES III, CWS #18



REVISION	DATE	DESCRIPTION

W-2 PROPOSED WATERSHED DETAIL
 LAND OF
 DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 COMMUNITY WAY
 BARRINGTON, NH
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603)332-2863
 SCALE : 1 IN. EQUALS 50 FT.
 DATE : JUNE 14, 2021
 FILE NO. : DB 2020 - 097



LEGEND:

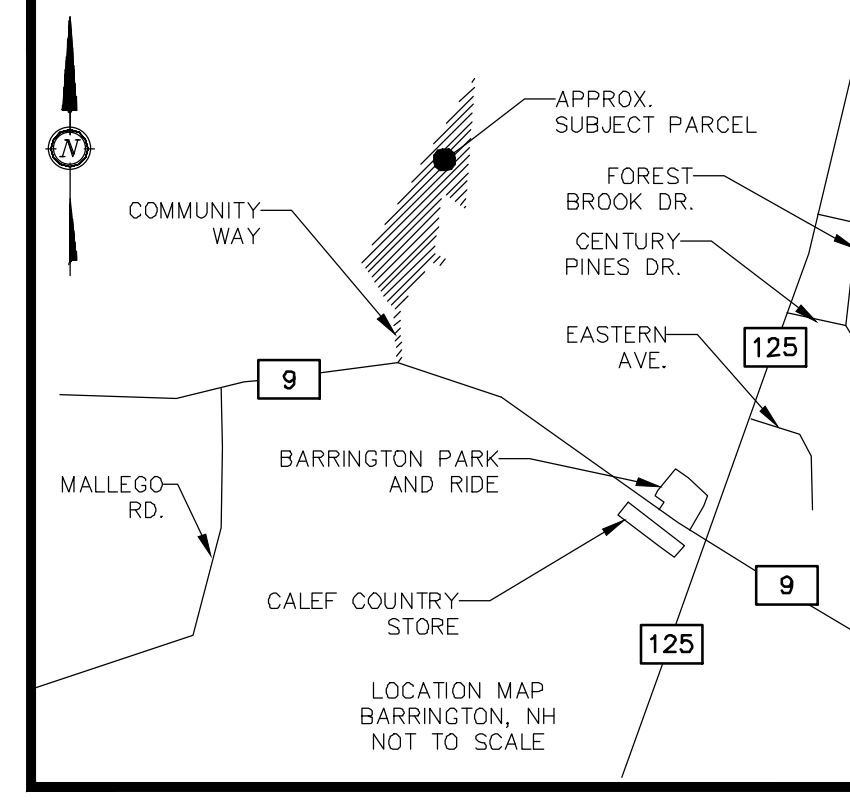
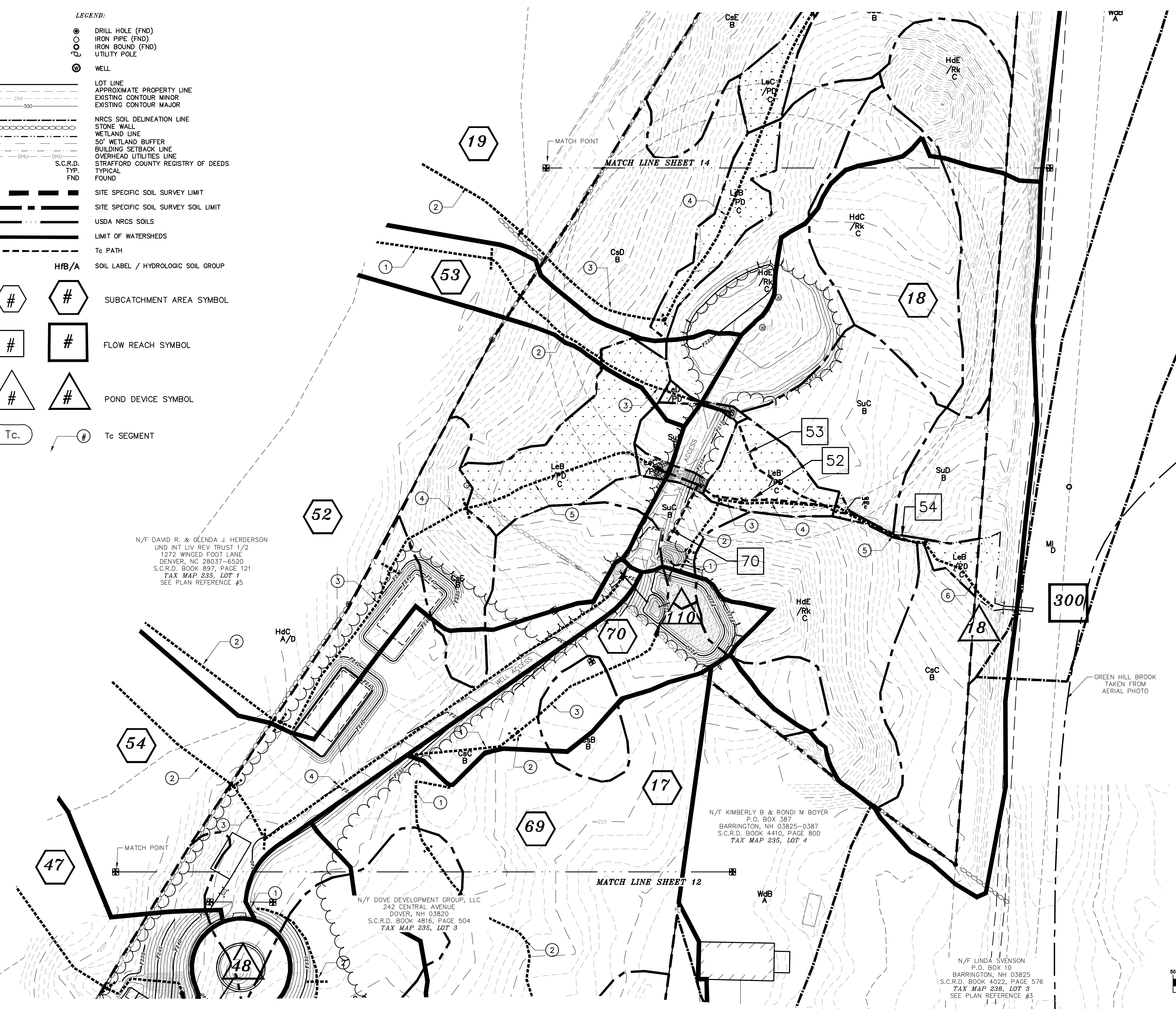
- DRILL HOLE (FND)
- IRON PIPE (FND)
- IRON BOUND (FND)
- UTILITY POLE
- ⊙ WELL
- LOT LINE
- - - APPROXIMATE PROPERTY LINE
- EXISTING CONTOUR MINOR
- EXISTING CONTOUR MAJOR
- NRCS SOIL DELINEATION LINE
- STONE WALL
- WETLAND LINE
- 50' WETLAND BUFFER
- BUILDING SETBACK LINE
- OVERHEAD UTILITIES LINE
- STRAFFORD COUNTY REGISTRY OF DEEDS
- TYPICAL
- FND
- SITE SPECIFIC SOIL SURVEY LIMIT
- SITE SPECIFIC SOIL SURVEY SOIL LIMIT
- USDA NRCS SOILS
- LIMIT OF WATERSHEDS
- Tc PATH
- HfB/A SOIL LABEL / HYDROLOGIC SOIL GROUP
- # SUBCATCHMENT AREA SYMBOL
- # FLOW REACH SYMBOL
- # POND DEVICE SYMBOL
- Tc. Tc SEGMENT

N/F DAVID R. & GLENDA J. HERDERSON
UND INT LIV REV TRUST 1/2
1272 WINGED FOOT LANE
DENVER, CO 80337-6520
S.C.R.D. BOOK 897, PAGE 121
TAX MAP 235, LOT 1
SEE PLAN REFERENCE #5

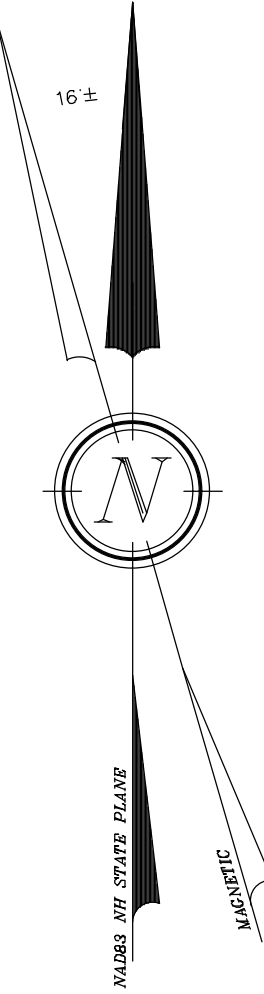
N/F KIMBERLY B & RONI M BOYER
P.O. BOX 357
BARRINGTON, NH 03825-0387
S.C.R.D. BOOK 4410, PAGE 800
TAX MAP 235, LOT 4

N/F DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVENUE
DOVER, NH 03820
S.C.R.D. BOOK 4816, PAGE 504
TAX MAP 235, LOT 3

N/F LINDA SVENSON
P.O. BOX 10
BARRINGTON, NH 03825
S.C.R.D. BOOK 4022, PAGE 576
TAX MAP 238, LOT 3
SEE PLAN REFERENCE #3

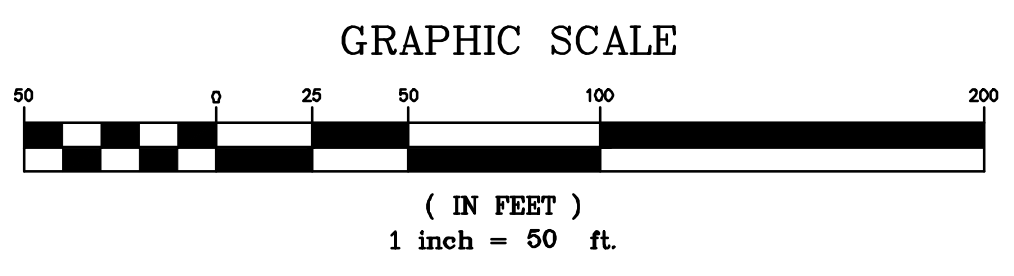


- NOTES:**
- 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
B.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
 - 2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
B.) TAX MAP 235, LOT 3
 - 3.) LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
B.) 743,421 Sq. Ft., 17.07 Ac.
 - 4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
B.) BOOK 4816, PAGE 504
 - 5.) VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS.
HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED
USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
 - 6.) THE INTENT OF THIS PLAN IS TO SHOW THE PROPOSED CONDITIONS
WATERSHEDS OF TAX MAP 235 LOT 1-1 AND TAX MAP 235 LOT 3.



JOHN P. HAYES III, CSS #87 JOHN P. HAYES III, CWS #18

- WETLAND NOTES:**
- WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE
DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING
THE FOLLOWING STANDARDS:
1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND
DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION,
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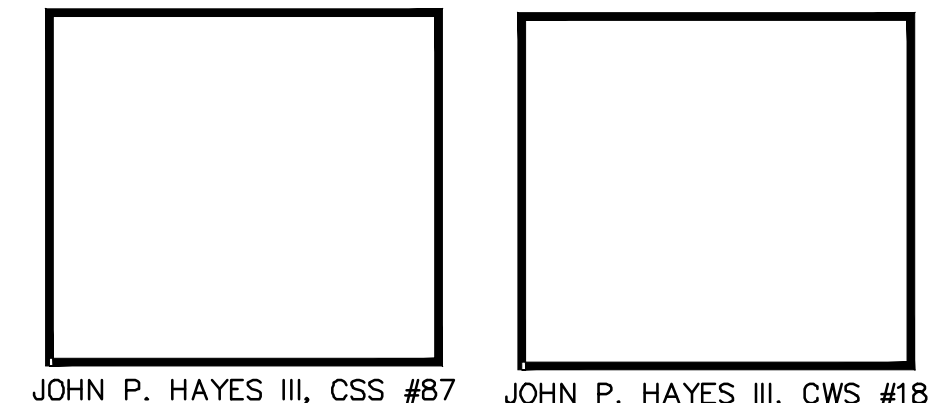
REVISION	DATE	DESCRIPTION

W-2 PROPOSED WATERSHED DETAIL
LAND OF
DOVE DEVELOPMENT GROUP, LLC
N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
COMMUNITY WAY
BARRINGTON, NH
TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863
SCALE : 1 IN. EQUALS 50 FT.
DATE : JUNE 14, 2021
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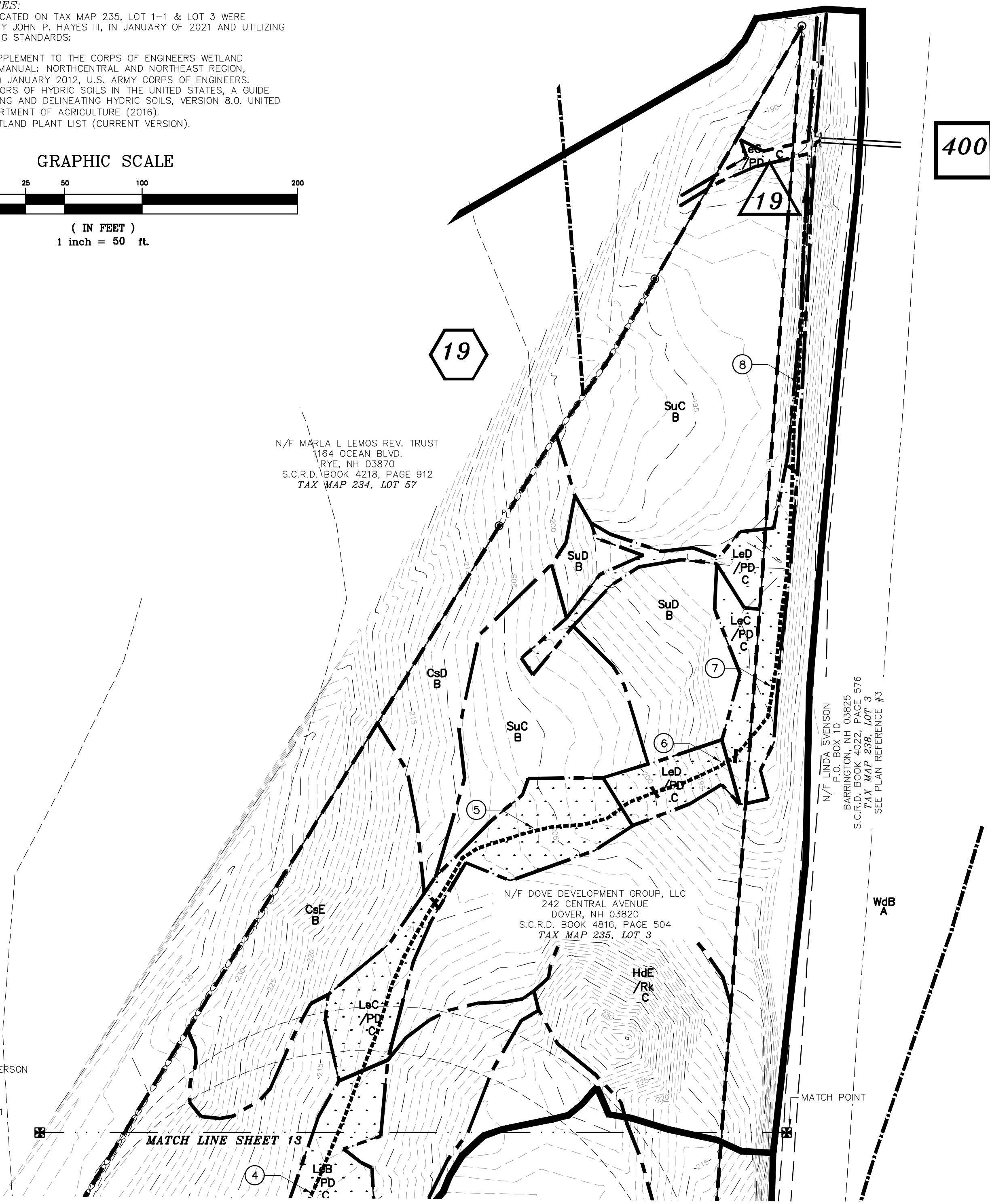
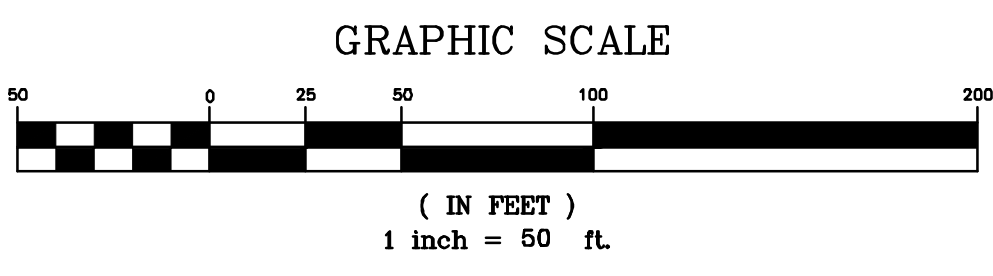
LEGEND:

- DRILL HOLE (FND)
- IRON PIPE (FND)
- IRON BOUND (FND)
- UTILITY POLE
- ⊙ WELL
- LOT LINE
- - - APPROXIMATE PROPERTY LINE
- - - EXISTING CONTOUR MINOR
- - - EXISTING CONTOUR MAJOR
- NRCS SOIL DELINEATION LINE
- STONE WALL
- WETLAND LINE
- 50' WETLAND BUFFER
- BUILDING SETBACK LINE
- OVERHEAD UTILITIES LINE
- S.C.R.D. STRAFFORD COUNTY REGISTRY OF DEEDS TYP. FND
- SITE SPECIFIC SOIL SURVEY LIMIT
- SITE SPECIFIC SOIL SURVEY SOIL LIMIT
- USDA NRCS SOILS
- LIMIT OF WATERSHEDS
- Tc PATH
- HB/A SOIL LABEL / HYDROLOGIC SOIL GROUP
- # SUBCATCHMENT AREA SYMBOL
- # FLOW REACH SYMBOL
- # POND DEVICE SYMBOL
- Tc. Tc SEGMENT



WETLAND NOTES:
 WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:

- REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS' WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
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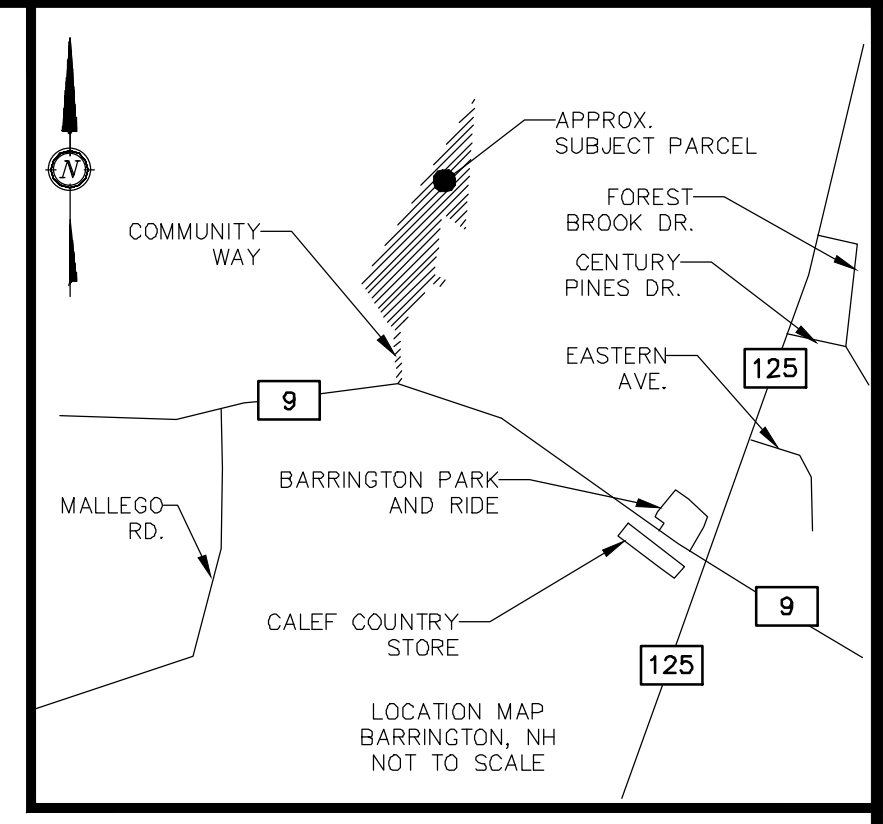


N/F MARLA L. LEMOS REV. TRUST
 164 OCEAN BLVD.
 RYE, NH 03870
 S.C.R.D. BOOK 4218, PAGE 912
 TAX MAP 234, LOT 57

N/F LINDA SVENSON
 BARRINGTON, NH 03825
 S.C.R.D. BOOK 4022, PAGE 976
 TAX MAP 238, LOT 3
 SEE PLAN REFERENCE #3

N/F DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVENUE
 DOVER, NH 03820
 S.C.R.D. BOOK 4816, PAGE 504
 TAX MAP 235, LOT 3

N/F DAVID R. & GLENDA J. HERDERSON
 UND. INT. LIV. REV. TRUST 1/2
 1272 WINGED FOOT LANE
 DENVER, CO 8037-6520
 S.C.R.D. BOOK 897, PAGE 1211
 TAX MAP 235, LOT 1
 SEE PLAN REFERENCE #5



- NOTES:**
- OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 B.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 - LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
 B.) TAX MAP 235, LOT 3
 - LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
 B.) 743,421 Sq. Ft., 17.07 Ac.
 - S.C.R.D.: A.) BOOK 4816, PAGE 500
 B.) BOOK 4816, PAGE 504
 - VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS. HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
 - THE INTENT OF THIS PLAN IS TO SHOW THE PROPOSED CONDITIONS WATERSHEDS OF TAX MAP 235 LOT 1-1 AND TAX MAP 235 LOT 3.

SITE SPECIFIC SOILS LEGEND		
SYMBOL	SOIL TAXONOMIC NAME	HYDROLOGIC SOIL GROUP
CsB	CHARLTON (VERY STONY)	B
CsC	CHARLTON (VERY STONY)	B
CsD	CHARLTON (VERY STONY)	B
CsE	CHARLTON (VERY STONY)	B
HcC	HOLLIS (VERY STONY)	C/D
HcD	HOLLIS (VERY STONY)	C/D
HcE	HOLLIS (VERY STONY)	C/D
HdD	HOLLIS CHARLTON COMPLEX (VERY STONY)	C/D
HdE	HOLLIS CHARLTON COMPLEX (VERY STONY)	C/D
LeB	LEICESTER (VERY STONY)	C
LeC	LEICESTER (VERY STONY)	C
LeD	LEICESTER (VERY STONY)	C
SuB	SUTTON	B
SuC	SUTTON	B
SuD	SUTTON	B

SLOPE: A = 0-3% B = 3-8% C = 8-15% D = 15-25% E = 25-50% F = 50%+
 DENOMINATOR: /VPD = VERY POORLY DRAINED /PD = POORLY DRAINED /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED

NRCS SOILS LEGEND		
SYMBOL	SOIL TAXONOMIC NAME	HYDROLOGIC SOIL GROUP
HdB	HOLLIS-CHARLTON (VERY ROCKY)	A/D
HdC	HOLLIS-CHARLTON (VERY ROCKY)	A/D
Mi	MIXED ALLUVIAL LAND	D
WdA	WNDSOR	A
WdB	WNDSOR	A

SLOPE: A = 0-3% B = 3-8% C = 8-15% D = 15-25% E = 25-50% F = 50%+
 DENOMINATOR: /VPD = VERY POORLY DRAINED /PD = POORLY DRAINED /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED

REVISION	DATE	DESCRIPTION

W-2 PROPOSED WATERSHED DETAIL
 LAND OF
 DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 COMMUNITY WAY
 BARRINGTON, NH
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603)332-2863
 SCALE: 1 IN. EQUALS 50 FT.
 DATE: JUNE 14, 2021
 FILE NO.: DB 2020 - 097

Appendix I - Existing Conditions Analysis

25 Yr - 24 Hr. Full Summary

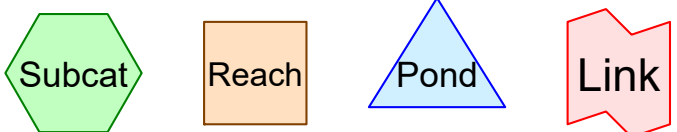
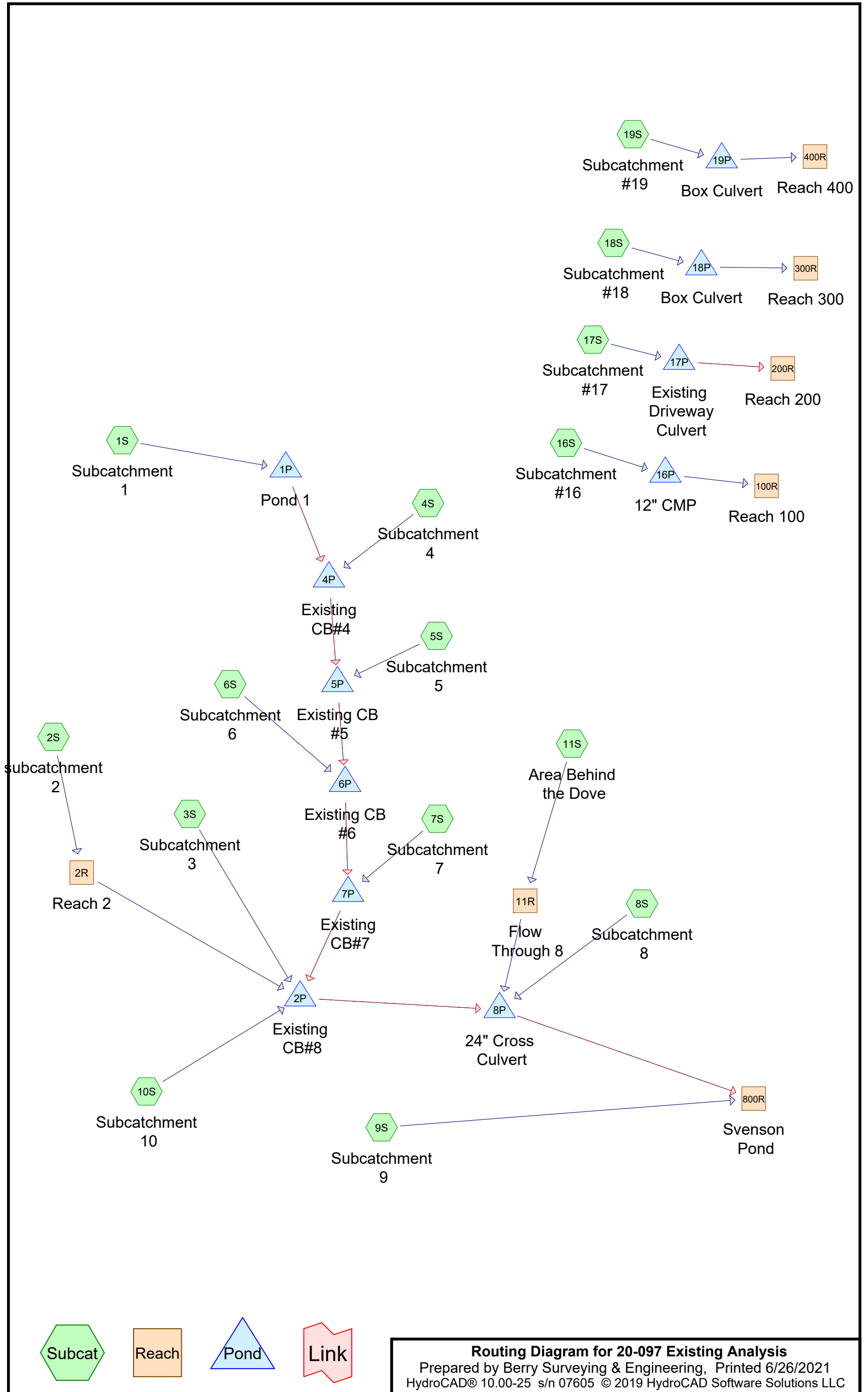
2 Yr - 24 Hr. Node Listing

10 Yr -24 Hr. Node Listing

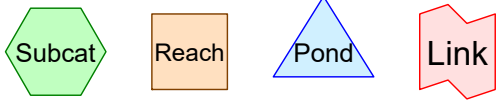
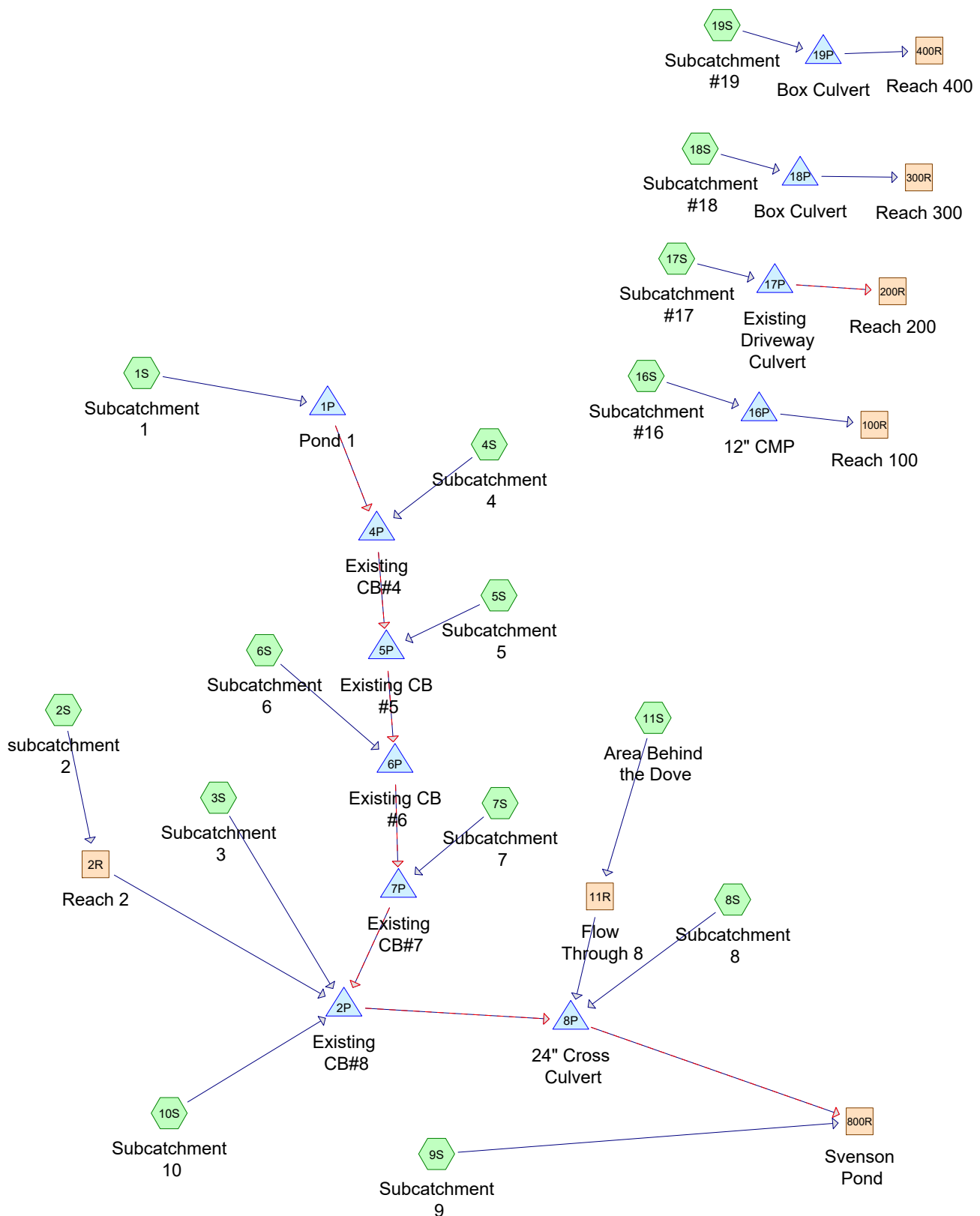
25 Yr - 24 Hr. Node Listing

50 Yr - 24 Hr. Node Listing

100 Yr - 24 Hr. Node Listing



Routing Diagram for 20-097 Existing Analysis
 Prepared by Berry Surveying & Engineering, Printed 6/26/2021
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Routing Diagram for 20-097 Existing Analysis
 Prepared by Berry Surveying & Engineering, Printed 6/26/2021
 HydroCAD® 10.00-25 s/n 07605 © 2019 HydroCAD Software Solutions LLC

20-097 Existing Analysis

Prepared by Berry Surveying & Engineering

HydroCAD® 10.00-25 s/n 07605 © 2019 HydroCAD Software Solutions LLC

Printed 6/26/2021

Page 2

Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
8.535	39	>75% Grass cover, Good, HSG A (1S, 2S, 3S, 4S, 5S, 6S, 7S, 8S, 9S, 10S, 11S, 16S, 17S)
0.038	61	>75% Grass cover, Good, HSG B (17S)
0.094	80	>75% Grass cover, Good, HSG D (16S, 17S)
0.543	98	Paved parking, HSG A (2S, 6S)
0.984	98	Unconnected pavement, HSG A (3S, 4S, 5S, 7S, 8S, 9S, 10S, 16S, 17S, 18S)
0.027	98	Unconnected pavement, HSG D (17S, 18S)
0.493	98	Unconnected roofs, HSG A (2S, 3S, 4S, 5S, 6S, 7S, 8S, 9S, 10S, 11S, 16S)
0.067	98	Water Surface, 0% imp, HSG A (2S)
25.389	30	Woods, Good, HSG A (1S, 2S, 3S, 11S, 16S, 17S, 18S, 19S)
0.333	30	Woods, Good, HSG A H-C (3S)
18.888	55	Woods, Good, HSG B (1S, 11S, 16S, 17S, 18S, 19S)
4.858	70	Woods, Good, HSG C (1S, 16S, 17S, 18S, 19S)
10.844	77	Woods, Good, HSG D (1S, 16S, 17S, 18S, 19S)
7.952	77	Woods, Good, HSG D H-C (2S, 3S)
79.043	52	TOTAL AREA

20-097 Existing Analysis

Prepared by Berry Surveying & Engineering

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Printed 6/26/2021

Page 3

Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
36.342	HSG A	1S, 2S, 3S, 4S, 5S, 6S, 7S, 8S, 9S, 10S, 11S, 16S, 17S, 18S, 19S
18.926	HSG B	1S, 11S, 16S, 17S, 18S, 19S
4.858	HSG C	1S, 16S, 17S, 18S, 19S
18.917	HSG D	1S, 2S, 3S, 16S, 17S, 18S, 19S
0.000	Other	
79.043		TOTAL AREA

20-097 Existing Analysis

Prepared by Berry Surveying & Engineering

Printed 6/26/2021

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Page 4

Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
8.535	0.038	0.000	0.094	0.000	8.667	>75% Grass cover, Good	1S, 2S, 3S, 4S, 5S, 6S, 7S, 8S, 9S, 10S, 11S, 16S, 17S
0.543	0.000	0.000	0.000	0.000	0.543	Paved parking	2S, 6S
0.984	0.000	0.000	0.027	0.000	1.010	Unconnected pavement	3S, 4S, 5S, 7S, 8S, 9S, 10S, 16S, 17S, 18S
0.493	0.000	0.000	0.000	0.000	0.493	Unconnected roofs	2S, 3S, 4S, 5S, 6S, 7S, 8S, 9S, 10S, 11S, 16S
0.067	0.000	0.000	0.000	0.000	0.067	Water Surface, 0% imp	2S
25.721	18.888	4.858	18.796	0.000	68.263	Woods, Good	1S, 2S, 3S, 11S, 16S, 17S, 18S, 19S
36.342	18.926	4.858	18.917	0.000	79.043	TOTAL AREA	

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Pipe Listing (all nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
1	1P	201.13	198.83	34.7	0.0663	0.025	12.0	0.0	0.0
2	2P	196.62	196.28	67.8	0.0050	0.025	24.0	0.0	0.0
3	4P	198.65	197.33	56.4	0.0234	0.025	12.0	0.0	0.0
4	5P	197.43	196.02	46.1	0.0306	0.025	12.0	0.0	0.0
5	6P	196.02	195.72	101.6	0.0030	0.025	12.0	0.0	0.0
6	7P	195.72	195.00	35.9	0.0201	0.025	24.0	0.0	0.0
7	8P	196.55	196.44	21.6	0.0051	0.012	24.0	0.0	0.0
8	16P	203.25	203.05	20.0	0.0100	0.025	12.0	0.0	0.0
9	18P	190.25	190.20	28.0	0.0018	0.012	36.0	36.0	0.0
10	19P	182.69	183.13	52.0	-0.0085	0.012	36.0	36.0	0.0

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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1	Runoff Area=303,964 sf 0.00% Impervious Runoff Depth>0.74" Flow Length=1,542' Tc=32.6 min CN=45 Runoff=2.15 cfs 0.428 af
Subcatchment 2S: subcatchment 2	Runoff Area=764,518 sf 0.65% Impervious Runoff Depth>1.19" Flow Length=2,418' Tc=59.1 min CN=52 Runoff=8.18 cfs 1.744 af
Subcatchment 3S: Subcatchment 3	Runoff Area=122,849 sf 0.64% Impervious Runoff Depth>0.40" Flow Length=993' Tc=20.7 min CN=39 Runoff=0.35 cfs 0.094 af
Subcatchment 4S: Subcatchment 4	Runoff Area=4,089 sf 98.95% Impervious Runoff Depth>5.50" Flow Length=85' Slope=0.0472 '/' Tc=6.0 min CN=97 Runoff=0.52 cfs 0.043 af
Subcatchment 5S: Subcatchment 5	Runoff Area=10,452 sf 82.66% Impervious Runoff Depth>4.49" Flow Length=75' Tc=6.0 min CN=88 Runoff=1.19 cfs 0.090 af
Subcatchment 6S: Subcatchment 6	Runoff Area=24,193 sf 93.83% Impervious Runoff Depth>5.15" Flow Length=216' Tc=6.0 min CN=94 Runoff=3.02 cfs 0.239 af
Subcatchment 7S: Subcatchment 7	Runoff Area=7,743 sf 65.07% Impervious Runoff Depth>3.35" Flow Length=98' Tc=9.7 min CN=77 Runoff=0.61 cfs 0.050 af
Subcatchment 8S: Subcatchment 8	Runoff Area=19,227 sf 32.64% Impervious Runoff Depth>1.67" Flow Length=152' Tc=10.4 min CN=58 Runoff=0.68 cfs 0.061 af
Subcatchment 9S: Subcatchment 9	Runoff Area=64,869 sf 22.90% Impervious Runoff Depth>0.80" Flow Length=484' Tc=19.3 min UI Adjusted CN=46 Runoff=0.63 cfs 0.100 af
Subcatchment 10S: Subcatchment 10	Runoff Area=53,175 sf 5.56% Impervious Runoff Depth>0.51" Flow Length=438' Tc=18.4 min UI Adjusted CN=41 Runoff=0.24 cfs 0.052 af
Subcatchment 11S: Area Behind the Dove	Runoff Area=107,916 sf 6.10% Impervious Runoff Depth>0.62" Flow Length=802' Tc=22.0 min UI Adjusted CN=43 Runoff=0.66 cfs 0.128 af
Subcatchment 16S: Subcatchment #16	Runoff Area=297,191 sf 2.76% Impervious Runoff Depth>1.21" Flow Length=1,113' Tc=27.2 min CN=52 Runoff=4.75 cfs 0.686 af
Subcatchment 17S: Subcatchment #17	Runoff Area=497,407 sf 0.60% Impervious Runoff Depth>1.35" Flow Length=1,540' Tc=35.5 min UI Adjusted CN=54 Runoff=8.25 cfs 1.283 af
Subcatchment 18S: Subcatchment #18	Runoff Area=474,696 sf 0.22% Impervious Runoff Depth>1.58" Flow Length=1,280' Tc=29.3 min CN=57 Runoff=10.53 cfs 1.433 af
Subcatchment 19S: Subcatchment #19	Runoff Area=690,822 sf 0.00% Impervious Runoff Depth>1.34" Flow Length=1,832' Tc=46.3 min CN=54 Runoff=9.97 cfs 1.775 af
Reach 2R: Reach 2	Avg. Flow Depth=0.55' Max Vel=3.59 fps Inflow=8.18 cfs 1.744 af n=0.022 L=329.8' S=0.0091 '/' Capacity=24.64 cfs Outflow=8.17 cfs 1.741 af

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Reach 11R: Flow Through 8	Avg. Flow Depth=0.16' Max Vel=1.09 fps Inflow=0.66 cfs 0.128 af n=0.035 L=76.0' S=0.0132 '/' Capacity=7.77 cfs Outflow=0.66 cfs 0.128 af
Reach 100R: Reach 100	Inflow=2.49 cfs 0.685 af Outflow=2.49 cfs 0.685 af
Reach 200R: Reach 200	Inflow=8.23 cfs 1.232 af Outflow=8.23 cfs 1.232 af
Reach 300R: Reach 300	Inflow=10.52 cfs 1.433 af Outflow=10.52 cfs 1.433 af
Reach 400R: Reach 400	Inflow=9.97 cfs 1.775 af Outflow=9.97 cfs 1.775 af
Reach 800R: Svenson Pond	Inflow=11.40 cfs 3.023 af Outflow=11.40 cfs 3.023 af
Pond 1P: Pond 1	Peak Elev=203.37' Storage=18 cf Inflow=2.15 cfs 0.428 af Primary=2.16 cfs 0.428 af Secondary=0.00 cfs 0.000 af Outflow=2.16 cfs 0.428 af
Pond 2P: Existing CB#8	Peak Elev=199.20' Storage=333 cf Inflow=10.78 cfs 2.736 af Primary=10.70 cfs 2.735 af Secondary=0.00 cfs 0.000 af Outflow=10.70 cfs 2.735 af
Pond 4P: Existing CB#4	Peak Elev=202.67' Storage=51 cf Inflow=2.22 cfs 0.471 af Primary=2.22 cfs 0.471 af Secondary=0.00 cfs 0.000 af Outflow=2.22 cfs 0.471 af
Pond 5P: Existing CB #5	Peak Elev=201.70' Storage=60 cf Inflow=2.38 cfs 0.561 af Primary=1.90 cfs 0.535 af Secondary=0.68 cfs 0.026 af Outflow=2.38 cfs 0.561 af
Pond 6P: Existing CB #6	Peak Elev=201.51' Storage=78 cf Inflow=4.72 cfs 0.800 af Primary=3.25 cfs 0.780 af Secondary=1.58 cfs 0.019 af Outflow=4.72 cfs 0.799 af
Pond 7P: Existing CB#7	Peak Elev=199.21' Storage=44 cf Inflow=5.29 cfs 0.849 af Primary=5.29 cfs 0.849 af Secondary=0.00 cfs 0.000 af Outflow=5.29 cfs 0.849 af
Pond 8P: 24" Cross Culvert	Peak Elev=198.43' Storage=1,221 cf Inflow=11.20 cfs 2.924 af Primary=11.15 cfs 2.923 af Secondary=0.00 cfs 0.000 af Outflow=11.15 cfs 2.923 af
Pond 16P: 12" CMP	Peak Elev=204.71' Storage=4,353 cf Inflow=4.75 cfs 0.686 af Outflow=2.49 cfs 0.685 af
Pond 17P: Existing Driveway Culvert	Peak Elev=204.15' Storage=3,126 cf Inflow=8.25 cfs 1.283 af Primary=5.93 cfs 1.086 af Secondary=2.30 cfs 0.146 af Outflow=8.23 cfs 1.232 af
Pond 18P: Box Culvert	Peak Elev=191.52' Storage=155 cf Inflow=10.53 cfs 1.433 af 36.0" x 36.0" Box Culvert n=0.012 L=28.0' S=0.0018 '/' Outflow=10.52 cfs 1.433 af
Pond 19P: Box Culvert	Peak Elev=184.15' Storage=24 cf Inflow=9.97 cfs 1.775 af 36.0" x 36.0" Box Culvert n=0.012 L=52.0' S=-0.0085 '/' Outflow=9.97 cfs 1.775 af

Total Runoff Area = 79.043 ac Runoff Volume = 8.205 af Average Runoff Depth = 1.25"
97.41% Pervious = 76.997 ac 2.59% Impervious = 2.046 ac

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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 1S: Subcatchment 1

Runoff = 2.15 cfs @ 12.62 hrs, Volume= 0.428 af, Depth> 0.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
3,011	39	>75% Grass cover, Good, HSG A
151,706	30	Woods, Good, HSG A
105,282	55	Woods, Good, HSG B
21,412	70	Woods, Good, HSG C
22,553	77	Woods, Good, HSG D
303,964	45	Weighted Average
303,964		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.8	100	0.1500	0.17		Sheet Flow, Segment 1 Woods: Light underbrush n= 0.400 P2= 3.08"
4.7	442	0.0973	1.56		Shallow Concentrated Flow, Segment 2 Woodland Kv= 5.0 fps
0.5	65	0.2153	2.32		Shallow Concentrated Flow, Segment 3 Woodland Kv= 5.0 fps
2.6	153	0.0395	0.99		Shallow Concentrated Flow, Segment 4 Woodland Kv= 5.0 fps
2.6	153	0.0393	0.99		Shallow Concentrated Flow, Segment 5 Woodland Kv= 5.0 fps
0.7	62	0.0806	1.42		Shallow Concentrated Flow, Segment 6 Woodland Kv= 5.0 fps
5.0	190	0.0158	0.63		Shallow Concentrated Flow, Segment 7 Woodland Kv= 5.0 fps
5.9	315	0.0317	0.89		Shallow Concentrated Flow, Segment 8 Woodland Kv= 5.0 fps
0.8	62	0.0645	1.27		Shallow Concentrated Flow, Segment 9 Woodland Kv= 5.0 fps
32.6	1,542	Total			

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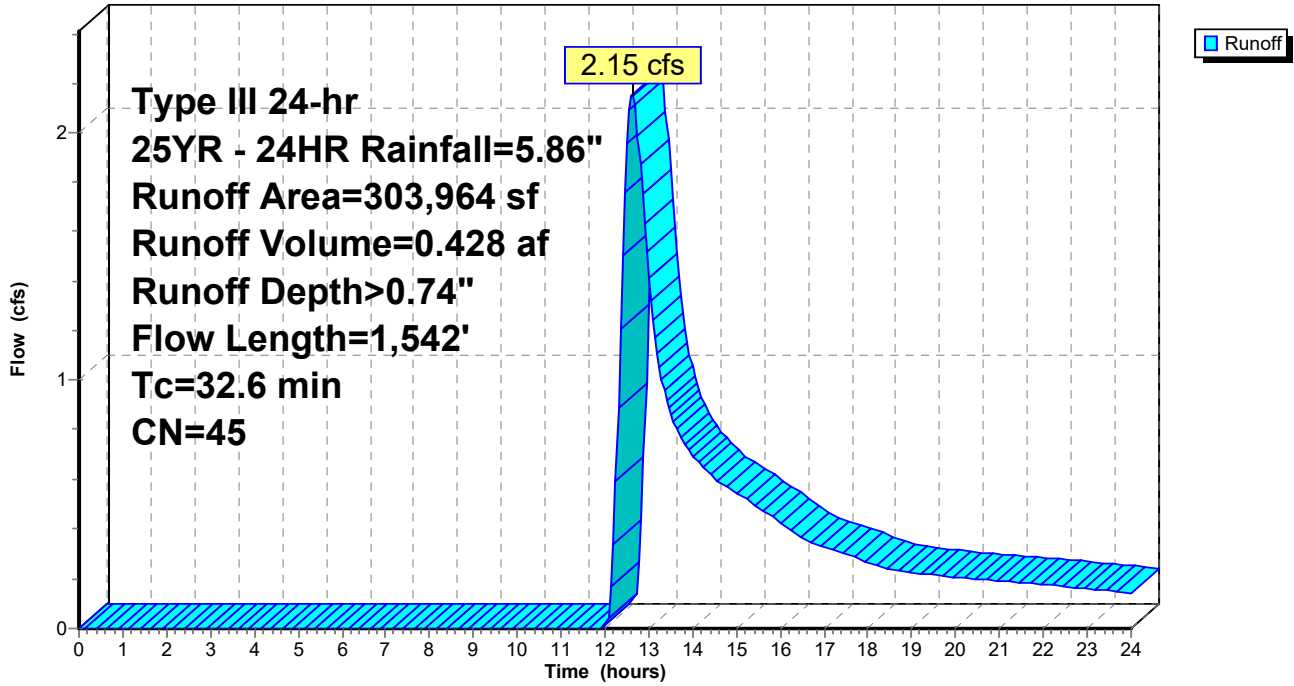
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 1S: Subcatchment 1

Hydrograph



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Summary for Subcatchment 2S: subcatchment 2

Runoff = 8.18 cfs @ 12.93 hrs, Volume= 1.744 af, Depth> 1.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
2,663	98	Unconnected roofs, HSG A
55,787	39	>75% Grass cover, Good, HSG A
2,337	98	Paved parking, HSG A
37,068	30	Woods, Good, HSG A
2,905	98	Water Surface, 0% imp, HSG A
* 331,879	77	Woods, Good, HSG D H-C
331,879	30	Woods, Good, HSG A
764,518	52	Weighted Average
759,518		99.35% Pervious Area
5,000		0.65% Impervious Area
2,663		53.26% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
15.2	100	0.0500	0.11		Sheet Flow, Segment 1 Woods: Light underbrush n= 0.400 P2= 3.08"
9.8	940	0.1032	1.61		Shallow Concentrated Flow, Segment 2 Woodland Kv= 5.0 fps
14.8	445	0.0101	0.50		Shallow Concentrated Flow, Segment 3 Woodland Kv= 5.0 fps
2.1	59	0.0085	0.46		Shallow Concentrated Flow, Segment 4 Woodland Kv= 5.0 fps
1.7	137	0.0728	1.35		Shallow Concentrated Flow, Segment 5 Woodland Kv= 5.0 fps
12.7	418	0.0120	0.55		Shallow Concentrated Flow, Segment 6 Woodland Kv= 5.0 fps
2.5	165	0.0242	1.09		Shallow Concentrated Flow, Segment 7 Short Grass Pasture Kv= 7.0 fps
0.1	68		12.69		Lake or Reservoir, Segment 8 Mean Depth= 5.00'
0.2	86	0.0174	6.81	23.84	Trap/Vee/Rect Channel Flow, Segment 9 Bot.W=3.00' D=1.00' Z= 0.5 '/' Top.W=4.00' n= 0.022 Earth, clean & straight
59.1	2,418	Total			

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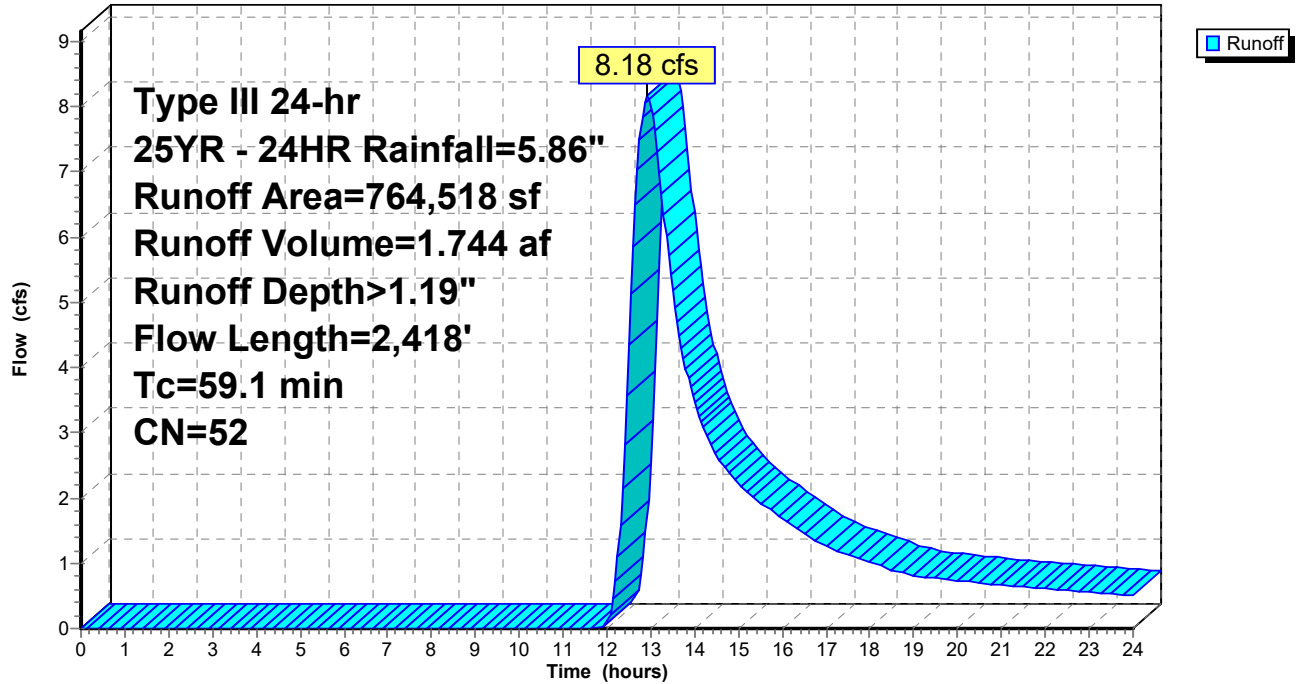
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Subcatchment 2S: subcatchment 2

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 3S: Subcatchment 3

Runoff = 0.35 cfs @ 12.58 hrs, Volume= 0.094 af, Depth> 0.40"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
357	98	Unconnected roofs, HSG A
38,528	39	>75% Grass cover, Good, HSG A
434	98	Unconnected pavement, HSG A
54,552	30	Woods, Good, HSG A
* 14,489	77	Woods, Good, HSG D H-C
* 14,489	30	Woods, Good, HSG A H-C
122,849	39	Weighted Average
122,058		99.36% Pervious Area
791		0.64% Impervious Area
791		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0	97	0.1334	0.16		Sheet Flow, Segment 1 Woods: Light underbrush n= 0.400 P2= 3.08"
2.7	155	0.0355	0.94		Shallow Concentrated Flow, Segment 2 Woodland Kv= 5.0 fps
5.3	290	0.0328	0.91		Shallow Concentrated Flow, Segment 3 Woodland Kv= 5.0 fps
1.6	132	0.0379	1.36		Shallow Concentrated Flow, Segment 4 Short Grass Pasture Kv= 7.0 fps
1.1	319	0.0094	5.01	17.52	Trap/Vee/Rect Channel Flow, Segment 5 Bot.W=3.00' D=1.00' Z= 0.5 '/' Top.W=4.00' n= 0.022 Earth, clean & straight
20.7	993	Total			

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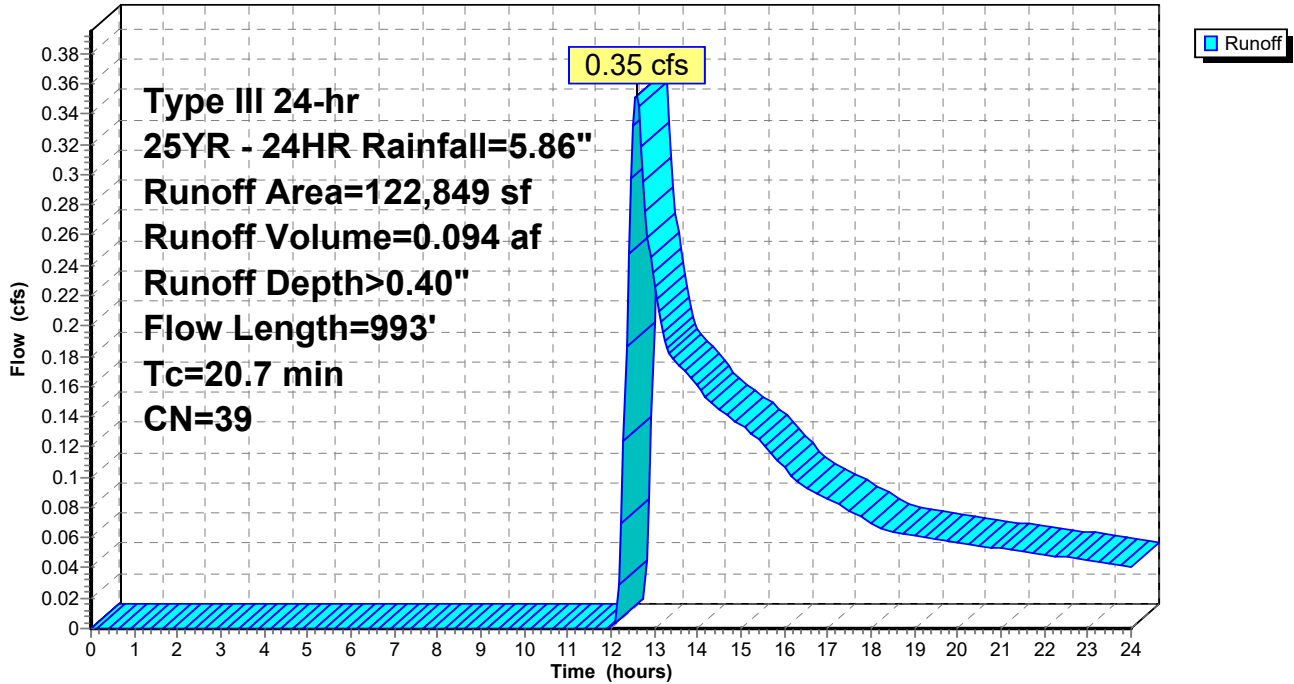
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Subcatchment 3S: Subcatchment 3

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Summary for Subcatchment 4S: Subcatchment 4

Runoff = 0.52 cfs @ 12.09 hrs, Volume= 0.043 af, Depth> 5.50"

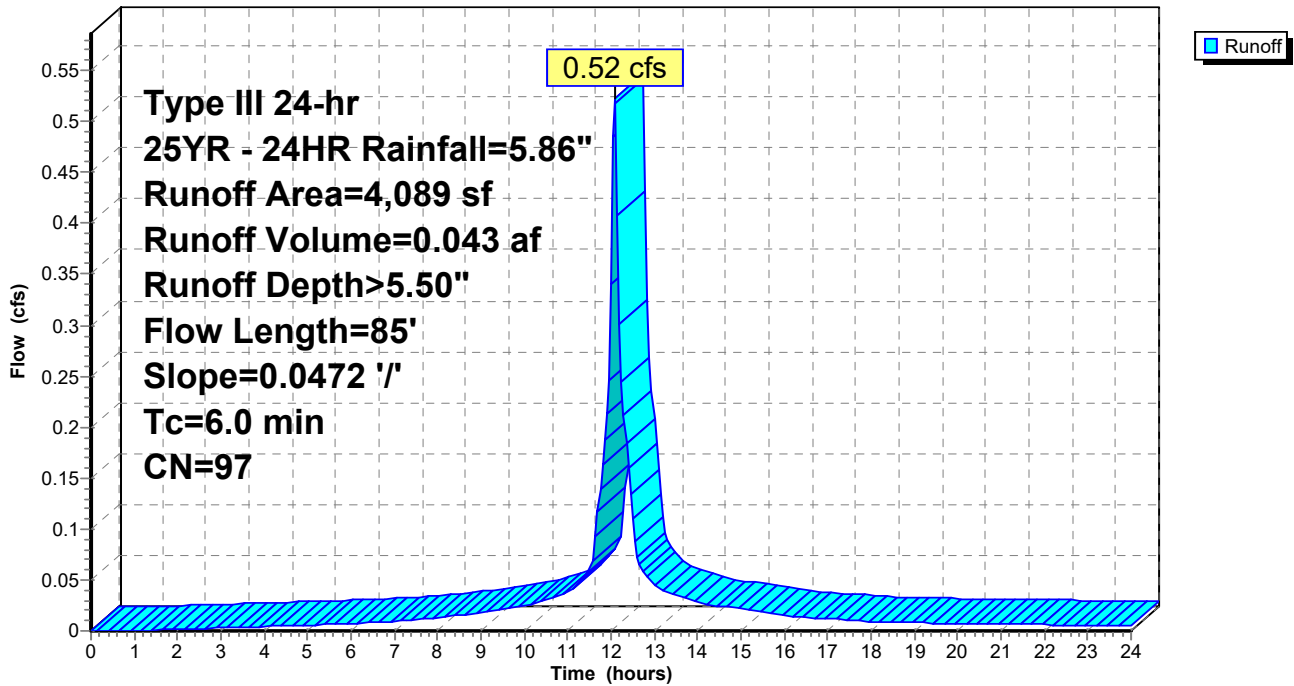
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
859	98	Unconnected roofs, HSG A
43	39	>75% Grass cover, Good, HSG A
3,187	98	Unconnected pavement, HSG A
4,089	97	Weighted Average
43		1.05% Pervious Area
4,046		98.95% Impervious Area
4,046		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.8	85	0.0472	1.84		Sheet Flow, Segment 1 Smooth surfaces n= 0.011 P2= 3.08"
0.8	85	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 4S: Subcatchment 4

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 5S: Subcatchment 5

Runoff = 1.19 cfs @ 12.09 hrs, Volume= 0.090 af, Depth> 4.49"

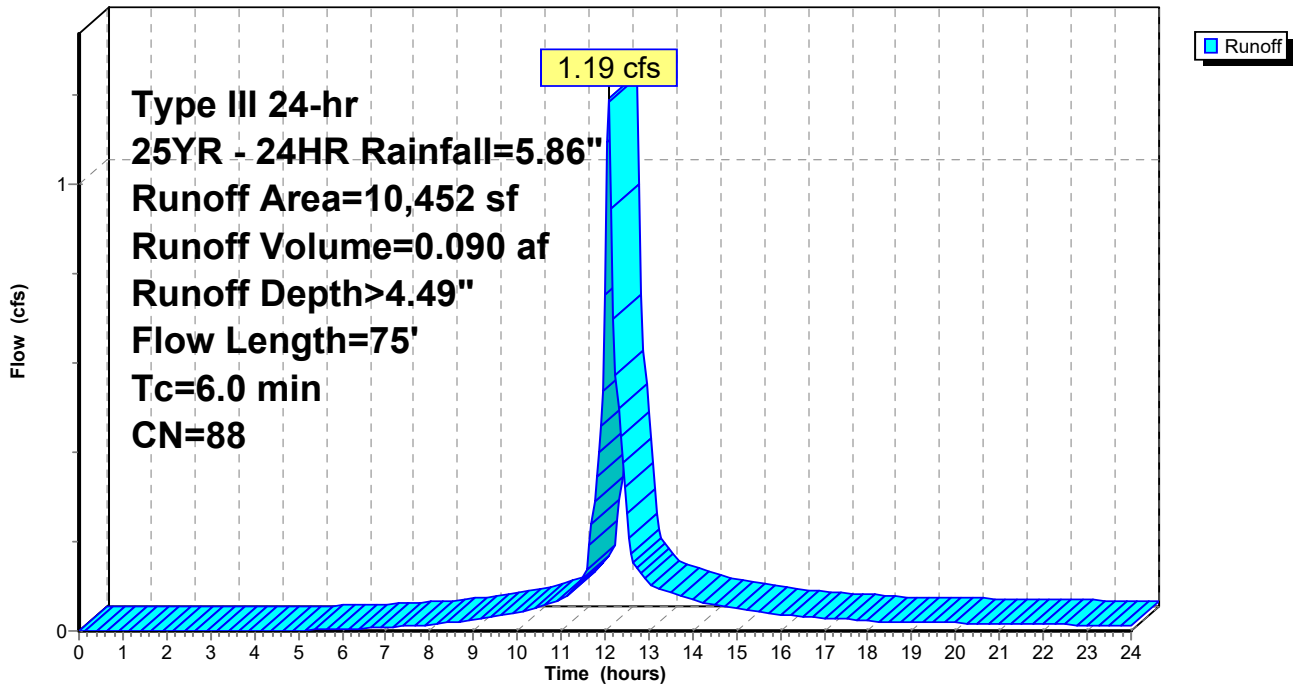
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
1,527	98	Unconnected roofs, HSG A
1,812	39	>75% Grass cover, Good, HSG A
7,113	98	Unconnected pavement, HSG A
10,452	88	Weighted Average
1,812		17.34% Pervious Area
8,640		82.66% Impervious Area
8,640		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.1	54	0.0553	0.22		Sheet Flow, Segment 1 Grass: Short n= 0.150 P2= 3.08"
0.1	21	0.0237	3.13		Shallow Concentrated Flow, Segment 2 Paved Kv= 20.3 fps
4.2	75	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 5S: Subcatchment 5

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Summary for Subcatchment 6S: Subcatchment 6

Runoff = 3.02 cfs @ 12.09 hrs, Volume= 0.239 af, Depth> 5.15"

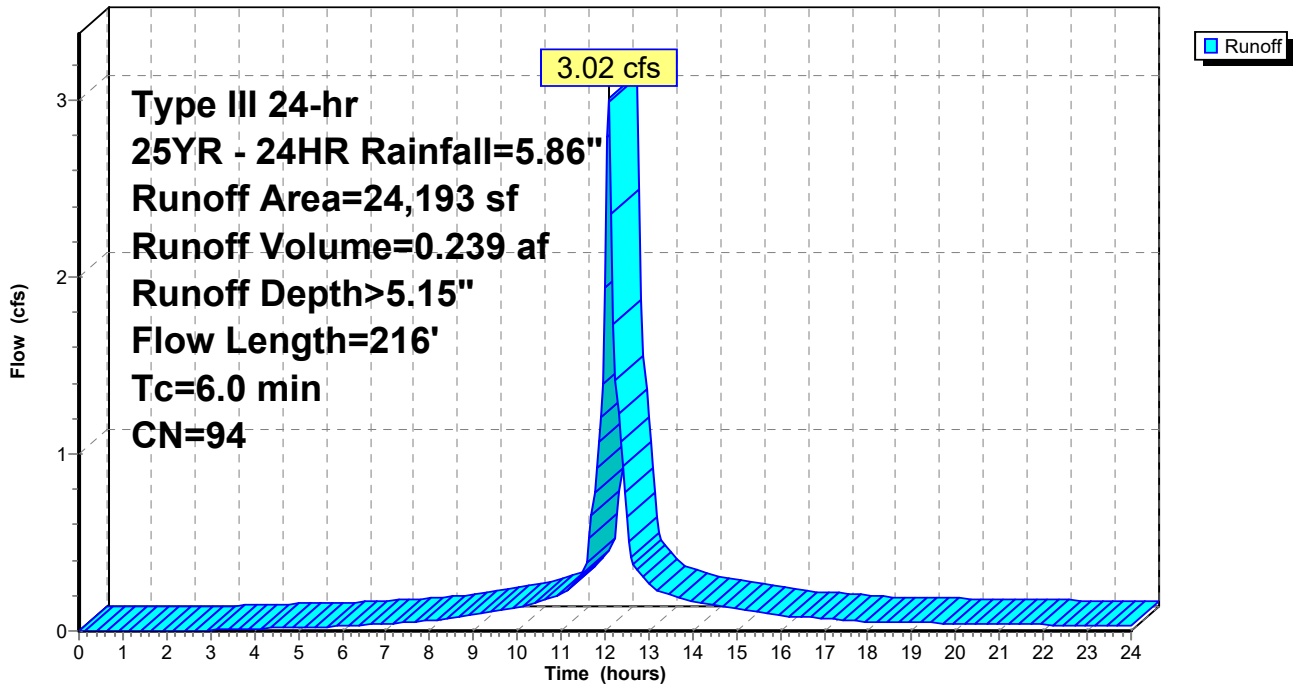
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
1,394	98	Unconnected roofs, HSG A
1,493	39	>75% Grass cover, Good, HSG A
21,306	98	Paved parking, HSG A
24,193	94	Weighted Average
1,493		6.17% Pervious Area
22,700		93.83% Impervious Area
1,394		6.14% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	100	0.0384	1.75		Sheet Flow, Segment 1 Smooth surfaces n= 0.011 P2= 3.08"
0.6	116	0.0259	3.27		Shallow Concentrated Flow, Segment 2 Paved Kv= 20.3 fps
1.6	216	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 6S: Subcatchment 6

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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 7S: Subcatchment 7

Runoff = 0.61 cfs @ 12.14 hrs, Volume= 0.050 af, Depth> 3.35"

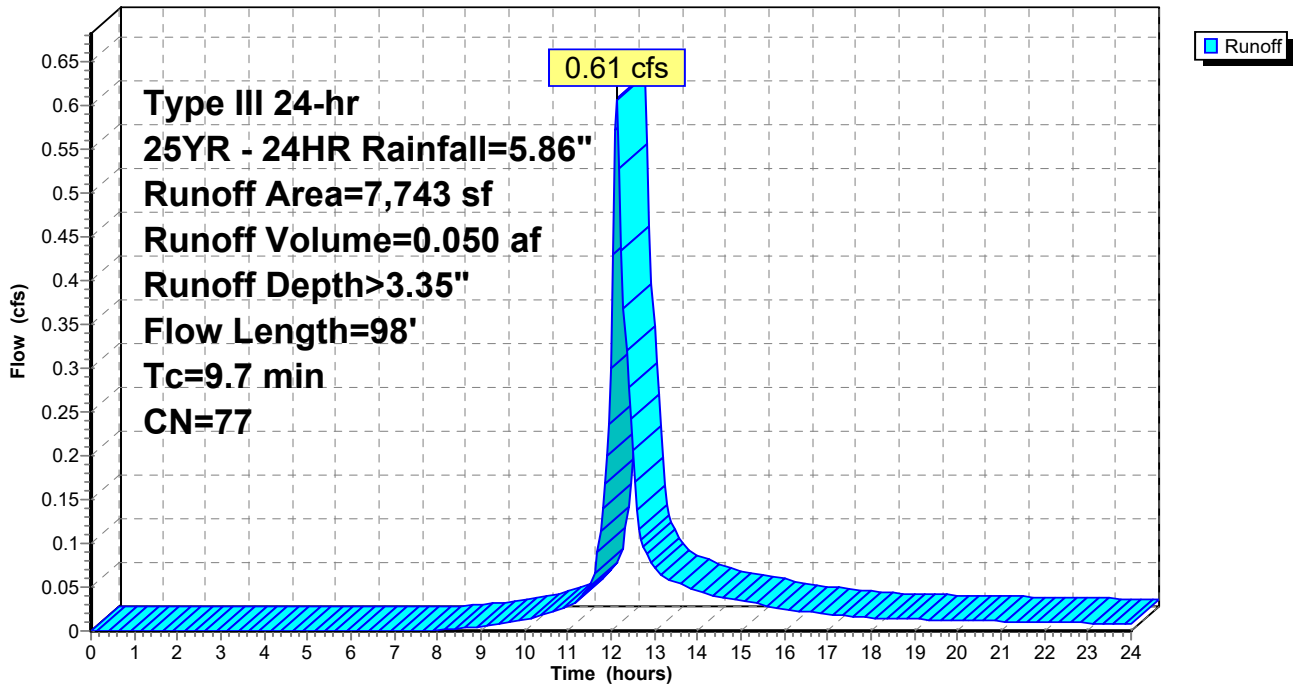
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
2,685	98	Unconnected roofs, HSG A
2,705	39	>75% Grass cover, Good, HSG A
2,353	98	Unconnected pavement, HSG A
7,743	77	Weighted Average
2,705		34.93% Pervious Area
5,038		65.07% Impervious Area
5,038		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.4	60	0.0083	0.11		Sheet Flow, Segment 1 Grass: Short n= 0.150 P2= 3.08"
0.3	38	0.0132	2.33		Shallow Concentrated Flow, Segment 2 Paved Kv= 20.3 fps
9.7	98	Total			

Subcatchment 7S: Subcatchment 7

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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 8S: Subcatchment 8

Runoff = 0.68 cfs @ 12.16 hrs, Volume= 0.061 af, Depth> 1.67"

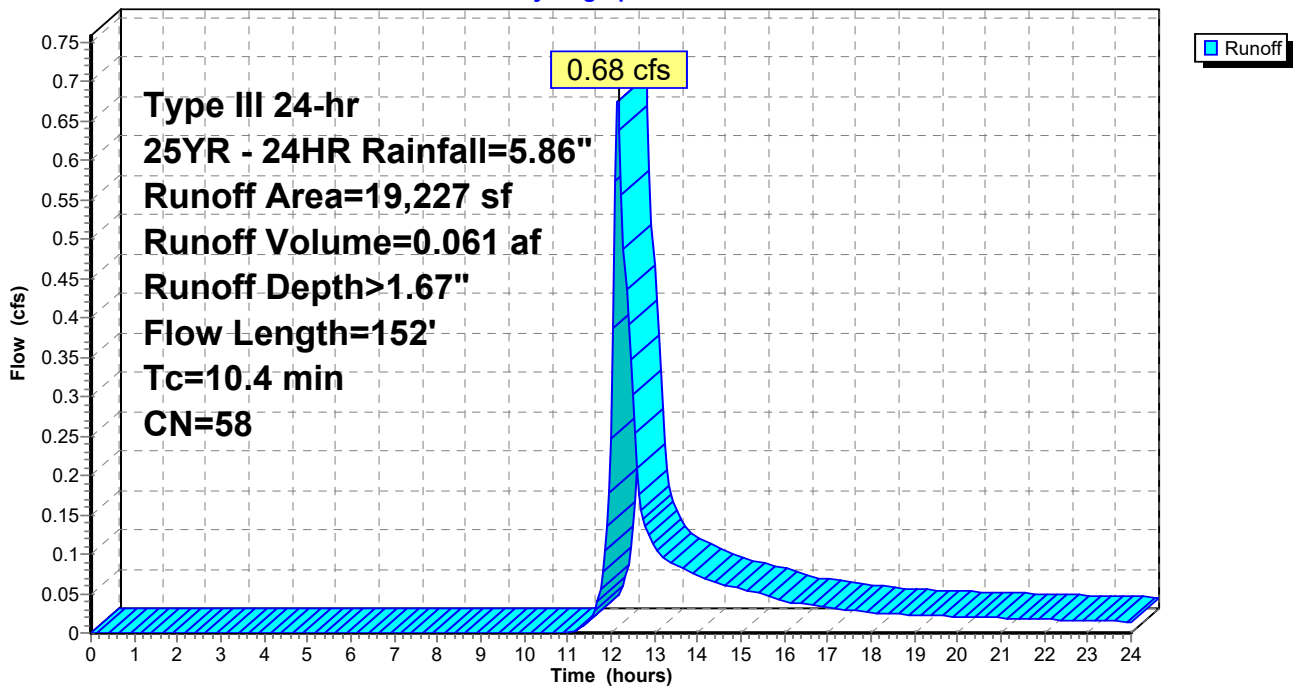
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
2,600	98	Unconnected roofs, HSG A
12,952	39	>75% Grass cover, Good, HSG A
3,675	98	Unconnected pavement, HSG A
19,227	58	Weighted Average
12,952		67.36% Pervious Area
6,275		32.64% Impervious Area
6,275		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.5	87	0.0172	0.15		Sheet Flow, Segment 1 Grass: Short n= 0.150 P2= 3.08"
0.9	65	0.0309	1.23		Shallow Concentrated Flow, Segment 2 Short Grass Pasture Kv= 7.0 fps
10.4	152	Total			

Subcatchment 8S: Subcatchment 8

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 9S: Subcatchment 9

Runoff = 0.63 cfs @ 12.39 hrs, Volume= 0.100 af, Depth> 0.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Adj	Description
606	98		Unconnected roofs, HSG A
50,011	39		>75% Grass cover, Good, HSG A
14,252	98		Unconnected pavement, HSG A
64,869	53	46	Weighted Average, UI Adjusted
50,011			77.10% Pervious Area
14,858			22.90% Impervious Area
14,858			100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0	100	0.0200	0.17		Sheet Flow, Segment 1 Grass: Short n= 0.150 P2= 3.08"
6.5	195	0.0051	0.50		Shallow Concentrated Flow, Segment 2 Short Grass Pasture Kv= 7.0 fps
1.6	88	0.0170	0.91		Shallow Concentrated Flow, Segment 3 Short Grass Pasture Kv= 7.0 fps
1.2	101	0.0397	1.39		Shallow Concentrated Flow, Segment 4 Short Grass Pasture Kv= 7.0 fps
19.3	484	Total			

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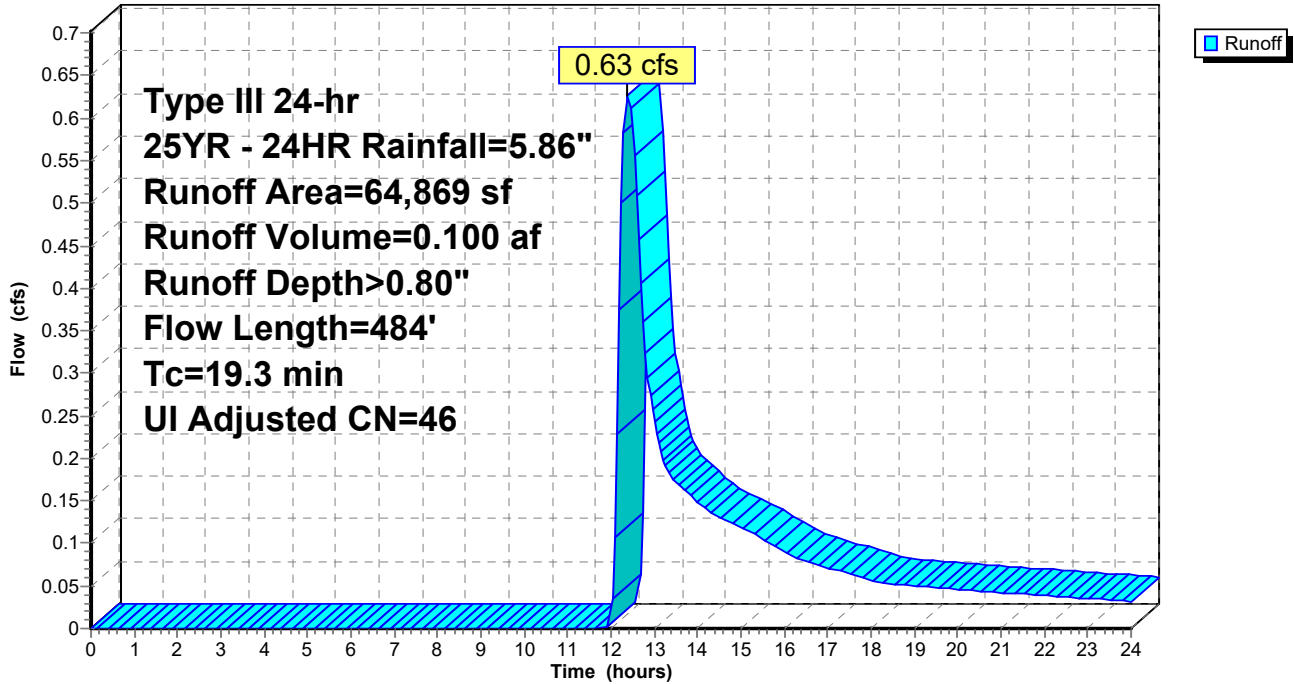
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 9S: Subcatchment 9

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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 10S: Subcatchment 10

Runoff = 0.24 cfs @ 12.50 hrs, Volume= 0.052 af, Depth> 0.51"

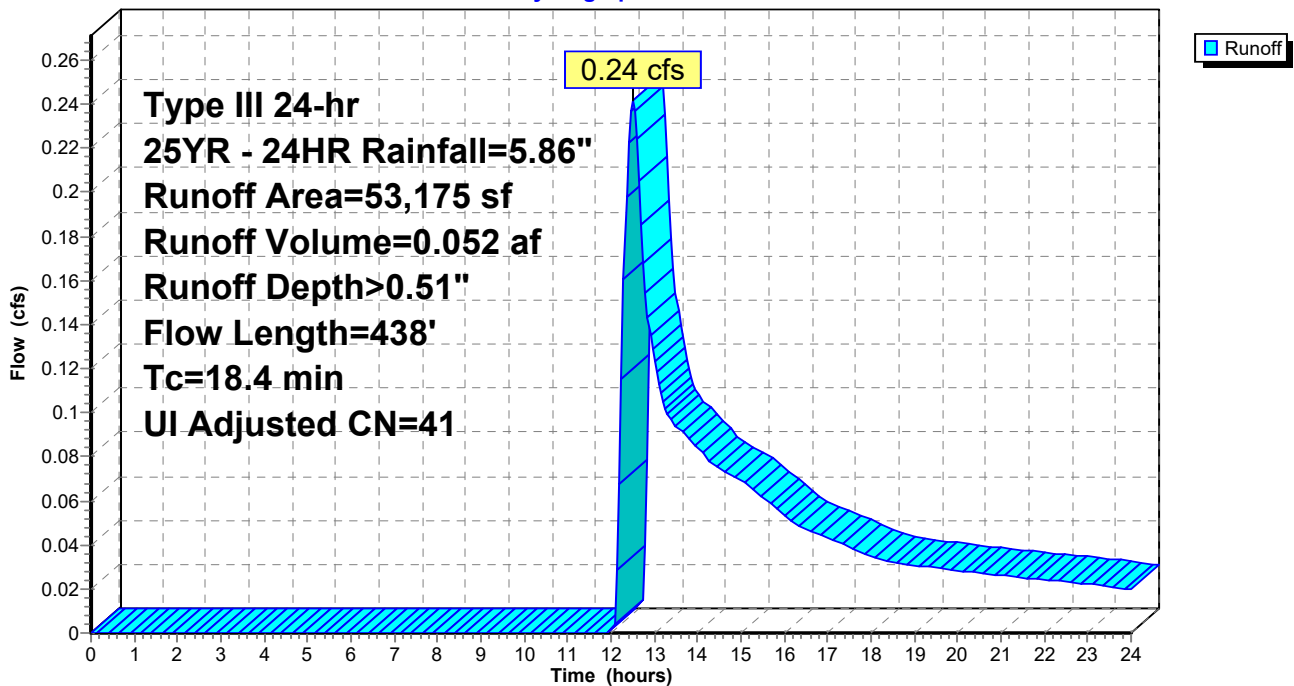
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Adj	Description
1,952	98		Unconnected roofs, HSG A
50,218	39		>75% Grass cover, Good, HSG A
1,005	98		Unconnected pavement, HSG A
53,175	42	41	Weighted Average, UI Adjusted
50,218			94.44% Pervious Area
2,957			5.56% Impervious Area
2,957			100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.1	99	0.0151	0.15		Sheet Flow, Segment 1 Grass: Short n= 0.150 P2= 3.08"
0.9	76	0.0394	1.39		Shallow Concentrated Flow, Segment 2 Short Grass Pasture Kv= 7.0 fps
6.4	263	0.0095	0.68		Shallow Concentrated Flow, Segment 3 Short Grass Pasture Kv= 7.0 fps
18.4	438	Total			

Subcatchment 10S: Subcatchment 10

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 11S: Area Behind the Dove

Runoff = 0.66 cfs @ 12.50 hrs, Volume= 0.128 af, Depth> 0.62"

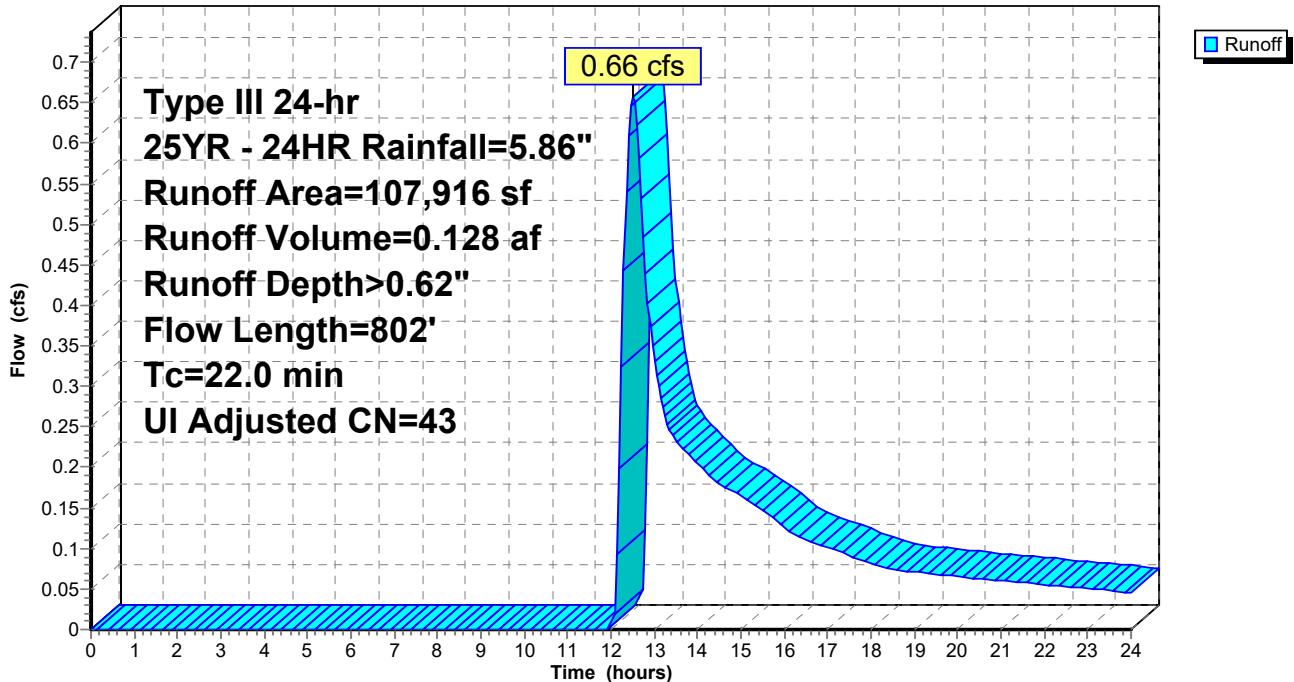
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Adj	Description
6,579	98		Unconnected roofs, HSG A
60,379	39		>75% Grass cover, Good, HSG A
16,182	30		Woods, Good, HSG A
24,776	55		Woods, Good, HSG B
107,916	45	43	Weighted Average, UI Adjusted
101,337			93.90% Pervious Area
6,579			6.10% Impervious Area
6,579			100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.3	100	0.0850	0.14		Sheet Flow, 1 Woods: Light underbrush n= 0.400 P2= 3.08"
3.6	314	0.0830	1.44		Shallow Concentrated Flow, 2 Woodland Kv= 5.0 fps
6.1	388	0.0230	1.06		Shallow Concentrated Flow, 3 Short Grass Pasture Kv= 7.0 fps
22.0	802	Total			

Subcatchment 11S: Area Behind the Dove

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 16S: Subcatchment #16

Runoff = 4.75 cfs @ 12.46 hrs, Volume= 0.686 af, Depth> 1.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
236	98	Unconnected roofs, HSG A
91,643	39	>75% Grass cover, Good, HSG A
7,961	98	Unconnected pavement, HSG A
13,631	30	Woods, Good, HSG A
147,179	55	Woods, Good, HSG B
21,267	70	Woods, Good, HSG C
1,743	80	>75% Grass cover, Good, HSG D
13,531	77	Woods, Good, HSG D
297,191	52	Weighted Average
288,994		97.24% Pervious Area
8,197		2.76% Impervious Area
8,197		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.1	100	0.1400	0.17		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
1.3	75	0.0398	1.00		Shallow Concentrated Flow, Segment #2 Woodland Kv= 5.0 fps
2.4	250	0.1202	1.73		Shallow Concentrated Flow, Segment #3 Woodland Kv= 5.0 fps
2.5	132	0.0302	0.87		Shallow Concentrated Flow, Segment #4 Woodland Kv= 5.0 fps
4.9	129	0.0078	0.44		Shallow Concentrated Flow, Segment #5 Woodland Kv= 5.0 fps
4.3	291	0.0515	1.13		Shallow Concentrated Flow, Segment #6 Woodland Kv= 5.0 fps
1.7	136	0.0369	1.34		Shallow Concentrated Flow, Segment #7 Short Grass Pasture Kv= 7.0 fps
27.2	1,113	Total			

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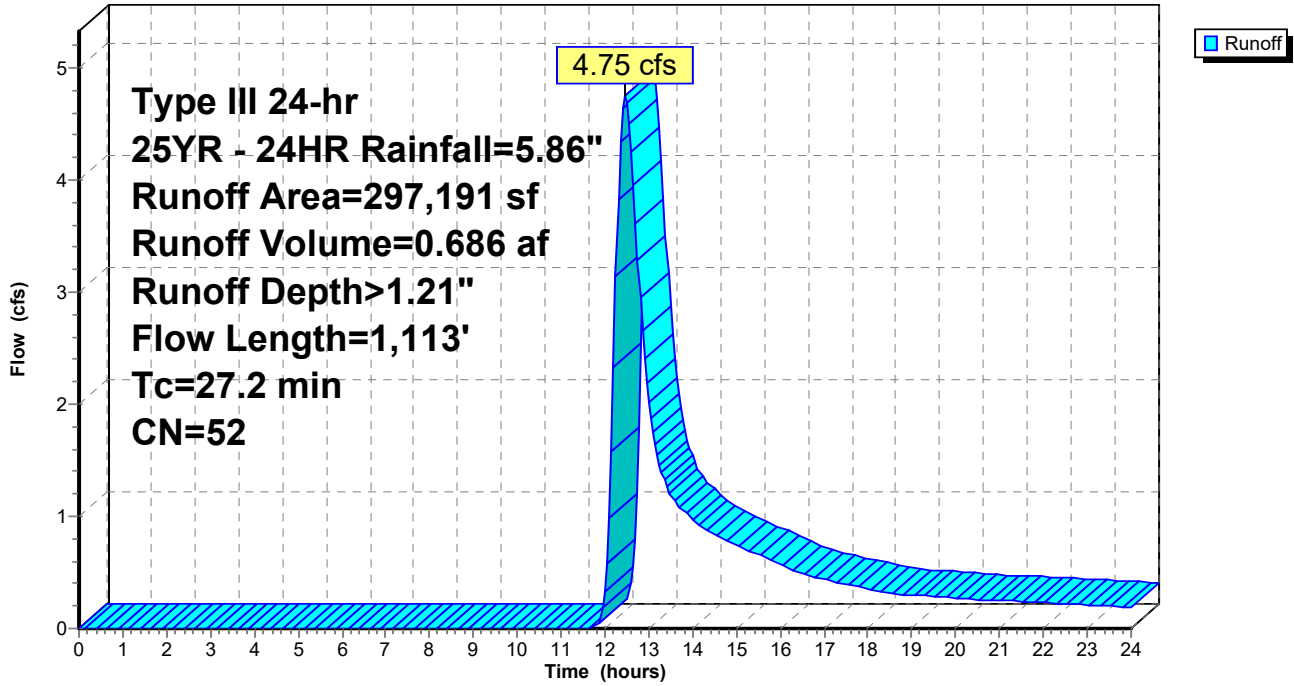
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 16S: Subcatchment #16

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 17S: Subcatchment #17

Runoff = 8.25 cfs @ 12.57 hrs, Volume= 1.283 af, Depth> 1.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Adj	Description
3,184	39		>75% Grass cover, Good, HSG A
1,944	98		Unconnected pavement, HSG A
103,461	30		Woods, Good, HSG A
1,668	61		>75% Grass cover, Good, HSG B
281,168	55		Woods, Good, HSG B
1,922	70		Woods, Good, HSG C
2,361	80		>75% Grass cover, Good, HSG D
1,055	98		Unconnected pavement, HSG D
100,644	77		Woods, Good, HSG D
497,407	55	54	Weighted Average, UI Adjusted
494,408			99.40% Pervious Area
2,999			0.60% Impervious Area
2,999			100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
15.2	100	0.0500	0.11		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
8.0	729	0.0919	1.52		Shallow Concentrated Flow, Segment #2 Woodland Kv= 5.0 fps
1.4	181	0.1752	2.09		Shallow Concentrated Flow, Segment #3 Woodland Kv= 5.0 fps
9.1	390	0.0205	0.72		Shallow Concentrated Flow, Segment #4 Woodland Kv= 5.0 fps
1.8	140	0.0648	1.27		Shallow Concentrated Flow, Segment #5 Woodland Kv= 5.0 fps
35.5	1,540	Total			

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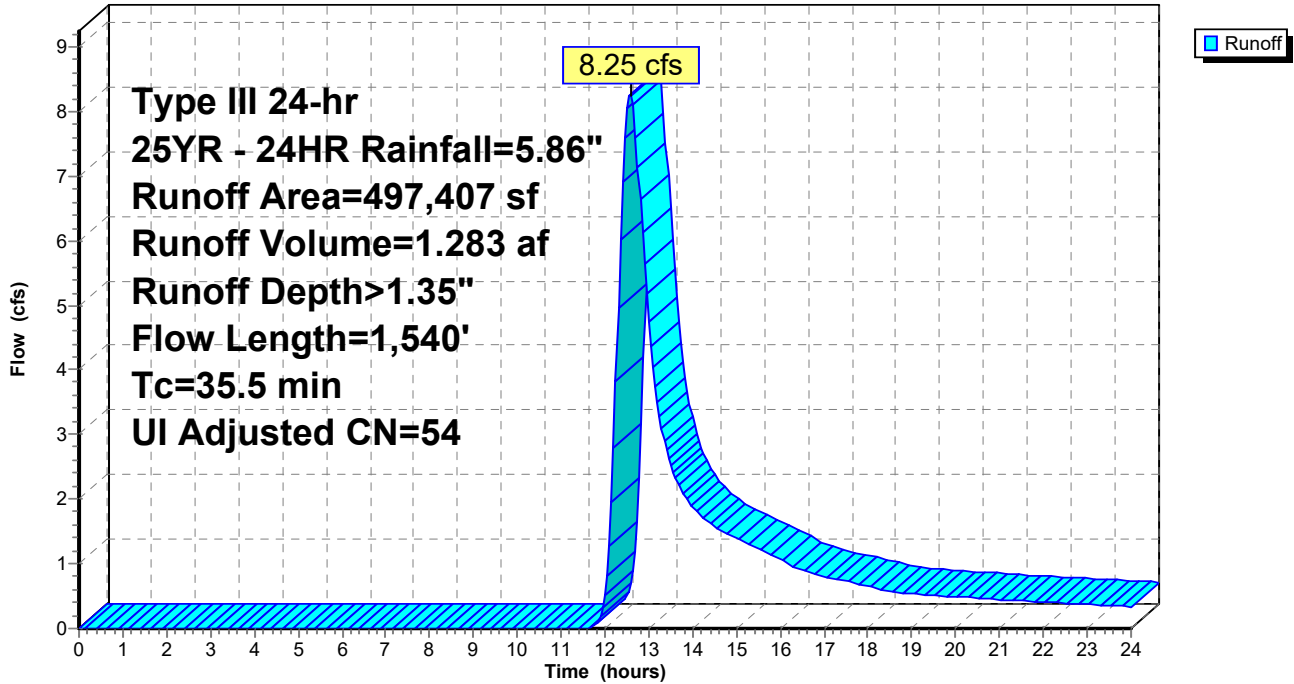
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 17S: Subcatchment #17

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Summary for Subcatchment 18S: Subcatchment #18

Runoff = 10.53 cfs @ 12.46 hrs, Volume= 1.433 af, Depth> 1.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
927	98	Unconnected pavement, HSG A
120,426	30	Woods, Good, HSG A
150,784	55	Woods, Good, HSG B
107,366	70	Woods, Good, HSG C
105	98	Unconnected pavement, HSG D
95,088	77	Woods, Good, HSG D
474,696	57	Weighted Average
473,664		99.78% Pervious Area
1,032		0.22% Impervious Area
1,032		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
15.2	100	0.0500	0.11		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
4.5	544	0.1637	2.02		Shallow Concentrated Flow, Segment #2 Woodland Kv= 5.0 fps
0.6	71	0.1840	2.14		Shallow Concentrated Flow, Segment #3 Woodland Kv= 5.0 fps
6.7	382	0.0366	0.96		Shallow Concentrated Flow, Segment #4 Woodland Kv= 5.0 fps
0.8	91	0.1422	1.89		Shallow Concentrated Flow, Segment #5 Woodland Kv= 5.0 fps
1.5	92	0.0436	1.04		Shallow Concentrated Flow, Segment #6 Woodland Kv= 5.0 fps
29.3	1,280	Total			

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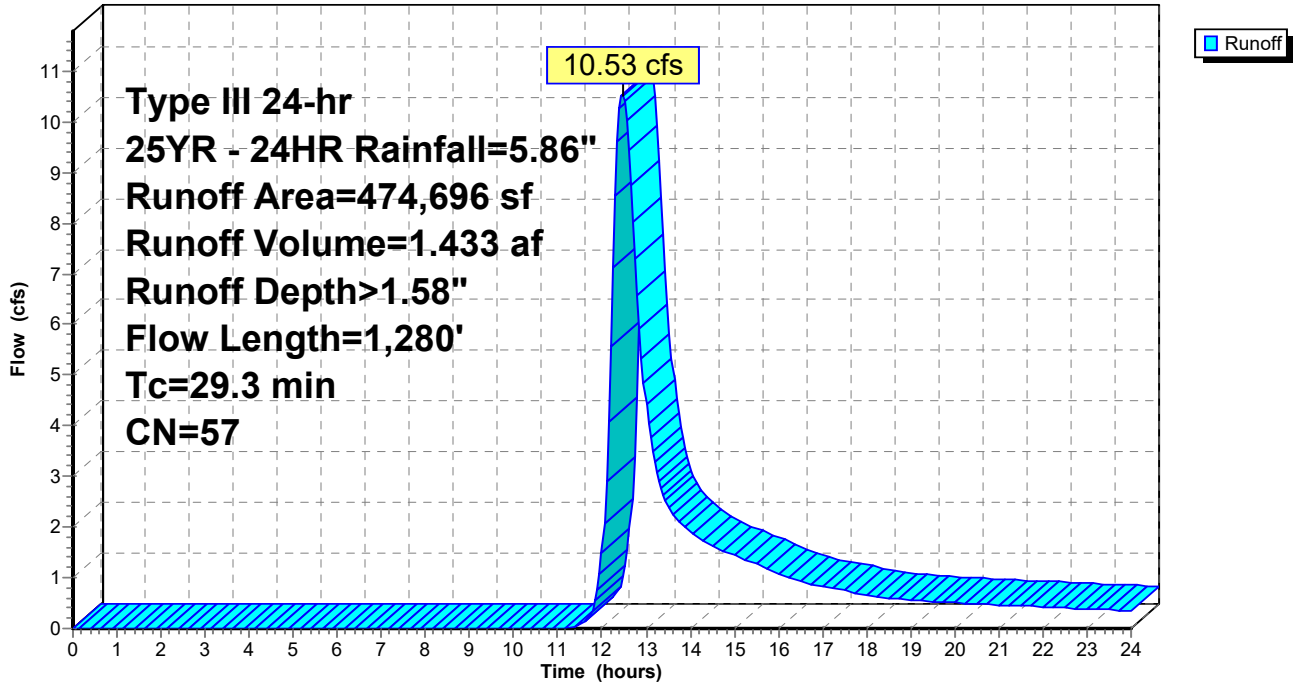
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 18S: Subcatchment #18

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 19S: Subcatchment #19

Runoff = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af, Depth> 1.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
277,033	30	Woods, Good, HSG A
113,562	55	Woods, Good, HSG B
59,667	70	Woods, Good, HSG C
240,560	77	Woods, Good, HSG D
690,822	54	Weighted Average
690,822		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.6	100	0.0400	0.10		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
6.0	653	0.1333	1.83		Shallow Concentrated Flow, Segment #2 Woodland Kv= 5.0 fps
1.5	167	0.1346	1.83		Shallow Concentrated Flow, Segment #3 Woodland Kv= 5.0 fps
7.7	327	0.0199	0.71		Shallow Concentrated Flow, Segment #4 Woodland Kv= 5.0 fps
2.4	161	0.0496	1.11		Shallow Concentrated Flow, Segment #5 Woodland Kv= 5.0 fps
0.5	59	0.1530	1.96		Shallow Concentrated Flow, Segment #6 Woodland Kv= 5.0 fps
6.3	193	0.0104	0.51		Shallow Concentrated Flow, Segment #7 Woodland Kv= 5.0 fps
5.3	172	0.0116	0.54		Shallow Concentrated Flow, Segment #8 Woodland Kv= 5.0 fps
46.3	1,832	Total			

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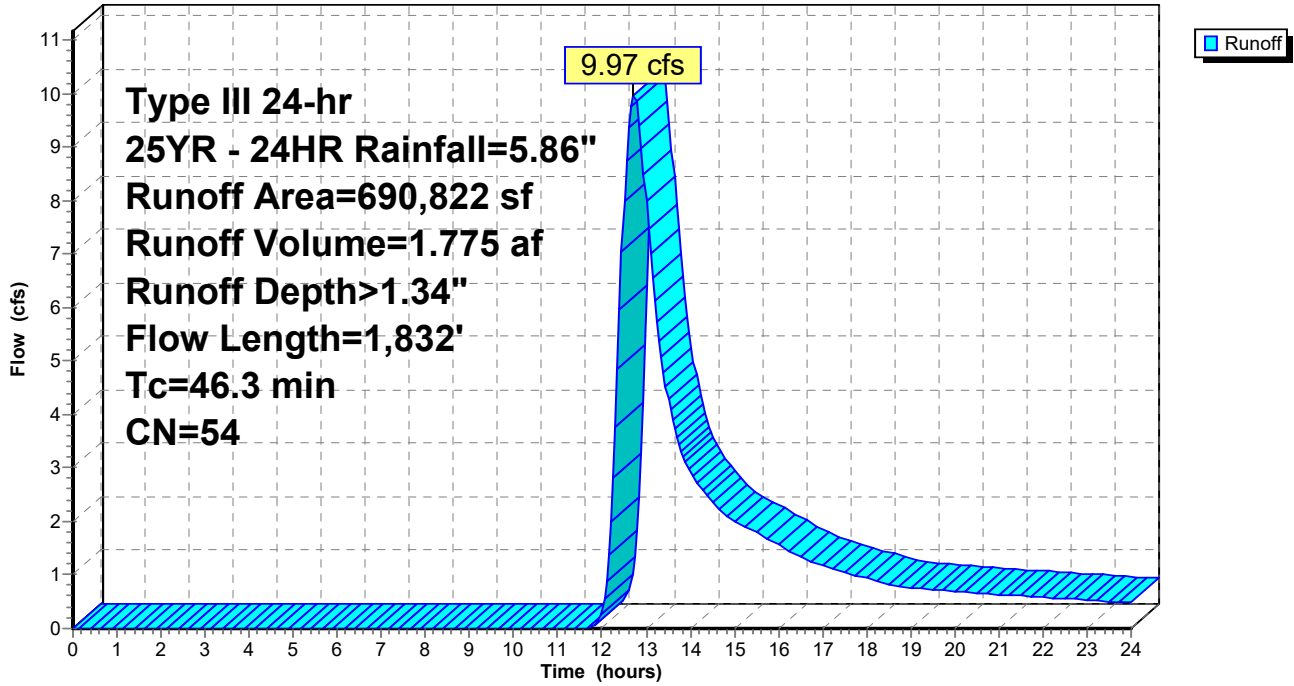
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 19S: Subcatchment #19

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Summary for Reach 2R: Reach 2

Inflow Area = 17.551 ac, 0.65% Impervious, Inflow Depth > 1.19" for 25YR - 24HR event
Inflow = 8.18 cfs @ 12.93 hrs, Volume= 1.744 af
Outflow = 8.17 cfs @ 12.95 hrs, Volume= 1.741 af, Atten= 0%, Lag= 1.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 3.59 fps, Min. Travel Time= 1.5 min
Avg. Velocity = 1.95 fps, Avg. Travel Time= 2.8 min

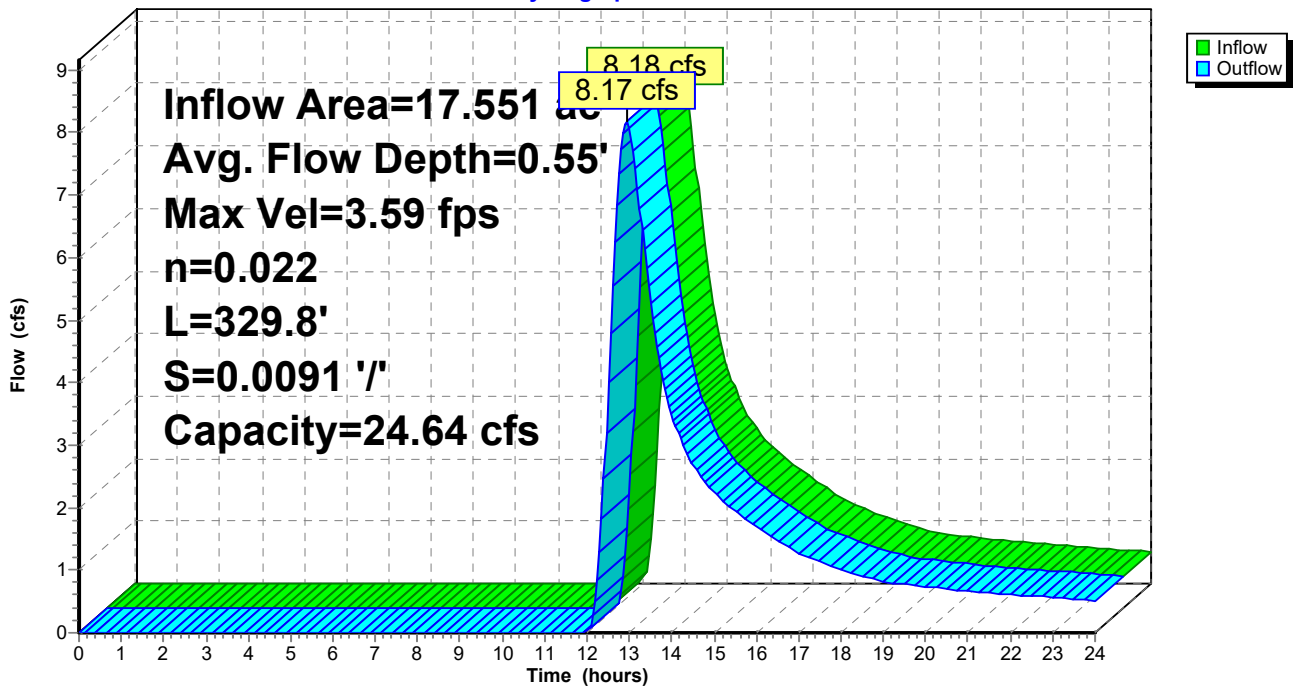
Peak Storage= 751 cf @ 12.95 hrs
Average Depth at Peak Storage= 0.55'
Bank-Full Depth= 1.00' Flow Area= 5.0 sf, Capacity= 24.64 cfs

3.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight
Side Slope Z-value= 2.0 ' / ' Top Width= 7.00'
Length= 329.8' Slope= 0.0091 ' / '
Inlet Invert= 202.00', Outlet Invert= 199.00'



Reach 2R: Reach 2

Hydrograph



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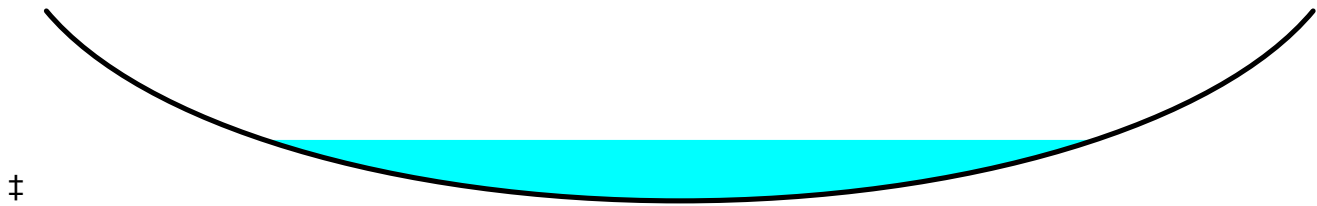
Summary for Reach 11R: Flow Through 8

Inflow Area = 2.477 ac, 6.10% Impervious, Inflow Depth > 0.62" for 25YR - 24HR event
Inflow = 0.66 cfs @ 12.50 hrs, Volume= 0.128 af
Outflow = 0.66 cfs @ 12.52 hrs, Volume= 0.128 af, Atten= 0%, Lag= 0.8 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 1.09 fps, Min. Travel Time= 1.2 min
Avg. Velocity = 0.62 fps, Avg. Travel Time= 2.0 min

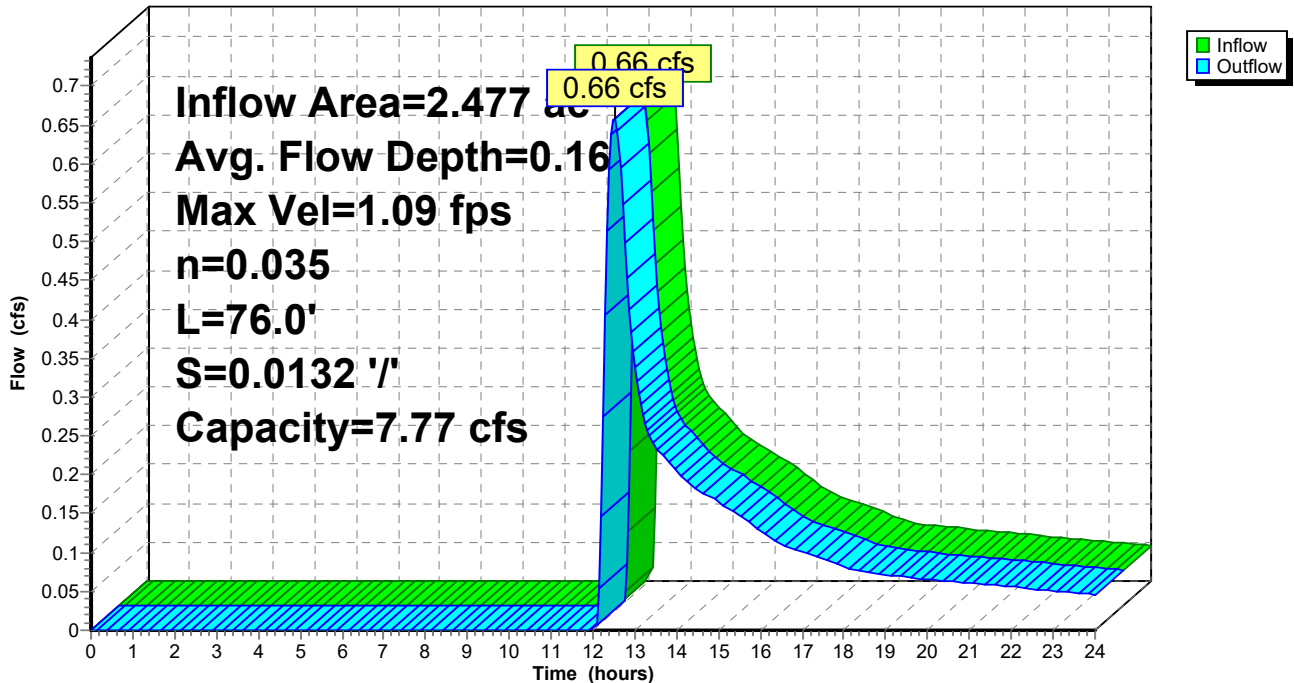
Peak Storage= 46 cf @ 12.52 hrs
Average Depth at Peak Storage= 0.16'
Bank-Full Depth= 0.50' Flow Area= 3.3 sf, Capacity= 7.77 cfs

10.00' x 0.50' deep Parabolic Channel, n= 0.035
Length= 76.0' Slope= 0.0132 '/'
Inlet Invert= 199.00', Outlet Invert= 198.00'



Reach 11R: Flow Through 8

Hydrograph



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Summary for Reach 100R: Reach 100

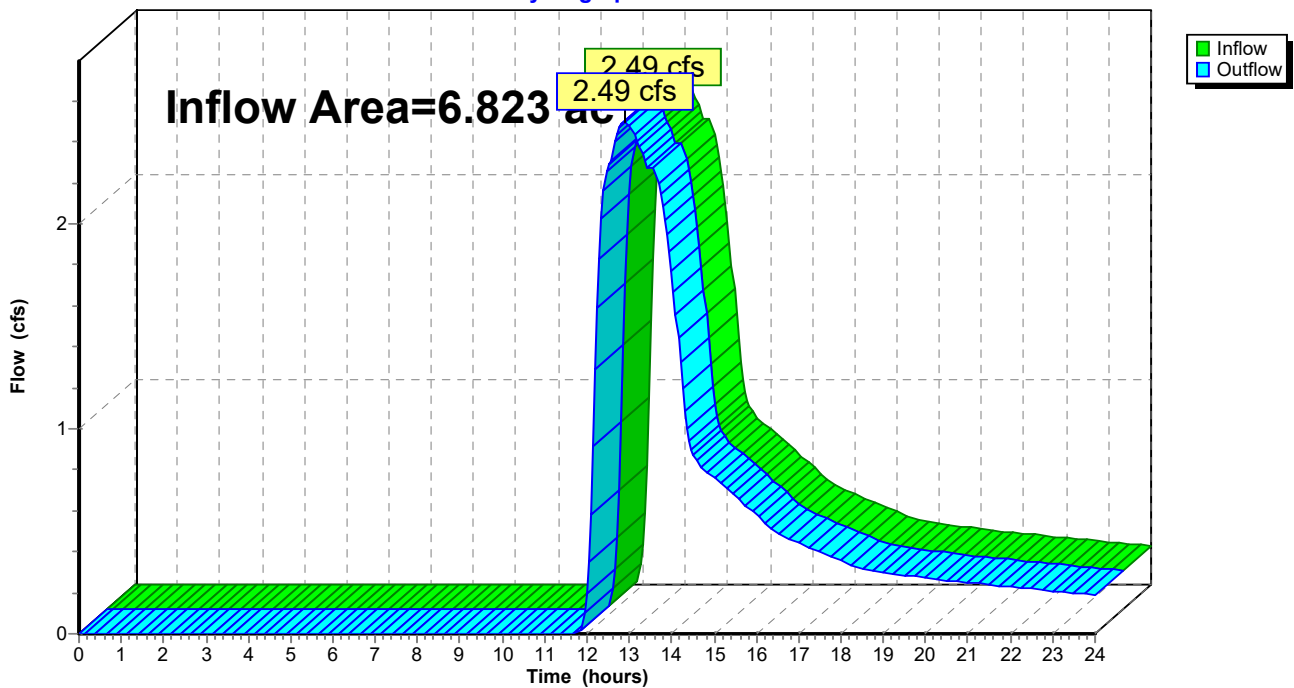
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 6.823 ac, 2.76% Impervious, Inflow Depth > 1.20" for 25YR - 24HR event
Inflow = 2.49 cfs @ 12.88 hrs, Volume= 0.685 af
Outflow = 2.49 cfs @ 12.88 hrs, Volume= 0.685 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Reach 100R: Reach 100

Hydrograph



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Summary for Reach 200R: Reach 200

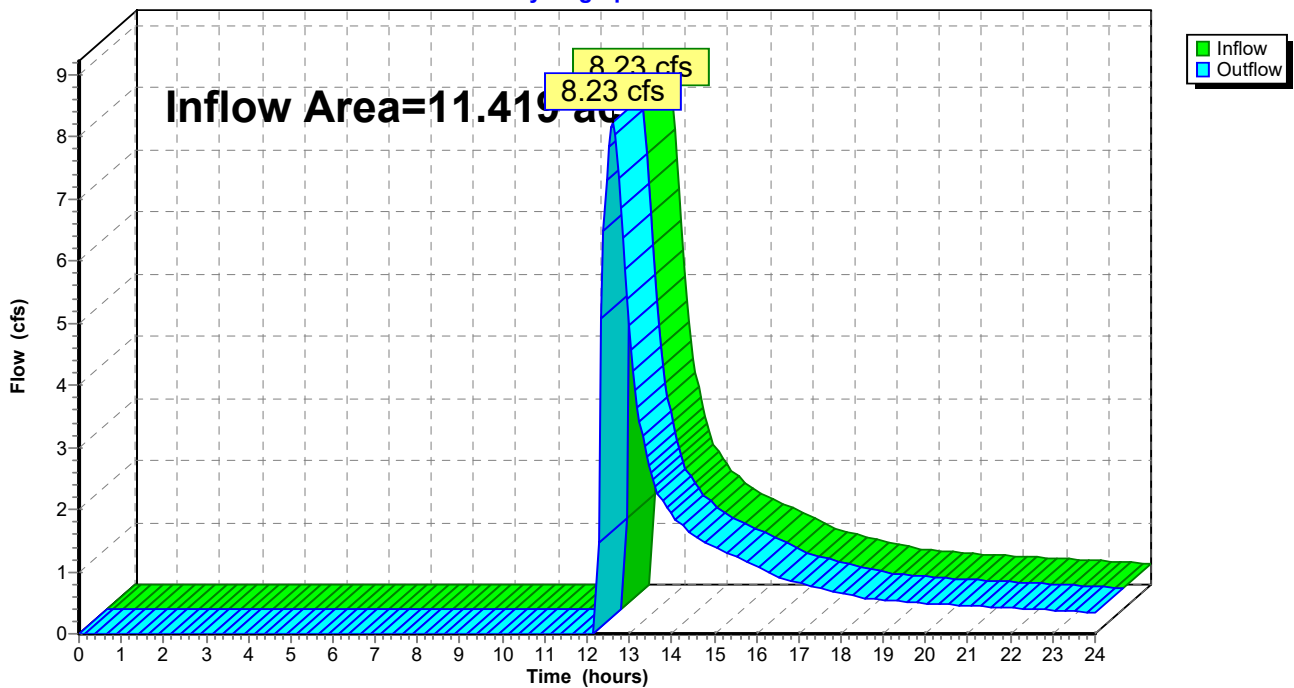
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 11.419 ac, 0.60% Impervious, Inflow Depth > 1.29" for 25YR - 24HR event
Inflow = 8.23 cfs @ 12.59 hrs, Volume= 1.232 af
Outflow = 8.23 cfs @ 12.59 hrs, Volume= 1.232 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Reach 200R: Reach 200

Hydrograph



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Summary for Reach 300R: Reach 300

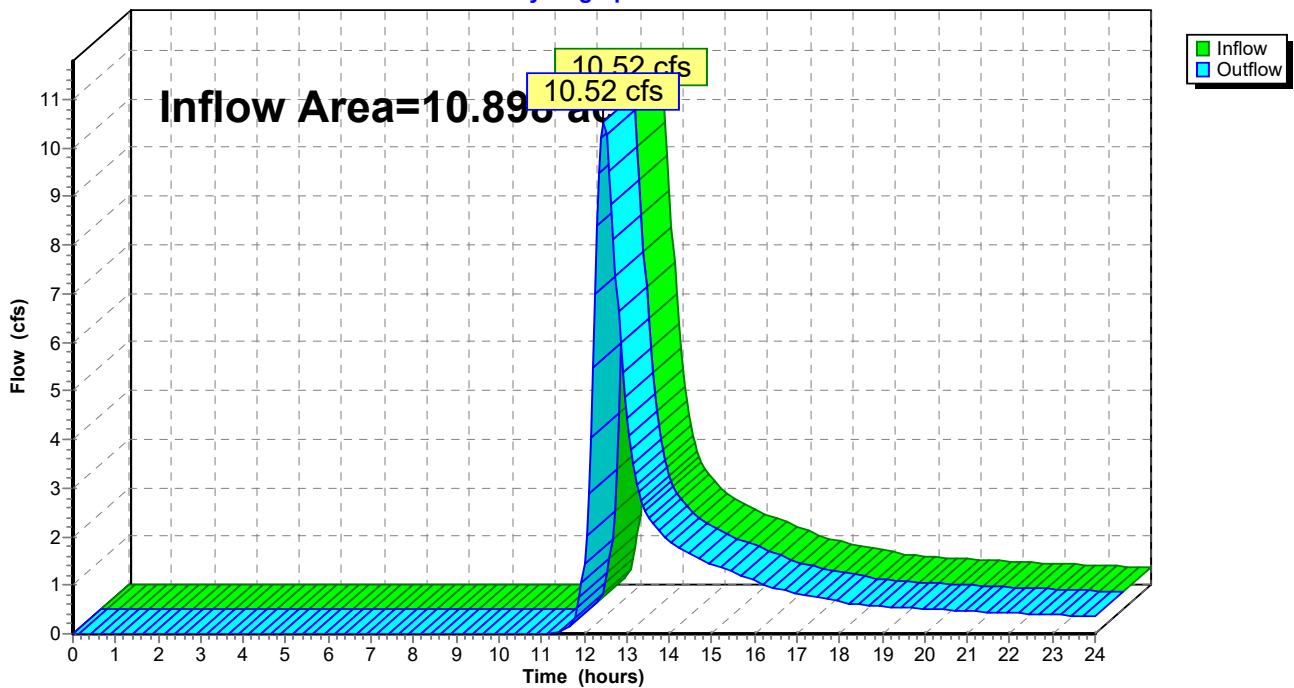
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 10.898 ac, 0.22% Impervious, Inflow Depth > 1.58" for 25YR - 24HR event
Inflow = 10.52 cfs @ 12.47 hrs, Volume= 1.433 af
Outflow = 10.52 cfs @ 12.47 hrs, Volume= 1.433 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Reach 300R: Reach 300

Hydrograph



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Summary for Reach 400R: Reach 400

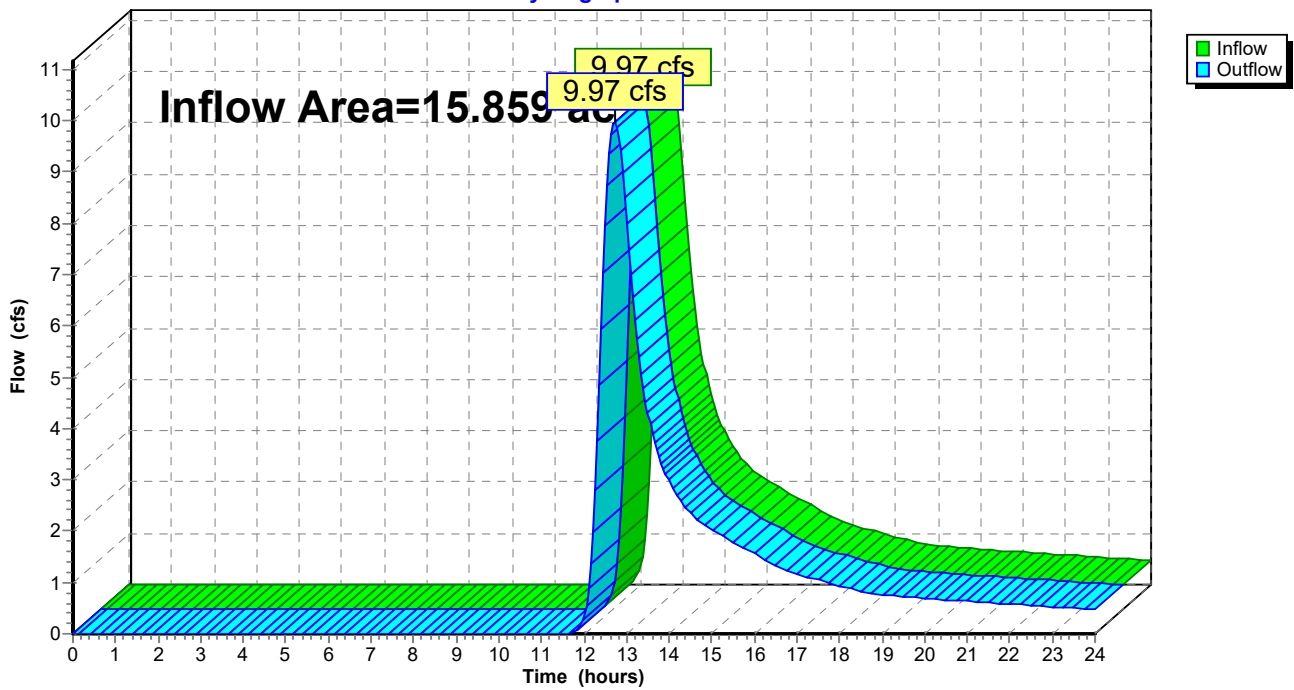
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 15.859 ac, 0.00% Impervious, Inflow Depth > 1.34" for 25YR - 24HR event
Inflow = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af
Outflow = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Reach 400R: Reach 400

Hydrograph



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Summary for Reach 800R: Svenson Pond

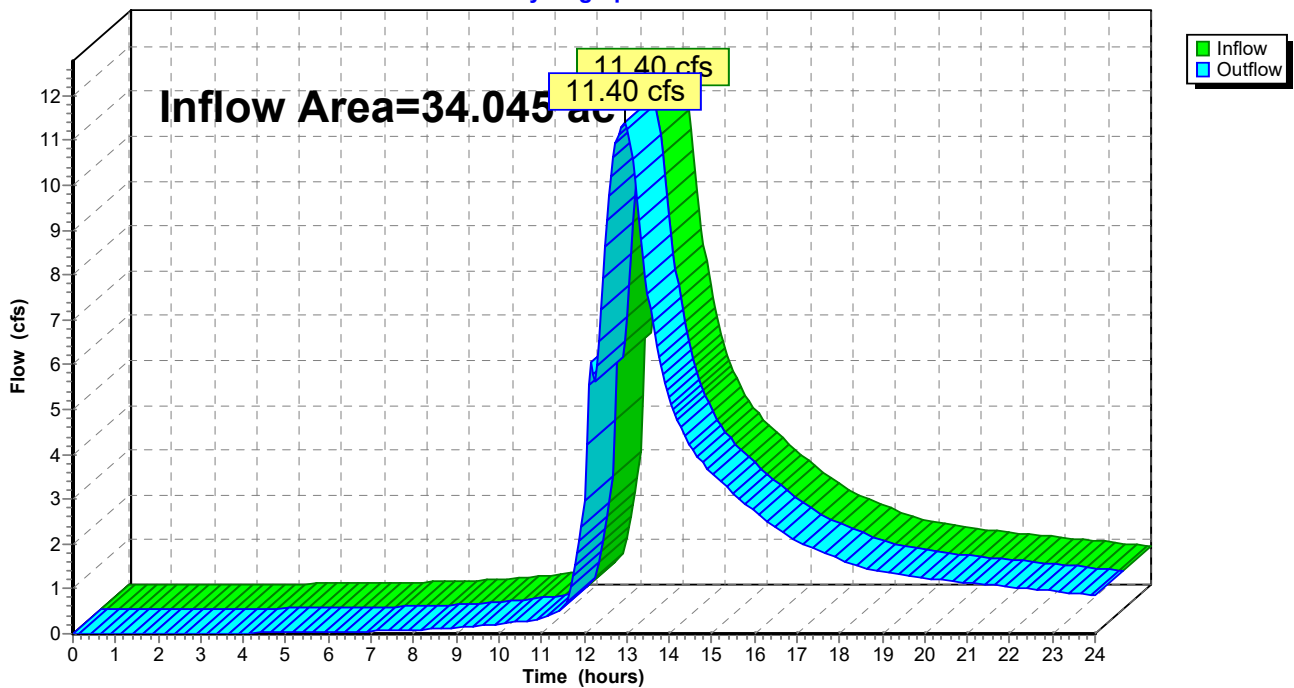
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 34.045 ac, 5.18% Impervious, Inflow Depth > 1.07" for 25YR - 24HR event
Inflow = 11.40 cfs @ 12.94 hrs, Volume= 3.023 af
Outflow = 11.40 cfs @ 12.94 hrs, Volume= 3.023 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Reach 800R: Svenson Pond

Hydrograph



20-097 Existing Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 1P: Pond 1

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

Inflow Area = 6.978 ac, 0.00% Impervious, Inflow Depth > 0.74" for 25YR - 24HR event
 Inflow = 2.15 cfs @ 12.62 hrs, Volume= 0.428 af
 Outflow = 2.16 cfs @ 12.64 hrs, Volume= 0.428 af, Atten= 0%, Lag= 1.4 min
 Primary = 2.16 cfs @ 12.64 hrs, Volume= 0.428 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 203.37' @ 12.63 hrs Surf.Area= 46 sf Storage= 18 cf
 Flood Elev= 205.00' Surf.Area= 8,255 sf Storage= 3,340 cf

Plug-Flow detention time= 0.1 min calculated for 0.427 af (100% of inflow)
 Center-of-Mass det. time= 0.1 min (938.5 - 938.5)

Volume	Invert	Avail.Storage	Storage Description			
#1	201.13'	3,340 cf	Open Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
201.13	5	9.6	0	0	5	
202.00	5	9.6	4	4	13	
203.00	6	10.7	5	10	24	
204.00	202	93.0	81	91	705	
205.00	8,255	814.0	3,249	3,340	52,746	

Device	Routing	Invert	Outlet Devices
#1	Primary	201.13'	12.0" Round 12" CMP L= 34.7' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 201.13' / 198.83' S= 0.0663 1' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 0.79 sf
#2	Secondary	204.67'	20.0' long x 10.0' breadth Edge of Parking Lot Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=2.15 cfs @ 12.64 hrs HW=203.36' TW=202.67' (Dynamic Tailwater)
 ↑1=12" CMP (Outlet Controls 2.15 cfs @ 2.74 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=201.13' TW=198.65' (Dynamic Tailwater)
 ↑2=Edge of Parking Lot (Controls 0.00 cfs)

20-097 Existing Analysis

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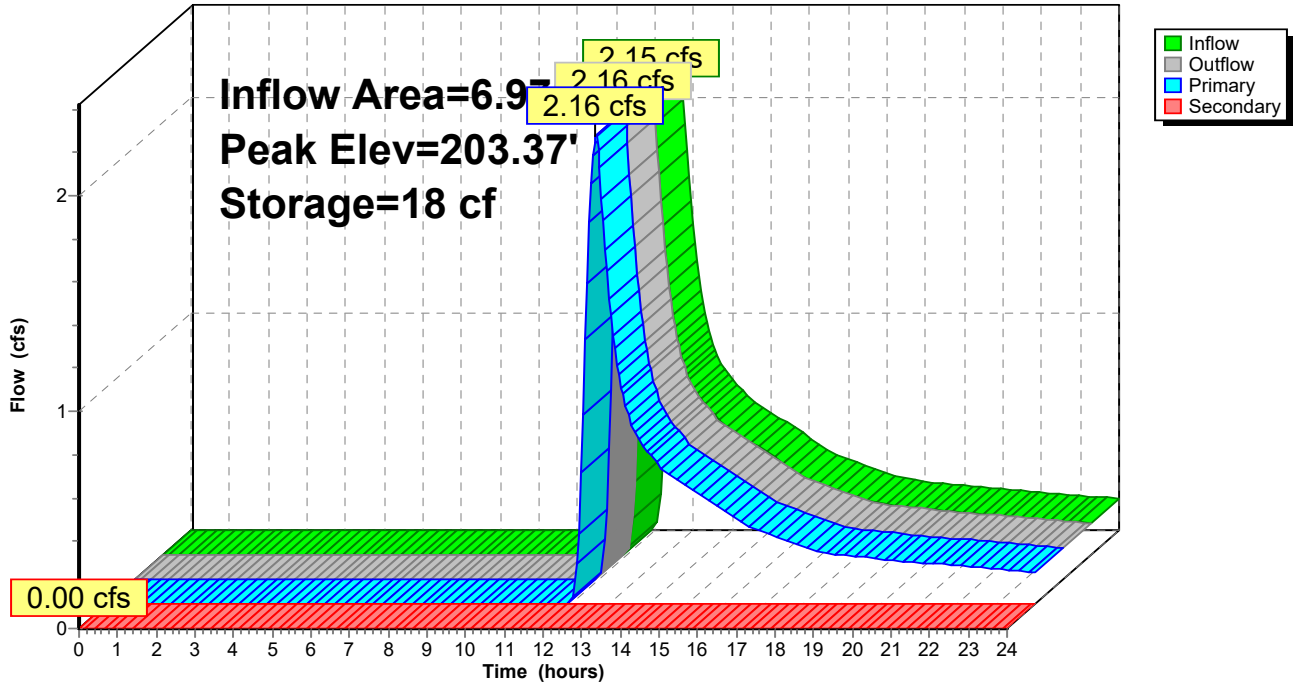
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Pond 1P: Pond 1

Hydrograph



20-097 Existing Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 2P: Existing CB#8

This Basin has an outlet culvert which is half in the basin, below the rim, and is mostly exposed above the rim. This structure also has incoming flow below the invert out. This model best represents the existing conditions.

[61] Hint: Exceeded Reach 2R outlet invert by 0.20' @ 12.95 hrs
 [80] Warning: Exceeded Pond 7P by 0.01' @ 5.35 hrs (0.42 cfs 0.014 af)

Inflow Area = 29.637 ac, 3.81% Impervious, Inflow Depth > 1.11" for 25YR - 24HR event
 Inflow = 10.78 cfs @ 12.88 hrs, Volume= 2.736 af
 Outflow = 10.70 cfs @ 12.92 hrs, Volume= 2.735 af, Atten= 1%, Lag= 2.4 min
 Primary = 10.70 cfs @ 12.92 hrs, Volume= 2.735 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 199.20' @ 12.93 hrs Surf.Area= 954 sf Storage= 333 cf
 Flood Elev= 200.07' Surf.Area= 5,143 sf Storage= 2,904 cf

Plug-Flow detention time= 0.4 min calculated for 2.735 af (100% of inflow)
 Center-of-Mass det. time= 0.3 min (909.9 - 909.7)

Volume	Invert	Avail.Storage	Storage Description
#1	195.00'	38 cf	4.00'D x 3.00'H Basin
#2	198.00'	7,638 cf	Open Water Storage (Irregular) Listed below (Recalc)
		7,675 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
198.00	8	15.0	0	0	8
199.00	425	170.0	164	164	2,292
200.00	5,130	630.0	2,344	2,508	31,579
201.00	5,130	630.0	5,130	7,638	32,209

Device	Routing	Invert	Outlet Devices
#1	Primary	196.62'	24.0" Round 24" CMP L= 67.8' Ke= 0.500 Inlet / Outlet Invert= 196.62' / 196.28' S= 0.0050 '/' Cc= 0.900 n= 0.025, Flow Area= 3.14 sf
#2	Secondary	200.07'	30.0' long x 10.0' breadth Flow Over Ex. Driveway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=10.69 cfs @ 12.92 hrs HW=199.19' TW=198.43' (Dynamic Tailwater)
 ←1=24" CMP (Outlet Controls 10.69 cfs @ 3.44 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=195.00' TW=196.55' (Dynamic Tailwater)
 ←2=Flow Over Ex. Driveway (Controls 0.00 cfs)

20-097 Existing Analysis

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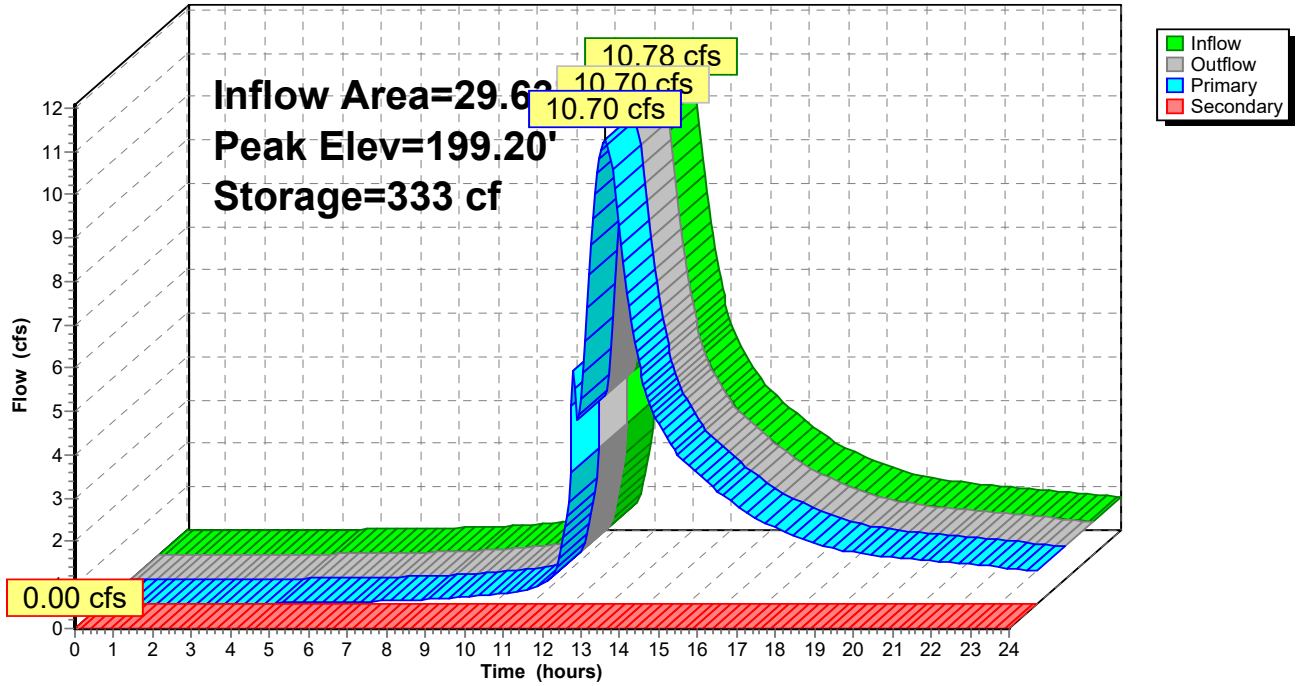
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Pond 2P: Existing CB#8

Hydrograph



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Summary for Pond 4P: Existing CB#4

[80] Warning: Exceeded Pond 1P by 0.04' @ 12.10 hrs (0.21 cfs 0.001 af)

Inflow Area = 7.072 ac, 1.31% Impervious, Inflow Depth > 0.80" for 25YR - 24HR event
 Inflow = 2.22 cfs @ 12.64 hrs, Volume= 0.471 af
 Outflow = 2.22 cfs @ 12.63 hrs, Volume= 0.471 af, Atten= 0%, Lag= 0.0 min
 Primary = 2.22 cfs @ 12.63 hrs, Volume= 0.471 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 202.67' @ 12.63 hrs Surf.Area= 13 sf Storage= 51 cf
 Flood Elev= 205.00' Surf.Area= 25 sf Storage= 85 cf

Plug-Flow detention time= 0.3 min calculated for 0.470 af (100% of inflow)
 Center-of-Mass det. time= 0.2 min (921.8 - 921.5)

Volume	Invert	Avail.Storage	Storage Description
#1	198.65'	80 cf	4.00'D x 6.39'H Basin
#2	203.54'	6 cf	Open Storage (Irregular) Listed below (Recalc)
		86 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
203.54	12	15.0	0	0	12
204.00	12	15.0	6	6	19

Device	Routing	Invert	Outlet Devices
#1	Primary	198.65'	12.0" Round 12" CMP L= 56.4' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 198.65' / 197.33' S= 0.0234 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 0.79 sf
#2	Secondary	203.54'	2.0' long x 2.0' breadth Rim Overflow Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32

Primary OutFlow Max=2.21 cfs @ 12.63 hrs HW=202.67' TW=201.68' (Dynamic Tailwater)
 ↖1=12" CMP (Outlet Controls 2.21 cfs @ 2.82 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=198.65' TW=197.43' (Dynamic Tailwater)
 ↖2=Rim Overflow (Controls 0.00 cfs)

20-097 Existing Analysis

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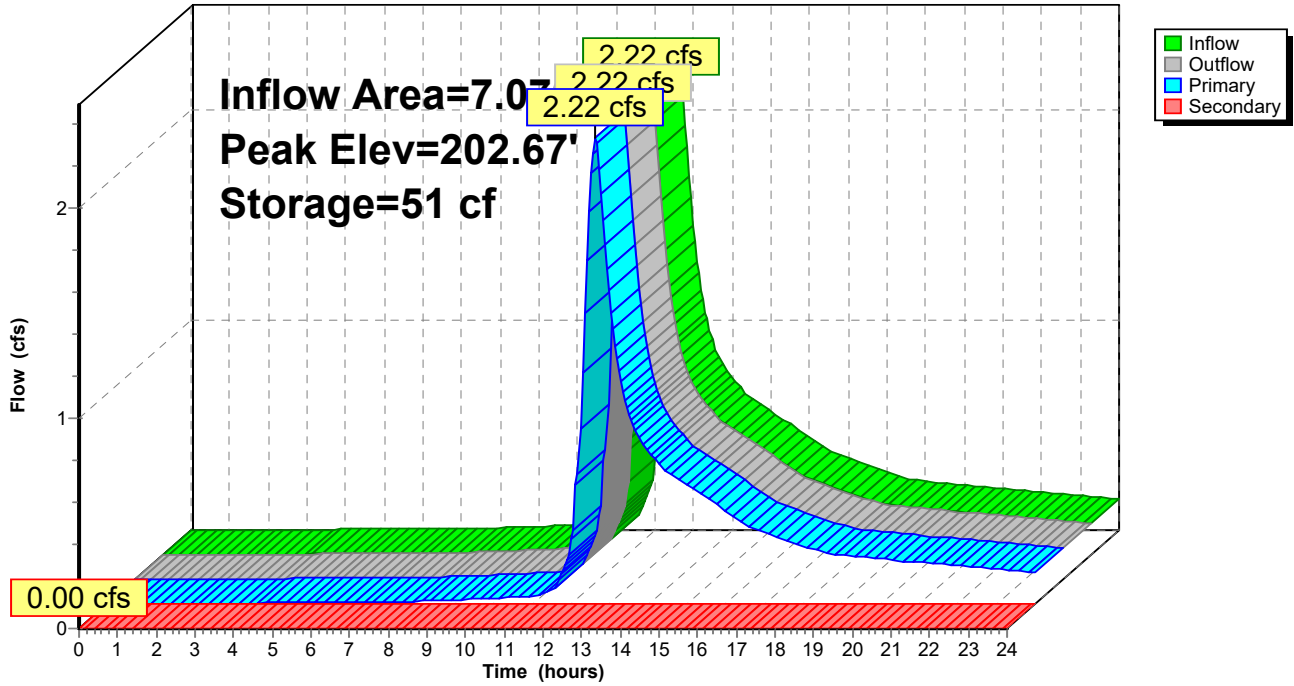
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Pond 4P: Existing CB#4

Hydrograph



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Summary for Pond 5P: Existing CB #5

[58] Hint: Peaked 0.27' above defined flood level

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[80] Warning: Exceeded Pond 4P by 1.25' @ 12.00 hrs (2.48 cfs 0.021 af)

Inflow Area = 7.312 ac, 3.98% Impervious, Inflow Depth > 0.92" for 25YR - 24HR event
 Inflow = 2.38 cfs @ 12.61 hrs, Volume= 0.561 af
 Outflow = 2.38 cfs @ 12.63 hrs, Volume= 0.561 af, Atten= 0%, Lag= 1.3 min
 Primary = 1.90 cfs @ 12.86 hrs, Volume= 0.535 af
 Secondary = 0.68 cfs @ 12.10 hrs, Volume= 0.026 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 201.70' @ 12.10 hrs Surf.Area= 65 sf Storage= 60 cf
 Flood Elev= 201.43' Surf.Area= 35 sf Storage= 50 cf

Plug-Flow detention time= 0.4 min calculated for 0.560 af (100% of inflow)
 Center-of-Mass det. time= 0.3 min (901.3 - 901.0)

Volume	Invert	Avail.Storage	Storage Description
#1	197.43'	50 cf	4.00'D x 4.00'H Basin
#2	201.43'	32 cf	Open Storage (Irregular) Listed below (Recalc)
		82 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
201.43	22	18.0	0	0	22
202.00	100	40.0	32	32	125

Device	Routing	Invert	Outlet Devices
#1	Primary	197.43'	12.0" Round 12" CMP L= 46.1' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 197.43' / 196.02' S= 0.0306 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 0.79 sf
#2	Secondary	201.43'	2.0' long x 2.0' breadth Rim Overflow Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32

Primary OutFlow Max=1.80 cfs @ 12.86 hrs HW=201.46' TW=200.90' (Dynamic Tailwater)
 ↑1=12" CMP (Outlet Controls 1.80 cfs @ 2.29 fps)

Secondary OutFlow Max=0.66 cfs @ 12.10 hrs HW=201.70' TW=201.50' (Dynamic Tailwater)
 ↑2=Rim Overflow (Weir Controls 0.66 cfs @ 1.24 fps)

20-097 Existing Analysis

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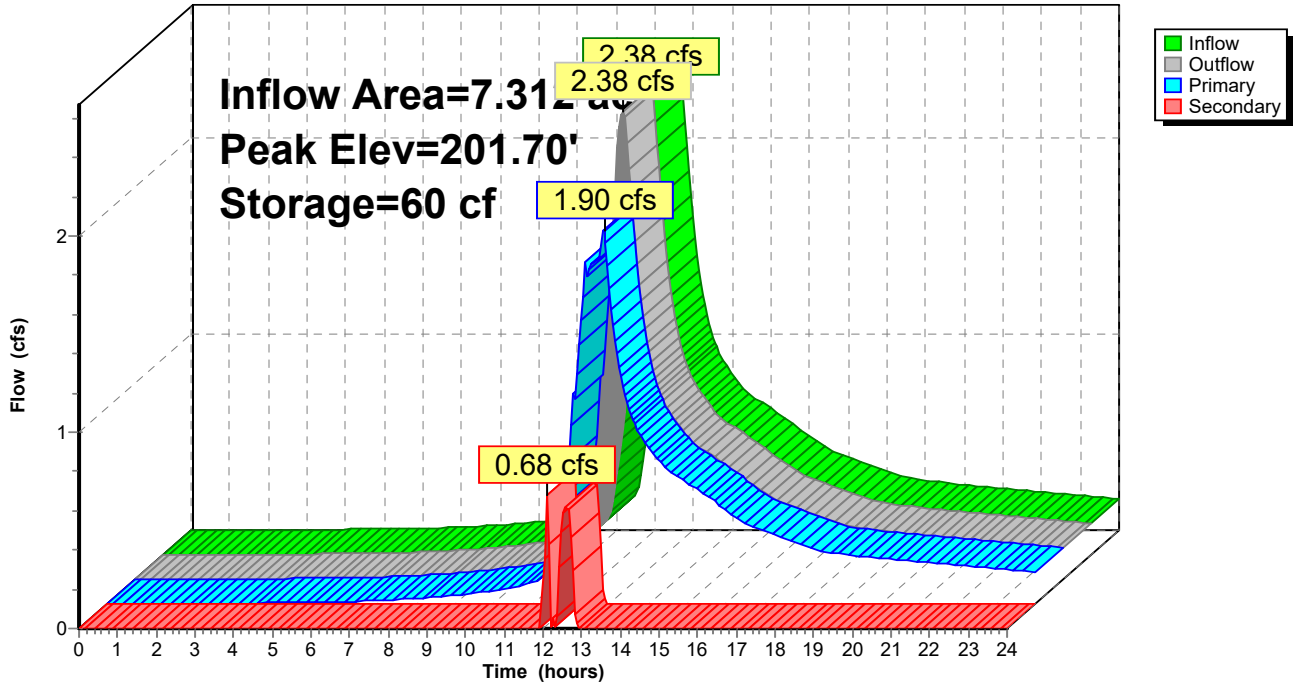
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Pond 5P: Existing CB #5

Hydrograph



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Summary for Pond 6P: Existing CB #6

Inflow Area = 7.867 ac, 10.33% Impervious, Inflow Depth > 1.22" for 25YR - 24HR event
 Inflow = 4.72 cfs @ 12.09 hrs, Volume= 0.800 af
 Outflow = 4.72 cfs @ 12.10 hrs, Volume= 0.799 af, Atten= 0%, Lag= 0.2 min
 Primary = 3.25 cfs @ 12.07 hrs, Volume= 0.780 af
 Secondary = 1.58 cfs @ 12.10 hrs, Volume= 0.019 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 201.51' @ 12.10 hrs Surf.Area= 75 sf Storage= 78 cf
 Flood Elev= 202.00' Surf.Area= 184 sf Storage= 133 cf

Plug-Flow detention time= 0.7 min calculated for 0.798 af (100% of inflow)
 Center-of-Mass det. time= 0.4 min (862.1 - 861.7)

Volume	Invert	Avail.Storage	Storage Description
#1	196.02'	63 cf	4.00'D x 5.04'H Basin
#2	201.06'	70 cf	Open Storage (Irregular) Listed below (Recalc)
		133 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
201.06	10	10.0	0	0	10
202.00	171	58.0	70	70	272

Device	Routing	Invert	Outlet Devices
#1	Primary	196.02'	12.0" Round 12" CMP L= 101.6' Ke= 0.500 Inlet / Outlet Invert= 196.02' / 195.72' S= 0.0030 '/' Cc= 0.900 n= 0.025, Flow Area= 0.79 sf
#2	Secondary	201.06'	2.0' long x 2.0' breadth Rim Overflow Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32

Primary OutFlow Max=3.12 cfs @ 12.07 hrs HW=201.43' TW=198.18' (Dynamic Tailwater)
 ↳1=12" CMP (Outlet Controls 3.12 cfs @ 3.97 fps)

Secondary OutFlow Max=1.56 cfs @ 12.10 hrs HW=201.51' TW=198.29' (Dynamic Tailwater)
 ↳2=Rim Overflow (Weir Controls 1.56 cfs @ 1.75 fps)

20-097 Existing Analysis

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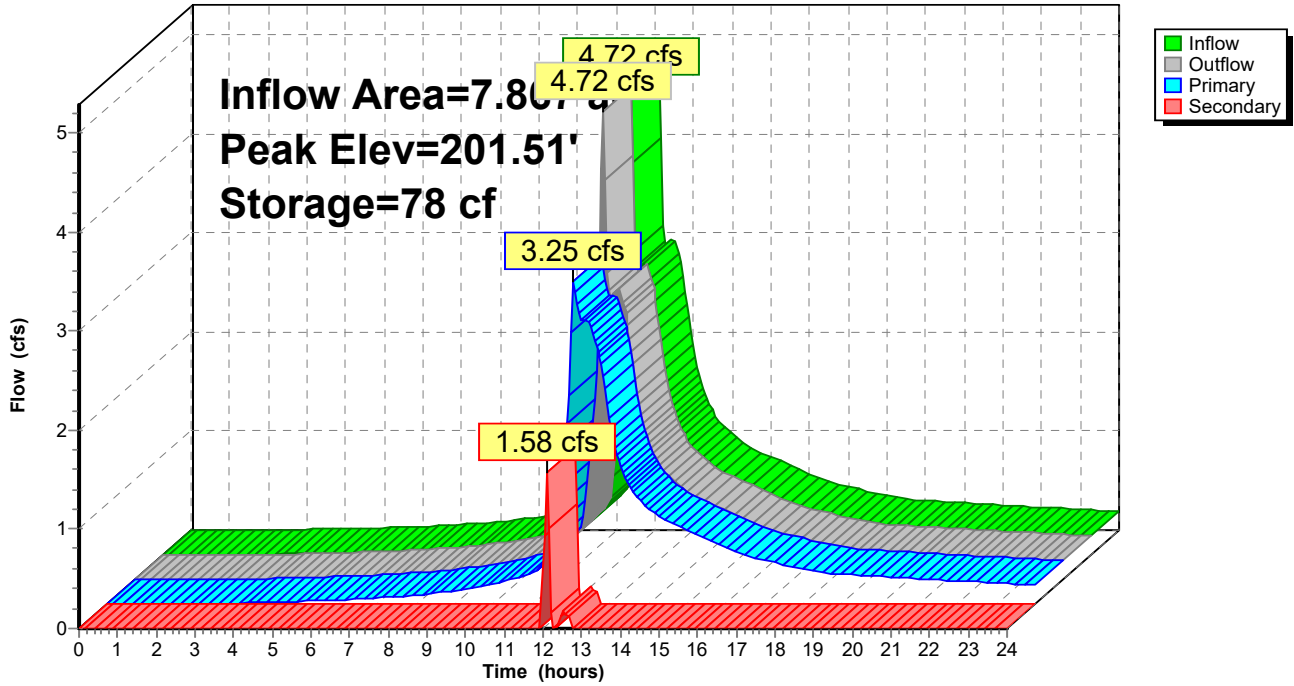
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Pond 6P: Existing CB #6

Hydrograph



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Summary for Pond 7P: Existing CB#7

[80] Warning: Exceeded Pond 6P by 0.21' @ 3.30 hrs (0.13 cfs 0.015 af)

Inflow Area = 8.045 ac, 11.54% Impervious, Inflow Depth > 1.27" for 25YR - 24HR event
 Inflow = 5.29 cfs @ 12.10 hrs, Volume= 0.849 af
 Outflow = 5.29 cfs @ 12.10 hrs, Volume= 0.849 af, Atten= 0%, Lag= 0.0 min
 Primary = 5.29 cfs @ 12.10 hrs, Volume= 0.849 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 199.21' @ 12.93 hrs Surf.Area= 13 sf Storage= 44 cf
 Flood Elev= 200.22' Surf.Area= 33 sf Storage= 57 cf

Plug-Flow detention time= 0.7 min calculated for 0.849 af (100% of inflow)
 Center-of-Mass det. time= 0.4 min (860.3 - 859.9)

Volume	Invert	Avail.Storage	Storage Description
#1	195.72'	57 cf	4.00'D x 4.50'H Basin
#2	200.22'	103 cf	Open Storage (Irregular) Listed below (Recalc)
		160 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
200.22	20	40.0	0	0	20
201.00	300	70.0	103	103	286

Device	Routing	Invert	Outlet Devices
#1	Primary	195.72'	24.0" Round 24" CMP L= 35.9' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 195.72' / 195.00' S= 0.0201 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 3.14 sf
#2	Secondary	200.22'	2.0' long x 2.0' breadth Rim Overflow Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32

Primary OutFlow Max=3.31 cfs @ 12.10 hrs HW=198.29' TW=198.24' (Dynamic Tailwater)
 ↖1=24" CMP (Outlet Controls 3.31 cfs @ 1.07 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=195.72' TW=195.00' (Dynamic Tailwater)
 ↖2=Rim Overflow (Controls 0.00 cfs)

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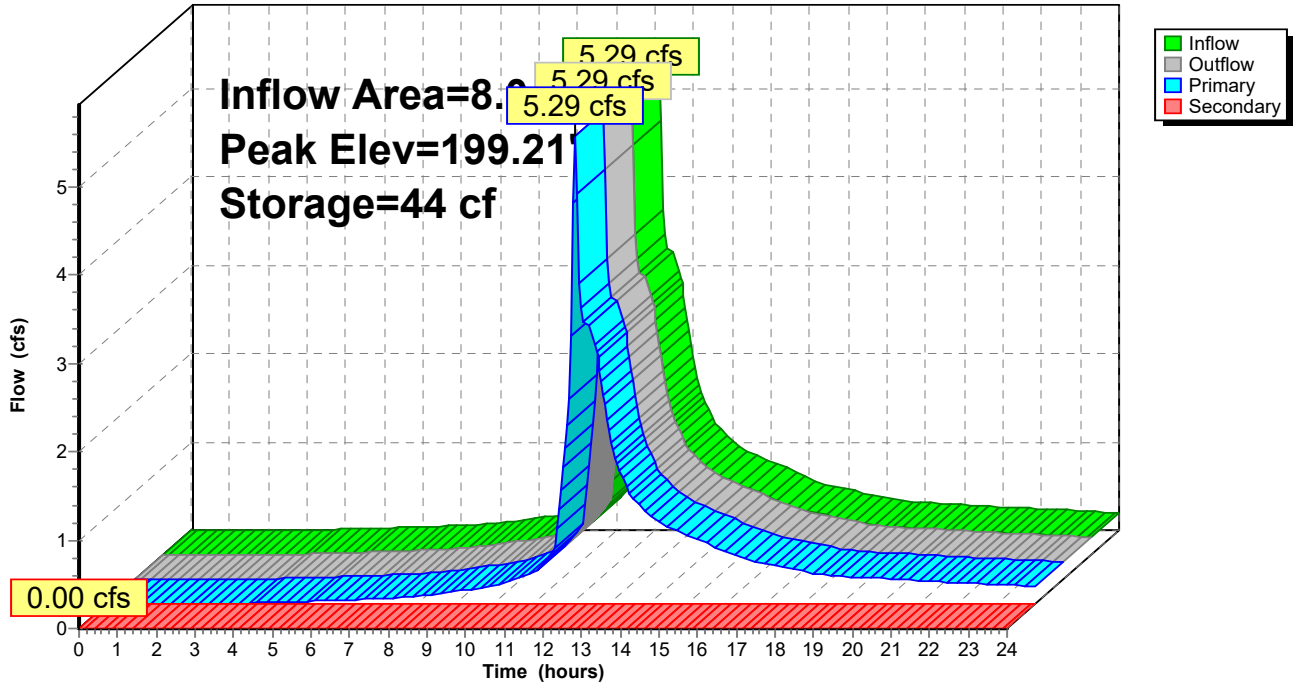
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Pond 7P: Existing CB#7

Hydrograph



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Summary for Pond 8P: 24" Cross Culvert

[62] Hint: Exceeded Reach 11R OUTLET depth by 0.31' @ 12.95 hrs

Inflow Area = 32.556 ac, 4.37% Impervious, Inflow Depth > 1.08" for 25YR - 24HR event
 Inflow = 11.20 cfs @ 12.90 hrs, Volume= 2.924 af
 Outflow = 11.15 cfs @ 12.95 hrs, Volume= 2.923 af, Atten= 0%, Lag= 3.3 min
 Primary = 11.15 cfs @ 12.95 hrs, Volume= 2.923 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 198.43' @ 12.95 hrs Surf.Area= 1,920 sf Storage= 1,221 cf
 Flood Elev= 199.55' Surf.Area= 3,482 sf Storage= 4,655 cf

Plug-Flow detention time= 1.1 min calculated for 2.917 af (100% of inflow)
 Center-of-Mass det. time= 1.0 min (911.6 - 910.7)

Volume	Invert	Avail.Storage	Storage Description			
#1	196.55'	6,222 cf	Open Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
196.55	10	10.0	0	0	10	
197.00	184	97.0	36	36	751	
198.00	1,049	166.0	557	593	2,201	
199.00	3,482	329.0	2,147	2,740	8,627	
200.00	3,482	329.0	3,482	6,222	8,956	

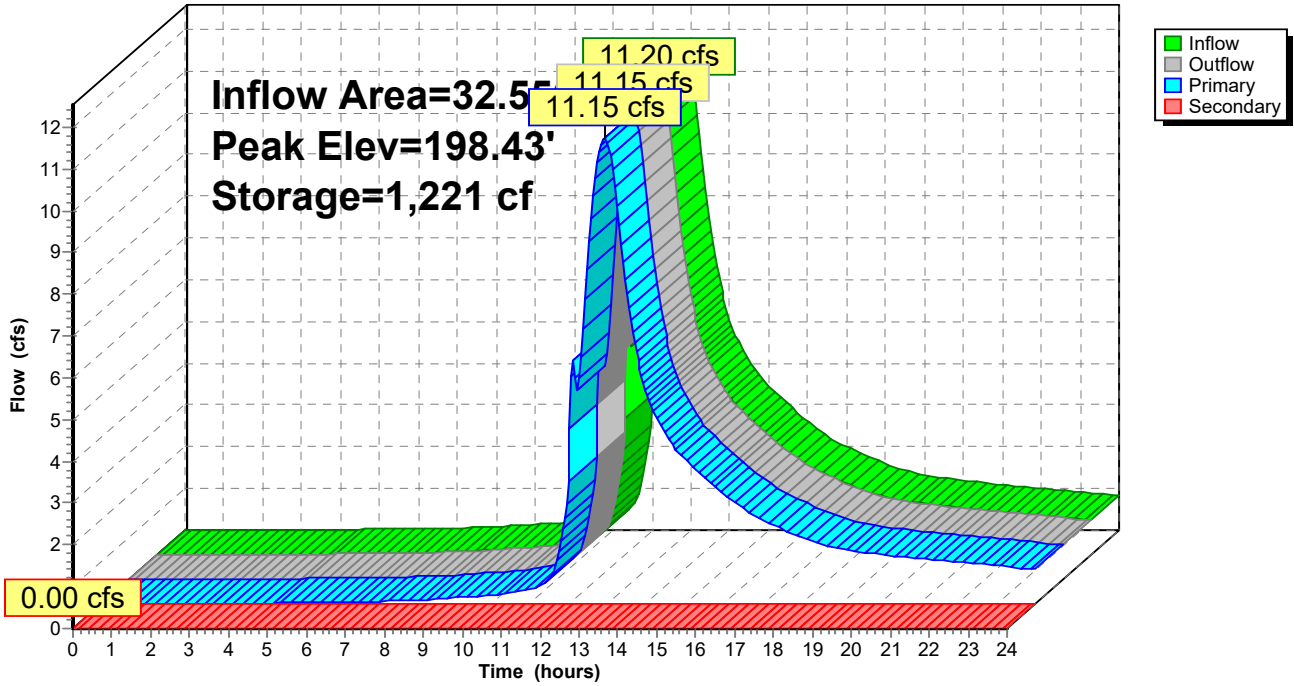
Device	Routing	Invert	Outlet Devices							
#1	Primary	196.55'	24.0" Round 24" HDPE N-12 L= 21.6' Ke= 0.500 Inlet / Outlet Invert= 196.55' / 196.44' S= 0.0051 '/' Cc= 0.900 n= 0.012, Flow Area= 3.14 sf							
#2	Secondary	199.55'	100.0' long x 10.0' breadth Flow Over The Driveway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64							

Primary OutFlow Max=11.15 cfs @ 12.95 hrs HW=198.43' TW=0.00' (Dynamic Tailwater)
 ↑1=24" HDPE N-12 (Barrel Controls 11.15 cfs @ 4.71 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=196.55' TW=0.00' (Dynamic Tailwater)
 ↑2=Flow Over The Driveway (Controls 0.00 cfs)

Pond 8P: 24" Cross Culvert

Hydrograph



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Summary for Pond 16P: 12" CMP

Inflow Area = 6.823 ac, 2.76% Impervious, Inflow Depth > 1.21" for 25YR - 24HR event
 Inflow = 4.75 cfs @ 12.46 hrs, Volume= 0.686 af
 Outflow = 2.49 cfs @ 12.88 hrs, Volume= 0.685 af, Atten= 48%, Lag= 25.6 min
 Primary = 2.49 cfs @ 12.88 hrs, Volume= 0.685 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 204.71' @ 12.88 hrs Surf.Area= 12,655 sf Storage= 4,353 cf

Plug-Flow detention time= 12.1 min calculated for 0.683 af (100% of inflow)
 Center-of-Mass det. time= 11.4 min (915.4 - 904.0)

Volume	Invert	Avail.Storage	Storage Description			
#1	203.25'	9,229 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
203.25	50	30.0	0	0	50	
204.00	962	127.1	308	308	1,265	
205.00	21,278	680.9	8,921	9,229	36,876	

Device	Routing	Invert	Outlet Devices									
#1	Primary	204.75'	50.0' long x 15.0' breadth Broad-Crested Rectangular Weir									
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60									
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63									
#2	Primary	203.25'	12.0" Round 12" CMP									
			L= 20.0' CMP, projecting, no headwall, Ke= 0.900									
			Inlet / Outlet Invert= 203.25' / 203.05' S= 0.0100 ' / ' Cc= 0.900									
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf									

Primary OutFlow Max=2.49 cfs @ 12.88 hrs HW=204.71' TW=0.00' (Dynamic Tailwater)

- 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)
- 2=12" CMP (Barrel Controls 2.49 cfs @ 3.17 fps)

20-097 Existing Analysis

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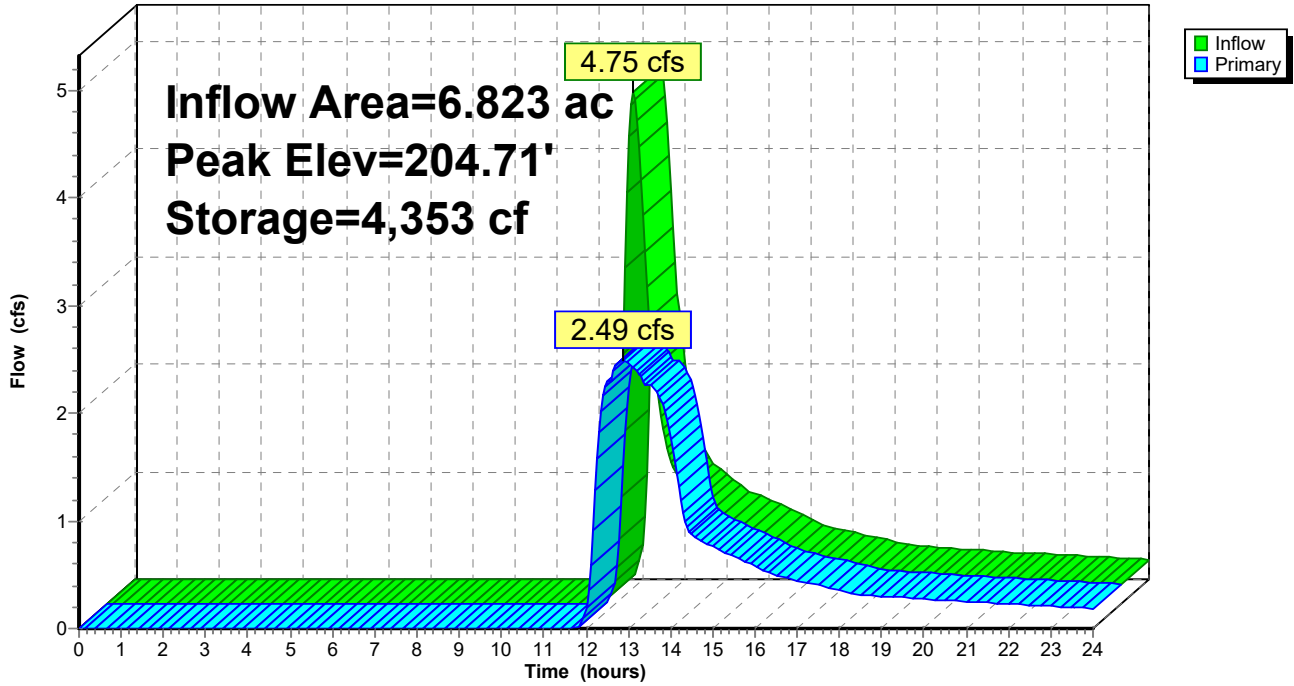
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Pond 16P: 12" CMP

Hydrograph



20-097 Existing Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 17P: Existing Driveway Culvert

Inflow Area = 11.419 ac, 0.60% Impervious, Inflow Depth > 1.35" for 25YR - 24HR event
 Inflow = 8.25 cfs @ 12.57 hrs, Volume= 1.283 af
 Outflow = 8.23 cfs @ 12.59 hrs, Volume= 1.232 af, Atten= 0%, Lag= 1.3 min
 Primary = 5.93 cfs @ 12.59 hrs, Volume= 1.086 af
 Secondary = 2.30 cfs @ 12.59 hrs, Volume= 0.146 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 204.15' @ 12.59 hrs Surf.Area= 7,143 sf Storage= 3,126 cf

Plug-Flow detention time= 29.4 min calculated for 1.232 af (96% of inflow)
 Center-of-Mass det. time= 9.3 min (912.8 - 903.4)

Volume	Invert	Avail.Storage	Storage Description			
#1	203.50'	3,838 cf	Open Water Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
203.50	1,694	166.7	0	0	1,694	
204.00	7,143	405.4	2,053	2,053	12,562	
204.25	7,143	405.4	1,786	3,838	12,663	

Device	Routing	Invert	Outlet Devices									
#1	Primary	204.00'	38.0' long x 15.0' breadth Broad-Crested Rectangular Weir									
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60									
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63									
#2	Secondary	204.05'	27.0' long x 15.0' breadth Broad-Crested Rectangular Weir									
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60									
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63									

Primary OutFlow Max=5.93 cfs @ 12.59 hrs HW=204.15' TW=0.00' (Dynamic Tailwater)
 ↗1=**Broad-Crested Rectangular Weir** (Weir Controls 5.93 cfs @ 1.04 fps)

Secondary OutFlow Max=2.29 cfs @ 12.59 hrs HW=204.15' TW=0.00' (Dynamic Tailwater)
 ↗2=**Broad-Crested Rectangular Weir** (Weir Controls 2.29 cfs @ 0.85 fps)

20-097 Existing Analysis

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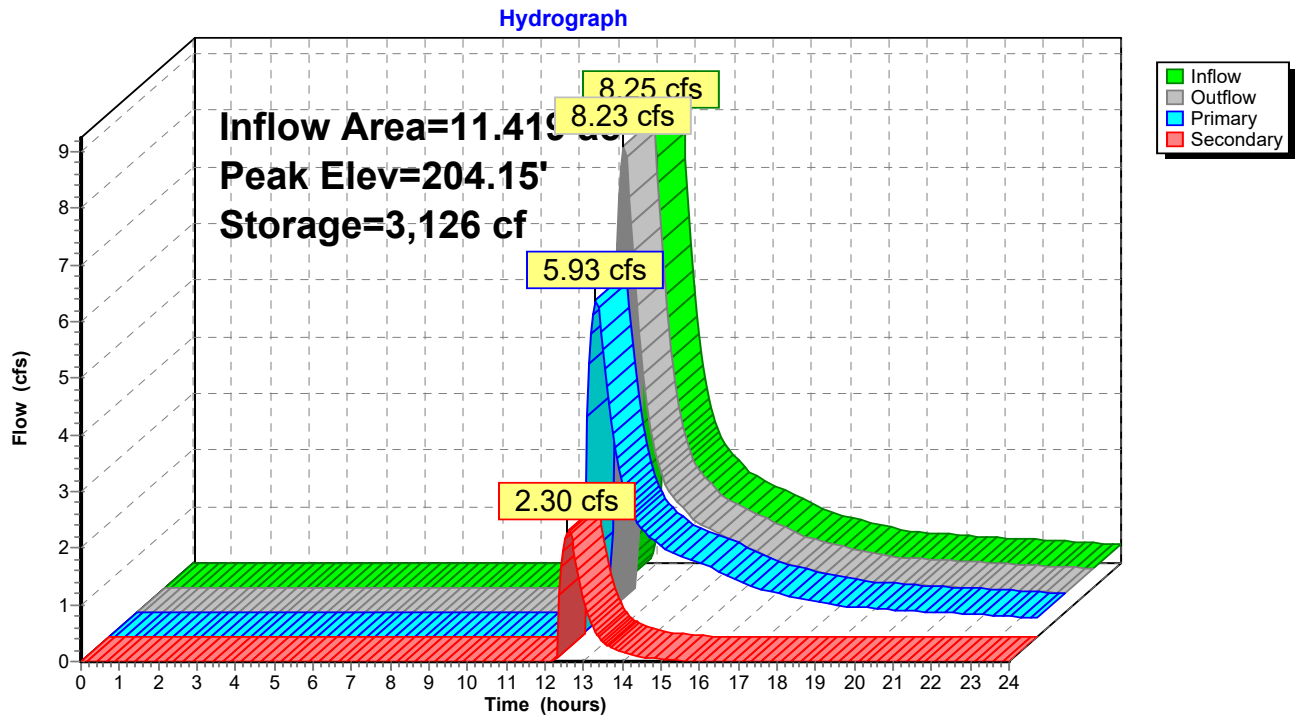
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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Pond 17P: Existing Driveway Culvert



20-097 Existing Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 18P: Box Culvert

Inflow Area = 10.898 ac, 0.22% Impervious, Inflow Depth > 1.58" for 25YR - 24HR event
 Inflow = 10.53 cfs @ 12.46 hrs, Volume= 1.433 af
 Outflow = 10.52 cfs @ 12.47 hrs, Volume= 1.433 af, Atten= 0%, Lag= 0.5 min
 Primary = 10.52 cfs @ 12.47 hrs, Volume= 1.433 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 191.52' @ 12.47 hrs Surf.Area= 391 sf Storage= 155 cf

Plug-Flow detention time= 0.2 min calculated for 1.430 af (100% of inflow)
 Center-of-Mass det. time= 0.2 min (889.9 - 889.7)

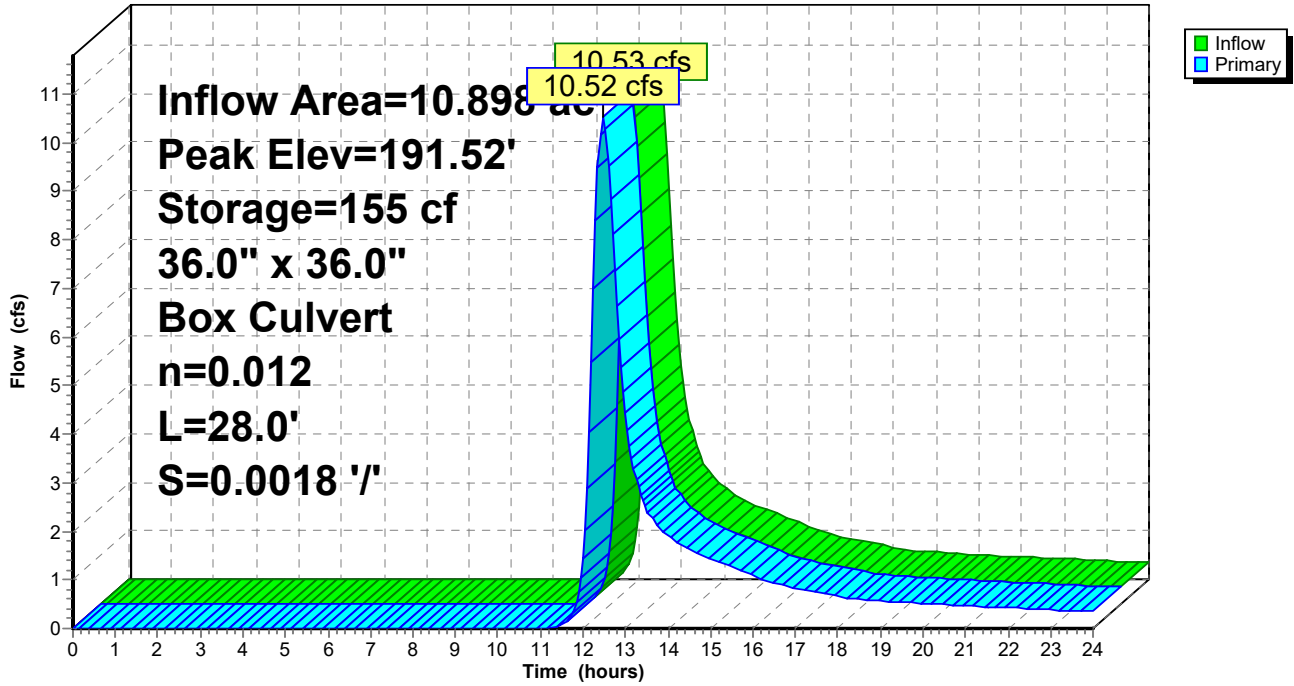
Volume	Invert	Avail.Storage	Storage Description			
#1	190.25'	56,817 cf	Open Water Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
190.25	50	30.0	0	0	50	
191.00	72	54.2	46	46	215	
192.00	912	215.6	413	459	3,683	
193.00	2,290	273.4	1,549	2,008	5,946	
194.00	4,070	334.6	3,138	5,146	8,922	
195.00	6,222	483.3	5,108	10,254	18,609	
196.00	8,396	606.1	7,282	17,536	29,269	
197.00	11,534	890.2	9,924	27,459	63,105	
198.00	15,764	977.3	13,594	41,053	76,083	
199.00	15,764	977.3	15,764	56,817	77,060	

Device	Routing	Invert	Outlet Devices			
#1	Primary	190.25'	36.0" W x 36.0" H Box Box Culvert N-12 L= 28.0' Ke= 0.500 Inlet / Outlet Invert= 190.25' / 190.20' S= 0.0018 '/' Cc= 0.900 n= 0.012, Flow Area= 9.00 sf			

Primary OutFlow Max=10.48 cfs @ 12.47 hrs HW=191.52' TW=0.00' (Dynamic Tailwater)
 ↑**1=Box Culvert N-12** (Barrel Controls 10.48 cfs @ 3.68 fps)

Pond 18P: Box Culvert

Hydrograph



20-097 Existing Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 19P: Box Culvert

Inflow Area = 15.859 ac, 0.00% Impervious, Inflow Depth > 1.34" for 25YR - 24HR event
 Inflow = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af
 Outflow = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af, Atten= 0%, Lag= 0.1 min
 Primary = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 184.15' @ 12.72 hrs Surf.Area= 49 sf Storage= 24 cf

Plug-Flow detention time= 0.0 min calculated for 1.771 af (100% of inflow)
 Center-of-Mass det. time= 0.0 min (911.5 - 911.4)

Volume	Invert	Avail.Storage	Storage Description			
#1	182.69'	612 cf	Open Water Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
182.69	1	5.1	0	0	1	
184.00	33	33.5	17	17	92	
185.00	195	111.6	103	120	997	
186.00	870	252.1	492	612	5,067	

Device	Routing	Invert	Outlet Devices			
#1	Primary	183.13'	36.0" W x 36.0" H Box Box Culvert N-12 L= 52.0' Ke= 0.500 Inlet / Outlet Invert= 182.69' / 183.13' S= -0.0085 '/' Cc= 0.900 n= 0.012, Flow Area= 9.00 sf			

Primary OutFlow Max=9.94 cfs @ 12.72 hrs HW=184.15' TW=0.00' (Dynamic Tailwater)
 ↑1=Box Culvert N-12 (Inlet Controls 9.94 cfs @ 3.24 fps)

20-097 Existing Analysis

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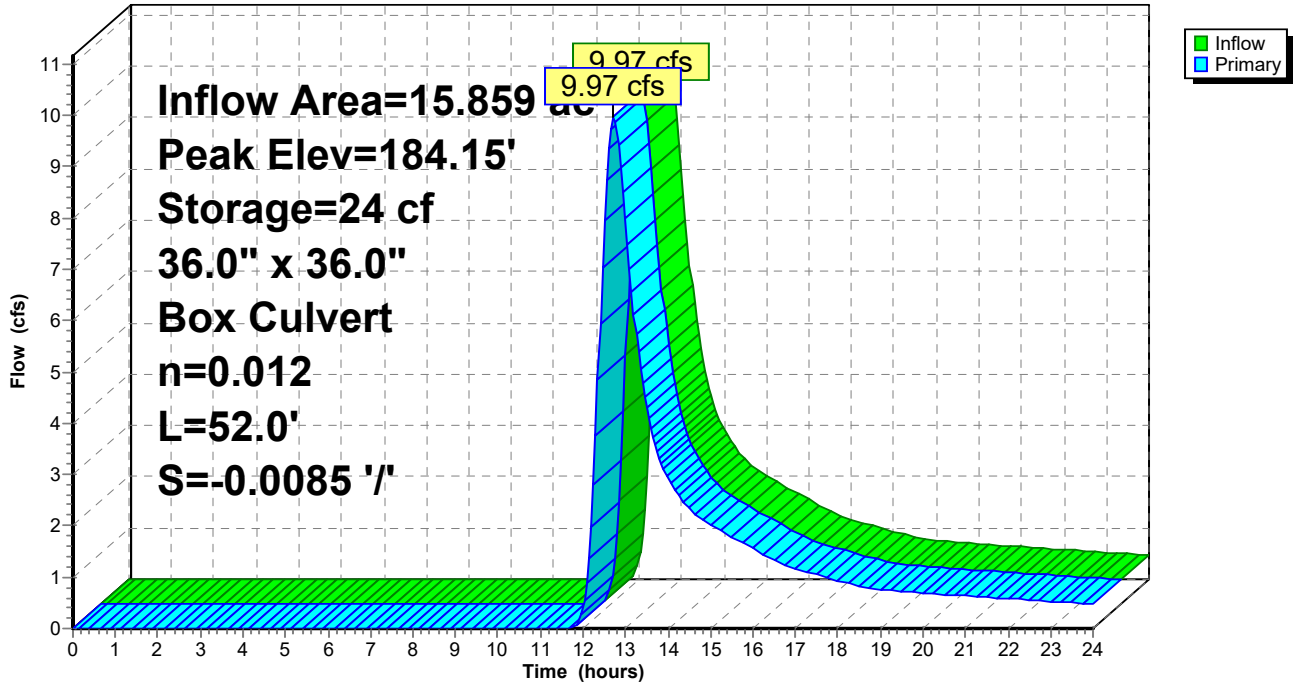
Type III 24-hr 25YR - 24HR Rainfall=5.86"

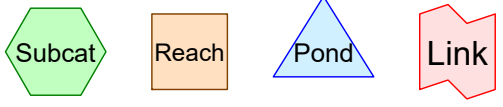
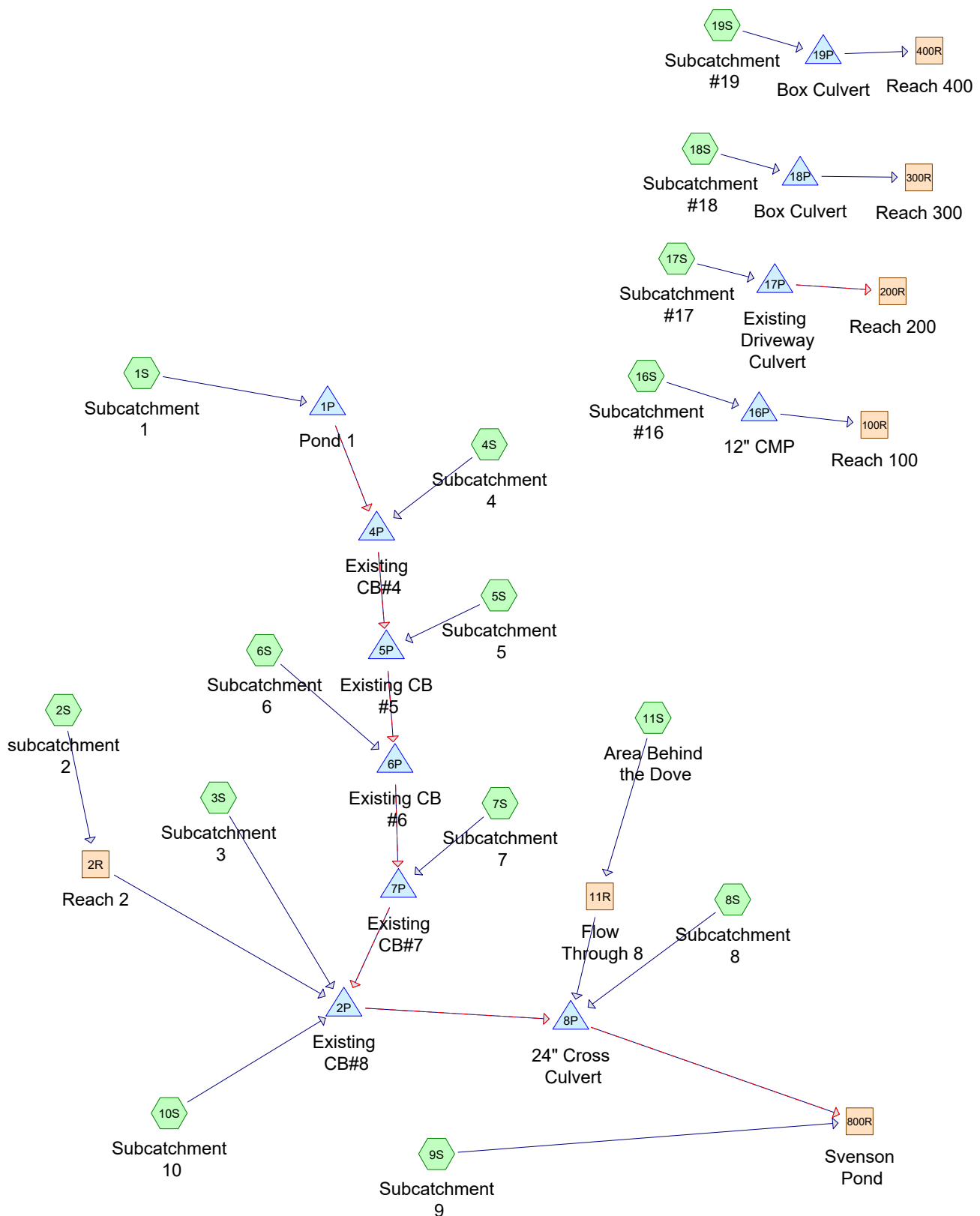
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Pond 19P: Box Culvert

Hydrograph





Routing Diagram for 20-097 Existing Analysis
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20-097 Existing Analysis

Type III 24-hr 2YR - 24HR Rainfall=3.08"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1	Runoff Area=303,964 sf 0.00% Impervious Runoff Depth>0.03" Flow Length=1,542' Tc=32.6 min CN=45 Runoff=0.03 cfs 0.018 af
Subcatchment 2S: subcatchment 2	Runoff Area=764,518 sf 0.65% Impervious Runoff Depth>0.14" Flow Length=2,418' Tc=59.1 min CN=52 Runoff=0.38 cfs 0.205 af
Subcatchment 3S: Subcatchment 3	Runoff Area=122,849 sf 0.64% Impervious Runoff Depth=0.00" Flow Length=993' Tc=20.7 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment 4S: Subcatchment 4	Runoff Area=4,089 sf 98.95% Impervious Runoff Depth>2.74" Flow Length=85' Slope=0.0472 '/' Tc=6.0 min CN=97 Runoff=0.27 cfs 0.021 af
Subcatchment 5S: Subcatchment 5	Runoff Area=10,452 sf 82.66% Impervious Runoff Depth>1.89" Flow Length=75' Tc=6.0 min CN=88 Runoff=0.52 cfs 0.038 af
Subcatchment 6S: Subcatchment 6	Runoff Area=24,193 sf 93.83% Impervious Runoff Depth>2.43" Flow Length=216' Tc=6.0 min CN=94 Runoff=1.48 cfs 0.112 af
Subcatchment 7S: Subcatchment 7	Runoff Area=7,743 sf 65.07% Impervious Runoff Depth>1.12" Flow Length=98' Tc=9.7 min CN=77 Runoff=0.20 cfs 0.017 af
Subcatchment 8S: Subcatchment 8	Runoff Area=19,227 sf 32.64% Impervious Runoff Depth>0.30" Flow Length=152' Tc=10.4 min CN=58 Runoff=0.06 cfs 0.011 af
Subcatchment 9S: Subcatchment 9	Runoff Area=64,869 sf 22.90% Impervious Runoff Depth>0.04" Flow Length=484' Tc=19.3 min UI Adjusted CN=46 Runoff=0.01 cfs 0.005 af
Subcatchment 10S: Subcatchment 10	Runoff Area=53,175 sf 5.56% Impervious Runoff Depth>0.00" Flow Length=438' Tc=18.4 min UI Adjusted CN=41 Runoff=0.00 cfs 0.000 af
Subcatchment 11S: Area Behind the Dove	Runoff Area=107,916 sf 6.10% Impervious Runoff Depth>0.01" Flow Length=802' Tc=22.0 min UI Adjusted CN=43 Runoff=0.00 cfs 0.003 af
Subcatchment 16S: Subcatchment #16	Runoff Area=297,191 sf 2.76% Impervious Runoff Depth>0.14" Flow Length=1,113' Tc=27.2 min CN=52 Runoff=0.18 cfs 0.081 af
Subcatchment 17S: Subcatchment #17	Runoff Area=497,407 sf 0.60% Impervious Runoff Depth>0.19" Flow Length=1,540' Tc=35.5 min UI Adjusted CN=54 Runoff=0.49 cfs 0.179 af
Subcatchment 18S: Subcatchment #18	Runoff Area=474,696 sf 0.22% Impervious Runoff Depth>0.27" Flow Length=1,280' Tc=29.3 min CN=57 Runoff=0.98 cfs 0.243 af
Subcatchment 19S: Subcatchment #19	Runoff Area=690,822 sf 0.00% Impervious Runoff Depth>0.19" Flow Length=1,832' Tc=46.3 min CN=54 Runoff=0.61 cfs 0.247 af
Reach 2R: Reach 2	Avg. Flow Depth=0.09' Max Vel=1.27 fps Inflow=0.38 cfs 0.205 af n=0.022 L=329.8' S=0.0091 '/' Capacity=24.64 cfs Outflow=0.38 cfs 0.204 af

20-097 Existing Analysis

Type III 24-hr 2YR - 24HR Rainfall=3.08"

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Reach 11R: Flow Through 8	Avg. Flow Depth=0.02' Max Vel=0.24 fps n=0.035 L=76.0' S=0.0132 '/ Capacity=7.77 cfs	Inflow=0.00 cfs 0.003 af Outflow=0.00 cfs 0.003 af
Reach 100R: Reach 100		Inflow=0.17 cfs 0.081 af Outflow=0.17 cfs 0.081 af
Reach 200R: Reach 200		Inflow=0.30 cfs 0.130 af Outflow=0.30 cfs 0.130 af
Reach 300R: Reach 300		Inflow=0.98 cfs 0.243 af Outflow=0.98 cfs 0.243 af
Reach 400R: Reach 400		Inflow=0.61 cfs 0.246 af Outflow=0.61 cfs 0.246 af
Reach 800R: Svenson Pond		Inflow=2.35 cfs 0.427 af Outflow=2.35 cfs 0.427 af
Pond 1P: Pond 1	Peak Elev=201.22' Storage=0 cf Primary=0.03 cfs 0.018 af Secondary=0.00 cfs 0.000 af	Inflow=0.03 cfs 0.018 af Outflow=0.03 cfs 0.018 af
Pond 2P: Existing CB#8	Peak Elev=197.67' Storage=34 cf Primary=2.40 cfs 0.408 af Secondary=0.00 cfs 0.000 af	Inflow=2.40 cfs 0.409 af Outflow=2.40 cfs 0.408 af
Pond 4P: Existing CB#4	Peak Elev=199.37' Storage=9 cf Primary=0.26 cfs 0.039 af Secondary=0.00 cfs 0.000 af	Inflow=0.27 cfs 0.039 af Outflow=0.26 cfs 0.039 af
Pond 5P: Existing CB #5	Peak Elev=199.46' Storage=25 cf Primary=0.77 cfs 0.077 af Secondary=0.00 cfs 0.000 af	Inflow=0.78 cfs 0.077 af Outflow=0.77 cfs 0.077 af
Pond 6P: Existing CB #6	Peak Elev=199.29' Storage=41 cf Primary=2.23 cfs 0.189 af Secondary=0.00 cfs 0.000 af	Inflow=2.24 cfs 0.189 af Outflow=2.23 cfs 0.189 af
Pond 7P: Existing CB#7	Peak Elev=197.69' Storage=25 cf Primary=2.40 cfs 0.205 af Secondary=0.00 cfs 0.000 af	Inflow=2.41 cfs 0.205 af Outflow=2.40 cfs 0.205 af
Pond 8P: 24" Cross Culvert	Peak Elev=197.31' Storage=121 cf Primary=2.35 cfs 0.422 af Secondary=0.00 cfs 0.000 af	Inflow=2.42 cfs 0.422 af Outflow=2.35 cfs 0.422 af
Pond 16P: 12" CMP	Peak Elev=203.53' Storage=38 cf	Inflow=0.18 cfs 0.081 af Outflow=0.17 cfs 0.081 af
Pond 17P: Existing Driveway Culvert	Peak Elev=204.02' Storage=2,201 cf Primary=0.30 cfs 0.130 af Secondary=0.00 cfs 0.000 af	Inflow=0.49 cfs 0.179 af Outflow=0.30 cfs 0.130 af
Pond 18P: Box Culvert	Peak Elev=190.51' Storage=14 cf 36.0" x 36.0" Box Culvert n=0.012 L=28.0' S=0.0018 '/	Inflow=0.98 cfs 0.243 af Outflow=0.98 cfs 0.243 af
Pond 19P: Box Culvert	Peak Elev=183.29' Storage=3 cf 36.0" x 36.0" Box Culvert n=0.012 L=52.0' S=-0.0085 '/	Inflow=0.61 cfs 0.247 af Outflow=0.61 cfs 0.246 af

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Type III 24-hr 10YR - 24HR Rainfall=4.64"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1	Runoff Area=303,964 sf 0.00% Impervious Runoff Depth>0.33" Flow Length=1,542' Tc=32.6 min CN=45 Runoff=0.63 cfs 0.191 af
Subcatchment 2S: subcatchment 2	Runoff Area=764,518 sf 0.65% Impervious Runoff Depth>0.63" Flow Length=2,418' Tc=59.1 min CN=52 Runoff=3.64 cfs 0.927 af
Subcatchment 3S: Subcatchment 3	Runoff Area=122,849 sf 0.64% Impervious Runoff Depth>0.13" Flow Length=993' Tc=20.7 min CN=39 Runoff=0.05 cfs 0.031 af
Subcatchment 4S: Subcatchment 4	Runoff Area=4,089 sf 98.95% Impervious Runoff Depth>4.29" Flow Length=85' Slope=0.0472 '/' Tc=6.0 min CN=97 Runoff=0.41 cfs 0.034 af
Subcatchment 5S: Subcatchment 5	Runoff Area=10,452 sf 82.66% Impervious Runoff Depth>3.33" Flow Length=75' Tc=6.0 min CN=88 Runoff=0.90 cfs 0.066 af
Subcatchment 6S: Subcatchment 6	Runoff Area=24,193 sf 93.83% Impervious Runoff Depth>3.95" Flow Length=216' Tc=6.0 min CN=94 Runoff=2.35 cfs 0.183 af
Subcatchment 7S: Subcatchment 7	Runoff Area=7,743 sf 65.07% Impervious Runoff Depth>2.32" Flow Length=98' Tc=9.7 min CN=77 Runoff=0.42 cfs 0.034 af
Subcatchment 8S: Subcatchment 8	Runoff Area=19,227 sf 32.64% Impervious Runoff Depth>0.97" Flow Length=152' Tc=10.4 min CN=58 Runoff=0.35 cfs 0.036 af
Subcatchment 9S: Subcatchment 9	Runoff Area=64,869 sf 22.90% Impervious Runoff Depth>0.37" Flow Length=484' Tc=19.3 min UI Adjusted CN=46 Runoff=0.20 cfs 0.046 af
Subcatchment 10S: Subcatchment 10	Runoff Area=53,175 sf 5.56% Impervious Runoff Depth>0.19" Flow Length=438' Tc=18.4 min UI Adjusted CN=41 Runoff=0.04 cfs 0.019 af
Subcatchment 11S: Area Behind the Dove	Runoff Area=107,916 sf 6.10% Impervious Runoff Depth>0.26" Flow Length=802' Tc=22.0 min UI Adjusted CN=43 Runoff=0.15 cfs 0.053 af
Subcatchment 16S: Subcatchment #16	Runoff Area=297,191 sf 2.76% Impervious Runoff Depth>0.64" Flow Length=1,113' Tc=27.2 min CN=52 Runoff=2.09 cfs 0.365 af
Subcatchment 17S: Subcatchment #17	Runoff Area=497,407 sf 0.60% Impervious Runoff Depth>0.74" Flow Length=1,540' Tc=35.5 min UI Adjusted CN=54 Runoff=3.92 cfs 0.707 af
Subcatchment 18S: Subcatchment #18	Runoff Area=474,696 sf 0.22% Impervious Runoff Depth>0.91" Flow Length=1,280' Tc=29.3 min CN=57 Runoff=5.45 cfs 0.826 af
Subcatchment 19S: Subcatchment #19	Runoff Area=690,822 sf 0.00% Impervious Runoff Depth>0.74" Flow Length=1,832' Tc=46.3 min CN=54 Runoff=4.74 cfs 0.978 af
Reach 2R: Reach 2	Avg. Flow Depth=0.35' Max Vel=2.79 fps Inflow=3.64 cfs 0.927 af n=0.022 L=329.8' S=0.0091 '/' Capacity=24.64 cfs Outflow=3.64 cfs 0.925 af

20-097 Existing Analysis

Type III 24-hr 10YR - 24HR Rainfall=4.64"

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Reach 11R: Flow Through 8	Avg. Flow Depth=0.08' Max Vel=0.70 fps Inflow=0.15 cfs 0.053 af n=0.035 L=76.0' S=0.0132 '/ Capacity=7.77 cfs Outflow=0.15 cfs 0.053 af
Reach 100R: Reach 100	Inflow=1.75 cfs 0.365 af Outflow=1.75 cfs 0.365 af
Reach 200R: Reach 200	Inflow=3.90 cfs 0.657 af Outflow=3.90 cfs 0.657 af
Reach 300R: Reach 300	Inflow=5.45 cfs 0.826 af Outflow=5.45 cfs 0.826 af
Reach 400R: Reach 400	Inflow=4.74 cfs 0.978 af Outflow=4.74 cfs 0.978 af
Reach 800R: Svenson Pond	Inflow=4.92 cfs 1.617 af Outflow=4.92 cfs 1.617 af
Pond 1P: Pond 1	Peak Elev=201.58' Storage=2 cf Inflow=0.63 cfs 0.191 af Primary=0.62 cfs 0.191 af Secondary=0.00 cfs 0.000 af Outflow=0.62 cfs 0.191 af
Pond 2P: Existing CB#8	Peak Elev=198.12' Storage=40 cf Inflow=4.63 cfs 1.483 af Primary=4.64 cfs 1.482 af Secondary=0.00 cfs 0.000 af Outflow=4.64 cfs 1.482 af
Pond 4P: Existing CB#4	Peak Elev=201.49' Storage=36 cf Inflow=0.67 cfs 0.225 af Primary=0.70 cfs 0.225 af Secondary=0.00 cfs 0.000 af Outflow=0.70 cfs 0.225 af
Pond 5P: Existing CB #5	Peak Elev=201.51' Storage=52 cf Inflow=1.15 cfs 0.291 af Primary=1.16 cfs 0.291 af Secondary=0.10 cfs 0.000 af Outflow=1.26 cfs 0.291 af
Pond 6P: Existing CB #6	Peak Elev=201.28' Storage=67 cf Inflow=3.59 cfs 0.474 af Primary=3.15 cfs 0.472 af Secondary=0.49 cfs 0.002 af Outflow=3.64 cfs 0.474 af
Pond 7P: Existing CB#7	Peak Elev=198.12' Storage=30 cf Inflow=4.04 cfs 0.508 af Primary=4.03 cfs 0.508 af Secondary=0.00 cfs 0.000 af Outflow=4.03 cfs 0.508 af
Pond 8P: 24" Cross Culvert	Peak Elev=197.68' Storage=318 cf Inflow=4.83 cfs 1.571 af Primary=4.81 cfs 1.571 af Secondary=0.00 cfs 0.000 af Outflow=4.81 cfs 1.571 af
Pond 16P: 12" CMP	Peak Elev=204.24' Storage=811 cf Inflow=2.09 cfs 0.365 af Outflow=1.75 cfs 0.365 af
Pond 17P: Existing Driveway Culvert	Peak Elev=204.10' Storage=2,754 cf Inflow=3.92 cfs 0.707 af Primary=3.14 cfs 0.624 af Secondary=0.77 cfs 0.033 af Outflow=3.90 cfs 0.657 af
Pond 18P: Box Culvert	Peak Elev=191.07' Storage=51 cf Inflow=5.45 cfs 0.826 af 36.0" x 36.0" Box Culvert n=0.012 L=28.0' S=0.0018 '/ Outflow=5.45 cfs 0.826 af
Pond 19P: Box Culvert	Peak Elev=183.75' Storage=10 cf Inflow=4.74 cfs 0.978 af 36.0" x 36.0" Box Culvert n=0.012 L=52.0' S=-0.0085 '/ Outflow=4.74 cfs 0.978 af

20-097 Existing Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1	Runoff Area=303,964 sf 0.00% Impervious Runoff Depth>0.74" Flow Length=1,542' Tc=32.6 min CN=45 Runoff=2.15 cfs 0.428 af
Subcatchment 2S: subcatchment 2	Runoff Area=764,518 sf 0.65% Impervious Runoff Depth>1.19" Flow Length=2,418' Tc=59.1 min CN=52 Runoff=8.18 cfs 1.744 af
Subcatchment 3S: Subcatchment 3	Runoff Area=122,849 sf 0.64% Impervious Runoff Depth>0.40" Flow Length=993' Tc=20.7 min CN=39 Runoff=0.35 cfs 0.094 af
Subcatchment 4S: Subcatchment 4	Runoff Area=4,089 sf 98.95% Impervious Runoff Depth>5.50" Flow Length=85' Slope=0.0472 '/' Tc=6.0 min CN=97 Runoff=0.52 cfs 0.043 af
Subcatchment 5S: Subcatchment 5	Runoff Area=10,452 sf 82.66% Impervious Runoff Depth>4.49" Flow Length=75' Tc=6.0 min CN=88 Runoff=1.19 cfs 0.090 af
Subcatchment 6S: Subcatchment 6	Runoff Area=24,193 sf 93.83% Impervious Runoff Depth>5.15" Flow Length=216' Tc=6.0 min CN=94 Runoff=3.02 cfs 0.239 af
Subcatchment 7S: Subcatchment 7	Runoff Area=7,743 sf 65.07% Impervious Runoff Depth>3.35" Flow Length=98' Tc=9.7 min CN=77 Runoff=0.61 cfs 0.050 af
Subcatchment 8S: Subcatchment 8	Runoff Area=19,227 sf 32.64% Impervious Runoff Depth>1.67" Flow Length=152' Tc=10.4 min CN=58 Runoff=0.68 cfs 0.061 af
Subcatchment 9S: Subcatchment 9	Runoff Area=64,869 sf 22.90% Impervious Runoff Depth>0.80" Flow Length=484' Tc=19.3 min UI Adjusted CN=46 Runoff=0.63 cfs 0.100 af
Subcatchment 10S: Subcatchment 10	Runoff Area=53,175 sf 5.56% Impervious Runoff Depth>0.51" Flow Length=438' Tc=18.4 min UI Adjusted CN=41 Runoff=0.24 cfs 0.052 af
Subcatchment 11S: Area Behind the Dove	Runoff Area=107,916 sf 6.10% Impervious Runoff Depth>0.62" Flow Length=802' Tc=22.0 min UI Adjusted CN=43 Runoff=0.66 cfs 0.128 af
Subcatchment 16S: Subcatchment #16	Runoff Area=297,191 sf 2.76% Impervious Runoff Depth>1.21" Flow Length=1,113' Tc=27.2 min CN=52 Runoff=4.75 cfs 0.686 af
Subcatchment 17S: Subcatchment #17	Runoff Area=497,407 sf 0.60% Impervious Runoff Depth>1.35" Flow Length=1,540' Tc=35.5 min UI Adjusted CN=54 Runoff=8.25 cfs 1.283 af
Subcatchment 18S: Subcatchment #18	Runoff Area=474,696 sf 0.22% Impervious Runoff Depth>1.58" Flow Length=1,280' Tc=29.3 min CN=57 Runoff=10.53 cfs 1.433 af
Subcatchment 19S: Subcatchment #19	Runoff Area=690,822 sf 0.00% Impervious Runoff Depth>1.34" Flow Length=1,832' Tc=46.3 min CN=54 Runoff=9.97 cfs 1.775 af
Reach 2R: Reach 2	Avg. Flow Depth=0.55' Max Vel=3.59 fps Inflow=8.18 cfs 1.744 af n=0.022 L=329.8' S=0.0091 '/' Capacity=24.64 cfs Outflow=8.17 cfs 1.741 af

20-097 Existing Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Reach 11R: Flow Through 8	Avg. Flow Depth=0.16' Max Vel=1.09 fps Inflow=0.66 cfs 0.128 af n=0.035 L=76.0' S=0.0132 '/' Capacity=7.77 cfs Outflow=0.66 cfs 0.128 af
Reach 100R: Reach 100	Inflow=2.49 cfs 0.685 af Outflow=2.49 cfs 0.685 af
Reach 200R: Reach 200	Inflow=8.23 cfs 1.232 af Outflow=8.23 cfs 1.232 af
Reach 300R: Reach 300	Inflow=10.52 cfs 1.433 af Outflow=10.52 cfs 1.433 af
Reach 400R: Reach 400	Inflow=9.97 cfs 1.775 af Outflow=9.97 cfs 1.775 af
Reach 800R: Svenson Pond	Inflow=11.40 cfs 3.023 af Outflow=11.40 cfs 3.023 af
Pond 1P: Pond 1	Peak Elev=203.37' Storage=18 cf Inflow=2.15 cfs 0.428 af Primary=2.16 cfs 0.428 af Secondary=0.00 cfs 0.000 af Outflow=2.16 cfs 0.428 af
Pond 2P: Existing CB#8	Peak Elev=199.20' Storage=333 cf Inflow=10.78 cfs 2.736 af Primary=10.70 cfs 2.735 af Secondary=0.00 cfs 0.000 af Outflow=10.70 cfs 2.735 af
Pond 4P: Existing CB#4	Peak Elev=202.67' Storage=51 cf Inflow=2.22 cfs 0.471 af Primary=2.22 cfs 0.471 af Secondary=0.00 cfs 0.000 af Outflow=2.22 cfs 0.471 af
Pond 5P: Existing CB #5	Peak Elev=201.70' Storage=60 cf Inflow=2.38 cfs 0.561 af Primary=1.90 cfs 0.535 af Secondary=0.68 cfs 0.026 af Outflow=2.38 cfs 0.561 af
Pond 6P: Existing CB #6	Peak Elev=201.51' Storage=78 cf Inflow=4.72 cfs 0.800 af Primary=3.25 cfs 0.780 af Secondary=1.58 cfs 0.019 af Outflow=4.72 cfs 0.799 af
Pond 7P: Existing CB#7	Peak Elev=199.21' Storage=44 cf Inflow=5.29 cfs 0.849 af Primary=5.29 cfs 0.849 af Secondary=0.00 cfs 0.000 af Outflow=5.29 cfs 0.849 af
Pond 8P: 24" Cross Culvert	Peak Elev=198.43' Storage=1,221 cf Inflow=11.20 cfs 2.924 af Primary=11.15 cfs 2.923 af Secondary=0.00 cfs 0.000 af Outflow=11.15 cfs 2.923 af
Pond 16P: 12" CMP	Peak Elev=204.71' Storage=4,353 cf Inflow=4.75 cfs 0.686 af Outflow=2.49 cfs 0.685 af
Pond 17P: Existing Driveway Culvert	Peak Elev=204.15' Storage=3,126 cf Inflow=8.25 cfs 1.283 af Primary=5.93 cfs 1.086 af Secondary=2.30 cfs 0.146 af Outflow=8.23 cfs 1.232 af
Pond 18P: Box Culvert	Peak Elev=191.52' Storage=155 cf Inflow=10.53 cfs 1.433 af 36.0" x 36.0" Box Culvert n=0.012 L=28.0' S=0.0018 '/' Outflow=10.52 cfs 1.433 af
Pond 19P: Box Culvert	Peak Elev=184.15' Storage=24 cf Inflow=9.97 cfs 1.775 af 36.0" x 36.0" Box Culvert n=0.012 L=52.0' S=-0.0085 '/' Outflow=9.97 cfs 1.775 af

20-097 Existing Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1	Runoff Area=303,964 sf 0.00% Impervious Runoff Depth>1.22" Flow Length=1,542' Tc=32.6 min CN=45 Runoff=4.27 cfs 0.711 af
Subcatchment 2S: subcatchment 2	Runoff Area=764,518 sf 0.65% Impervious Runoff Depth>1.81" Flow Length=2,418' Tc=59.1 min CN=52 Runoff=13.44 cfs 2.652 af
Subcatchment 3S: Subcatchment 3	Runoff Area=122,849 sf 0.64% Impervious Runoff Depth>0.76" Flow Length=993' Tc=20.7 min CN=39 Runoff=0.95 cfs 0.179 af
Subcatchment 4S: Subcatchment 4	Runoff Area=4,089 sf 98.95% Impervious Runoff Depth>6.64" Flow Length=85' Slope=0.0472 '/' Tc=6.0 min CN=97 Runoff=0.63 cfs 0.052 af
Subcatchment 5S: Subcatchment 5	Runoff Area=10,452 sf 82.66% Impervious Runoff Depth>5.59" Flow Length=75' Tc=6.0 min CN=88 Runoff=1.47 cfs 0.112 af
Subcatchment 6S: Subcatchment 6	Runoff Area=24,193 sf 93.83% Impervious Runoff Depth>6.28" Flow Length=216' Tc=6.0 min CN=94 Runoff=3.64 cfs 0.291 af
Subcatchment 7S: Subcatchment 7	Runoff Area=7,743 sf 65.07% Impervious Runoff Depth>4.36" Flow Length=98' Tc=9.7 min CN=77 Runoff=0.79 cfs 0.065 af
Subcatchment 8S: Subcatchment 8	Runoff Area=19,227 sf 32.64% Impervious Runoff Depth>2.40" Flow Length=152' Tc=10.4 min CN=58 Runoff=1.02 cfs 0.088 af
Subcatchment 9S: Subcatchment 9	Runoff Area=64,869 sf 22.90% Impervious Runoff Depth>1.31" Flow Length=484' Tc=19.3 min UI Adjusted CN=46 Runoff=1.23 cfs 0.163 af
Subcatchment 10S: Subcatchment 10	Runoff Area=53,175 sf 5.56% Impervious Runoff Depth>0.91" Flow Length=438' Tc=18.4 min UI Adjusted CN=41 Runoff=0.57 cfs 0.093 af
Subcatchment 11S: Area Behind the Dove	Runoff Area=107,916 sf 6.10% Impervious Runoff Depth>1.07" Flow Length=802' Tc=22.0 min UI Adjusted CN=43 Runoff=1.42 cfs 0.220 af
Subcatchment 16S: Subcatchment #16	Runoff Area=297,191 sf 2.76% Impervious Runoff Depth>1.83" Flow Length=1,113' Tc=27.2 min CN=52 Runoff=7.82 cfs 1.042 af
Subcatchment 17S: Subcatchment #17	Runoff Area=497,407 sf 0.60% Impervious Runoff Depth>2.01" Flow Length=1,540' Tc=35.5 min UI Adjusted CN=54 Runoff=13.09 cfs 1.913 af
Subcatchment 18S: Subcatchment #18	Runoff Area=474,696 sf 0.22% Impervious Runoff Depth>2.30" Flow Length=1,280' Tc=29.3 min CN=57 Runoff=15.99 cfs 2.085 af
Subcatchment 19S: Subcatchment #19	Runoff Area=690,822 sf 0.00% Impervious Runoff Depth>2.00" Flow Length=1,832' Tc=46.3 min CN=54 Runoff=15.83 cfs 2.648 af
Reach 2R: Reach 2	Avg. Flow Depth=0.73' Max Vel=4.15 fps Inflow=13.44 cfs 2.652 af n=0.022 L=329.8' S=0.0091 '/' Capacity=24.64 cfs Outflow=13.44 cfs 2.649 af

20-097 Existing Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Reach 11R: Flow Through 8	Avg. Flow Depth=0.23' Max Vel=1.38 fps Inflow=1.42 cfs 0.220 af n=0.035 L=76.0' S=0.0132 '/' Capacity=7.77 cfs Outflow=1.42 cfs 0.220 af
Reach 100R: Reach 100	Inflow=6.51 cfs 1.040 af Outflow=6.51 cfs 1.040 af
Reach 200R: Reach 200	Inflow=13.07 cfs 1.861 af Outflow=13.07 cfs 1.861 af
Reach 300R: Reach 300	Inflow=15.97 cfs 2.085 af Outflow=15.97 cfs 2.085 af
Reach 400R: Reach 400	Inflow=15.83 cfs 2.648 af Outflow=15.83 cfs 2.648 af
Reach 800R: Svenson Pond	Inflow=18.46 cfs 4.622 af Outflow=18.46 cfs 4.622 af
Pond 1P: Pond 1	Peak Elev=204.76' Storage=1,722 cf Inflow=4.27 cfs 0.711 af Primary=2.92 cfs 0.681 af Secondary=1.30 cfs 0.030 af Outflow=3.77 cfs 0.711 af
Pond 2P: Existing CB#8	Peak Elev=200.26' Storage=3,895 cf Inflow=18.41 cfs 4.153 af Primary=13.50 cfs 3.903 af Secondary=6.34 cfs 0.249 af Outflow=18.01 cfs 4.152 af
Pond 4P: Existing CB#4	Peak Elev=203.84' Storage=69 cf Inflow=3.84 cfs 0.763 af Primary=2.98 cfs 0.744 af Secondary=0.86 cfs 0.022 af Outflow=3.85 cfs 0.763 af
Pond 5P: Existing CB #5	Peak Elev=202.07' Storage=82 cf Inflow=4.02 cfs 0.877 af Primary=1.66 cfs 0.689 af Secondary=2.46 cfs 0.189 af Outflow=4.03 cfs 0.877 af
Pond 6P: Existing CB #6	Peak Elev=201.74' Storage=97 cf Inflow=6.05 cfs 1.168 af Primary=3.19 cfs 0.969 af Secondary=2.92 cfs 0.199 af Outflow=5.98 cfs 1.168 af
Pond 7P: Existing CB#7	Peak Elev=200.33' Storage=60 cf Inflow=6.73 cfs 1.233 af Primary=6.73 cfs 1.227 af Secondary=0.16 cfs 0.005 af Outflow=6.73 cfs 1.232 af
Pond 8P: 24" Cross Culvert	Peak Elev=199.33' Storage=3,889 cf Inflow=18.89 cfs 4.460 af Primary=18.09 cfs 4.459 af Secondary=0.00 cfs 0.000 af Outflow=18.09 cfs 4.459 af
Pond 16P: 12" CMP	Peak Elev=204.84' Storage=6,280 cf Inflow=7.82 cfs 1.042 af Outflow=6.51 cfs 1.040 af
Pond 17P: Existing Driveway Culvert	Peak Elev=204.20' Storage=3,466 cf Inflow=13.09 cfs 1.913 af Primary=8.96 cfs 1.556 af Secondary=4.11 cfs 0.306 af Outflow=13.07 cfs 1.861 af
Pond 18P: Box Culvert	Peak Elev=191.93' Storage=398 cf Inflow=15.99 cfs 2.085 af 36.0" x 36.0" Box Culvert n=0.012 L=28.0' S=0.0018 '/' Outflow=15.97 cfs 2.085 af
Pond 19P: Box Culvert	Peak Elev=184.52' Storage=51 cf Inflow=15.83 cfs 2.648 af 36.0" x 36.0" Box Culvert n=0.012 L=52.0' S=-0.0085 '/' Outflow=15.83 cfs 2.648 af

Appendix II - Proposed Conditions Analysis

25 Yr - 24 Hr. Full Summary

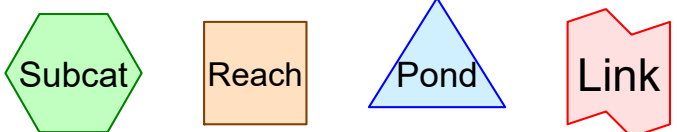
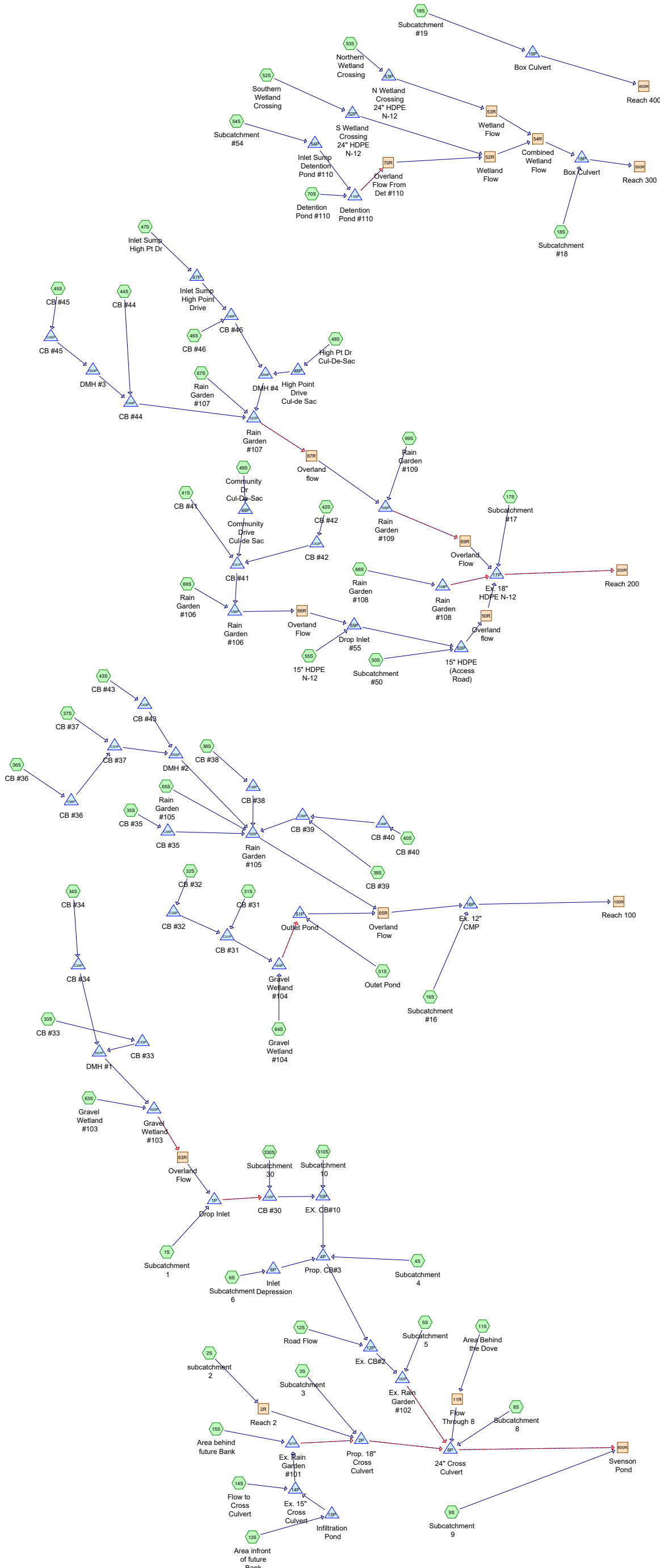
2 Yr - 24 Hr. Node Listing

10 Yr - 24 Hr. Node Listing

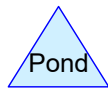
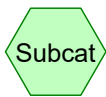
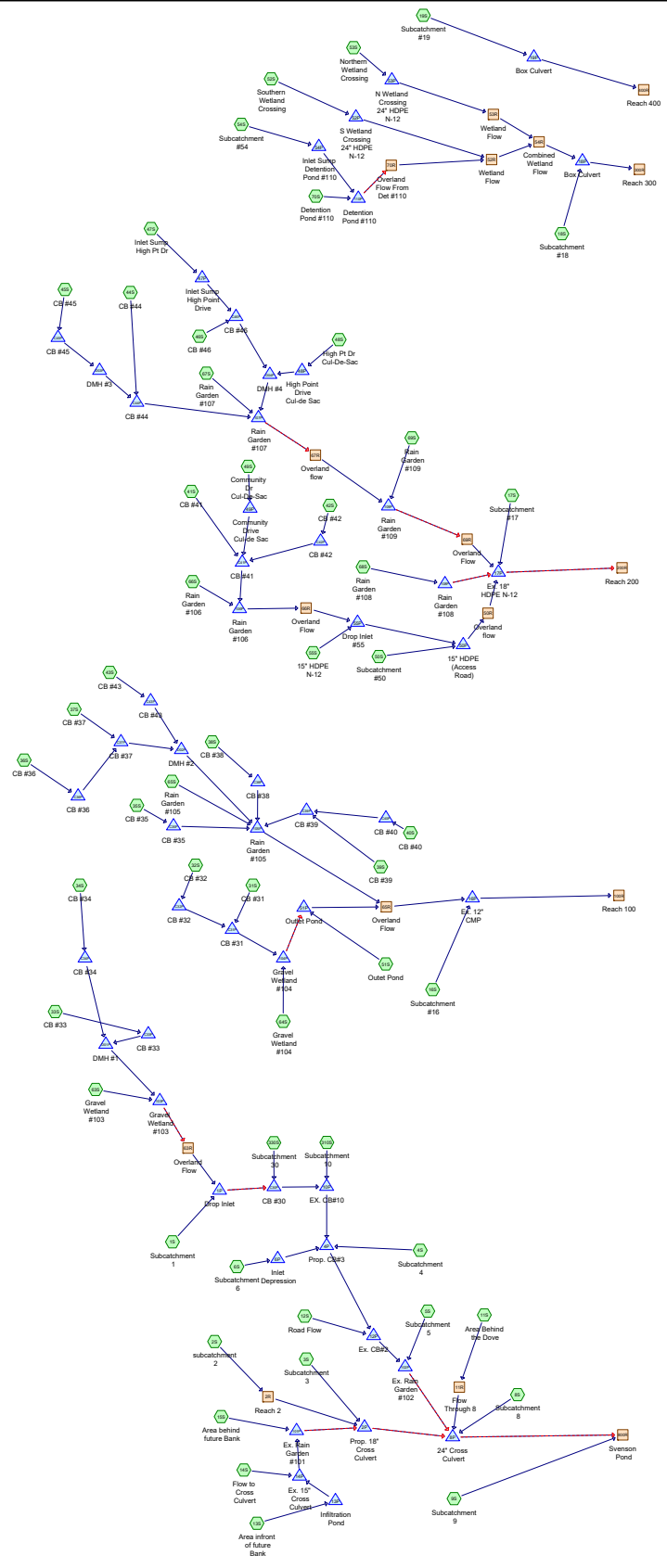
25 Yr - 24 Hr. Node Listing

50 Yr - 24 Hr. Node Listing

100 Yr - 24 Hr. Ponds Only



Routing Diagram for 20-097 Proposed Analysis
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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
8.146	39	>75% Grass cover, Good, HSG A (1S, 2S, 3S, 5S, 6S, 8S, 9S, 11S, 13S, 14S, 15S, 16S, 17S, 50S, 310S)
7.267	61	>75% Grass cover, Good, HSG B (1S, 11S, 16S, 17S, 18S, 31S, 32S, 33S, 35S, 36S, 37S, 38S, 39S, 41S, 42S, 43S, 44S, 45S, 47S, 48S, 49S, 50S, 51S, 52S, 53S, 54S, 55S, 63S, 64S, 65S, 66S, 67S, 68S, 69S, 70S, 310S, 330S)
0.883	74	>75% Grass cover, Good, HSG C (1S, 16S, 18S, 19S, 31S, 32S, 35S, 39S, 41S, 42S, 43S, 45S, 50S, 65S, 66S, 69S, 70S)
0.268	96	Gravel surface, HSG B (18S, 31S, 43S, 44S, 47S, 48S, 49S, 54S, 66S, 69S)
0.016	96	Gravel surface, HSG C (18S, 66S)
1.113	98	Paved parking, HSG A (2S, 4S, 6S, 12S, 15S)
2.198	98	Paved parking, HSG B (31S, 32S, 33S, 34S, 35S, 36S, 37S, 38S, 39S, 40S, 41S, 42S, 43S, 44S, 46S, 48S, 49S, 65S, 68S, 310S, 330S)
0.150	98	Paved parking, HSG C (31S, 32S, 35S, 38S, 40S, 41S, 42S, 43S, 65S)
0.089	98	Roofs, HSG B (1S, 44S, 54S)
0.012	98	Roofs, HSG C (1S)
0.800	98	Unconnected pavement, HSG A (5S, 8S, 9S, 11S, 13S, 14S, 16S, 17S, 18S)
0.025	98	Unconnected pavement, HSG D (17S, 18S)
0.469	98	Unconnected roofs, HSG A (2S, 4S, 5S, 8S, 9S, 11S, 13S)
0.509	98	Unconnected roofs, HSG B (33S, 34S, 36S, 37S, 43S, 45S, 46S, 47S, 66S)
0.046	98	Unconnected roofs, HSG C (35S, 43S, 45S)
0.067	98	Water Surface, 0% imp, HSG A (2S)
25.415	30	Woods, Good, HSG A (1S, 2S, 3S, 6S, 11S, 16S, 17S, 18S, 19S, 44S, 45S, 47S, 50S, 52S, 53S, 54S, 310S)
0.333	30	Woods, Good, HSG A H-C (3S)
8.595	55	Woods, Good, HSG B (1S, 17S, 18S, 19S, 52S, 53S, 54S, 69S, 70S)
3.751	70	Woods, Good, HSG C (1S, 18S, 19S, 52S, 53S, 70S)
10.940	77	Woods, Good, HSG D (1S, 11S, 16S, 17S, 18S, 19S, 44S, 45S, 47S, 50S, 52S, 53S, 54S)
7.952	77	Woods, Good, HSG D H-C (2S, 3S)
79.043	55	TOTAL AREA

20-097 Proposed Analysis

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
36.342	HSG A	1S, 2S, 3S, 4S, 5S, 6S, 8S, 9S, 11S, 12S, 13S, 14S, 15S, 16S, 17S, 18S, 19S, 44S, 45S, 47S, 50S, 52S, 53S, 54S, 310S
18.926	HSG B	1S, 11S, 16S, 17S, 18S, 19S, 31S, 32S, 33S, 34S, 35S, 36S, 37S, 38S, 39S, 40S, 41S, 42S, 43S, 44S, 45S, 46S, 47S, 48S, 49S, 50S, 51S, 52S, 53S, 54S, 55S, 63S, 64S, 65S, 66S, 67S, 68S, 69S, 70S, 310S, 330S
4.858	HSG C	1S, 16S, 18S, 19S, 31S, 32S, 35S, 38S, 39S, 40S, 41S, 42S, 43S, 45S, 50S, 52S, 53S, 65S, 66S, 69S, 70S
18.917	HSG D	1S, 2S, 3S, 11S, 16S, 17S, 18S, 19S, 44S, 45S, 47S, 50S, 52S, 53S, 54S
0.000	Other	
79.043		TOTAL AREA

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
8.146	7.267	0.883	0.000	0.000	16.296	>75% Grass cover, Good	1S, 2S, 3S, 5S, 6S, 8S, 9S, 11S, 13S, 14S, 15S, 16S, 17S, 18S, 19S, 31S, 32S, 33S, 35S, 36S, 37S, 38S, 39S, 41S, 42S, 43S, 44S, 45S, 47S, 48S, 49S, 50S, 51S, 52S, 53S, 54S, 55S, 63S, 64S, 65S, 66S, 67S, 68S, 69S, 70S, 310S, 330S

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Ground Covers (all nodes) (continued)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.268	0.016	0.000	0.000	0.284	Gravel surface	18S, 31S, 43S, 44S, 47S, 48S, 49S, 54S, 66S, 69S
1.113	2.198	0.150	0.000	0.000	3.461	Paved parking	2S, 4S, 6S, 12S, 15S, 31S, 32S, 33S, 34S, 35S, 36S, 37S, 38S, 39S, 40S, 41S, 42S, 43S, 44S, 46S, 48S, 49S, 65S, 68S, 310S, 330S
0.000	0.089	0.012	0.000	0.000	0.101	Roofs	1S, 44S, 54S
0.800	0.000	0.000	0.025	0.000	0.826	Unconnected pavement	5S, 8S, 9S, 11S, 13S, 14S, 16S, 17S, 18S
0.469	0.509	0.046	0.000	0.000	1.024	Unconnected roofs	2S, 4S, 5S, 8S, 9S, 11S, 13S, 33S,

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Ground Covers (all nodes) (continued)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.067	0.000	0.000	0.000	0.000	0.067	Water Surface, 0% imp	2S
25.747	8.595	3.751	18.892	0.000	56.984	Woods, Good	1S, 2S, 3S, 6S, 11S, 16S, 17S, 18S, 19S, 44S, 45S, 47S, 50S, 52S, 53S, 54S, 69S, 70S, 310S
36.342	18.926	4.858	18.917	0.000	79.043	TOTAL AREA	

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Pipe Listing (all nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
1	1P	200.75	200.40	11.5	0.0304	0.012	15.0	0.0	0.0
2	2P	198.10	197.50	60.0	0.0100	0.012	18.0	0.0	0.0
3	4P	199.20	198.70	93.7	0.0053	0.012	15.0	0.0	0.0
4	6P	200.00	199.30	30.0	0.0233	0.012	15.0	0.0	0.0
5	8P	196.55	196.44	21.6	0.0051	0.012	24.0	0.0	0.0
6	10P	200.07	199.30	153.9	0.0050	0.012	15.0	0.0	0.0
7	12P	198.60	198.50	20.0	0.0050	0.012	15.0	0.0	0.0
8	14P	201.50	201.00	50.0	0.0100	0.012	15.0	0.0	0.0
9	16P	203.25	203.05	20.0	0.0100	0.025	12.0	0.0	0.0
10	17P	202.25	202.00	37.0	0.0068	0.012	18.0	0.0	0.0
11	18P	190.25	190.20	28.0	0.0018	0.012	36.0	36.0	0.0
12	19P	182.69	183.13	52.0	-0.0085	0.012	36.0	36.0	0.0
13	47P	236.75	235.35	23.0	0.0609	0.012	15.0	0.0	0.0
14	48P	236.00	235.35	50.0	0.0130	0.012	15.0	0.0	0.0
15	49P	216.50	215.85	53.5	0.0121	0.012	15.0	0.0	0.0
16	50P	203.25	203.00	42.0	0.0060	0.012	15.0	0.0	0.0
17	52P	213.00	212.00	36.0	0.0278	0.024	24.0	0.0	6.0
18	53P	215.00	213.50	25.0	0.0600	0.024	24.0	0.0	6.0
19	54P	222.00	220.00	35.0	0.0571	0.012	15.0	0.0	0.0
20	55P	203.75	203.25	93.2	0.0054	0.012	15.0	0.0	0.0
21	101P	198.50	198.30	20.0	0.0100	0.012	6.0	0.0	0.0
22	102P	196.50	196.40	20.0	0.0050	0.012	6.0	0.0	0.0
23	103P	211.67	211.00	20.0	0.0335	0.012	15.0	0.0	0.0
24	104P	213.67	213.00	20.0	0.0335	0.012	15.0	0.0	0.0
25	105P	212.75	212.00	85.0	0.0088	0.012	18.0	0.0	0.0
26	106P	211.75	211.00	95.0	0.0079	0.012	15.0	0.0	0.0
27	107P	223.50	223.00	20.0	0.0250	0.012	15.0	0.0	0.0
28	108P	202.50	202.25	22.5	0.0111	0.012	6.0	0.0	0.0
29	109P	210.75	209.00	33.0	0.0530	0.012	15.0	0.0	0.0
30	110P	217.50	217.00	12.5	0.0400	0.012	15.0	0.0	0.0
31	C30P	200.30	200.17	25.0	0.0052	0.012	15.0	0.0	0.0
32	C31P	214.15	214.00	18.0	0.0083	0.012	15.0	0.0	0.0
33	C32P	214.40	214.25	26.0	0.0058	0.012	15.0	0.0	0.0
34	C33P	212.50	212.30	28.7	0.0070	0.012	15.0	0.0	0.0
35	C34P	216.55	212.30	63.5	0.0669	0.012	15.0	0.0	0.0
36	C35P	216.80	216.50	10.0	0.0300	0.012	15.0	0.0	0.0
37	C36P	224.69	223.88	162.0	0.0050	0.012	15.0	0.0	0.0
38	C37P	223.64	222.10	84.0	0.0183	0.012	15.0	0.0	0.0
39	C38P	219.18	219.00	13.0	0.0138	0.012	15.0	0.0	0.0
40	C39P	216.50	216.25	15.0	0.0167	0.012	15.0	0.0	0.0
41	C40P	217.00	216.60	31.7	0.0126	0.012	15.0	0.0	0.0
42	C41P	215.75	215.50	17.5	0.0143	0.012	15.0	0.0	0.0

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Pipe Listing (all nodes) (continued)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
43	C42P	216.25	215.85	26.0	0.0154	0.012	15.0	0.0	0.0
44	C43P	223.88	222.10	48.0	0.0371	0.012	15.0	0.0	0.0
45	C44P	228.63	227.00	87.0	0.0187	0.012	15.0	0.0	0.0
46	C45P	230.50	229.80	65.0	0.0108	0.012	15.0	0.0	0.0
47	C46P	235.25	228.10	105.0	0.0681	0.012	15.0	0.0	0.0
48	D01P	212.20	212.00	22.5	0.0089	0.012	15.0	0.0	0.0
49	D02P	222.00	217.75	95.0	0.0447	0.012	15.0	0.0	0.0
50	D03P	229.70	228.73	65.5	0.0148	0.012	15.0	0.0	0.0
51	D04P	228.00	227.50	50.0	0.0100	0.012	15.0	0.0	0.0

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1	Runoff Area=257,558 sf 0.40% Impervious Runoff Depth>0.62" Flow Length=1,542' Tc=32.6 min CN=43 Runoff=1.36 cfs 0.304 af
Subcatchment 2S: subcatchment 2	Runoff Area=764,518 sf 0.65% Impervious Runoff Depth>1.19" Flow Length=2,418' Tc=59.1 min CN=52 Runoff=8.18 cfs 1.744 af
Subcatchment 3S: Subcatchment 3	Runoff Area=118,503 sf 0.00% Impervious Runoff Depth>0.35" Flow Length=993' Tc=20.7 min CN=38 Runoff=0.26 cfs 0.080 af
Subcatchment 4S: Subcatchment 4	Runoff Area=9,068 sf 100.00% Impervious Runoff Depth>5.62" Flow Length=207' Tc=6.0 min CN=98 Runoff=1.17 cfs 0.097 af
Subcatchment 5S: Subcatchment 5	Runoff Area=22,497 sf 40.08% Impervious Runoff Depth>2.08" Flow Length=212' Tc=7.0 min CN=63 Runoff=1.16 cfs 0.089 af
Subcatchment 6S: Subcatchment 6	Runoff Area=25,520 sf 84.67% Impervious Runoff Depth>4.60" Tc=6.0 min CN=89 Runoff=2.97 cfs 0.224 af
Subcatchment 8S: Subcatchment 8	Runoff Area=25,776 sf 25.48% Impervious Runoff Depth>0.87" Flow Length=152' Tc=10.4 min UI Adjusted CN=47 Runoff=0.34 cfs 0.043 af
Subcatchment 9S: Subcatchment 9	Runoff Area=45,641 sf 11.38% Impervious Runoff Depth>0.56" Flow Length=259' Tc=13.4 min UI Adjusted CN=42 Runoff=0.26 cfs 0.049 af
Subcatchment 11S: Area Behind the Dove	Runoff Area=84,194 sf 13.93% Impervious Runoff Depth>0.68" Flow Length=636' Tc=29.3 min UI Adjusted CN=44 Runoff=0.54 cfs 0.109 af
Subcatchment 12S: Road Flow	Runoff Area=4,388 sf 100.00% Impervious Runoff Depth>5.62" Tc=6.0 min CN=98 Runoff=0.56 cfs 0.047 af
Subcatchment 13S: Area in front of future	Runoff Area=29,777 sf 30.66% Impervious Runoff Depth>1.59" Flow Length=175' Tc=12.4 min CN=57 Runoff=0.92 cfs 0.090 af
Subcatchment 14S: Flow to Cross Culvert	Runoff Area=7,713 sf 59.39% Impervious Runoff Depth>3.06" Tc=6.0 min CN=74 Runoff=0.62 cfs 0.045 af
Subcatchment 15S: Area behind future	Runoff Area=17,796 sf 67.02% Impervious Runoff Depth>3.55" Tc=6.0 min CN=79 Runoff=1.66 cfs 0.121 af
Subcatchment 16S: Subcatchment #16	Runoff Area=124,823 sf 1.96% Impervious Runoff Depth>0.62" Flow Length=344' Tc=16.5 min UI Adjusted CN=43 Runoff=0.82 cfs 0.148 af
Subcatchment 17S: Subcatchment #17	Runoff Area=152,689 sf 2.08% Impervious Runoff Depth>1.50" Flow Length=591' Tc=30.6 min CN=56 Runoff=3.12 cfs 0.438 af
Subcatchment 18S: Subcatchment #18	Runoff Area=170,513 sf 0.61% Impervious Runoff Depth>1.82" Flow Length=376' Tc=17.1 min CN=60 Runoff=5.61 cfs 0.595 af

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Subcatchment 19S: Subcatchment #19	Runoff Area=690,822 sf 0.00% Impervious Runoff Depth>1.34" Flow Length=1,832' Tc=46.3 min CN=54 Runoff=9.97 cfs 1.775 af
Subcatchment 31S: CB #31	Runoff Area=6,795 sf 55.78% Impervious Runoff Depth>4.06" Tc=6.0 min CN=84 Runoff=0.72 cfs 0.053 af
Subcatchment 32S: CB #32	Runoff Area=5,694 sf 79.08% Impervious Runoff Depth>4.71" Tc=6.0 min CN=90 Runoff=0.67 cfs 0.051 af
Subcatchment 33S: CB #33	Runoff Area=14,734 sf 60.85% Impervious Runoff Depth>4.06" Tc=6.0 min CN=84 Runoff=1.56 cfs 0.115 af
Subcatchment 34S: CB #34	Runoff Area=5,164 sf 100.00% Impervious Runoff Depth>5.62" Tc=6.0 min CN=98 Runoff=0.66 cfs 0.056 af
Subcatchment 35S: CB #35	Runoff Area=6,367 sf 67.93% Impervious Runoff Depth>4.27" Tc=6.0 min CN=86 Runoff=0.70 cfs 0.052 af
Subcatchment 36S: CB #36	Runoff Area=7,548 sf 93.27% Impervious Runoff Depth>5.38" Tc=6.0 min CN=96 Runoff=0.96 cfs 0.078 af
Subcatchment 37S: CB #37	Runoff Area=9,102 sf 80.61% Impervious Runoff Depth>4.82" Tc=6.0 min CN=91 Runoff=1.09 cfs 0.084 af
Subcatchment 38S: CB #38	Runoff Area=8,387 sf 77.58% Impervious Runoff Depth>4.71" Tc=6.0 min CN=90 Runoff=0.99 cfs 0.076 af
Subcatchment 39S: CB #39	Runoff Area=9,406 sf 38.75% Impervious Runoff Depth>3.35" Tc=6.0 min CN=77 Runoff=0.83 cfs 0.060 af
Subcatchment 40S: CB #40	Runoff Area=3,206 sf 100.00% Impervious Runoff Depth>5.62" Tc=6.0 min CN=98 Runoff=0.41 cfs 0.034 af
Subcatchment 41S: CB #41	Runoff Area=3,664 sf 87.72% Impervious Runoff Depth>5.15" Tc=6.0 min CN=94 Runoff=0.46 cfs 0.036 af
Subcatchment 42S: CB #42	Runoff Area=4,646 sf 81.42% Impervious Runoff Depth>4.93" Tc=6.0 min CN=92 Runoff=0.57 cfs 0.044 af
Subcatchment 43S: CB #43	Runoff Area=14,297 sf 87.98% Impervious Runoff Depth>5.15" Tc=6.0 min CN=94 Runoff=1.78 cfs 0.141 af
Subcatchment 44S: CB #44	Runoff Area=30,768 sf 38.03% Impervious Runoff Depth>2.96" Flow Length=493' Tc=14.6 min CN=73 Runoff=1.87 cfs 0.174 af
Subcatchment 45S: CB #45	Runoff Area=30,969 sf 18.55% Impervious Runoff Depth>2.51" Flow Length=265' Tc=10.4 min UI Adjusted CN=68 Runoff=1.77 cfs 0.149 af
Subcatchment 46S: CB #46	Runoff Area=7,198 sf 100.00% Impervious Runoff Depth>5.62" Tc=6.0 min CN=98 Runoff=0.93 cfs 0.077 af
Subcatchment 47S: Inlet Sump High Pt Dr	Runoff Area=95,547 sf 3.02% Impervious Runoff Depth>1.43" Flow Length=862' Tc=26.2 min UI Adjusted CN=55 Runoff=1.95 cfs 0.261 af

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Subcatchment48S: High Pt Dr Cul-De-Sac	Runoff Area=7,531 sf 77.93% Impervious Runoff Depth>4.82" Tc=6.0 min CN=91 Runoff=0.90 cfs 0.069 af
Subcatchment49S: Community Dr	Runoff Area=10,872 sf 69.81% Impervious Runoff Depth>4.49" Tc=6.0 min CN=88 Runoff=1.24 cfs 0.093 af
Subcatchment50S: Subcatchment#50	Runoff Area=20,749 sf 0.00% Impervious Runoff Depth>1.43" Flow Length=209' Tc=15.8 min CN=55 Runoff=0.52 cfs 0.057 af
Subcatchment51S: Outlet Pond	Runoff Area=2,846 sf 0.00% Impervious Runoff Depth>1.91" Tc=6.0 min CN=61 Runoff=0.14 cfs 0.010 af
Subcatchment52S: Southern Wetland	Runoff Area=237,763 sf 0.00% Impervious Runoff Depth>1.43" Flow Length=1,157' Tc=26.8 min CN=55 Runoff=4.80 cfs 0.649 af
Subcatchment53S: Northern Wetland	Runoff Area=23,588 sf 0.00% Impervious Runoff Depth>1.51" Flow Length=497' Tc=20.6 min CN=56 Runoff=0.57 cfs 0.068 af
Subcatchment54S: Subcatchment#54	Runoff Area=118,144 sf 0.71% Impervious Runoff Depth>1.66" Flow Length=1,159' Tc=25.9 min CN=58 Runoff=2.93 cfs 0.375 af
Subcatchment55S: 15" HDPE N-12	Runoff Area=4,389 sf 0.00% Impervious Runoff Depth>1.91" Tc=6.0 min CN=61 Runoff=0.21 cfs 0.016 af
Subcatchment63S: Gravel Wetland #103	Runoff Area=4,821 sf 0.00% Impervious Runoff Depth>1.91" Tc=6.0 min CN=61 Runoff=0.23 cfs 0.018 af
Subcatchment64S: Gravel Wetland #104	Runoff Area=1,940 sf 0.00% Impervious Runoff Depth>1.91" Tc=6.0 min CN=61 Runoff=0.09 cfs 0.007 af
Subcatchment65S: Rain Garden #105	Runoff Area=12,647 sf 3.41% Impervious Runoff Depth>2.42" Tc=6.0 min CN=67 Runoff=0.80 cfs 0.059 af
Subcatchment66S: Rain Garden #106	Runoff Area=34,434 sf 4.69% Impervious Runoff Depth>2.24" Flow Length=211' Tc=15.3 min UI Adjusted CN=65 Runoff=1.51 cfs 0.148 af
Subcatchment67S: Rain Garden #107	Runoff Area=22,575 sf 0.00% Impervious Runoff Depth>1.91" Flow Length=92' Tc=10.9 min CN=61 Runoff=0.93 cfs 0.082 af
Subcatchment68S: Rain Garden #108	Runoff Area=7,430 sf 45.91% Impervious Runoff Depth>3.45" Tc=6.0 min CN=78 Runoff=0.68 cfs 0.049 af
Subcatchment69S: Rain Garden #109	Runoff Area=78,911 sf 0.00% Impervious Runoff Depth>1.91" Flow Length=493' Tc=14.4 min CN=61 Runoff=2.93 cfs 0.288 af
Subcatchment70S: Detention Pond #110	Runoff Area=24,497 sf 0.00% Impervious Runoff Depth>1.74" Flow Length=273' Tc=12.3 min CN=59 Runoff=0.86 cfs 0.082 af
Subcatchment310S: Subcatchment 10	Runoff Area=9,312 sf 47.01% Impervious Runoff Depth>2.69" Tc=6.0 min CN=70 Runoff=0.66 cfs 0.048 af

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Subcatchment 330S: Subcatchment 30	Runoff Area=5,360 sf	77.01% Impervious	Runoff Depth>4.60"						
	Tc=6.0 min	CN=89	Runoff=0.62 cfs	0.047 af					
Reach 2R: Reach 2	Avg. Flow Depth=0.55'	Max Vel=3.59 fps	Inflow=8.18 cfs	1.744 af	n=0.022	L=220.0'	S=0.0091 '/'	Capacity=24.64 cfs	Outflow=8.18 cfs 1.742 af
Reach 11R: Flow Through 8	Avg. Flow Depth=0.15'	Max Vel=1.03 fps	Inflow=0.54 cfs	0.109 af	n=0.035	L=76.0'	S=0.0132 '/'	Capacity=7.77 cfs	Outflow=0.54 cfs 0.109 af
Reach 50R: Overland flow	Avg. Flow Depth=0.16'	Max Vel=1.80 fps	Inflow=0.83 cfs	0.303 af	n=0.025	L=42.0'	S=0.0179 '/'	Capacity=186.81 cfs	Outflow=0.83 cfs 0.303 af
Reach 52R: Wetland Flow	Avg. Flow Depth=0.28'	Max Vel=1.84 fps	Inflow=5.25 cfs	1.063 af	n=0.045	L=123.0'	S=0.0285 '/'	Capacity=17.83 cfs	Outflow=5.25 cfs 1.062 af
Reach 53R: Wetland Flow	Avg. Flow Depth=0.10'	Max Vel=1.01 fps	Inflow=0.57 cfs	0.068 af	n=0.045	L=135.0'	S=0.0370 '/'	Capacity=20.35 cfs	Outflow=0.56 cfs 0.068 af
Reach 54R: Combined Wetland Flow	Avg. Flow Depth=0.33'	Max Vel=5.20 fps	Inflow=5.76 cfs	1.130 af	n=0.045	L=87.0'	S=0.1379 '/'	Capacity=610.11 cfs	Outflow=5.76 cfs 1.130 af
Reach 63R: Overland Flow	Avg. Flow Depth=0.04'	Max Vel=1.00 fps	Inflow=0.20 cfs	0.119 af	n=0.030	L=126.0'	S=0.0476 '/'	Capacity=43.27 cfs	Outflow=0.20 cfs 0.119 af
Reach 65R: Overland Flow	Avg. Flow Depth=0.16'	Max Vel=1.60 fps	Inflow=2.24 cfs	0.471 af	n=0.035	L=342.1'	S=0.0270 '/'	Capacity=22.35 cfs	Outflow=2.02 cfs 0.469 af
Reach 66R: Overland Flow	Avg. Flow Depth=0.06'	Max Vel=1.90 fps	Inflow=0.30 cfs	0.231 af	n=0.025	L=48.0'	S=0.0677 '/'	Capacity=24.68 cfs	Outflow=0.30 cfs 0.231 af
Reach 67R: Overland flow	Avg. Flow Depth=0.14'	Max Vel=1.62 fps	Inflow=0.58 cfs	0.483 af	n=0.030	L=180.0'	S=0.0250 '/'	Capacity=39.17 cfs	Outflow=0.58 cfs 0.482 af
Reach 69R: Overland Flow	Avg. Flow Depth=0.11'	Max Vel=1.54 fps	Inflow=0.94 cfs	0.624 af	n=0.035	L=70.0'	S=0.0429 '/'	Capacity=111.48 cfs	Outflow=0.94 cfs 0.624 af
Reach 70R: Overland Flow From Det	Avg. Flow Depth=0.12'	Max Vel=2.29 fps	Inflow=0.66 cfs	0.415 af	n=0.035	L=61.0'	S=0.0820 '/'	Capacity=60.79 cfs	Outflow=0.66 cfs 0.415 af
Reach 100R: Reach 100			Inflow=2.05 cfs	0.617 af				Outflow=2.05 cfs	0.617 af
Reach 200R: Reach 200			Inflow=4.20 cfs	1.391 af				Outflow=4.20 cfs	1.391 af
Reach 300R: Reach 300			Inflow=10.32 cfs	1.724 af				Outflow=10.32 cfs	1.724 af
Reach 400R: Reach 400			Inflow=9.97 cfs	1.775 af				Outflow=9.97 cfs	1.775 af
Reach 800R: Svenson Pond			Inflow=10.76 cfs	3.096 af				Outflow=10.76 cfs	3.096 af

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Pond 1P: Drop Inlet	Peak Elev=201.47' Storage=2 cf Inflow=1.56 cfs 0.422 af Primary=1.55 cfs 0.422 af Secondary=0.00 cfs 0.000 af Outflow=1.55 cfs 0.422 af
Pond 2P: Prop. 18" Cross Culvert	Peak Elev=199.81' Storage=1,414 cf Inflow=8.76 cfs 1.976 af 18.0" Round Culvert n=0.012 L=60.0' S=0.0100 '/' Outflow=8.33 cfs 1.976 af
Pond 4P: Prop. CB#3	Peak Elev=201.27' Storage=0.001 af Inflow=4.46 cfs 0.839 af 15.0" Round Culvert n=0.012 L=93.7' S=0.0053 '/' Outflow=4.46 cfs 0.839 af
Pond 6P: Inlet Depression	Peak Elev=201.51' Storage=516 cf Inflow=2.97 cfs 0.224 af 15.0" Round Culvert n=0.012 L=30.0' S=0.0233 '/' Outflow=2.43 cfs 0.224 af
Pond 8P: 24" Cross Culvert	Peak Elev=198.37' Storage=1,119 cf Inflow=10.68 cfs 3.048 af Primary=10.66 cfs 3.047 af Secondary=0.00 cfs 0.000 af Outflow=10.66 cfs 3.047 af
Pond 10P: EX. CB#10	Peak Elev=201.46' Storage=17 cf Inflow=1.74 cfs 0.517 af 15.0" Round Culvert n=0.012 L=153.9' S=0.0050 '/' Outflow=1.75 cfs 0.517 af
Pond 12P: Ex. CB#2	Peak Elev=200.74' Storage=0.001 af Inflow=5.03 cfs 0.886 af 15.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=5.01 cfs 0.886 af
Pond 13P: Infiltration Pond	Peak Elev=203.42' Storage=1,247 cf Inflow=0.92 cfs 0.090 af Discarded=0.07 cfs 0.058 af Primary=0.24 cfs 0.023 af Outflow=0.31 cfs 0.081 af
Pond 14P: Ex. 15" Cross Culvert	Peak Elev=202.12' Storage=651 cf Inflow=0.62 cfs 0.068 af Discarded=0.02 cfs 0.015 af Primary=0.28 cfs 0.053 af Outflow=0.30 cfs 0.068 af
Pond 16P: Ex. 12" CMP	Peak Elev=204.38' Storage=1,402 cf Inflow=2.80 cfs 0.618 af Outflow=2.05 cfs 0.617 af
Pond 17P: Ex. 18" HDPE N-12	Peak Elev=203.44' Storage=402 cf Inflow=4.24 cfs 1.392 af Primary=4.20 cfs 1.391 af Secondary=0.00 cfs 0.000 af Outflow=4.20 cfs 1.391 af
Pond 18P: Box Culvert	Peak Elev=191.50' Storage=148 cf Inflow=10.32 cfs 1.724 af 36.0" x 36.0" Box Culvert n=0.012 L=28.0' S=0.0018 '/' Outflow=10.32 cfs 1.724 af
Pond 19P: Box Culvert	Peak Elev=184.15' Storage=24 cf Inflow=9.97 cfs 1.775 af 36.0" x 36.0" Box Culvert n=0.012 L=52.0' S=-0.0085 '/' Outflow=9.97 cfs 1.775 af
Pond 47P: Inlet Sump High Point Drive	Peak Elev=237.44' Storage=64 cf Inflow=1.95 cfs 0.261 af 15.0" Round Culvert n=0.012 L=23.0' S=0.0609 '/' Outflow=1.95 cfs 0.261 af
Pond 48P: High Point Drive Cul-de Sac	Peak Elev=236.43' Storage=180 cf Inflow=0.90 cfs 0.069 af 15.0" Round Culvert n=0.012 L=50.0' S=0.0130 '/' Outflow=0.84 cfs 0.069 af
Pond 49P: Community Drive Cul-de Sac	Peak Elev=218.85' Storage=636 cf Inflow=1.24 cfs 0.093 af 15.0" Round Culvert n=0.012 L=53.5' S=0.0121 '/' Outflow=0.99 cfs 0.089 af
Pond 50P: 15" HDPE (Access Road)	Peak Elev=203.75' Storage=60 cf Inflow=0.83 cfs 0.304 af 15.0" Round Culvert n=0.012 L=42.0' S=0.0060 '/' Outflow=0.83 cfs 0.303 af

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Pond 51P: Outlet Pond	Peak Elev=214.07' Storage=949 cf Inflow=0.87 cfs 0.087 af Outflow=0.83 cfs 0.066 af
Pond 52P: S Wetland Crossing 24" HDPE N-12	Peak Elev=214.35' Storage=86 cf Inflow=4.80 cfs 0.649 af 24.0" Round Culvert w/ 6.0" inside fill n=0.024 L=36.0' S=0.0278 '/' Outflow=4.80 cfs 0.649 af
Pond 53P: N Wetland Crossing 24" HDPE N-12	Peak Elev=215.71' Storage=6 cf Inflow=0.57 cfs 0.068 af 24.0" Round Culvert w/ 6.0" inside fill n=0.024 L=25.0' S=0.0600 '/' Outflow=0.57 cfs 0.068 af
Pond 54P: Inlet Sump Detention Pond #110	Peak Elev=222.88' Storage=79 cf Inflow=2.93 cfs 0.375 af 15.0" Round Culvert n=0.012 L=35.0' S=0.0571 '/' Outflow=2.93 cfs 0.375 af
Pond 55P: Drop Inlet #55	Peak Elev=204.09' Storage=0.000 af Inflow=0.33 cfs 0.247 af 15.0" Round Culvert n=0.012 L=93.2' S=0.0054 '/' Outflow=0.33 cfs 0.247 af
Pond 101P: Ex. Rain Garden #101	Peak Elev=202.10' Storage=2,682 cf Inflow=1.94 cfs 0.174 af Primary=0.39 cfs 0.155 af Secondary=0.00 cfs 0.000 af Outflow=0.39 cfs 0.155 af
Pond 102P: Ex. Rain Garden #102	Peak Elev=200.21' Storage=6,276 cf Inflow=6.14 cfs 0.975 af Primary=0.46 cfs 0.545 af Secondary=4.50 cfs 0.375 af Outflow=4.96 cfs 0.920 af
Pond 103P: Gravel Wetland #103	Peak Elev=214.46' Storage=4,554 cf Inflow=2.43 cfs 0.187 af Primary=0.20 cfs 0.119 af Secondary=0.00 cfs 0.000 af Outflow=0.20 cfs 0.119 af
Pond 104P: Gravel Wetland #104	Peak Elev=216.47' Storage=1,882 cf Inflow=1.46 cfs 0.110 af Primary=0.79 cfs 0.076 af Secondary=0.00 cfs 0.000 af Outflow=0.79 cfs 0.076 af
Pond 105P: Rain Garden #105	Peak Elev=219.61' Storage=13,225 cf Inflow=7.52 cfs 0.582 af Outflow=1.51 cfs 0.405 af
Pond 106P: Rain Garden #106	Peak Elev=218.85' Storage=7,015 cf Inflow=3.02 cfs 0.315 af Outflow=0.30 cfs 0.231 af
Pond 107P: Rain Garden #107	Peak Elev=229.12' Storage=20,541 cf Inflow=6.78 cfs 0.812 af Discarded=0.01 cfs 0.017 af Primary=0.58 cfs 0.483 af Secondary=0.00 cfs 0.000 af Outflow=0.59 cfs 0.500 af
Pond 108P: Rain Garden #108	Peak Elev=206.51' Storage=1,314 cf Inflow=0.68 cfs 0.049 af Primary=0.02 cfs 0.025 af Secondary=0.02 cfs 0.002 af Outflow=0.05 cfs 0.027 af
Pond 109P: Rain Garden #109	Peak Elev=217.80' Storage=6,590 cf Inflow=2.93 cfs 0.770 af Primary=0.94 cfs 0.624 af Secondary=0.00 cfs 0.000 af Outflow=0.94 cfs 0.624 af
Pond 110P: Detention Pond #110	Peak Elev=220.33' Storage=7,901 cf Inflow=3.50 cfs 0.456 af Primary=0.66 cfs 0.415 af Secondary=0.00 cfs 0.000 af Outflow=0.66 cfs 0.415 af
Pond C30P: CB #30	Peak Elev=201.36' Storage=13 cf Inflow=1.63 cfs 0.470 af 15.0" Round Culvert n=0.012 L=25.0' S=0.0052 '/' Outflow=1.64 cfs 0.469 af
Pond C31P: CB #31	Peak Elev=216.49' Storage=29 cf Inflow=1.38 cfs 0.104 af 15.0" Round Culvert n=0.012 L=18.0' S=0.0083 '/' Outflow=1.36 cfs 0.103 af
Pond C32P: CB #32	Peak Elev=216.49' Storage=26 cf Inflow=0.67 cfs 0.051 af 15.0" Round Culvert n=0.012 L=26.0' S=0.0058 '/' Outflow=0.66 cfs 0.051 af

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Pond C33P: CB #33	Peak Elev=214.47' Storage=25 cf Inflow=1.56 cfs 0.115 af 15.0" Round Culvert n=0.012 L=28.7' S=0.0070 '/' Outflow=1.55 cfs 0.114 af
Pond C34P: CB #34	Peak Elev=216.93' Storage=9 cf Inflow=0.66 cfs 0.056 af 15.0" Round Culvert n=0.012 L=63.5' S=0.0669 '/' Outflow=0.67 cfs 0.055 af
Pond C35P: CB #35	Peak Elev=219.62' Storage=35 cf Inflow=0.70 cfs 0.052 af 15.0" Round Culvert n=0.012 L=10.0' S=0.0300 '/' Outflow=0.68 cfs 0.051 af
Pond C36P: CB #36	Peak Elev=225.21' Storage=7 cf Inflow=0.96 cfs 0.078 af 15.0" Round Culvert n=0.012 L=162.0' S=0.0050 '/' Outflow=0.96 cfs 0.078 af
Pond C37P: CB #37	Peak Elev=224.35' Storage=9 cf Inflow=2.05 cfs 0.162 af 15.0" Round Culvert n=0.012 L=84.0' S=0.0183 '/' Outflow=2.06 cfs 0.162 af
Pond C38P: CB #38	Peak Elev=219.68' Storage=6 cf Inflow=0.99 cfs 0.076 af 15.0" Round Culvert n=0.012 L=13.0' S=0.0138 '/' Outflow=0.99 cfs 0.075 af
Pond C39P: CB #39	Peak Elev=219.62' Storage=39 cf Inflow=1.23 cfs 0.094 af 15.0" Round Culvert n=0.012 L=15.0' S=0.0167 '/' Outflow=1.20 cfs 0.094 af
Pond C40P: CB #40	Peak Elev=219.62' Storage=33 cf Inflow=0.41 cfs 0.034 af 15.0" Round Culvert n=0.012 L=31.7' S=0.0126 '/' Outflow=0.39 cfs 0.034 af
Pond C41P: CB #41	Peak Elev=218.85' Storage=39 cf Inflow=1.99 cfs 0.168 af 15.0" Round Culvert n=0.012 L=17.5' S=0.0143 '/' Outflow=1.98 cfs 0.168 af
Pond C42P: CB #42	Peak Elev=218.85' Storage=33 cf Inflow=0.57 cfs 0.044 af 15.0" Round Culvert n=0.012 L=26.0' S=0.0154 '/' Outflow=0.55 cfs 0.043 af
Pond C43P: CB #43	Peak Elev=224.53' Storage=8 cf Inflow=1.78 cfs 0.141 af 15.0" Round Culvert n=0.012 L=48.0' S=0.0371 '/' Outflow=1.79 cfs 0.141 af
Pond C44P: CB #44	Peak Elev=229.62' Storage=12 cf Inflow=3.54 cfs 0.323 af 15.0" Round Culvert n=0.012 L=87.0' S=0.0187 '/' Outflow=3.54 cfs 0.323 af
Pond C45P: CB #45	Peak Elev=231.15' Storage=8 cf Inflow=1.77 cfs 0.149 af 15.0" Round Culvert n=0.012 L=65.0' S=0.0108 '/' Outflow=1.77 cfs 0.149 af
Pond C46P: CB #46	Peak Elev=235.99' Storage=9 cf Inflow=2.21 cfs 0.338 af 15.0" Round Culvert n=0.012 L=105.0' S=0.0681 '/' Outflow=2.21 cfs 0.338 af
Pond D01P: DMH #1	Peak Elev=214.47' Storage=28 cf Inflow=2.21 cfs 0.169 af 15.0" Round Culvert n=0.012 L=22.5' S=0.0089 '/' Outflow=2.20 cfs 0.169 af
Pond D02P: DMH #2	Peak Elev=223.05' Storage=13 cf Inflow=3.84 cfs 0.303 af 15.0" Round Culvert n=0.012 L=95.0' S=0.0447 '/' Outflow=3.84 cfs 0.303 af
Pond D03P: DMH #3	Peak Elev=230.36' Storage=8 cf Inflow=1.77 cfs 0.149 af 15.0" Round Culvert n=0.012 L=65.5' S=0.0148 '/' Outflow=1.77 cfs 0.149 af

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Pond D04P: DMH #4

Peak Elev=229.13' Storage=14 cf Inflow=2.55 cfs 0.407 af
15.0" Round Culvert n=0.012 L=50.0' S=0.0100 '/' Outflow=2.55 cfs 0.407 af

Total Runoff Area = 79.043 ac Runoff Volume = 9.705 af Average Runoff Depth = 1.47"
93.15% Pervious = 73.631 ac 6.85% Impervious = 5.412 ac

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Summary for Subcatchment 1S: Subcatchment 1

Runoff = 1.36 cfs @ 12.66 hrs, Volume= 0.304 af, Depth> 0.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
1,508	39	>75% Grass cover, Good, HSG A
152,098	30	Woods, Good, HSG A
490	98	Roofs, HSG B
23,651	61	>75% Grass cover, Good, HSG B
44,989	55	Woods, Good, HSG B
531	98	Roofs, HSG C
1,231	74	>75% Grass cover, Good, HSG C
12,010	70	Woods, Good, HSG C
21,050	77	Woods, Good, HSG D
257,558	43	Weighted Average
256,537		99.60% Pervious Area
1,021		0.40% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.8	100	0.1500	0.17		Sheet Flow, Segment 1 Woods: Light underbrush n= 0.400 P2= 3.08"
4.7	442	0.0973	1.56		Shallow Concentrated Flow, Segment 2 Woodland Kv= 5.0 fps
0.5	65	0.2153	2.32		Shallow Concentrated Flow, Segment 3 Woodland Kv= 5.0 fps
2.6	153	0.0395	0.99		Shallow Concentrated Flow, Segment 4 Woodland Kv= 5.0 fps
2.6	153	0.0393	0.99		Shallow Concentrated Flow, Segment 5 Woodland Kv= 5.0 fps
0.7	62	0.0806	1.42		Shallow Concentrated Flow, Segment 6 Woodland Kv= 5.0 fps
5.0	190	0.0158	0.63		Shallow Concentrated Flow, Segment 7 Woodland Kv= 5.0 fps
5.9	315	0.0317	0.89		Shallow Concentrated Flow, Segment 8 Woodland Kv= 5.0 fps
0.8	62	0.0645	1.27		Shallow Concentrated Flow, Segment 9 Woodland Kv= 5.0 fps
32.6	1,542	Total			

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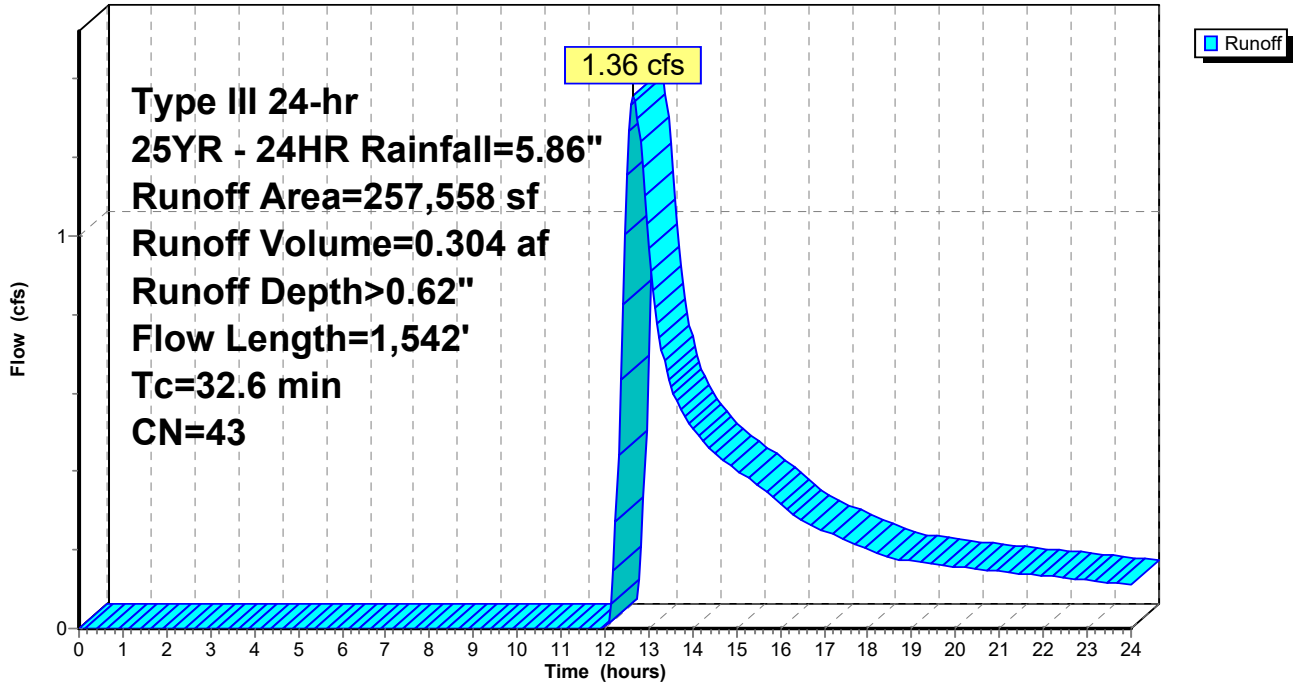
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Subcatchment 1S: Subcatchment 1

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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 2S: subcatchment 2

Runoff = 8.18 cfs @ 12.93 hrs, Volume= 1.744 af, Depth> 1.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
2,663	98	Unconnected roofs, HSG A
55,787	39	>75% Grass cover, Good, HSG A
2,337	98	Paved parking, HSG A
37,068	30	Woods, Good, HSG A
2,905	98	Water Surface, 0% imp, HSG A
* 331,879	77	Woods, Good, HSG D H-C
331,879	30	Woods, Good, HSG A
764,518	52	Weighted Average
759,518		99.35% Pervious Area
5,000		0.65% Impervious Area
2,663		53.26% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
15.2	100	0.0500	0.11		Sheet Flow, Segment 1 Woods: Light underbrush n= 0.400 P2= 3.08"
9.8	940	0.1032	1.61		Shallow Concentrated Flow, Segment 2 Woodland Kv= 5.0 fps
14.8	445	0.0101	0.50		Shallow Concentrated Flow, Segment 3 Woodland Kv= 5.0 fps
2.1	59	0.0085	0.46		Shallow Concentrated Flow, Segment 4 Woodland Kv= 5.0 fps
1.7	137	0.0728	1.35		Shallow Concentrated Flow, Segment 5 Woodland Kv= 5.0 fps
12.7	418	0.0120	0.55		Shallow Concentrated Flow, Segment 6 Woodland Kv= 5.0 fps
2.5	165	0.0242	1.09		Shallow Concentrated Flow, Segment 7 Short Grass Pasture Kv= 7.0 fps
0.1	68		12.69		Lake or Reservoir, Segment 8 Mean Depth= 5.00'
0.2	86	0.0174	6.81	23.84	Trap/Vee/Rect Channel Flow, Segment 9 Bot.W=3.00' D=1.00' Z= 0.5 '/' Top.W=4.00' n= 0.022 Earth, clean & straight
59.1	2,418	Total			

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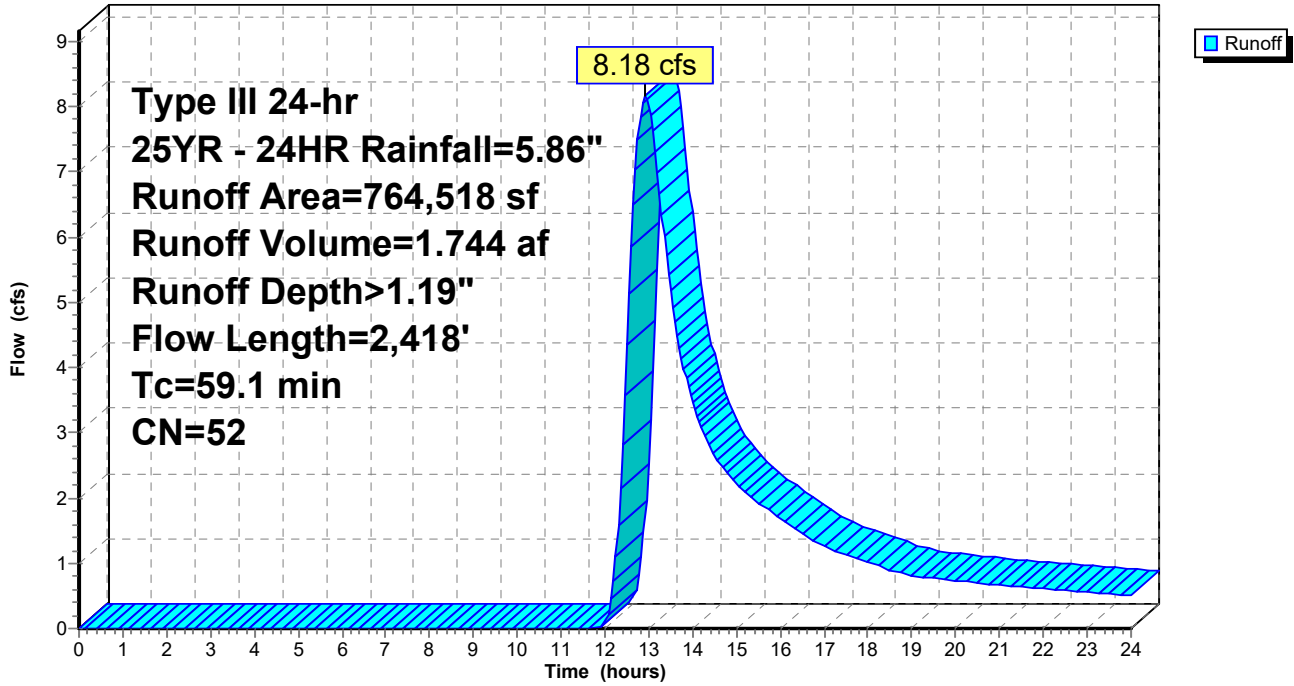
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Subcatchment 2S: subcatchment 2

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 3S: Subcatchment 3

Runoff = 0.26 cfs @ 12.61 hrs, Volume= 0.080 af, Depth> 0.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
33,586	39	>75% Grass cover, Good, HSG A
55,939	30	Woods, Good, HSG A
* 14,489	77	Woods, Good, HSG D H-C
* 14,489	30	Woods, Good, HSG A H-C
118,503	38	Weighted Average
118,503		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0	97	0.1334	0.16		Sheet Flow, Segment 1 Woods: Light underbrush n= 0.400 P2= 3.08"
2.7	155	0.0355	0.94		Shallow Concentrated Flow, Segment 2 Woodland Kv= 5.0 fps
5.3	290	0.0328	0.91		Shallow Concentrated Flow, Segment 3 Woodland Kv= 5.0 fps
1.6	132	0.0379	1.36		Shallow Concentrated Flow, Segment 4 Short Grass Pasture Kv= 7.0 fps
1.1	319	0.0094	5.01	17.52	Trap/Vee/Rect Channel Flow, Segment 5 Bot.W=3.00' D=1.00' Z= 0.5 '/' Top.W=4.00' n= 0.022 Earth, clean & straight
20.7	993	Total			

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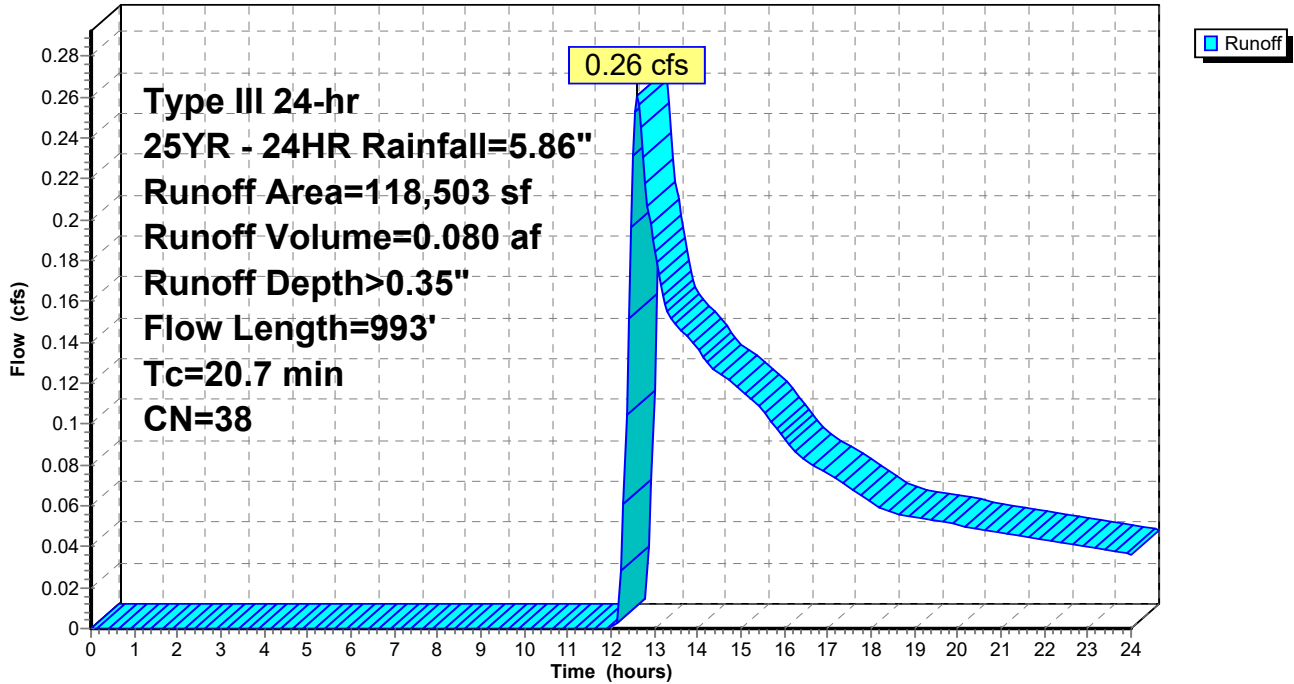
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Subcatchment 3S: Subcatchment 3

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Summary for Subcatchment 4S: Subcatchment 4

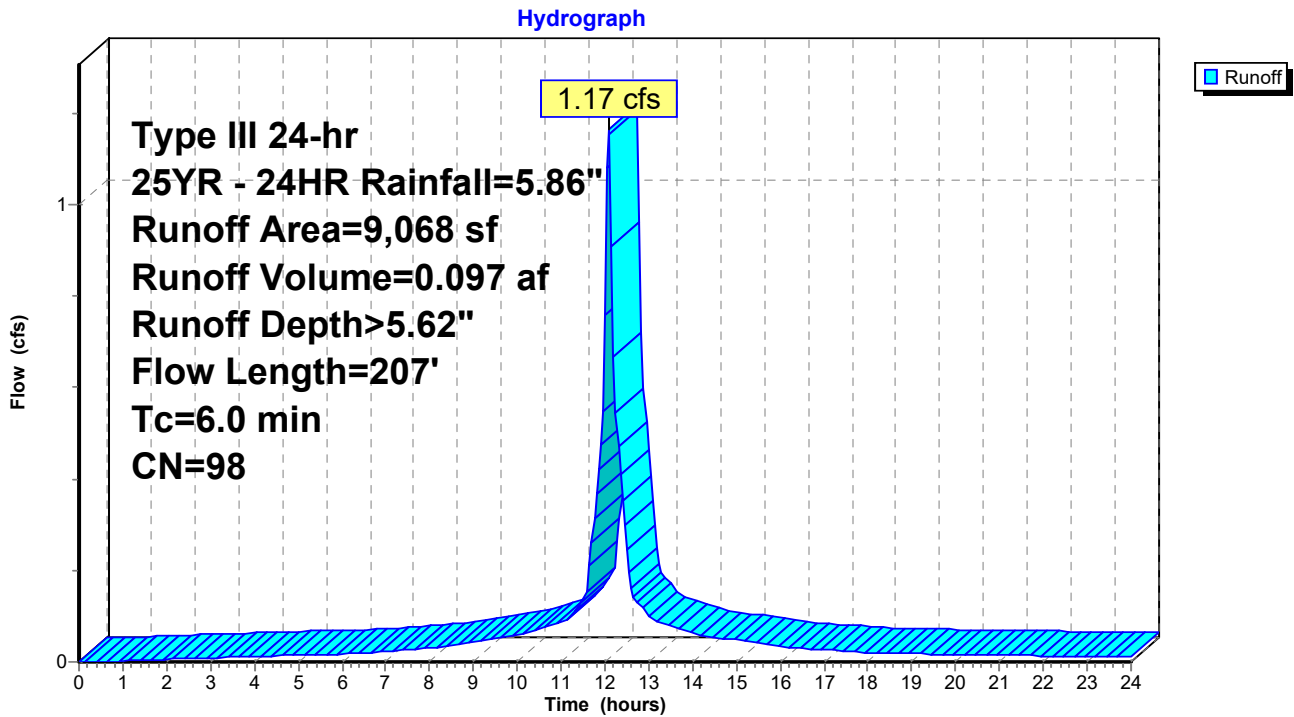
Runoff = 1.17 cfs @ 12.09 hrs, Volume= 0.097 af, Depth> 5.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
859	98	Unconnected roofs, HSG A
8,209	98	Paved parking, HSG A
9,068	98	Weighted Average
9,068		100.00% Impervious Area
859		9.47% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.7	71	0.0472	1.78		Sheet Flow, Segment 1 Smooth surfaces n= 0.011 P2= 3.08"
1.1	136	0.0100	2.03		Shallow Concentrated Flow, 2 Paved Kv= 20.3 fps
1.8	207	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 4S: Subcatchment 4



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 5S: Subcatchment 5

Runoff = 1.16 cfs @ 12.11 hrs, Volume= 0.089 af, Depth> 2.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
6,050	98	Unconnected roofs, HSG A
13,481	39	>75% Grass cover, Good, HSG A
2,966	98	Unconnected pavement, HSG A
22,497	63	Weighted Average
13,481		59.92% Pervious Area
9,016		40.08% Impervious Area
9,016		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.7	65	0.0553	0.23		Sheet Flow, Segment 1 Grass: Short n= 0.150 P2= 3.08"
0.0	8	0.0200	2.87		Shallow Concentrated Flow, Segment 2 Paved Kv= 20.3 fps
1.0	40	0.0100	0.70		Shallow Concentrated Flow, 3 Short Grass Pasture Kv= 7.0 fps
0.3	56	0.0200	2.87		Shallow Concentrated Flow, 4 Paved Kv= 20.3 fps
1.0	43	0.0100	0.70		Shallow Concentrated Flow, 4 Short Grass Pasture Kv= 7.0 fps
7.0	212	Total			

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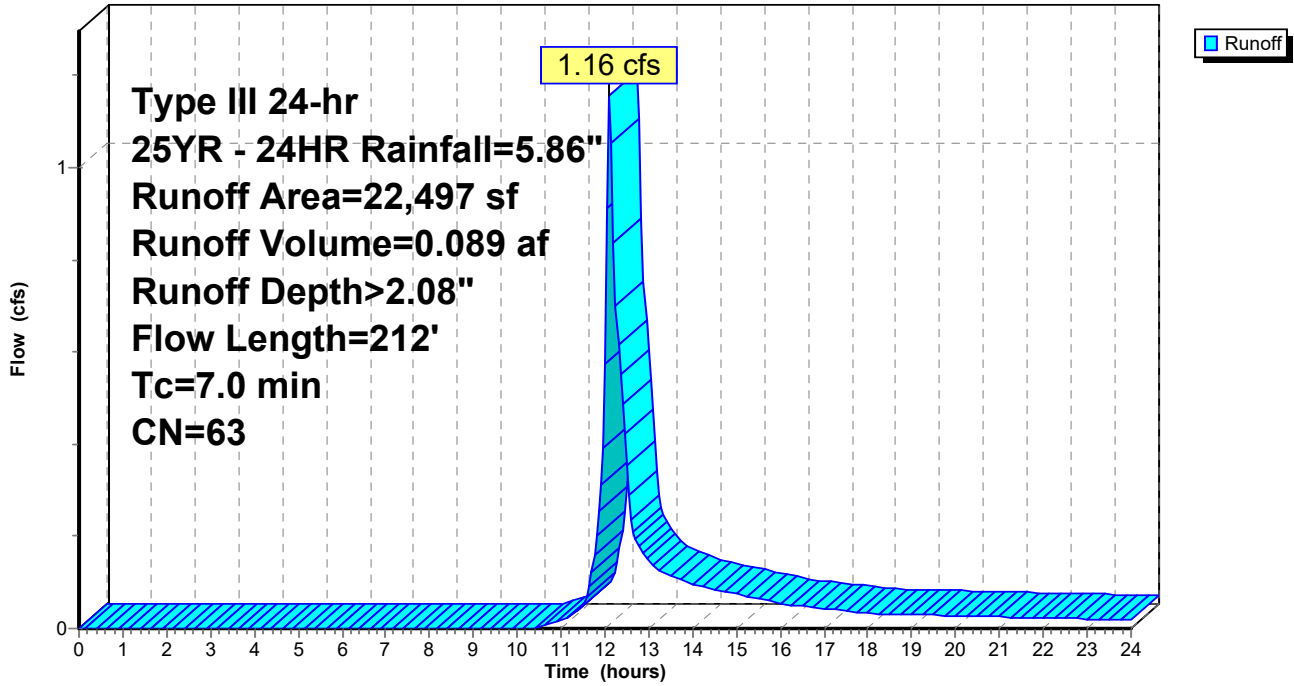
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Subcatchment 5S: Subcatchment 5

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Summary for Subcatchment 6S: Subcatchment 6

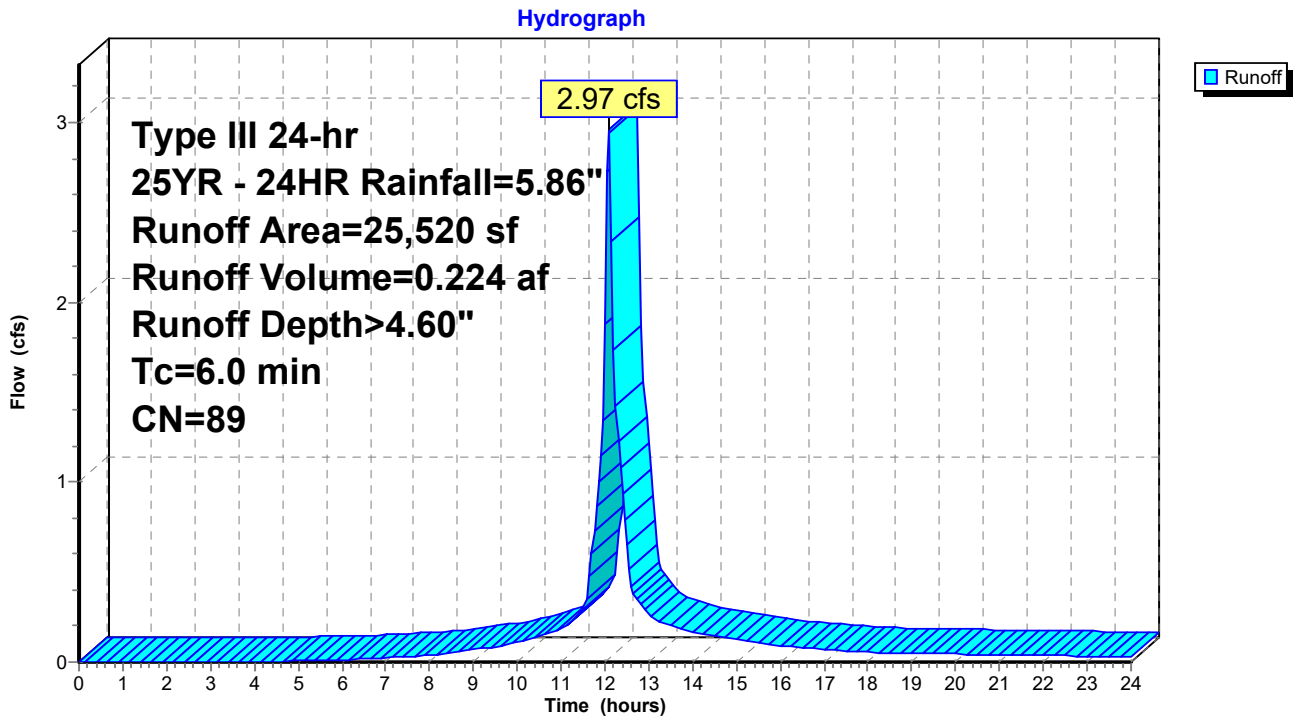
Runoff = 2.97 cfs @ 12.09 hrs, Volume= 0.224 af, Depth> 4.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
3,588	39	>75% Grass cover, Good, HSG A
21,608	98	Paved parking, HSG A
324	30	Woods, Good, HSG A
25,520	89	Weighted Average
3,912		15.33% Pervious Area
21,608		84.67% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Direct Entry

Subcatchment 6S: Subcatchment 6



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 8S: Subcatchment 8

Runoff = 0.34 cfs @ 12.20 hrs, Volume= 0.043 af, Depth> 0.87"

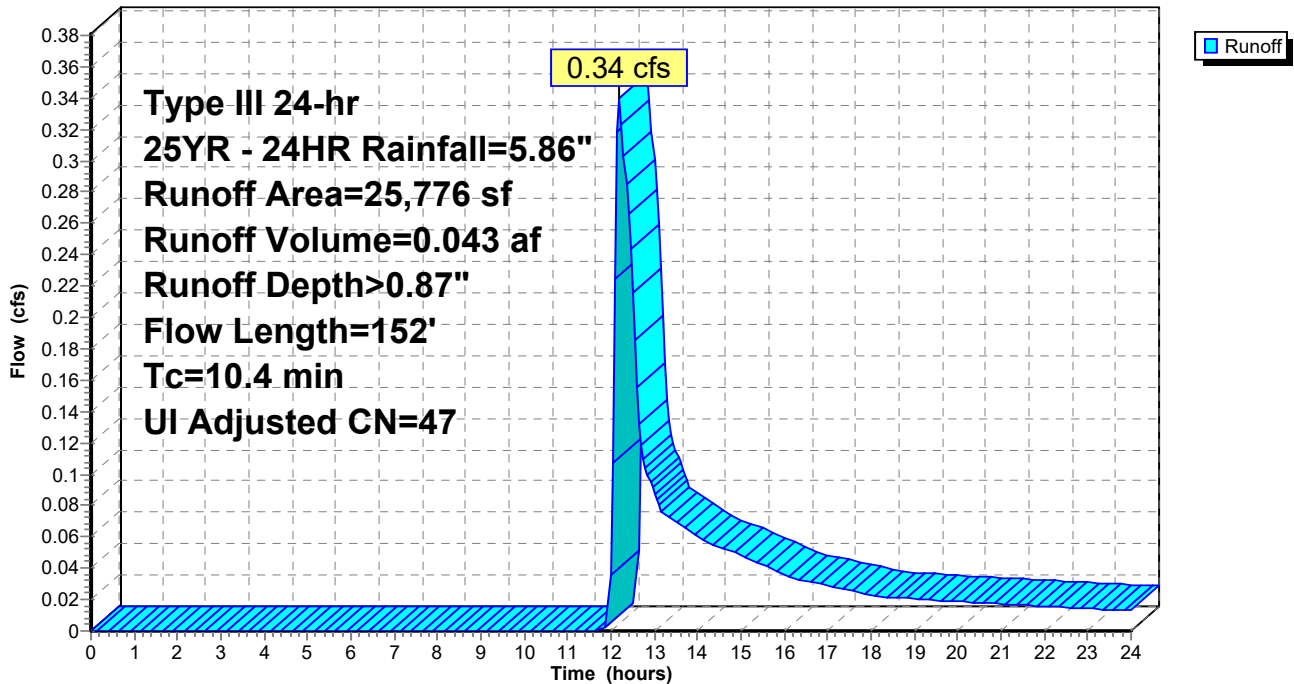
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Adj	Description
2,022	98		Unconnected roofs, HSG A
19,207	39		>75% Grass cover, Good, HSG A
4,547	98		Unconnected pavement, HSG A
25,776	54	47	Weighted Average, UI Adjusted
19,207			74.52% Pervious Area
6,569			25.48% Impervious Area
6,569			100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.5	87	0.0172	0.15		Sheet Flow, Segment 1 Grass: Short n= 0.150 P2= 3.08"
0.9	65	0.0309	1.23		Shallow Concentrated Flow, Segment 2 Short Grass Pasture Kv= 7.0 fps
10.4	152	Total			

Subcatchment 8S: Subcatchment 8

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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 9S: Subcatchment 9

Runoff = 0.26 cfs @ 12.40 hrs, Volume= 0.049 af, Depth> 0.56"

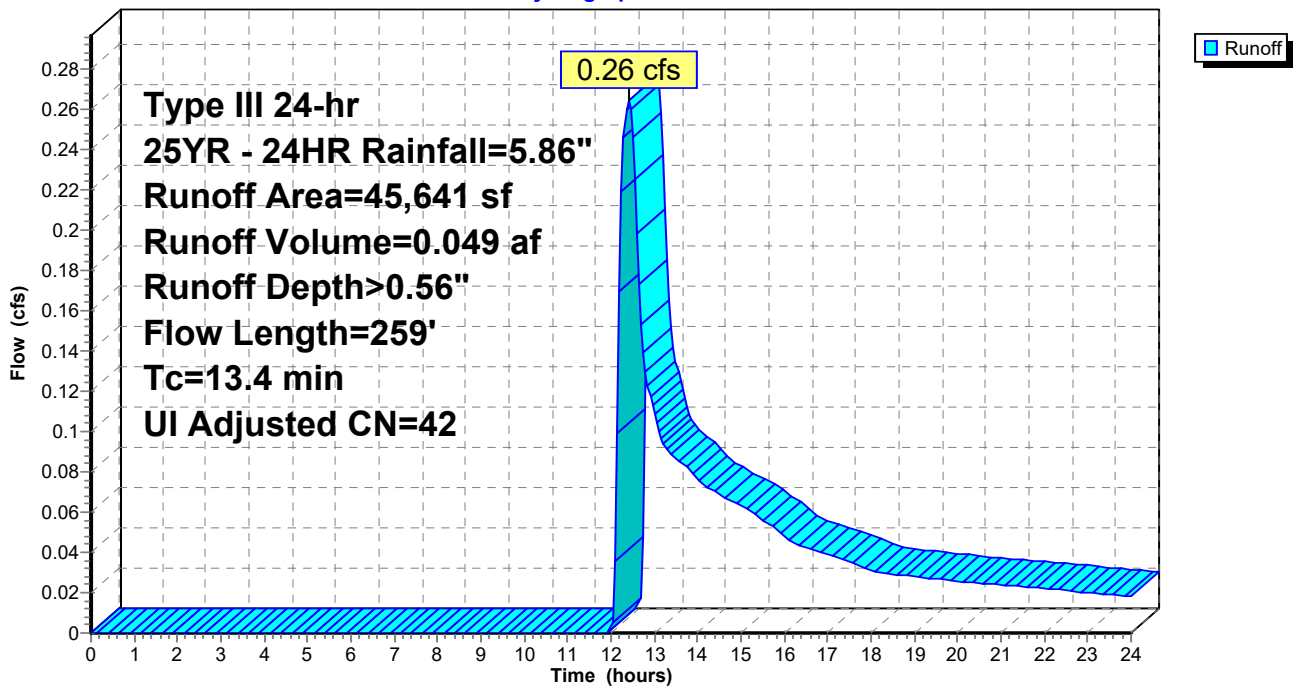
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Adj	Description
606	98		Unconnected roofs, HSG A
40,448	39		>75% Grass cover, Good, HSG A
4,587	98		Unconnected pavement, HSG A
45,641	46	42	Weighted Average, UI Adjusted
40,448			88.62% Pervious Area
5,193			11.38% Impervious Area
5,193			100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.2	100	0.0150	0.15		Sheet Flow, Segment 1 Grass: Short n= 0.150 P2= 3.08"
1.0	58	0.0200	0.99		Shallow Concentrated Flow, Segment 2 Short Grass Pasture Kv= 7.0 fps
1.2	101	0.0397	1.39		Shallow Concentrated Flow, Segment 4 Short Grass Pasture Kv= 7.0 fps
13.4	259	Total			

Subcatchment 9S: Subcatchment 9

Hydrograph



20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 11S: Area Behind the Dove

Runoff = 0.54 cfs @ 12.59 hrs, Volume= 0.109 af, Depth> 0.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Adj	Description
6,511	98		Unconnected roofs, HSG A
55,227	39		>75% Grass cover, Good, HSG A
5,216	98		Unconnected pavement, HSG A
12,577	30		Woods, Good, HSG A
1,621	61		>75% Grass cover, Good, HSG B
3,042	77		Woods, Good, HSG D
84,194	48	44	Weighted Average, UI Adjusted
72,467			86.07% Pervious Area
11,727			13.93% Impervious Area
11,727			100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	32	0.1905	0.15		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
14.0	69	0.0292	0.08		Sheet Flow, Segment #2 Woods: Light underbrush n= 0.400 P2= 3.08"
3.1	215	0.0280	1.17		Shallow Concentrated Flow, Segment #3 Short Grass Pasture Kv= 7.0 fps
8.6	320	0.0078	0.62		Shallow Concentrated Flow, Segment #4 Short Grass Pasture Kv= 7.0 fps
29.3	636	Total			

20-097 Proposed Analysis

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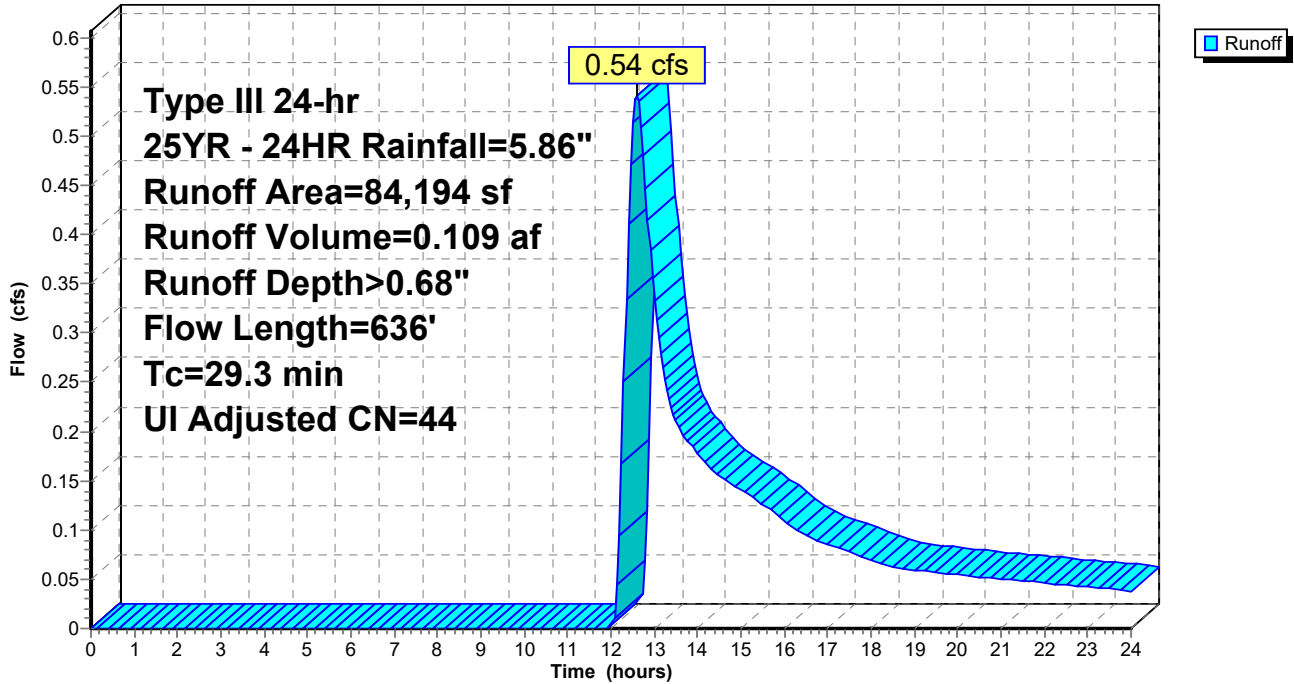
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 11S: Area Behind the Dove

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 12S: Road Flow

Runoff = 0.56 cfs @ 12.09 hrs, Volume= 0.047 af, Depth> 5.62"

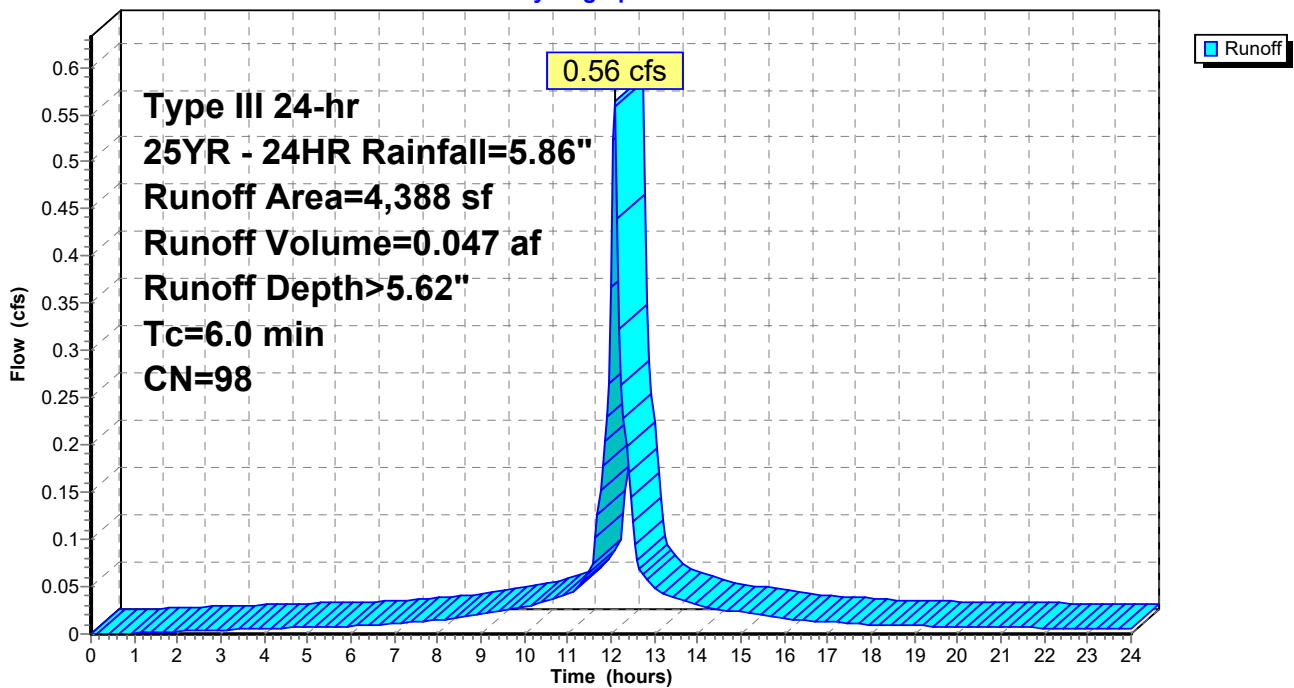
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
4,388	98	Paved parking, HSG A
4,388		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Direct Entry

Subcatchment 12S: Road Flow

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 13S: Area in front of future Bank

Runoff = 0.92 cfs @ 12.20 hrs, Volume= 0.090 af, Depth> 1.59"

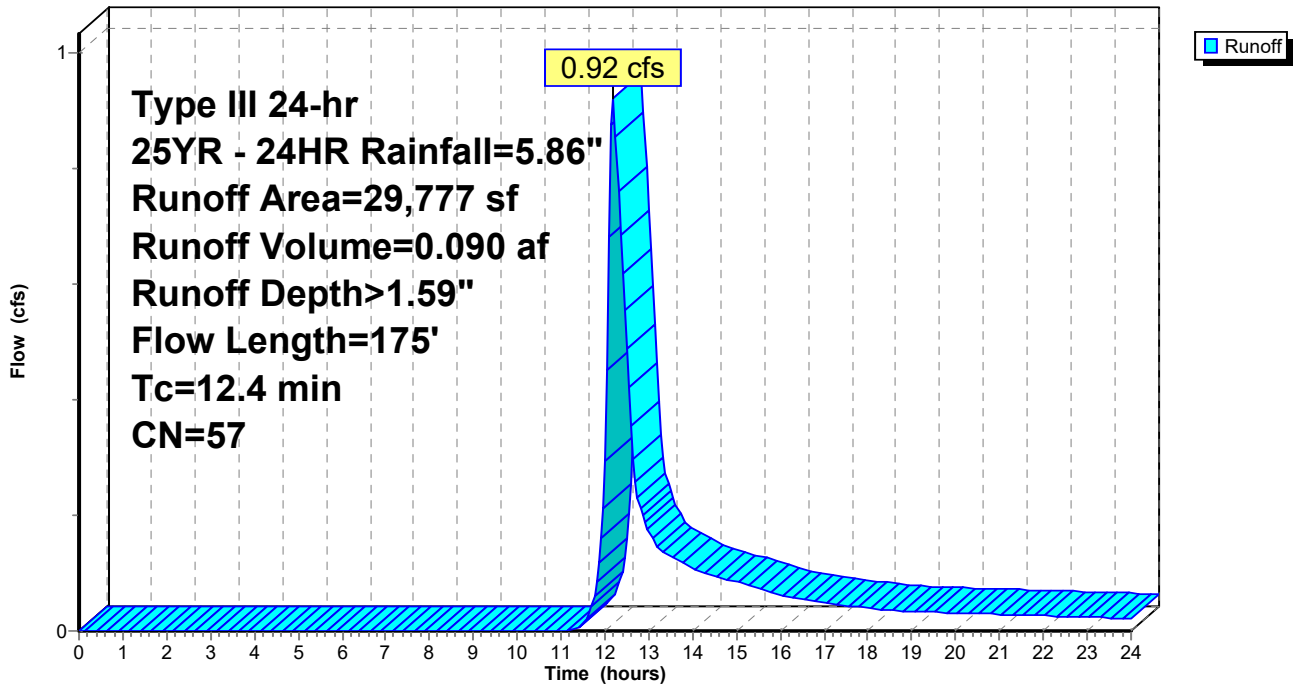
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
1,730	98	Unconnected roofs, HSG A
20,647	39	>75% Grass cover, Good, HSG A
7,400	98	Unconnected pavement, HSG A
29,777	57	Weighted Average
20,647		69.34% Pervious Area
9,130		30.66% Impervious Area
9,130		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.1	99	0.0151	0.15		Sheet Flow, Segment 1 Grass: Short n= 0.150 P2= 3.08"
1.3	76	0.0200	0.99		Shallow Concentrated Flow, Segment 2 Short Grass Pasture Kv= 7.0 fps
12.4	175	Total			

Subcatchment 13S: Area in front of future Bank

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 14S: Flow to Cross Culvert

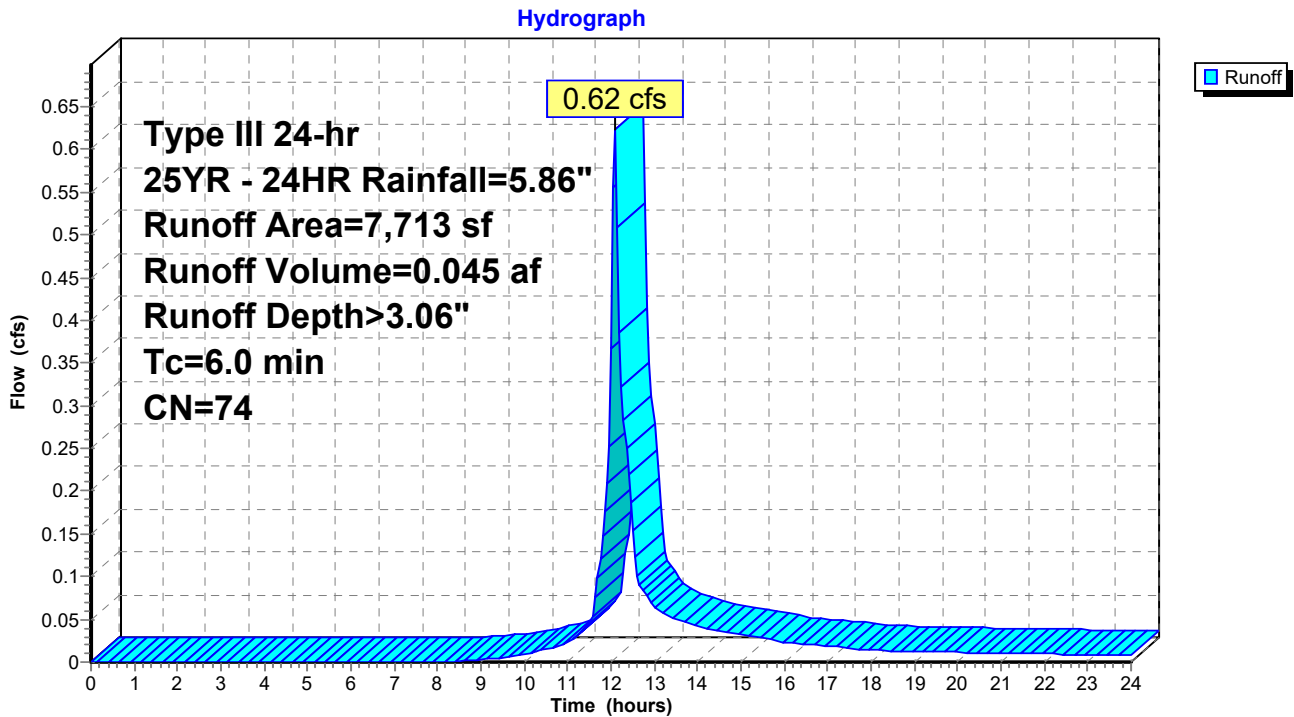
Runoff = 0.62 cfs @ 12.09 hrs, Volume= 0.045 af, Depth> 3.06"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
4,581	98	Unconnected pavement, HSG A
3,132	39	>75% Grass cover, Good, HSG A
7,713	74	Weighted Average
3,132		40.61% Pervious Area
4,581		59.39% Impervious Area
4,581		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Direct

Subcatchment 14S: Flow to Cross Culvert



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 15S: Area behind future Bank

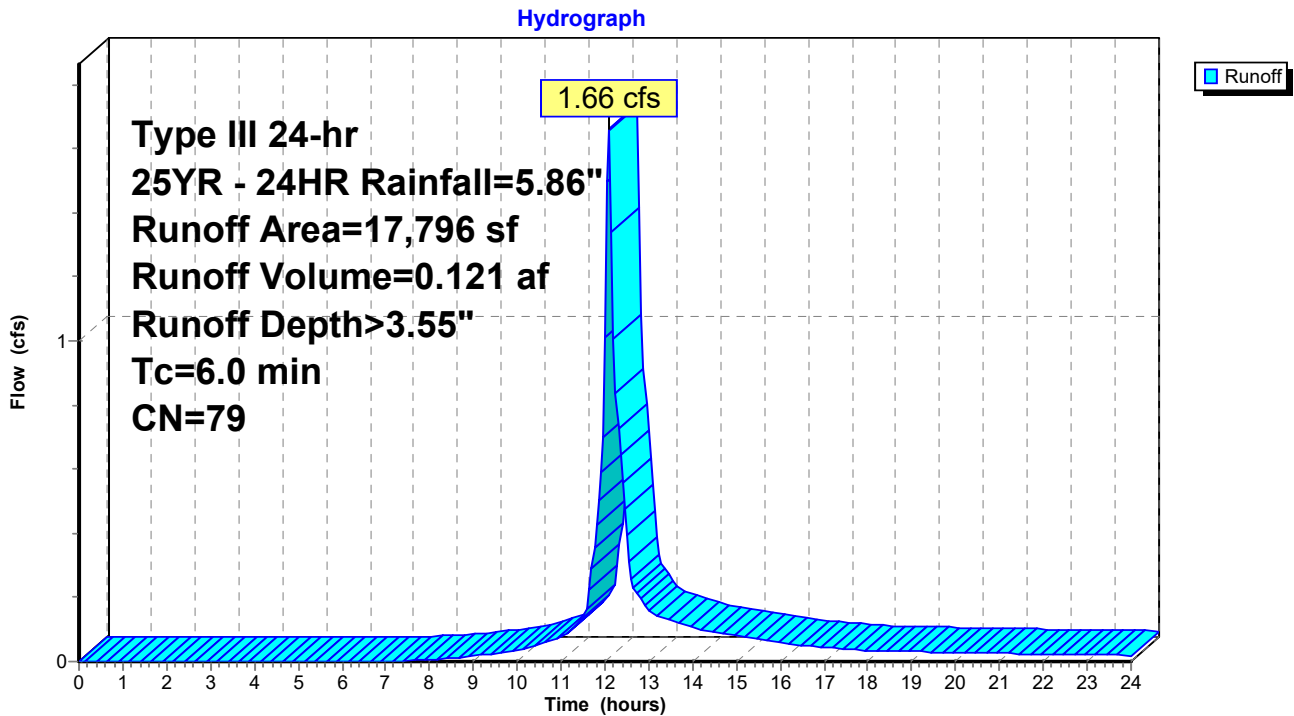
Runoff = 1.66 cfs @ 12.09 hrs, Volume= 0.121 af, Depth> 3.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
5,870	39	>75% Grass cover, Good, HSG A
11,926	98	Paved parking, HSG A
17,796	79	Weighted Average
5,870		32.98% Pervious Area
11,926		67.02% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Direct Entry

Subcatchment 15S: Area behind future Bank



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 16S: Subcatchment #16

Runoff = 0.82 cfs @ 12.42 hrs, Volume= 0.148 af, Depth> 0.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Adj	Description
98,278	39		>75% Grass cover, Good, HSG A
2,451	98		Unconnected pavement, HSG A
8,822	30		Woods, Good, HSG A
4,860	61		>75% Grass cover, Good, HSG B
1,590	74		>75% Grass cover, Good, HSG C
8,822	77		Woods, Good, HSG D
124,823	44	43	Weighted Average, UI Adjusted
122,372			98.04% Pervious Area
2,451			1.96% Impervious Area
2,451			100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.0	49	0.0600	0.10		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
4.1	51	0.0490	0.21		Sheet Flow, Segment #2 Grass: Short n= 0.150 P2= 3.08"
0.4	39	0.0640	1.77		Shallow Concentrated Flow, Segment #3 Short Grass Pasture Kv= 7.0 fps
4.0	205	0.0146	0.85		Shallow Concentrated Flow, Segment #4 Short Grass Pasture Kv= 7.0 fps
16.5	344	Total			

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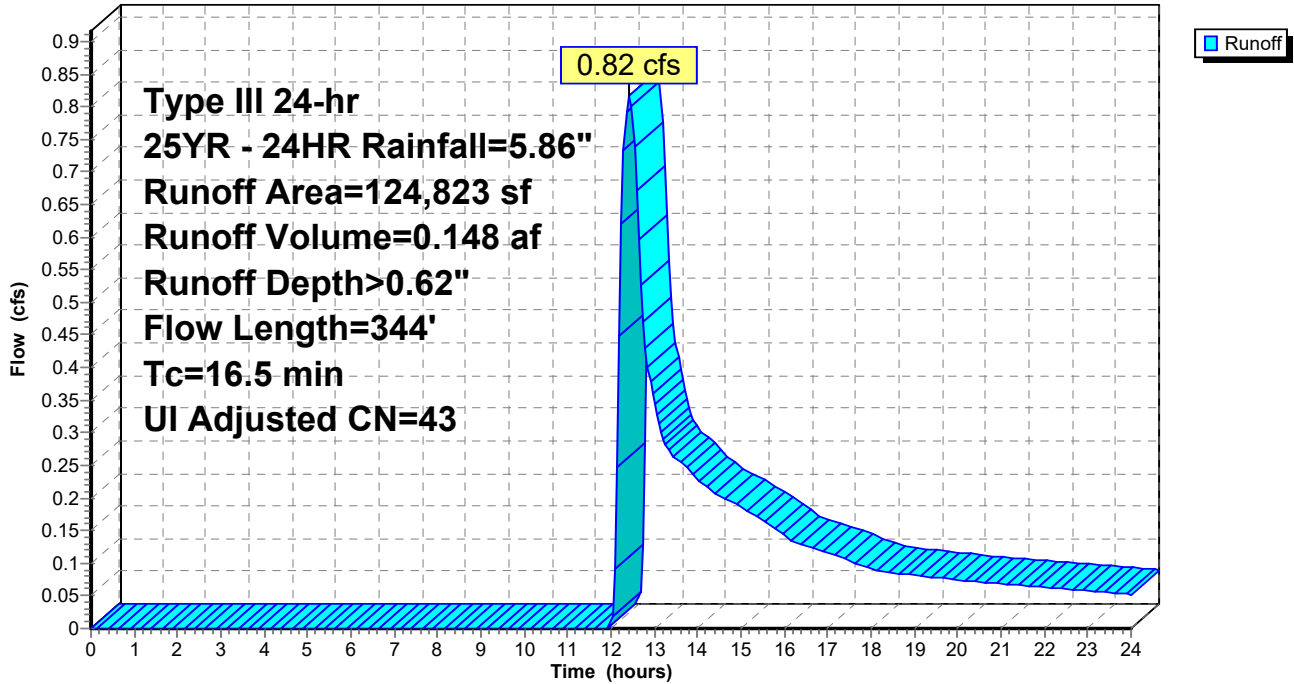
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 16S: Subcatchment #16

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 17S: Subcatchment #17

Runoff = 3.12 cfs @ 12.49 hrs, Volume= 0.438 af, Depth> 1.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
1,337	39	>75% Grass cover, Good, HSG A
2,187	98	Unconnected pavement, HSG A
15,239	30	Woods, Good, HSG A
15,416	61	>75% Grass cover, Good, HSG B
102,265	55	Woods, Good, HSG B
992	98	Unconnected pavement, HSG D
15,253	77	Woods, Good, HSG D
152,689	56	Weighted Average
149,510		97.92% Pervious Area
3,179		2.08% Impervious Area
3,179		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
23.1	100	0.0175	0.07		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
2.9	195	0.0513	1.13		Shallow Concentrated Flow, Segment #2 Woodland Kv= 5.0 fps
1.2	122	0.1148	1.69		Shallow Concentrated Flow, Segment #3 Woodland Kv= 5.0 fps
1.0	57	0.0351	0.94		Shallow Concentrated Flow, Segment #4 Woodland Kv= 5.0 fps
2.4	117	0.0256	0.80		Shallow Concentrated Flow, Segment #5 Woodland Kv= 5.0 fps
30.6	591	Total			

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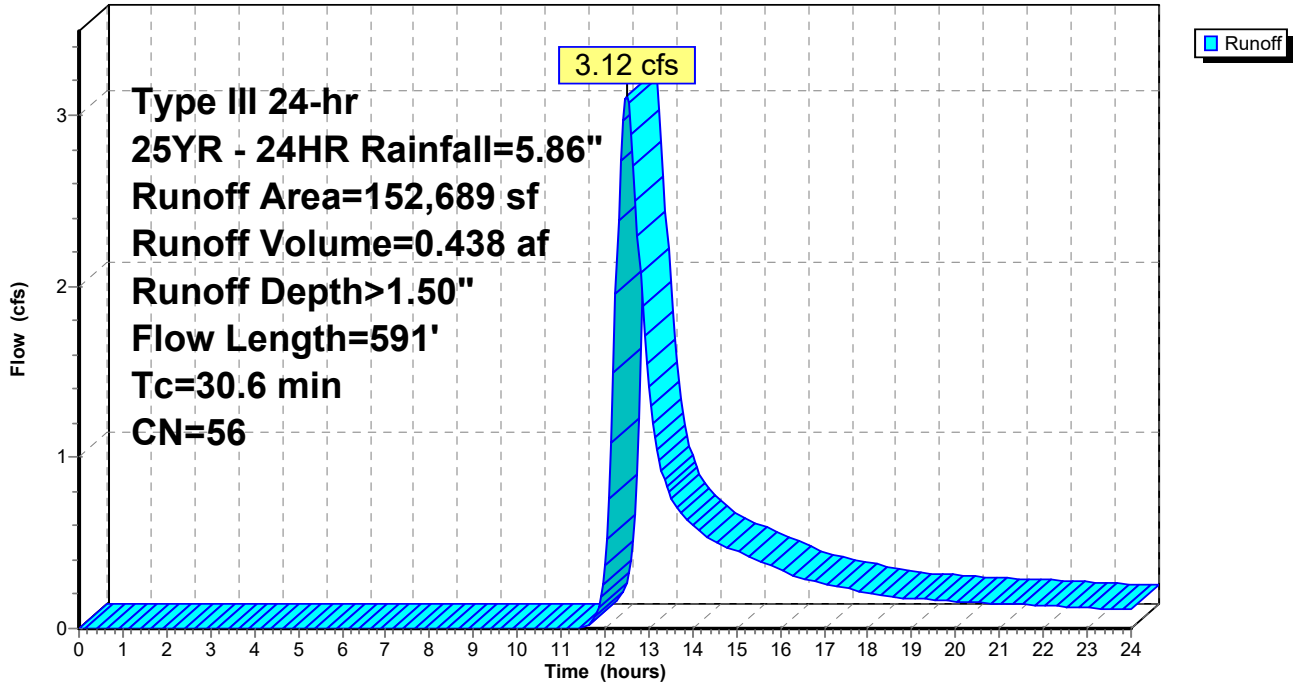
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 17S: Subcatchment #17

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 18S: Subcatchment #18

Runoff = 5.61 cfs @ 12.26 hrs, Volume= 0.595 af, Depth> 1.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
927	98	Unconnected pavement, HSG A
27,078	30	Woods, Good, HSG A
51,833	55	Woods, Good, HSG B
1,999	61	>75% Grass cover, Good, HSG B
78,276	70	Woods, Good, HSG C
6,847	74	>75% Grass cover, Good, HSG C
105	98	Unconnected pavement, HSG D
915	77	Woods, Good, HSG D
1,870	96	Gravel surface, HSG B
663	96	Gravel surface, HSG C
170,513	60	Weighted Average
169,481		99.39% Pervious Area
1,032		0.61% Impervious Area
1,032		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.6	22	0.2315	0.23		Sheet Flow, Segment #1 Grass: Dense n= 0.240 P2= 3.08"
7.3	58	0.1042	0.13		Sheet Flow, Segment #2 Woods: Light underbrush n= 0.400 P2= 3.08"
4.4	21	0.0481	0.08		Sheet Flow, Segment #3 Woods: Light underbrush n= 0.400 P2= 3.08"
1.5	92	0.0435	1.04		Shallow Concentrated Flow, Segment #4 Woodland Kv= 5.0 fps
0.8	91	0.1422	1.89		Shallow Concentrated Flow, Segment #5 Woodland Kv= 5.0 fps
1.5	92	0.0436	1.04		Shallow Concentrated Flow, Segment #6 Woodland Kv= 5.0 fps
17.1	376	Total			

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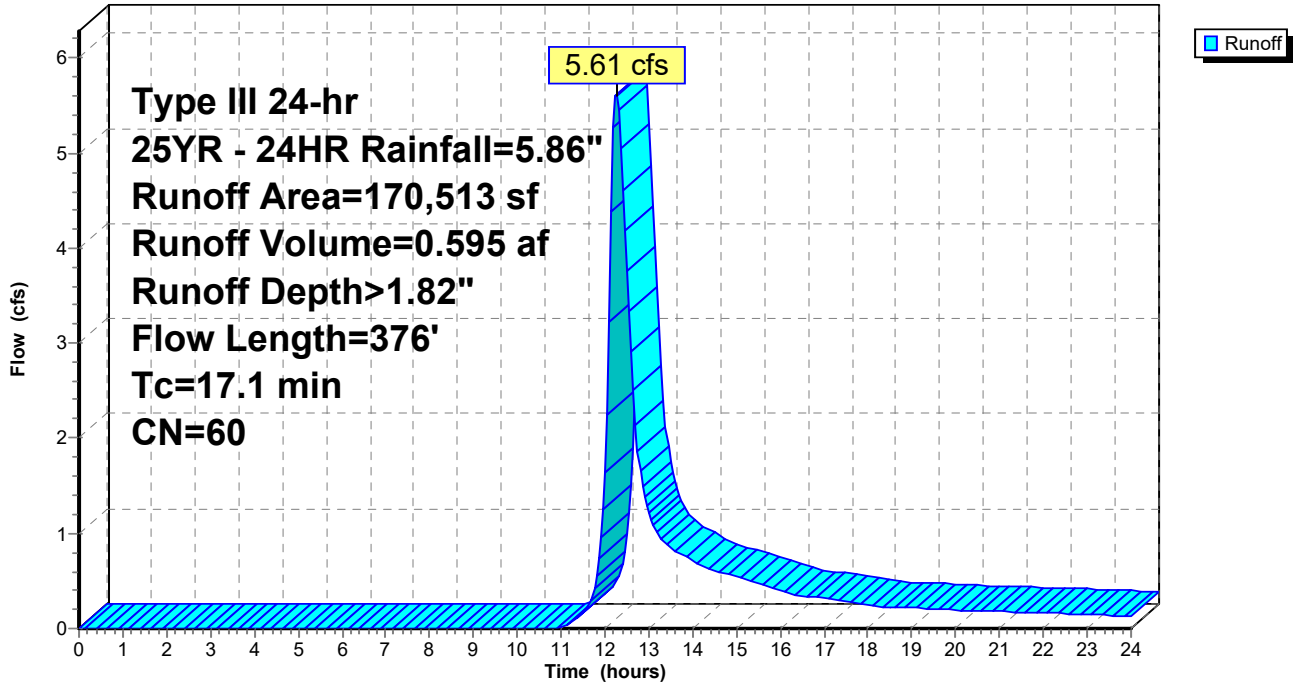
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 18S: Subcatchment #18

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 19S: Subcatchment #19

Runoff = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af, Depth> 1.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
277,033	30	Woods, Good, HSG A
113,562	55	Woods, Good, HSG B
56,177	70	Woods, Good, HSG C
3,490	74	>75% Grass cover, Good, HSG C
240,560	77	Woods, Good, HSG D
690,822	54	Weighted Average
690,822		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.6	100	0.0400	0.10		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
6.0	653	0.1333	1.83		Shallow Concentrated Flow, Segment #2 Woodland Kv= 5.0 fps
1.5	167	0.1346	1.83		Shallow Concentrated Flow, Segment #3 Woodland Kv= 5.0 fps
7.7	327	0.0199	0.71		Shallow Concentrated Flow, Segment #4 Woodland Kv= 5.0 fps
2.4	161	0.0496	1.11		Shallow Concentrated Flow, Segment #5 Woodland Kv= 5.0 fps
0.5	59	0.1530	1.96		Shallow Concentrated Flow, Segment #6 Woodland Kv= 5.0 fps
6.3	193	0.0104	0.51		Shallow Concentrated Flow, Segment #7 Woodland Kv= 5.0 fps
5.3	172	0.0116	0.54		Shallow Concentrated Flow, Segment #8 Woodland Kv= 5.0 fps
46.3	1,832	Total			

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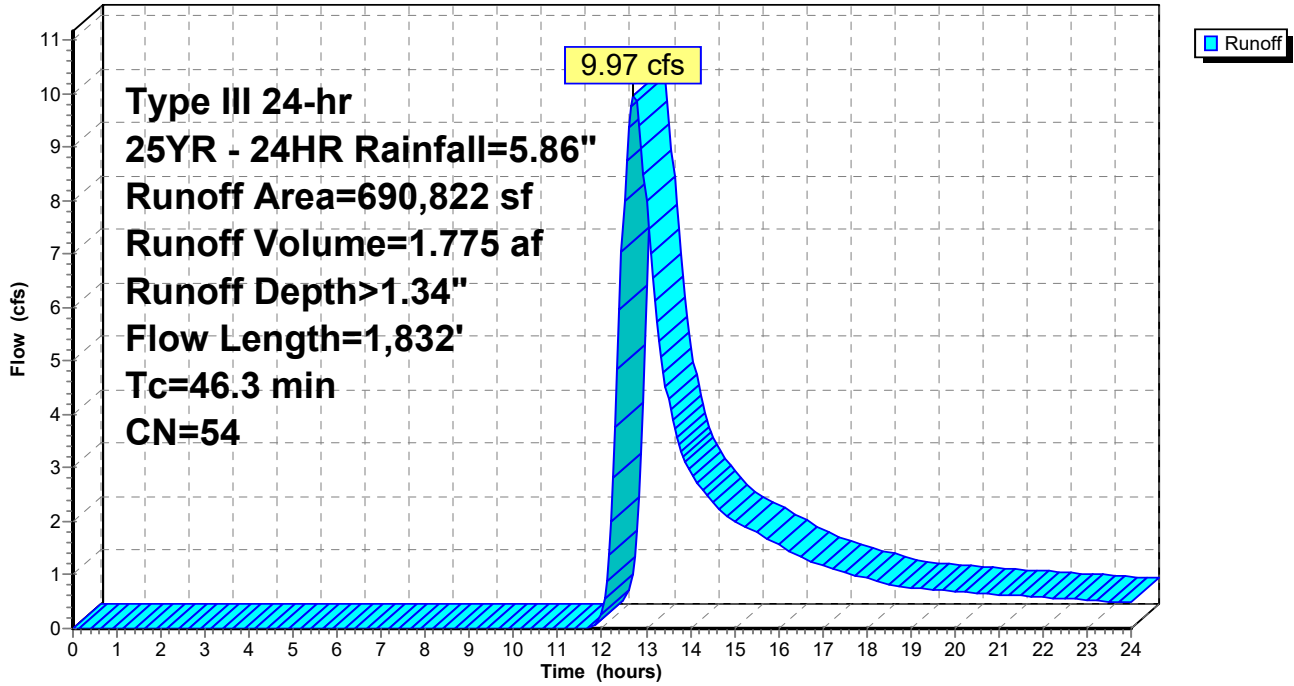
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 19S: Subcatchment #19

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 31S: CB #31

Runoff = 0.72 cfs @ 12.09 hrs, Volume= 0.053 af, Depth> 4.06"

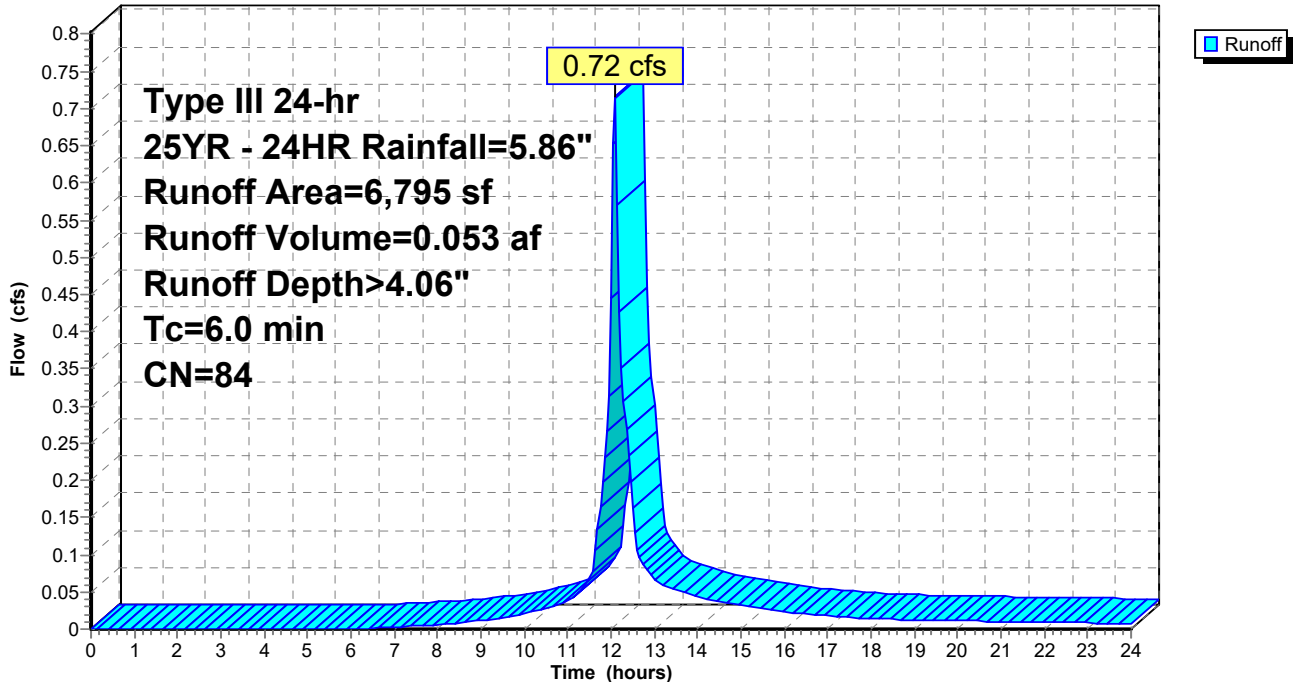
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
2,581	61	>75% Grass cover, Good, HSG B
3,654	98	Paved parking, HSG B
365	96	Gravel surface, HSG B
59	74	>75% Grass cover, Good, HSG C
136	98	Paved parking, HSG C
6,795	84	Weighted Average
3,005		44.22% Pervious Area
3,790		55.78% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 31S: CB #31

Hydrograph



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Summary for Subcatchment 32S: CB #32

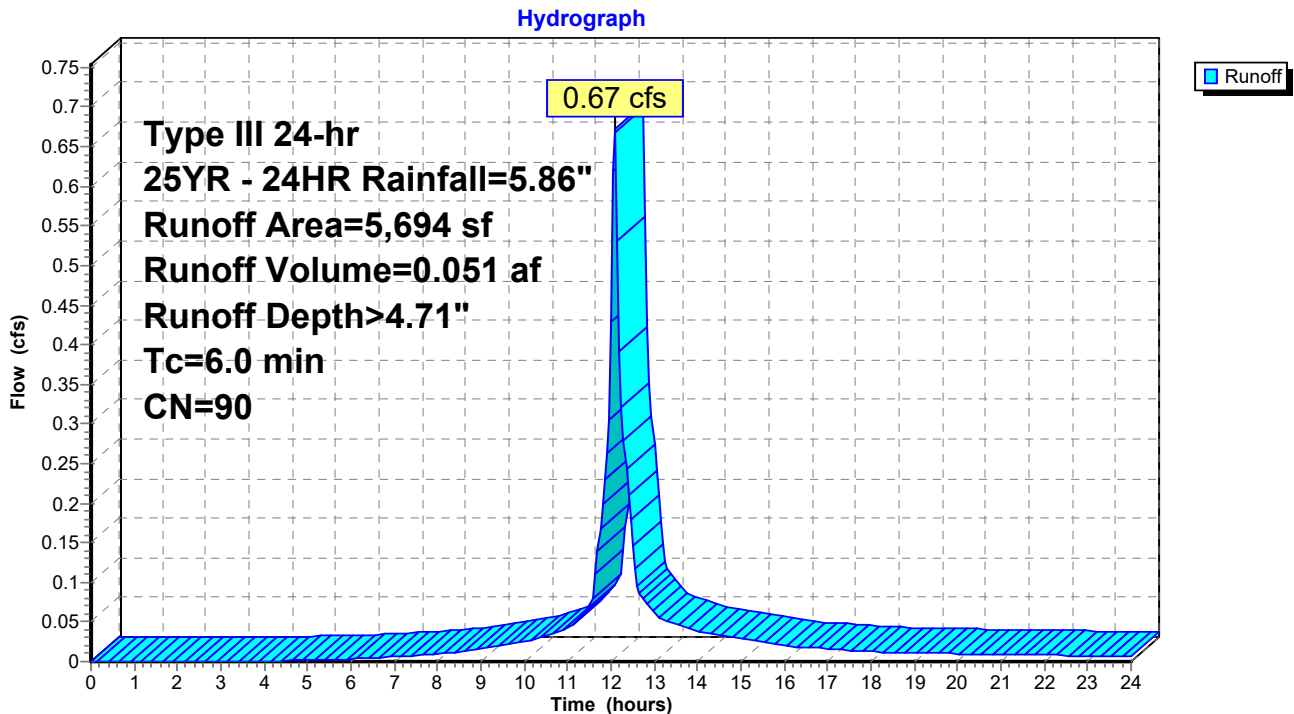
Runoff = 0.67 cfs @ 12.09 hrs, Volume= 0.051 af, Depth> 4.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
1,098	61	>75% Grass cover, Good, HSG B
4,238	98	Paved parking, HSG B
93	74	>75% Grass cover, Good, HSG C
265	98	Paved parking, HSG C
5,694	90	Weighted Average
1,191		20.92% Pervious Area
4,503		79.08% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 32S: CB #32



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 33S: CB #33

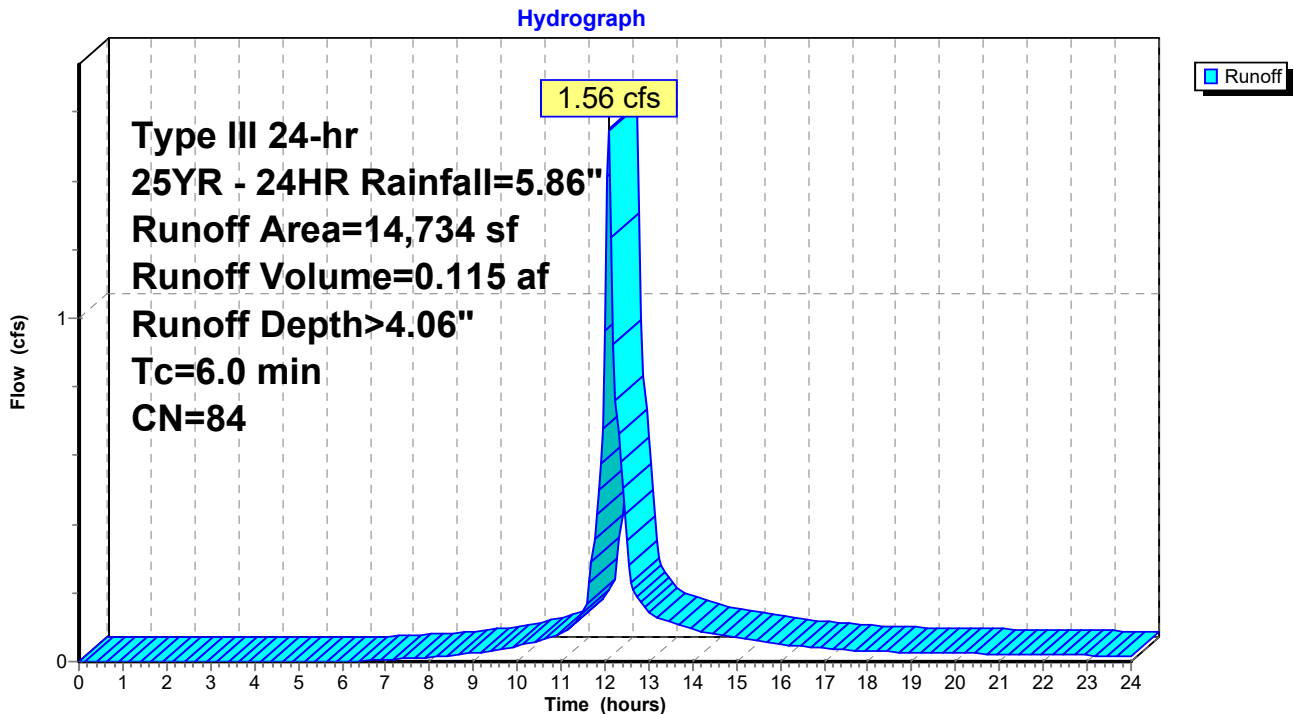
Runoff = 1.56 cfs @ 12.09 hrs, Volume= 0.115 af, Depth> 4.06"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
5,769	61	>75% Grass cover, Good, HSG B
8,008	98	Paved parking, HSG B
957	98	Unconnected roofs, HSG B
14,734	84	Weighted Average
5,769		39.15% Pervious Area
8,965		60.85% Impervious Area
957		10.67% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 33S: CB #33



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 34S: CB #34

Runoff = 0.66 cfs @ 12.09 hrs, Volume= 0.056 af, Depth> 5.62"

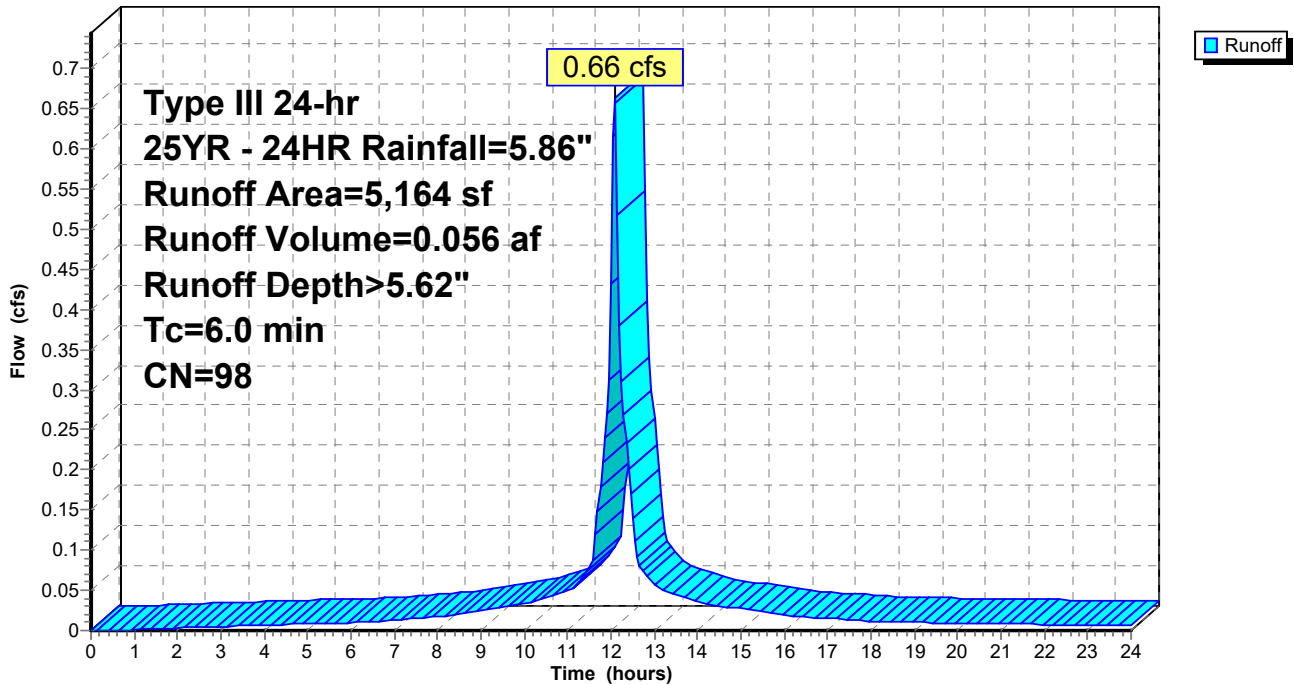
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
2,125	98	Unconnected roofs, HSG B
3,039	98	Paved parking, HSG B
5,164	98	Weighted Average
5,164		100.00% Impervious Area
2,125		41.15% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 34S: CB #34

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 35S: CB #35

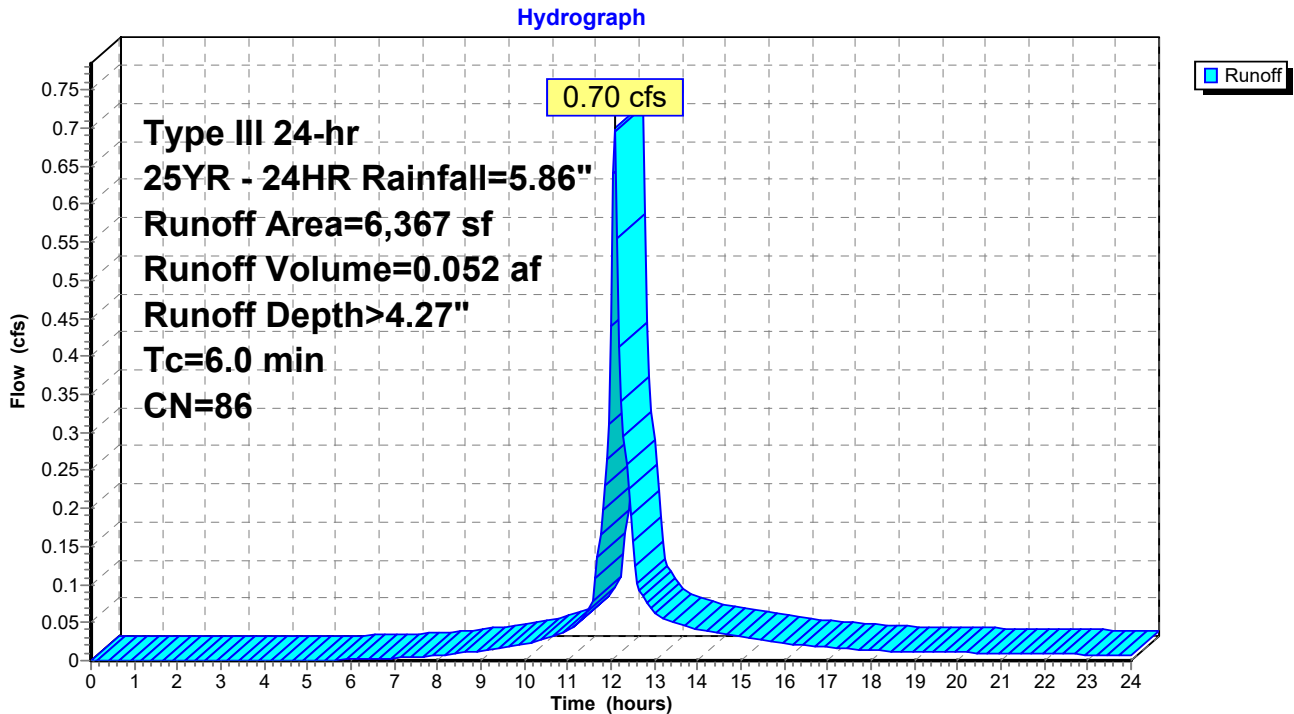
Runoff = 0.70 cfs @ 12.09 hrs, Volume= 0.052 af, Depth> 4.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
2,013	61	>75% Grass cover, Good, HSG B
3,871	98	Paved parking, HSG B
29	74	>75% Grass cover, Good, HSG C
299	98	Paved parking, HSG C
155	98	Unconnected roofs, HSG C
6,367	86	Weighted Average
2,042		32.07% Pervious Area
4,325		67.93% Impervious Area
155		3.58% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 35S: CB #35



20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 36S: CB #36

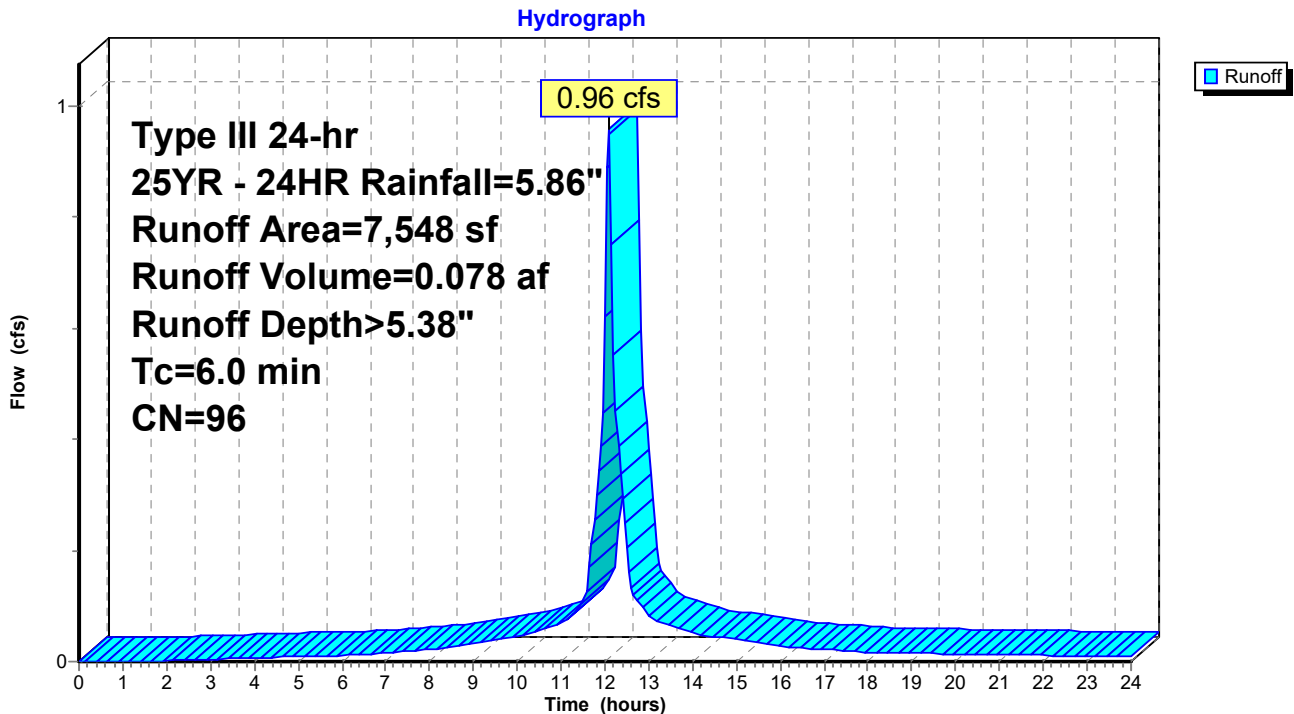
Runoff = 0.96 cfs @ 12.09 hrs, Volume= 0.078 af, Depth> 5.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
508	61	>75% Grass cover, Good, HSG B
4,423	98	Paved parking, HSG B
2,617	98	Unconnected roofs, HSG B
7,548	96	Weighted Average
508		6.73% Pervious Area
7,040		93.27% Impervious Area
2,617		37.17% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 36S: CB #36



20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 37S: CB #37

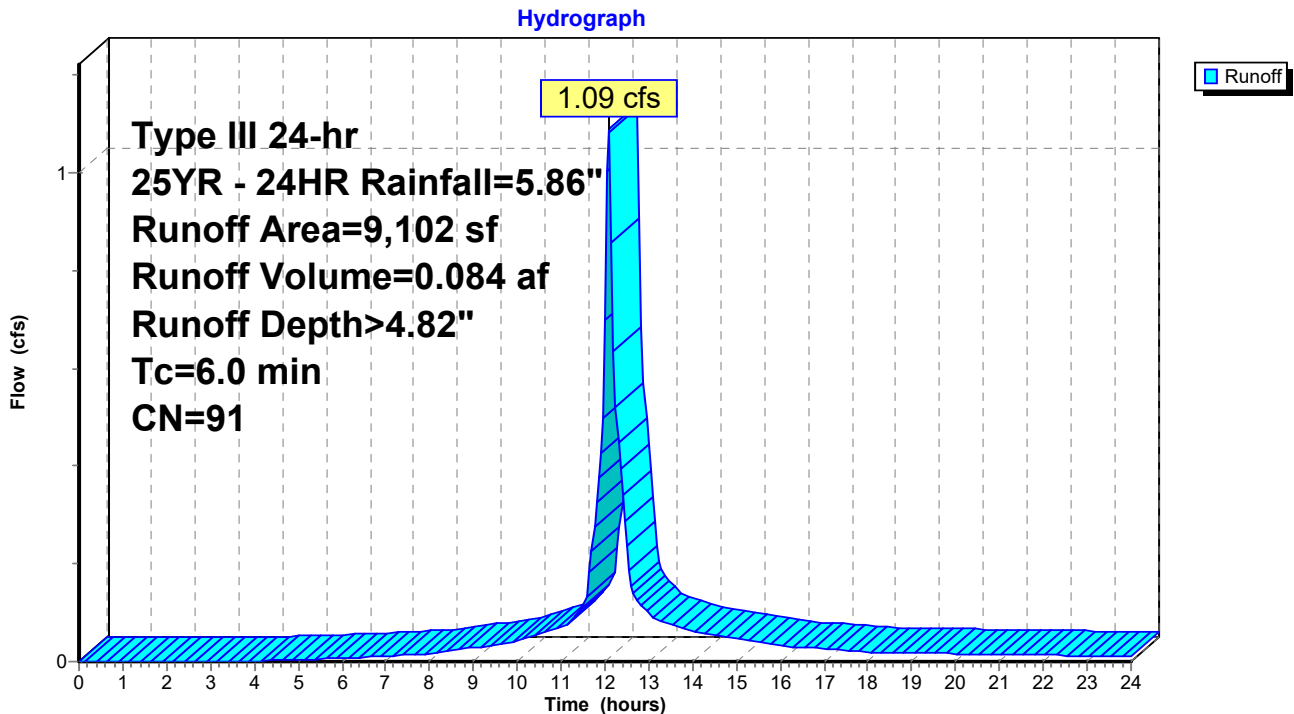
Runoff = 1.09 cfs @ 12.09 hrs, Volume= 0.084 af, Depth> 4.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
1,765	61	>75% Grass cover, Good, HSG B
4,702	98	Paved parking, HSG B
2,635	98	Unconnected roofs, HSG B
9,102	91	Weighted Average
1,765		19.39% Pervious Area
7,337		80.61% Impervious Area
2,635		35.91% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 37S: CB #37



20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 38S: CB #38

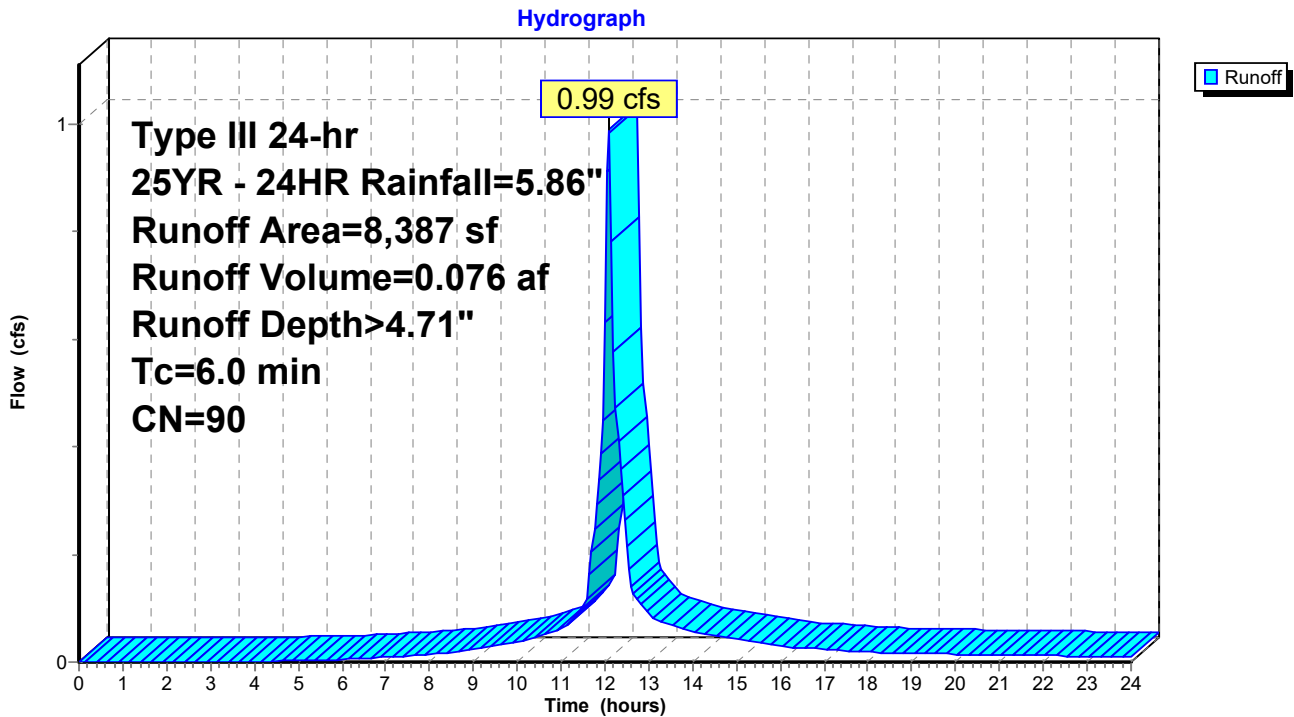
Runoff = 0.99 cfs @ 12.09 hrs, Volume= 0.076 af, Depth> 4.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
1,880	61	>75% Grass cover, Good, HSG B
3,863	98	Paved parking, HSG B
2,644	98	Paved parking, HSG C
8,387	90	Weighted Average
1,880		22.42% Pervious Area
6,507		77.58% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 38S: CB #38



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 39S: CB #39

Runoff = 0.83 cfs @ 12.09 hrs, Volume= 0.060 af, Depth> 3.35"

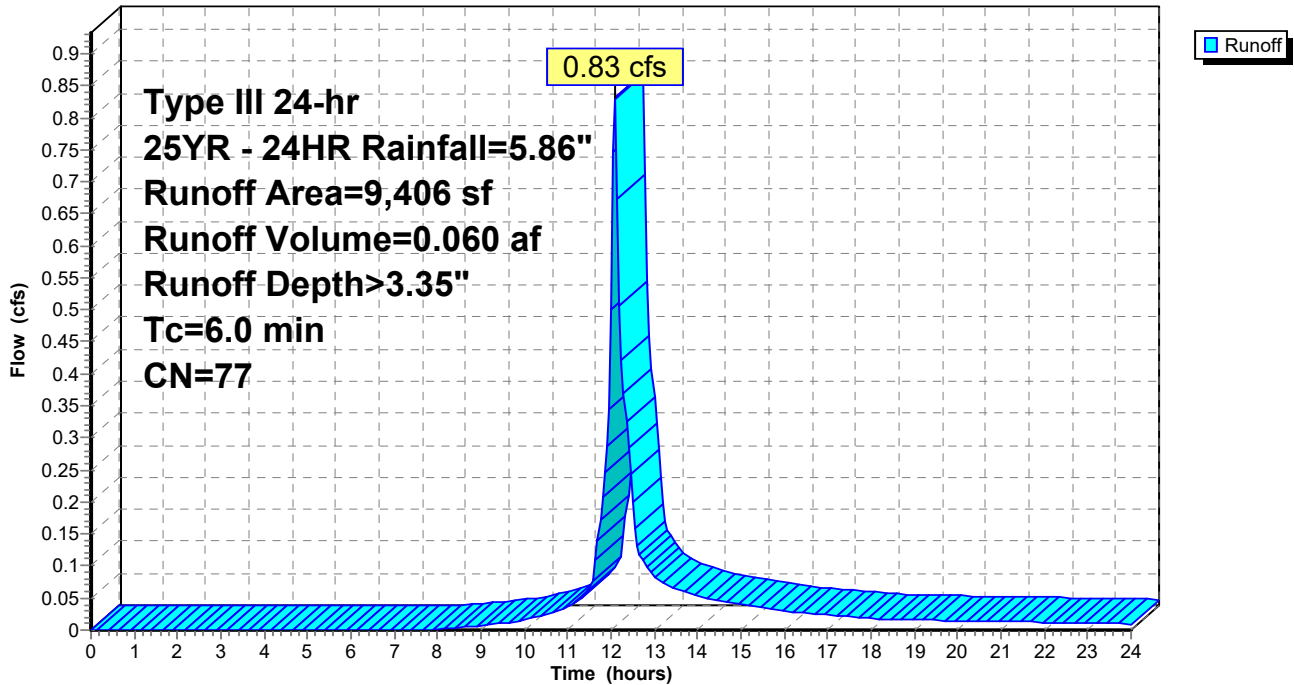
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
4,584	61	>75% Grass cover, Good, HSG B
3,645	98	Paved parking, HSG B
1,177	74	>75% Grass cover, Good, HSG C
9,406	77	Weighted Average
5,761		61.25% Pervious Area
3,645		38.75% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 39S: CB #39

Hydrograph



20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 40S: CB #40

Runoff = 0.41 cfs @ 12.09 hrs, Volume= 0.034 af, Depth> 5.62"

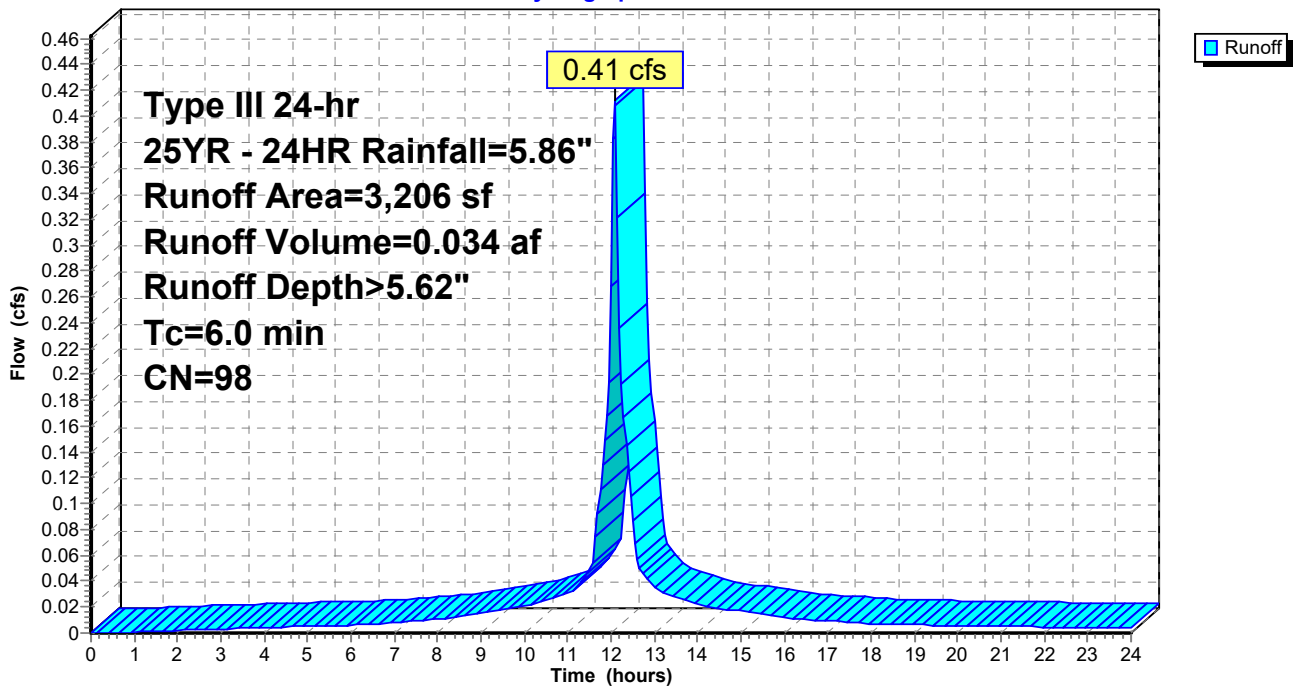
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
2,301	98	Paved parking, HSG B
905	98	Paved parking, HSG C
3,206	98	Weighted Average
3,206		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 40S: CB #40

Hydrograph



20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 41S: CB #41

Runoff = 0.46 cfs @ 12.09 hrs, Volume= 0.036 af, Depth> 5.15"

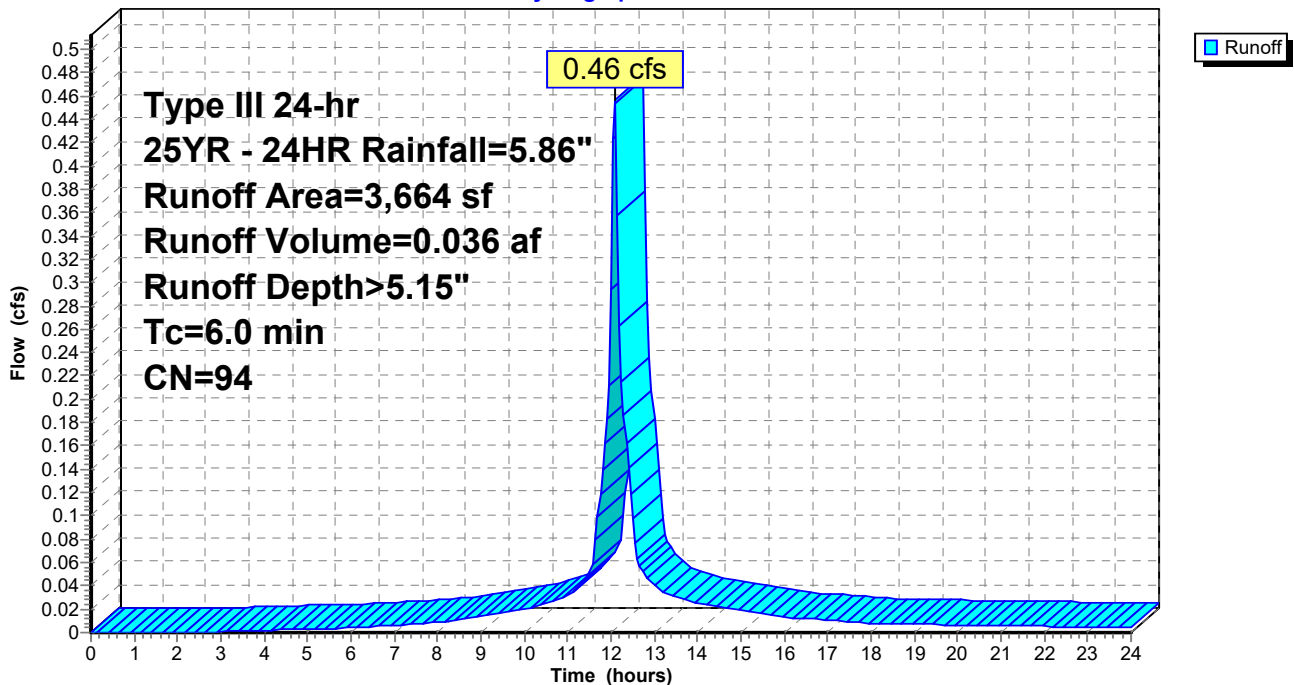
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
314	61	>75% Grass cover, Good, HSG B
1,969	98	Paved parking, HSG B
136	74	>75% Grass cover, Good, HSG C
1,245	98	Paved parking, HSG C
3,664	94	Weighted Average
450		12.28% Pervious Area
3,214		87.72% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 41S: CB #41

Hydrograph



20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 42S: CB #42

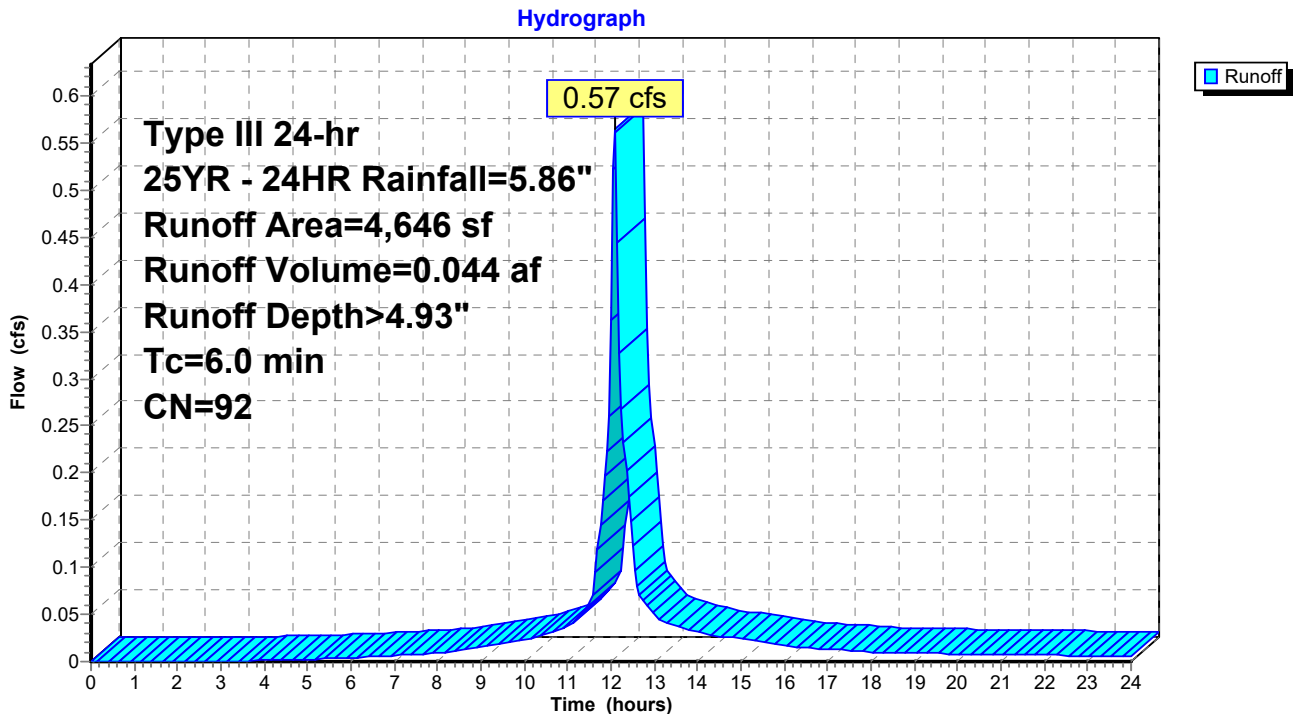
Runoff = 0.57 cfs @ 12.09 hrs, Volume= 0.044 af, Depth> 4.93"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
647	61	>75% Grass cover, Good, HSG B
3,009	98	Paved parking, HSG B
216	74	>75% Grass cover, Good, HSG C
774	98	Paved parking, HSG C
4,646	92	Weighted Average
863		18.58% Pervious Area
3,783		81.42% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 42S: CB #42



20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 43S: CB #43

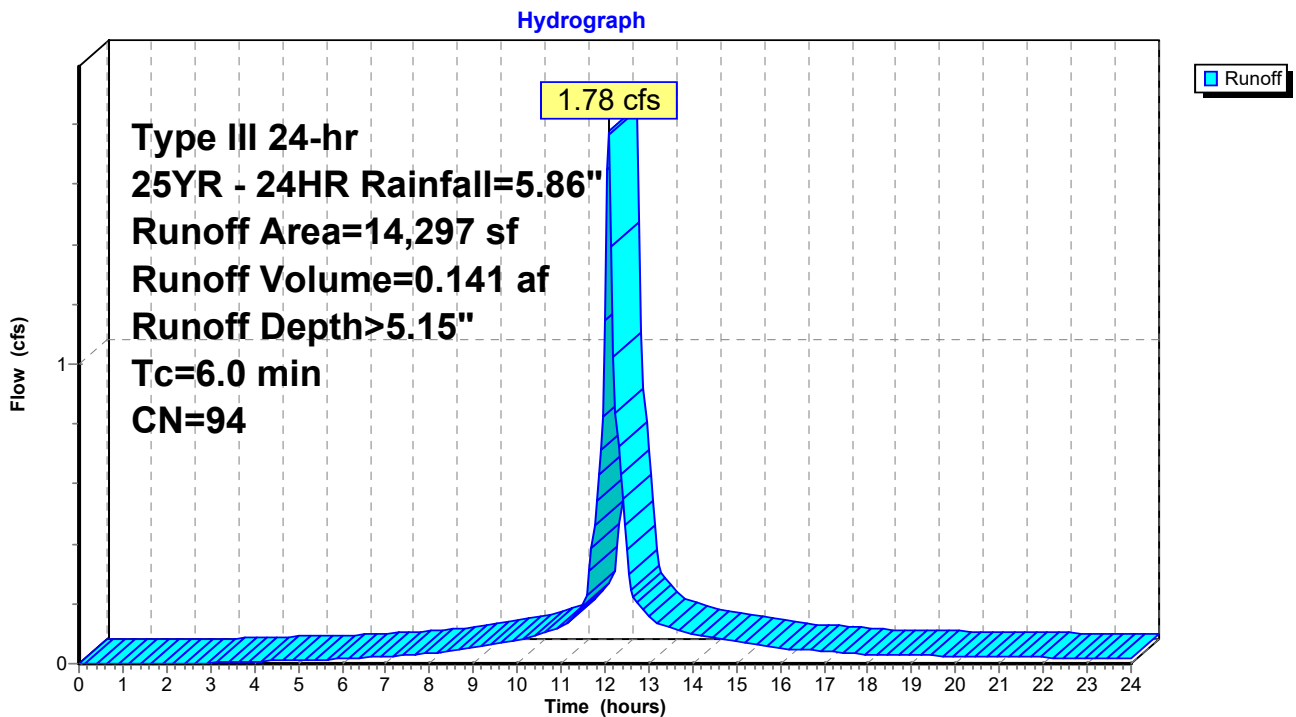
Runoff = 1.78 cfs @ 12.09 hrs, Volume= 0.141 af, Depth> 5.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
8,901	98	Paved parking, HSG B
2,731	98	Unconnected roofs, HSG B
924	61	>75% Grass cover, Good, HSG B
16	96	Gravel surface, HSG B
779	74	>75% Grass cover, Good, HSG C
800	98	Unconnected roofs, HSG C
146	98	Paved parking, HSG C
14,297	94	Weighted Average
1,719		12.02% Pervious Area
12,578		87.98% Impervious Area
3,531		28.07% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 43S: CB #43



20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 44S: CB #44

Runoff = 1.87 cfs @ 12.21 hrs, Volume= 0.174 af, Depth> 2.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
4,678	30	Woods, Good, HSG A
4,678	77	Woods, Good, HSG D
9,377	61	>75% Grass cover, Good, HSG B
2,556	98	Roofs, HSG B
9,144	98	Paved parking, HSG B
335	96	Gravel surface, HSG B
30,768	73	Weighted Average
19,068		61.97% Pervious Area
11,700		38.03% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.0	100	0.0900	0.14		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
0.9	88	0.0969	1.56		Shallow Concentrated Flow, Segment #2 Woodland Kv= 5.0 fps
0.7	66	0.0534	1.62		Shallow Concentrated Flow, Segment #3 Short Grass Pasture Kv= 7.0 fps
0.1	16	0.3125	3.91		Shallow Concentrated Flow, Segment #4 Short Grass Pasture Kv= 7.0 fps
0.9	223	0.0449	4.30		Shallow Concentrated Flow, Segment #5 Paved Kv= 20.3 fps
14.6	493	Total			

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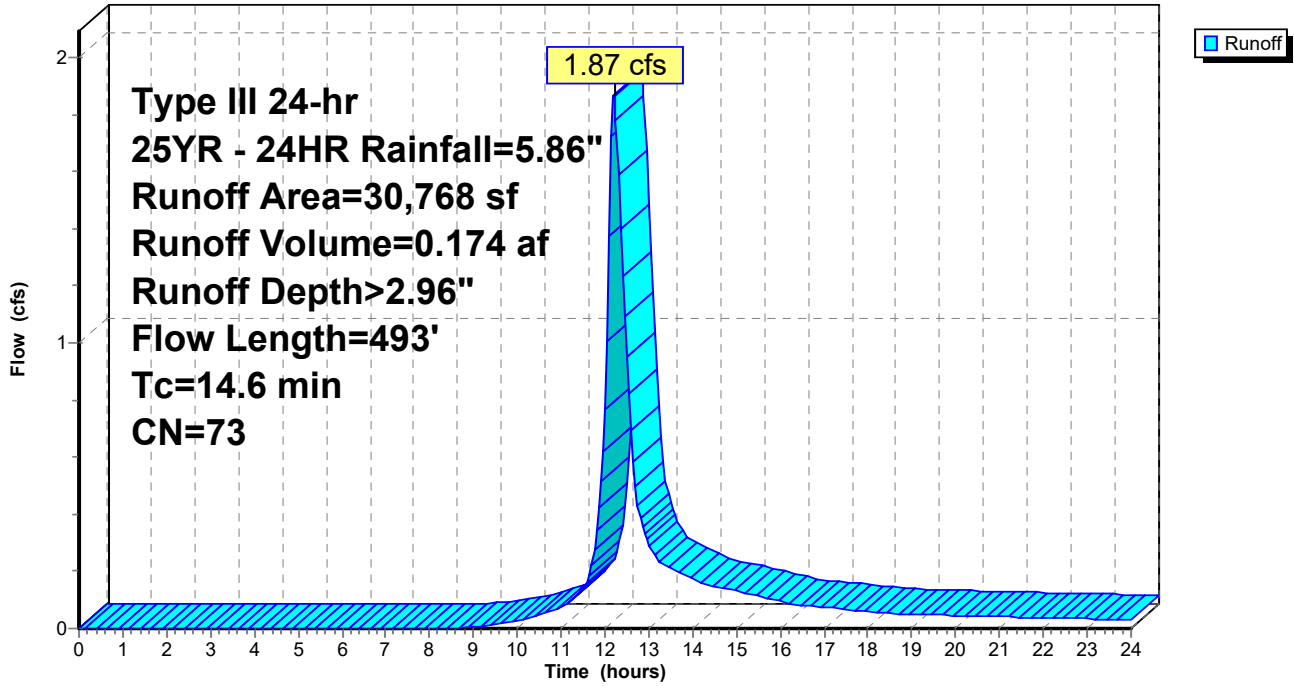
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 44S: CB #44

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 45S: CB #45

Runoff = 1.77 cfs @ 12.15 hrs, Volume= 0.149 af, Depth> 2.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Adj	Description
16,329	61		>75% Grass cover, Good, HSG B
4,696	98		Unconnected roofs, HSG B
8,408	74		>75% Grass cover, Good, HSG C
1,050	98		Unconnected roofs, HSG C
243	30		Woods, Good, HSG A
243	77		Woods, Good, HSG D
30,969	71	68	Weighted Average, UI Adjusted
25,223			81.45% Pervious Area
5,746			18.55% Impervious Area
5,746			100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.2	35	0.0567	0.09		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
2.5	45	0.1348	0.31		Sheet Flow, Segment #2 Grass: Short n= 0.150 P2= 3.08"
1.1	135	0.0815	2.00		Shallow Concentrated Flow, Segment #3 Short Grass Pasture Kv= 7.0 fps
0.1	27	0.2593	3.56		Shallow Concentrated Flow, Segment #4 Short Grass Pasture Kv= 7.0 fps
0.5	23	0.0108	0.73		Shallow Concentrated Flow, Segment #5 Short Grass Pasture Kv= 7.0 fps
10.4	265	Total			

20-097 Proposed Analysis

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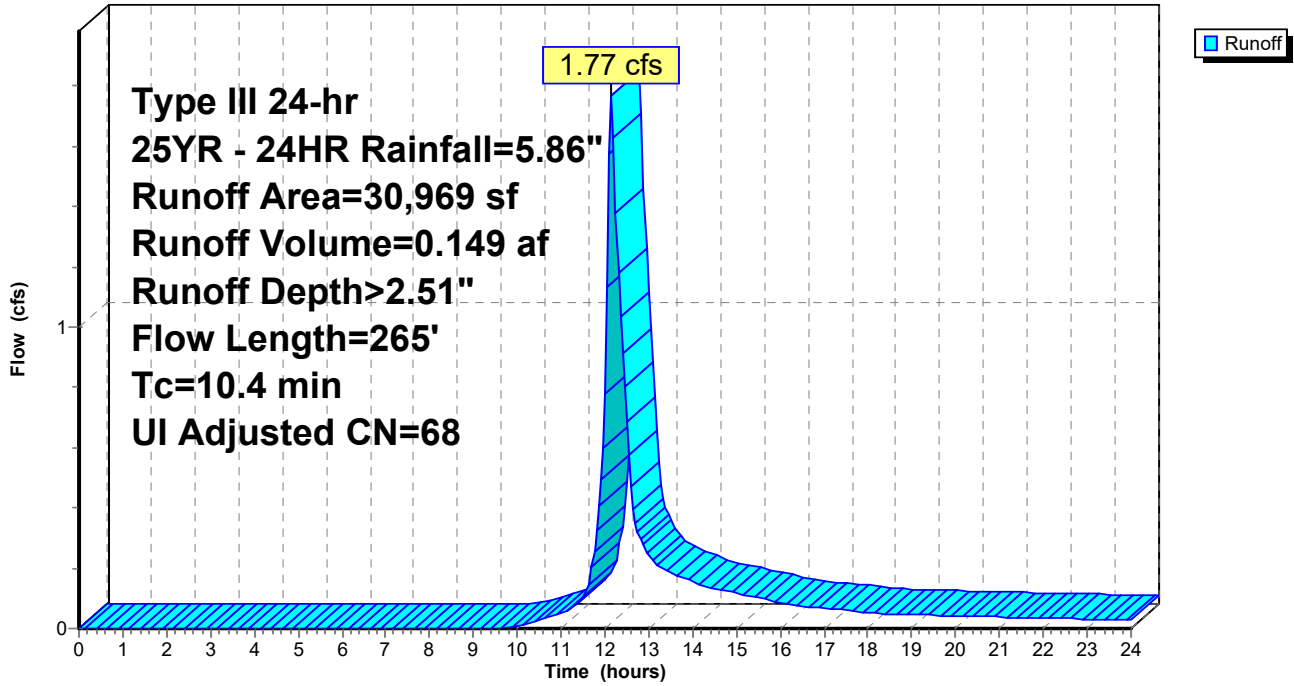
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 45S: CB #45

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 46S: CB #46

Runoff = 0.93 cfs @ 12.09 hrs, Volume= 0.077 af, Depth> 5.62"

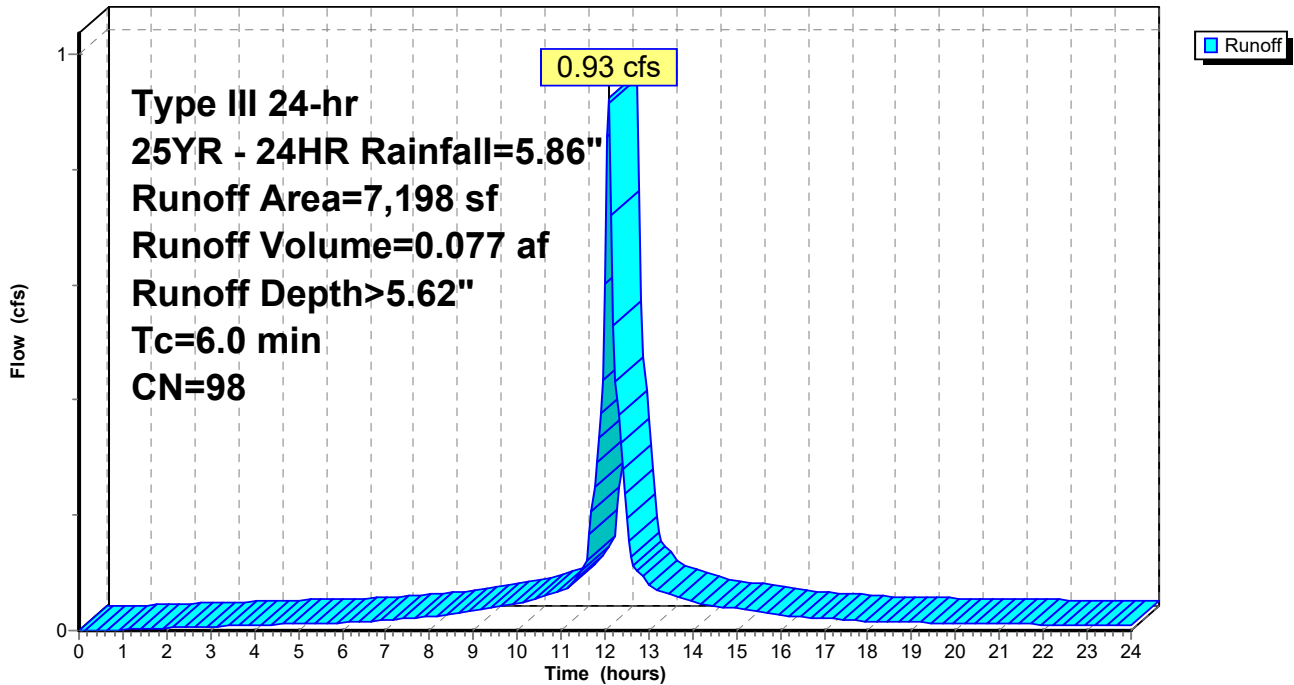
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
5,291	98	Paved parking, HSG B
1,907	98	Unconnected roofs, HSG B
7,198	98	Weighted Average
7,198		100.00% Impervious Area
1,907		26.49% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 46S: CB #46

Hydrograph



20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 47S: Inlet Sump High Pt Dr

Runoff = 1.95 cfs @ 12.42 hrs, Volume= 0.261 af, Depth> 1.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Adj	Description
9,625	61		>75% Grass cover, Good, HSG B
2,882	98		Unconnected roofs, HSG B
346	96		Gravel surface, HSG B
41,347	30		Woods, Good, HSG A
41,347	77		Woods, Good, HSG D
95,547	56	55	Weighted Average, UI Adjusted
92,665			96.98% Pervious Area
2,882			3.02% Impervious Area
2,882			100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
18.6	100	0.0300	0.09		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
6.7	665	0.1090	1.65		Shallow Concentrated Flow, Segment #2 Woodland Kv= 5.0 fps
0.9	97	0.1310	1.81		Shallow Concentrated Flow, Segment #3 Woodland Kv= 5.0 fps
26.2	862	Total			

20-097 Proposed Analysis

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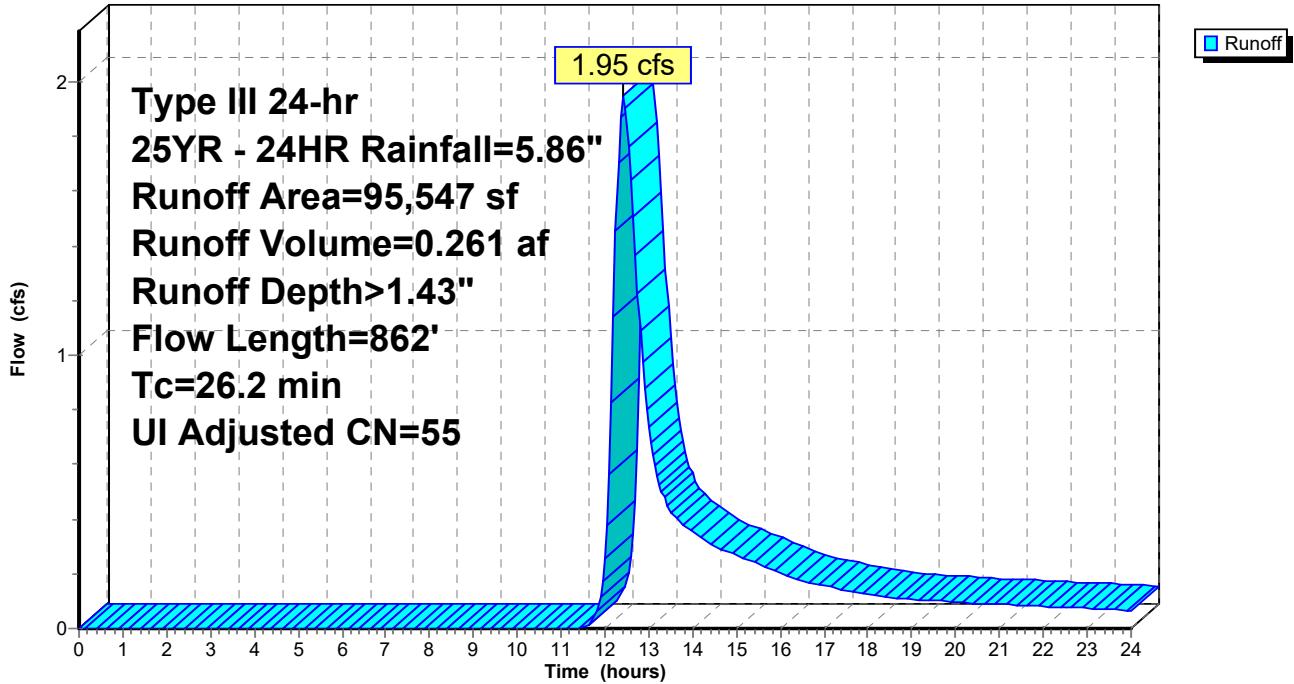
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 47S: Inlet Sump High Pt Dr

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 48S: High Pt Dr Cul-De-Sac

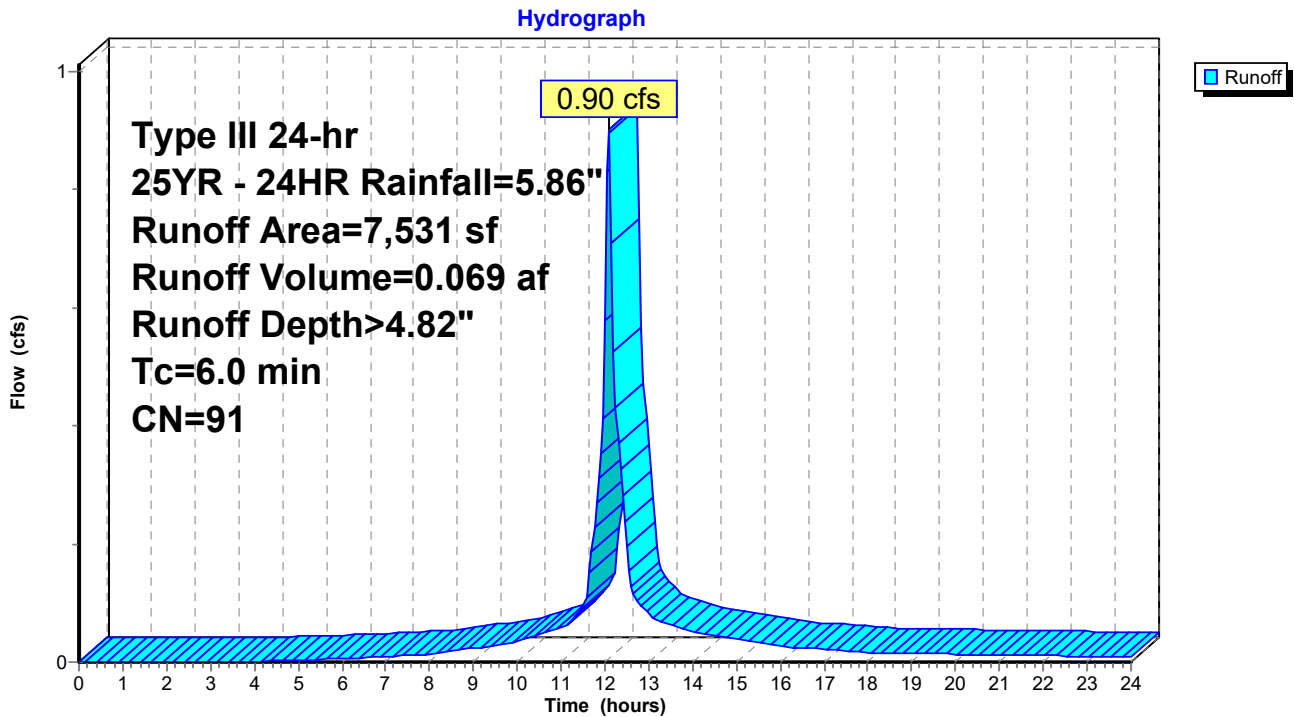
Runoff = 0.90 cfs @ 12.09 hrs, Volume= 0.069 af, Depth> 4.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
1,385	61	>75% Grass cover, Good, HSG B
5,869	98	Paved parking, HSG B
277	96	Gravel surface, HSG B
7,531	91	Weighted Average
1,662		22.07% Pervious Area
5,869		77.93% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 48S: High Pt Dr Cul-De-Sac



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 49S: Community Dr Cul-De-Sac

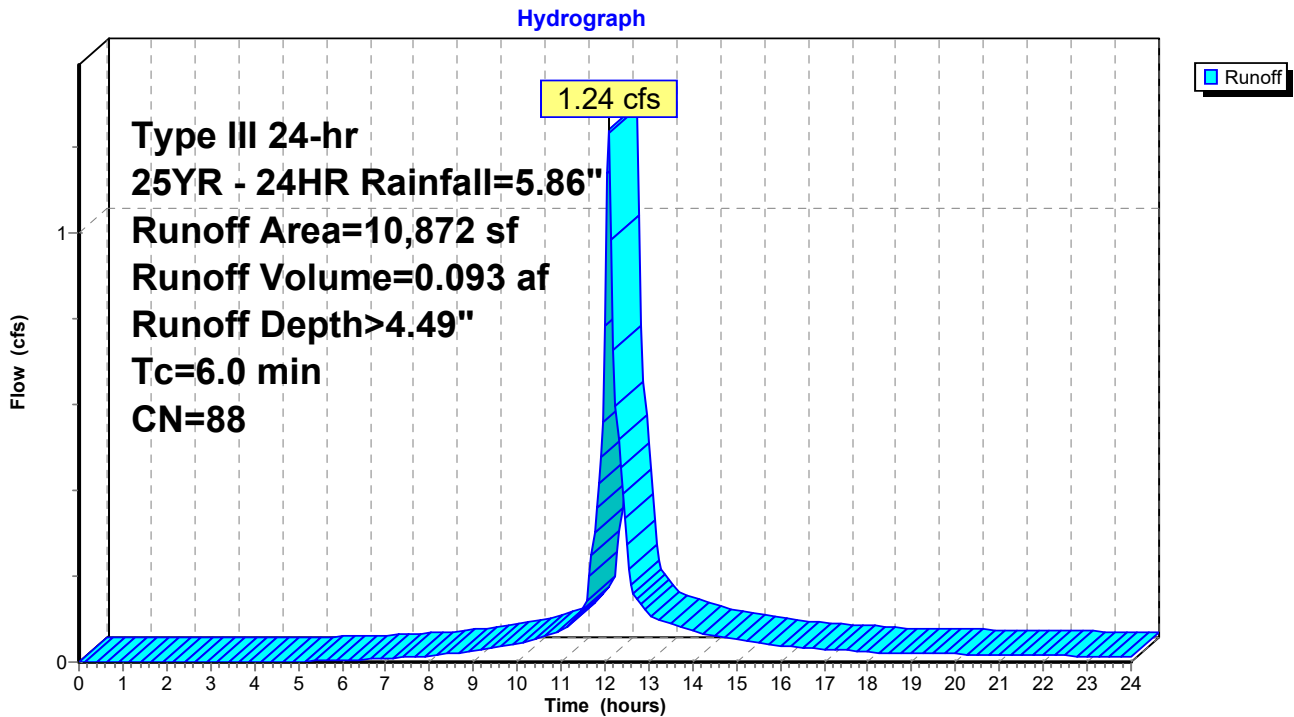
Runoff = 1.24 cfs @ 12.09 hrs, Volume= 0.093 af, Depth> 4.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
2,892	61	>75% Grass cover, Good, HSG B
7,590	98	Paved parking, HSG B
390	96	Gravel surface, HSG B
10,872	88	Weighted Average
3,282		30.19% Pervious Area
7,590		69.81% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 49S: Community Dr Cul-De-Sac



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 50S: Subcatchment #50

Runoff = 0.52 cfs @ 12.25 hrs, Volume= 0.057 af, Depth> 1.43"

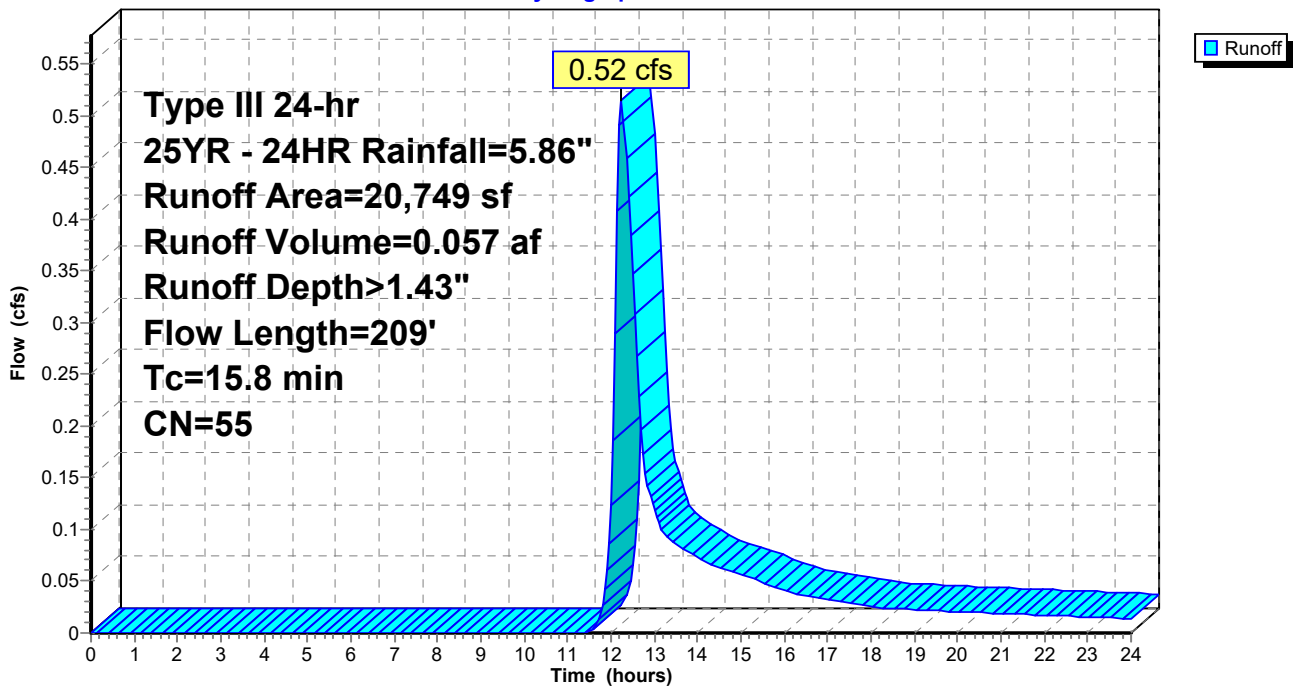
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
1,989	39	>75% Grass cover, Good, HSG A
5,470	30	Woods, Good, HSG A
7,739	61	>75% Grass cover, Good, HSG B
81	74	>75% Grass cover, Good, HSG C
5,470	77	Woods, Good, HSG D
20,749	55	Weighted Average
20,749		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
14.1	100	0.0600	0.12		Sheet Flow, Segment 1 Woods: Light underbrush n= 0.400 P2= 3.08"
0.4	26	0.0400	1.00		Shallow Concentrated Flow, Segment 2 Woodland Kv= 5.0 fps
1.3	83	0.0240	1.08		Shallow Concentrated Flow, Segment 3 Short Grass Pasture Kv= 7.0 fps
15.8	209	Total			

Subcatchment 50S: Subcatchment #50

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 51S: Outet Pond

Runoff = 0.14 cfs @ 12.10 hrs, Volume= 0.010 af, Depth> 1.91"

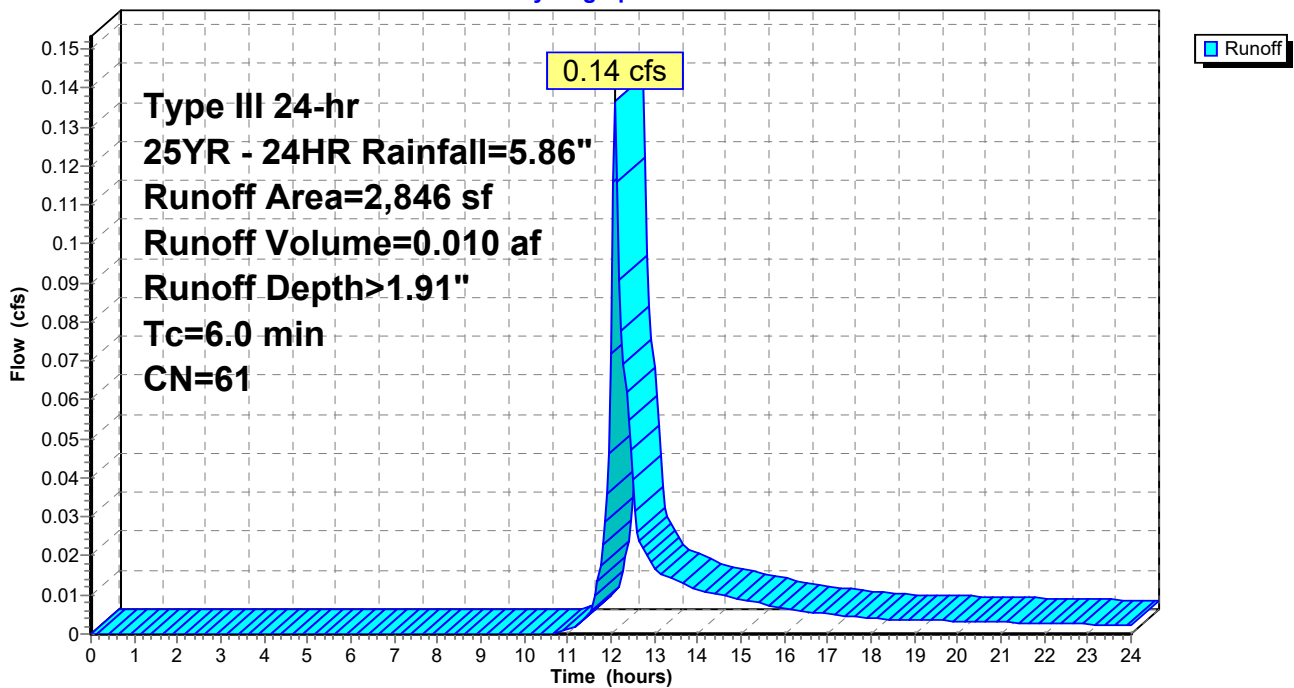
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
2,846	61	>75% Grass cover, Good, HSG B
2,846		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 51S: Outet Pond

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 52S: Southern Wetland Crossing

Runoff = 4.80 cfs @ 12.43 hrs, Volume= 0.649 af, Depth> 1.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
87,789	30	Woods, Good, HSG A
34,131	55	Woods, Good, HSG B
14,500	61	>75% Grass cover, Good, HSG B
13,554	70	Woods, Good, HSG C
87,789	77	Woods, Good, HSG D
237,763	55	Weighted Average
237,763		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
15.2	100	0.0500	0.11		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
5.0	560	0.1411	1.88		Shallow Concentrated Flow, Segment #2 Woodland Kv= 5.0 fps
1.9	194	0.0568	1.67		Shallow Concentrated Flow, Segment #3 Short Grass Pasture Kv= 7.0 fps
0.9	95	0.1365	1.85		Shallow Concentrated Flow, Segment #4 Woodland Kv= 5.0 fps
3.8	208	0.0337	0.92		Shallow Concentrated Flow, Segment #5 Woodland Kv= 5.0 fps
26.8	1,157	Total			

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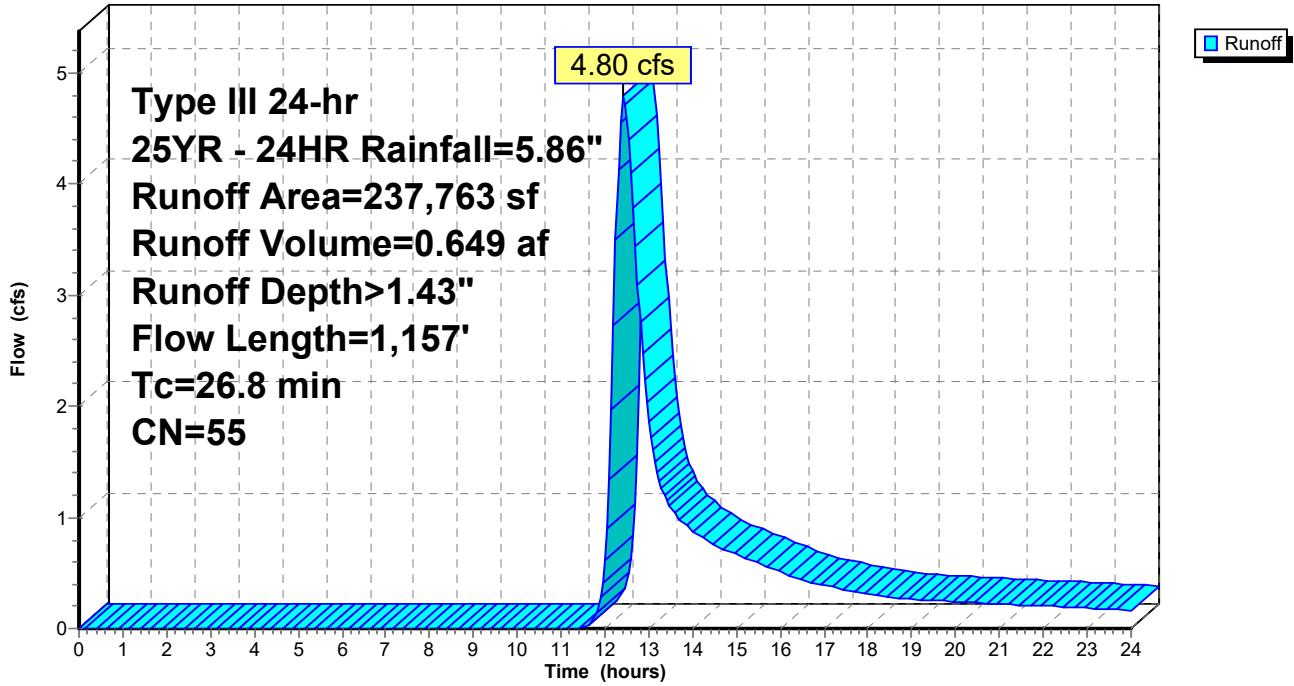
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 52S: Southern Wetland Crossing

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 53S: Northern Wetland Crossing

Runoff = 0.57 cfs @ 12.32 hrs, Volume= 0.068 af, Depth> 1.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
6,599	30	Woods, Good, HSG A
6,789	55	Woods, Good, HSG B
867	61	>75% Grass cover, Good, HSG B
2,734	70	Woods, Good, HSG C
6,599	77	Woods, Good, HSG D
23,588	56	Weighted Average
23,588		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.8	100	0.0390	0.10		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
0.9	150	0.2809	2.65		Shallow Concentrated Flow, Segment #2 Woodland Kv= 5.0 fps
1.1	145	0.2042	2.26		Shallow Concentrated Flow, Segment #3 Woodland Kv= 5.0 fps
1.8	102	0.0342	0.92		Shallow Concentrated Flow, Segment #4 Woodland Kv= 5.0 fps
20.6	497	Total			

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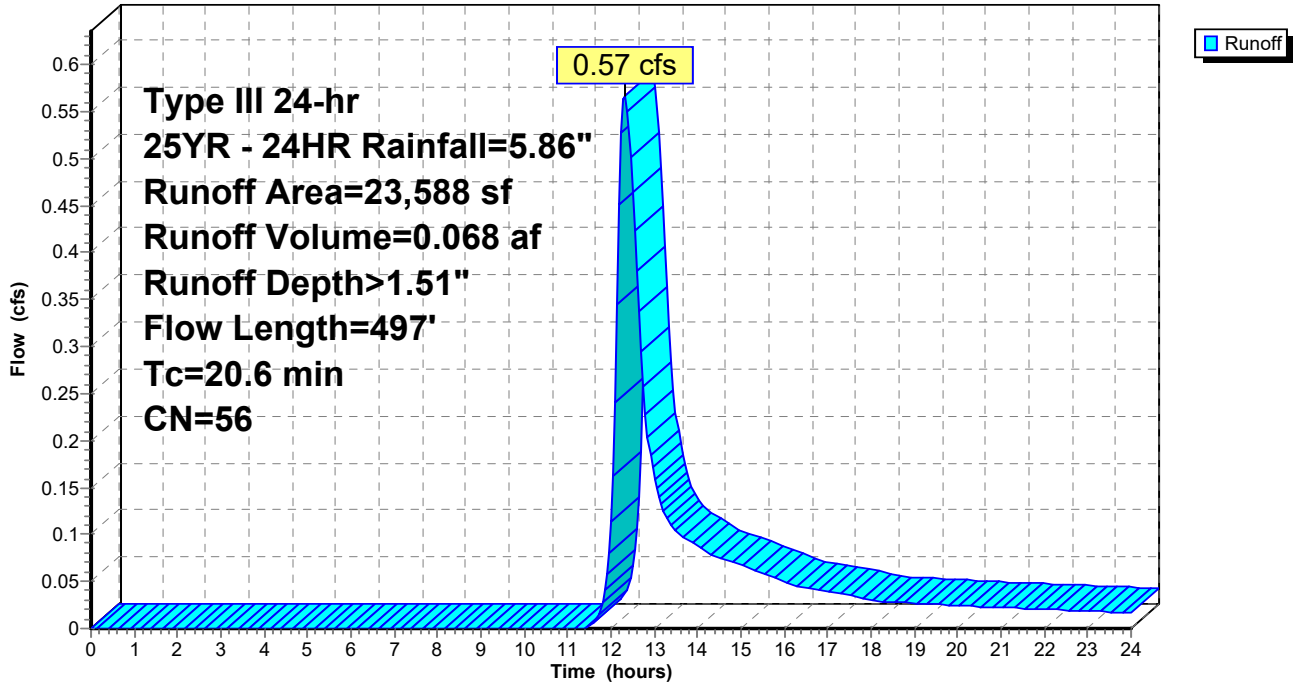
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 53S: Northern Wetland Crossing

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 54S: Subcatchment #54

Runoff = 2.93 cfs @ 12.40 hrs, Volume= 0.375 af, Depth> 1.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
40,782	30	Woods, Good, HSG A
1,023	55	Woods, Good, HSG B
28,635	61	>75% Grass cover, Good, HSG B
6,082	96	Gravel surface, HSG B
40,782	77	Woods, Good, HSG D
840	98	Roofs, HSG B
118,144	58	Weighted Average
117,304		99.29% Pervious Area
840		0.71% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
15.2	100	0.0500	0.11		Sheet Flow, Segment #1 Woods: Light underbrush n= 0.400 P2= 3.08"
5.1	570	0.1388	1.86		Shallow Concentrated Flow, Segment #2 Woodland Kv= 5.0 fps
0.4	59	0.1017	2.23		Shallow Concentrated Flow, Segment #3 Short Grass Pasture Kv= 7.0 fps
5.2	430	0.0395	1.39		Shallow Concentrated Flow, Segment #4 Short Grass Pasture Kv= 7.0 fps
25.9	1,159	Total			

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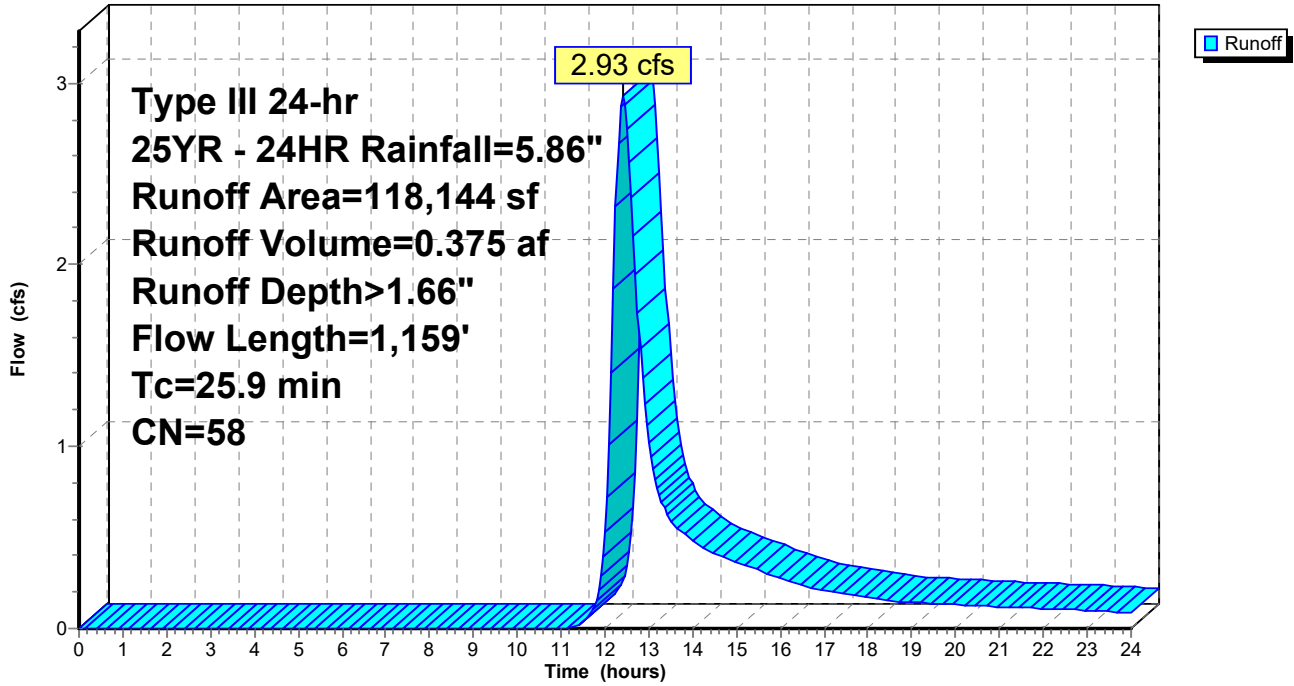
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Subcatchment 54S: Subcatchment #54

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 55S: 15" HDPE N-12

Runoff = 0.21 cfs @ 12.10 hrs, Volume= 0.016 af, Depth> 1.91"

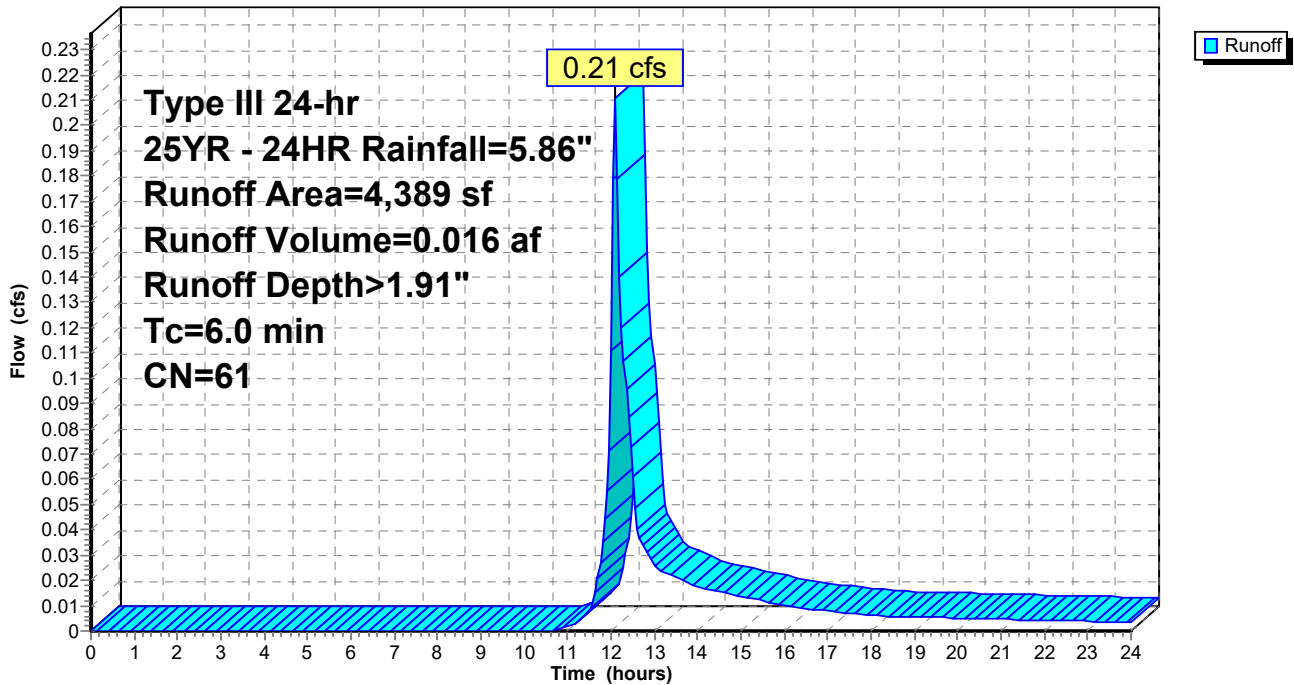
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
4,389	61	>75% Grass cover, Good, HSG B
4,389		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Segment #1

Subcatchment 55S: 15" HDPE N-12

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 63S: Gravel Wetland #103

Runoff = 0.23 cfs @ 12.10 hrs, Volume= 0.018 af, Depth> 1.91"

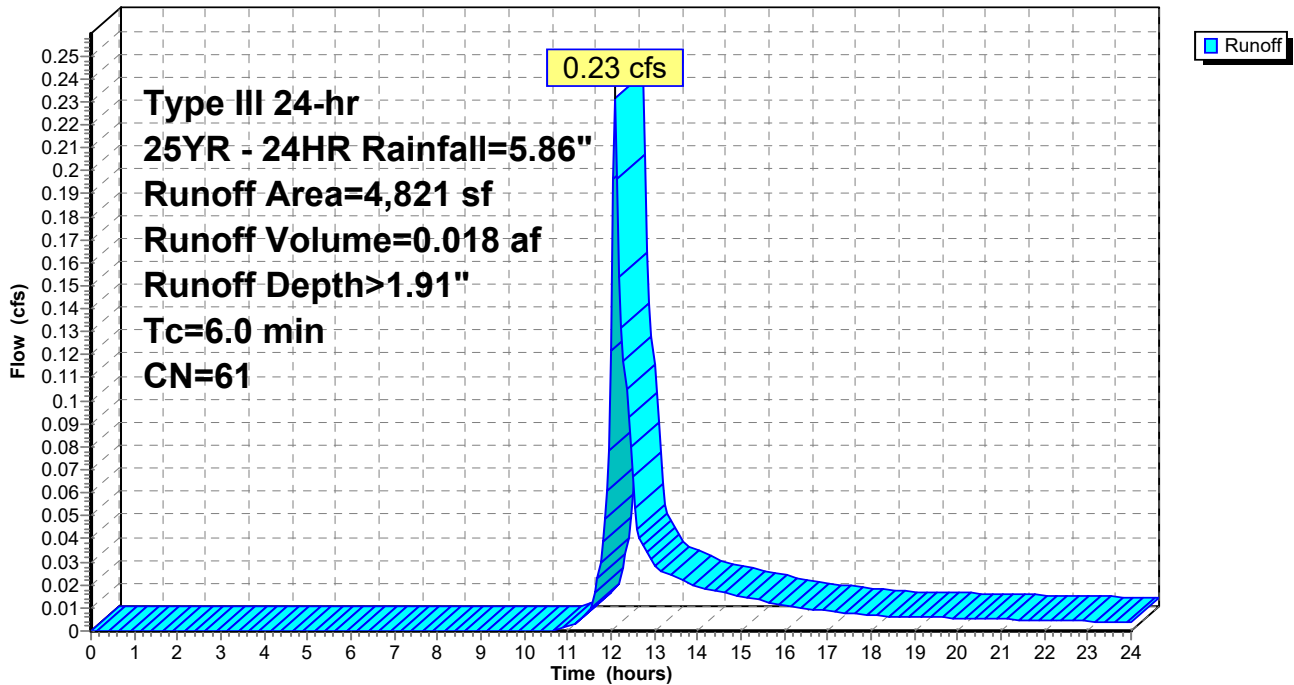
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
4,821	61	>75% Grass cover, Good, HSG B
4,821		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 63S: Gravel Wetland #103

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 64S: Gravel Wetland #104

Runoff = 0.09 cfs @ 12.10 hrs, Volume= 0.007 af, Depth> 1.91"

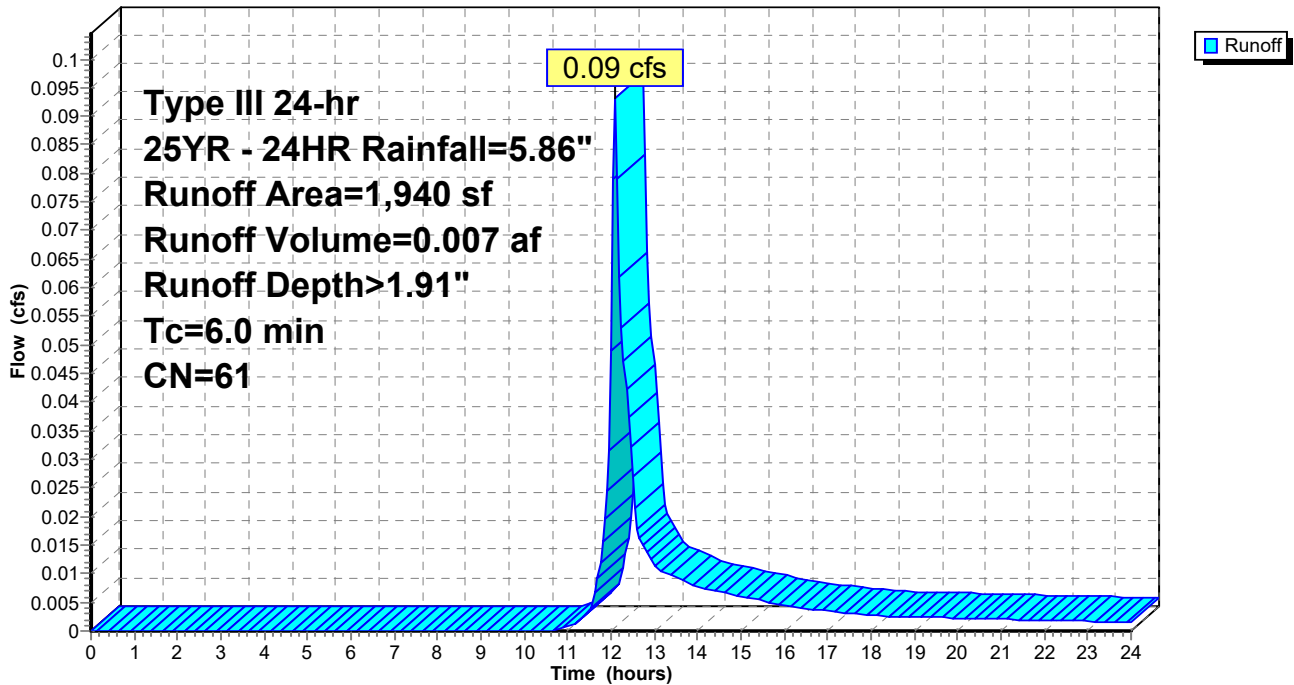
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
1,940	61	>75% Grass cover, Good, HSG B
1,940		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 64S: Gravel Wetland #104

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 65S: Rain Garden #105

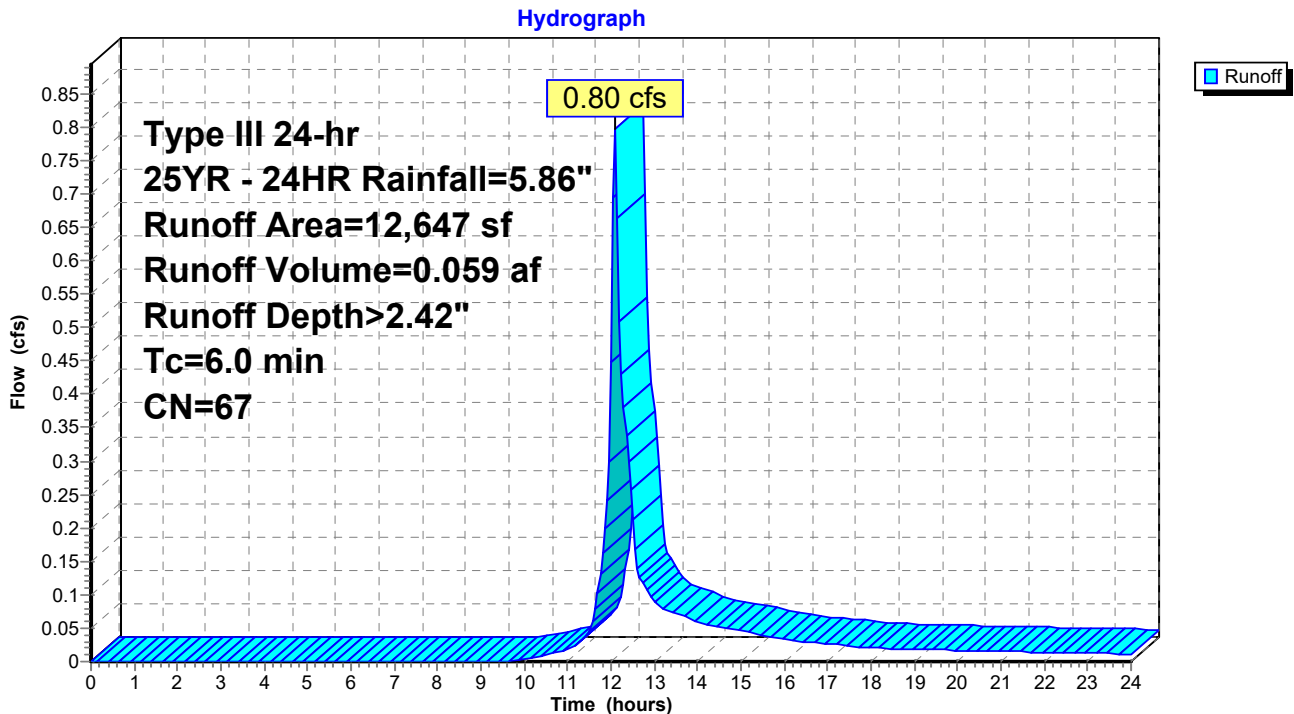
Runoff = 0.80 cfs @ 12.10 hrs, Volume= 0.059 af, Depth> 2.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
7,443	61	>75% Grass cover, Good, HSG B
328	98	Paved parking, HSG B
4,773	74	>75% Grass cover, Good, HSG C
103	98	Paved parking, HSG C
12,647	67	Weighted Average
12,216		96.59% Pervious Area
431		3.41% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Subcatchment 65S: Rain Garden #105



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 66S: Rain Garden #106

Runoff = 1.51 cfs @ 12.22 hrs, Volume= 0.148 af, Depth> 2.24"

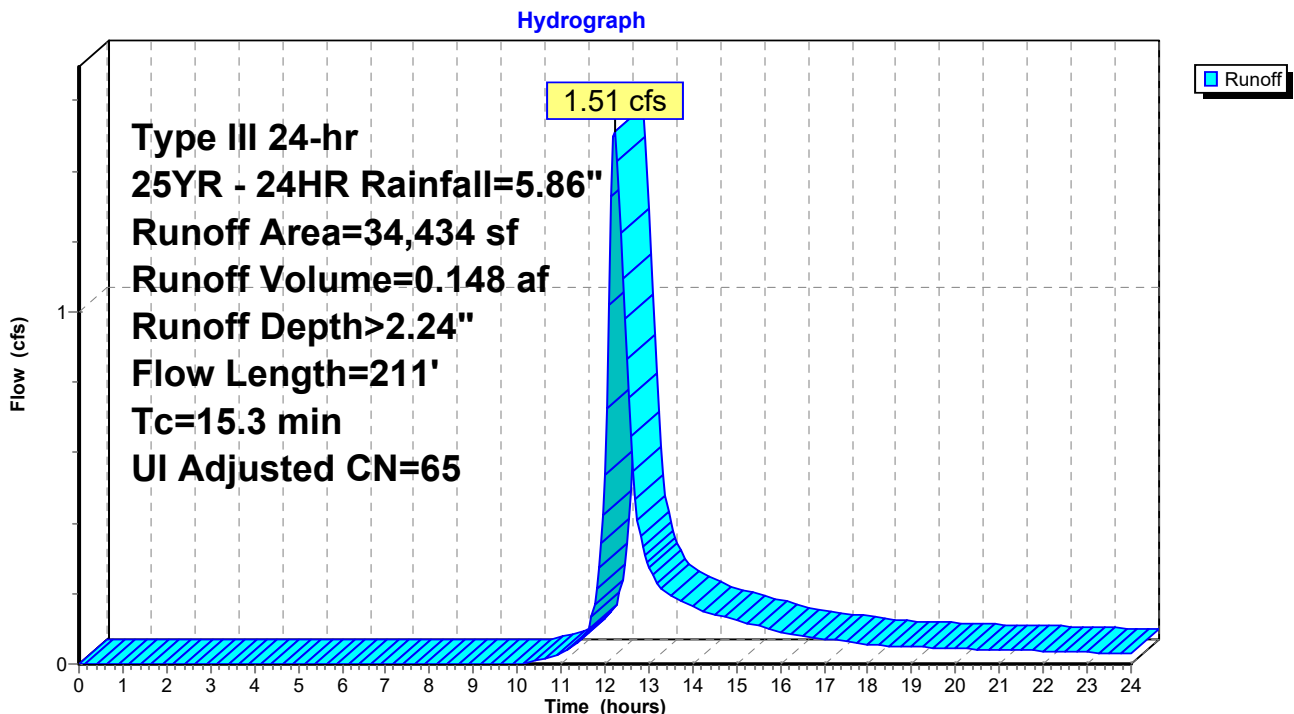
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Adj	Description
26,041	61		>75% Grass cover, Good, HSG B
1,614	98		Unconnected roofs, HSG B
720	96		Gravel surface, HSG B
6,008	74		>75% Grass cover, Good, HSG C
51	96		Gravel surface, HSG C

34,434	66	65	Weighted Average, UI Adjusted
32,820			95.31% Pervious Area
1,614			4.69% Impervious Area
1,614			100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.0	100	0.0325	0.14		Sheet Flow, Segment #1 Grass: Dense n= 0.240 P2= 3.08"
3.3	111	0.0063	0.56		Shallow Concentrated Flow, Segment #2 Short Grass Pasture Kv= 7.0 fps
15.3	211	Total			

Subcatchment 66S: Rain Garden #106



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Summary for Subcatchment 67S: Rain Garden #107

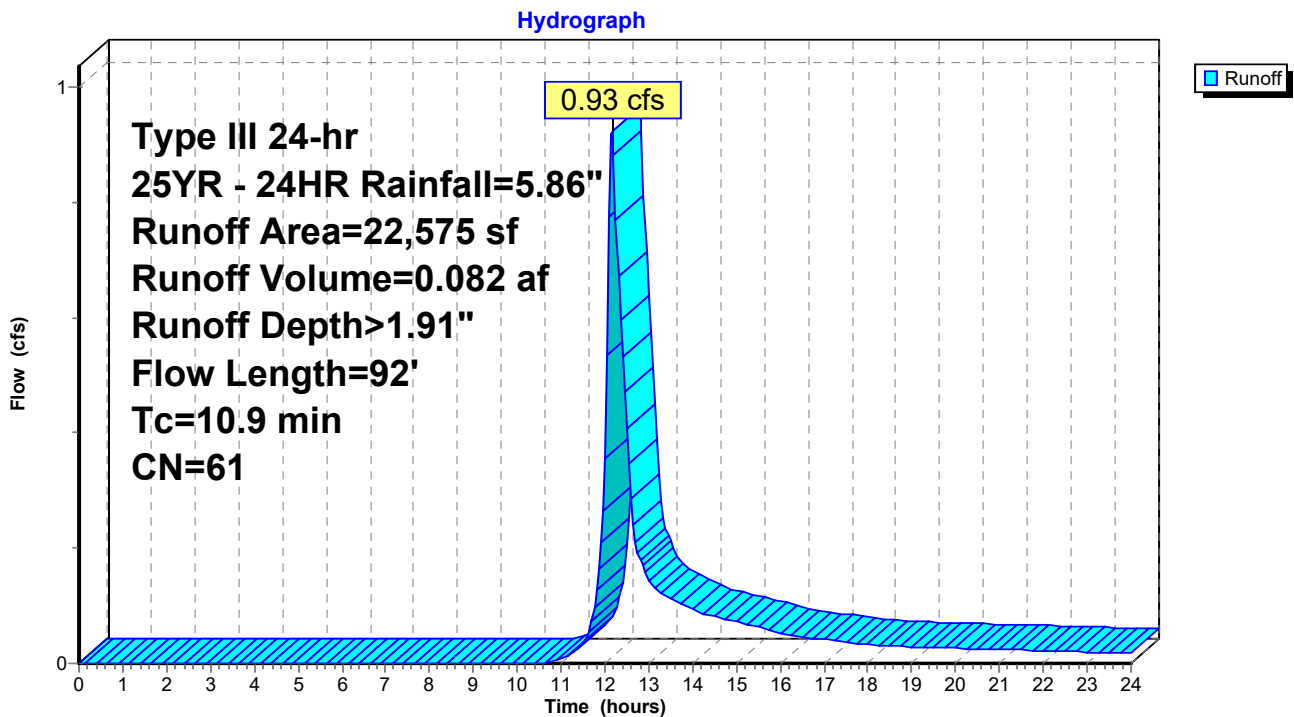
Runoff = 0.93 cfs @ 12.17 hrs, Volume= 0.082 af, Depth> 1.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
22,575	61	>75% Grass cover, Good, HSG B
22,575		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.6	56	0.0090	0.11		Sheet Flow, Segment #1 Grass: Short n= 0.150 P2= 3.08"
0.7	18	0.5000	0.43		Sheet Flow, Segment #2 Grass: Short n= 0.150 P2= 3.08"
1.6	18	0.0667	0.19		Sheet Flow, Segment #3 Grass: Short n= 0.150 P2= 3.08"
10.9	92	Total			

Subcatchment 67S: Rain Garden #107



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 68S: Rain Garden #108

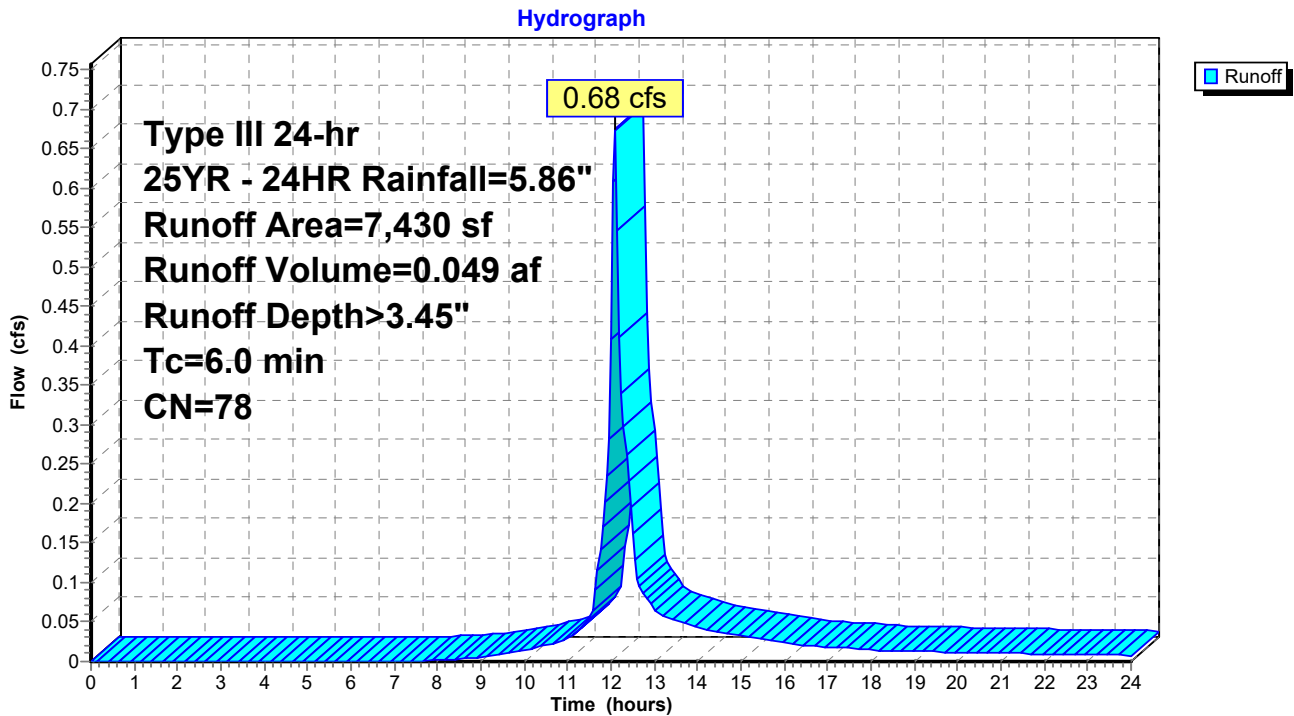
Runoff = 0.68 cfs @ 12.09 hrs, Volume= 0.049 af, Depth> 3.45"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
3,411	98	Paved parking, HSG B
4,019	61	>75% Grass cover, Good, HSG B
7,430	78	Weighted Average
4,019		54.09% Pervious Area
3,411		45.91% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Segment 1

Subcatchment 68S: Rain Garden #108



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 69S: Rain Garden #109

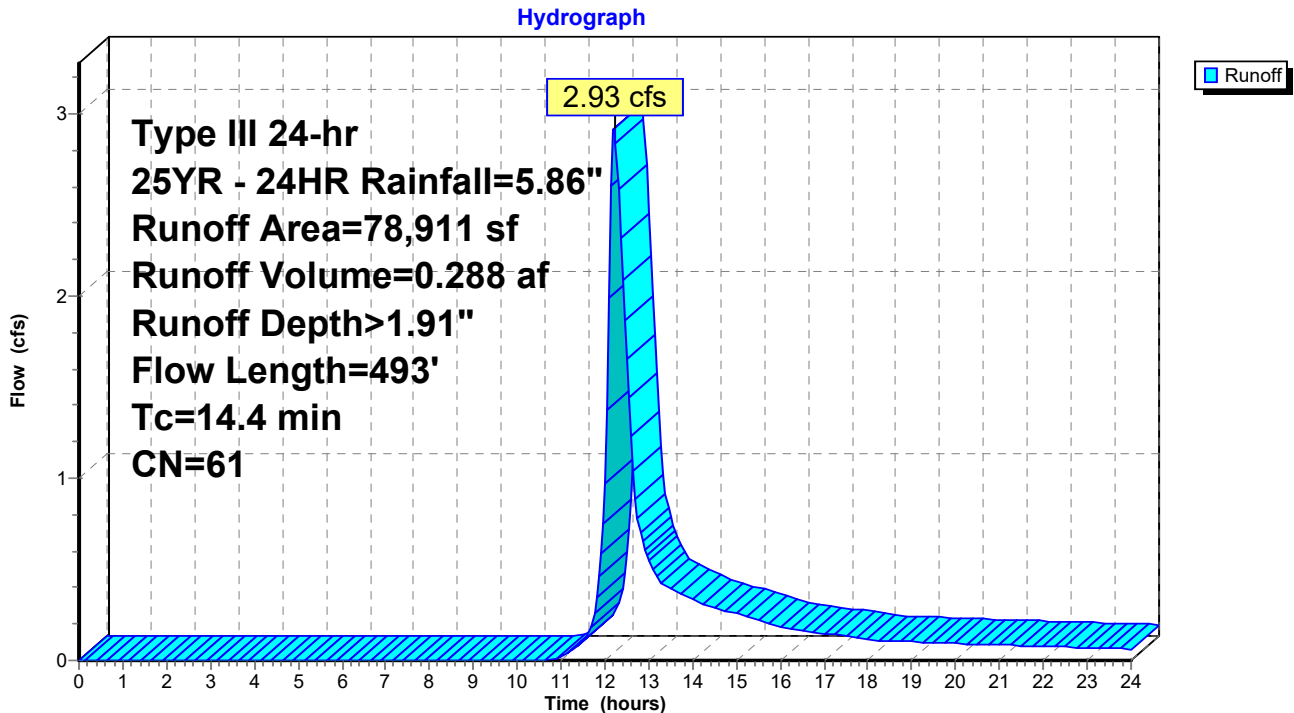
Runoff = 2.93 cfs @ 12.22 hrs, Volume= 0.288 af, Depth> 1.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
67,693	61	>75% Grass cover, Good, HSG B
8,324	55	Woods, Good, HSG B
1,264	96	Gravel surface, HSG B
1,630	74	>75% Grass cover, Good, HSG C
78,911	61	Weighted Average
78,911		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.4	100	0.0600	0.18		Sheet Flow, Segment #1 Grass: Dense n= 0.240 P2= 3.08"
5.0	393	0.0356	1.32		Shallow Concentrated Flow, Segment #2 Short Grass Pasture Kv= 7.0 fps
14.4	493	Total			

Subcatchment 69S: Rain Garden #109



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Summary for Subcatchment 70S: Detention Pond #110

Runoff = 0.86 cfs @ 12.19 hrs, Volume= 0.082 af, Depth> 1.74"

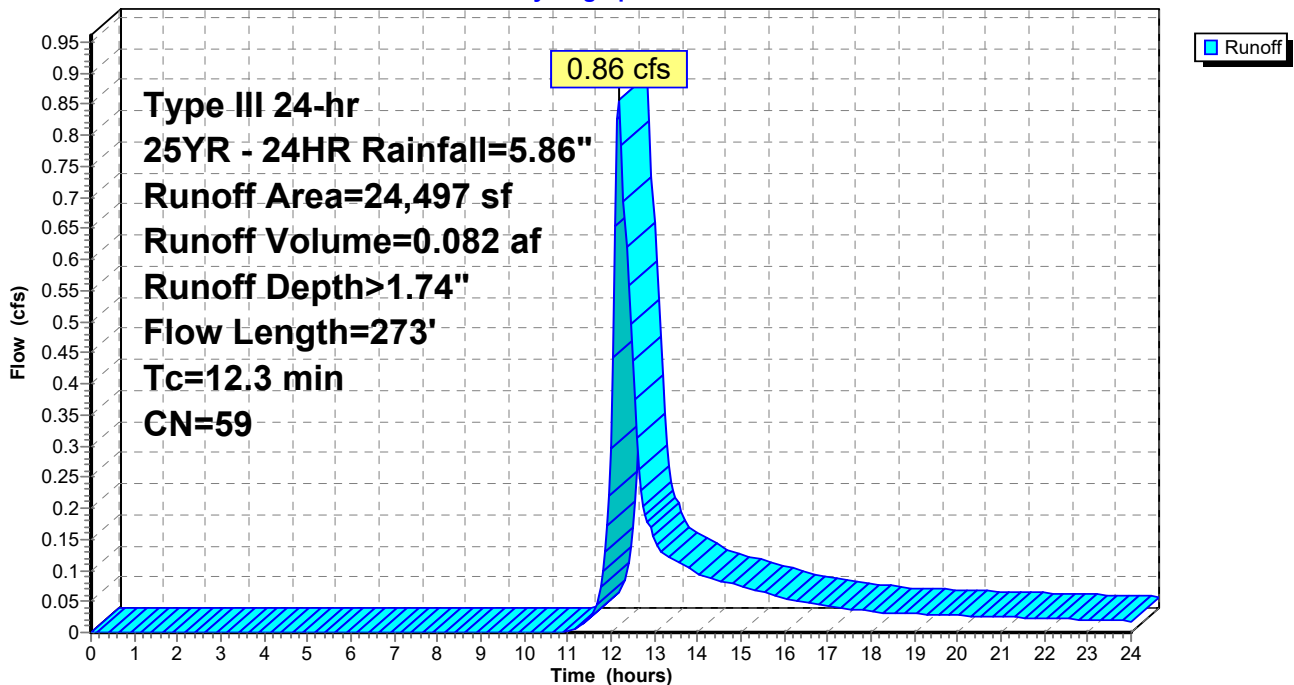
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
10,491	61	>75% Grass cover, Good, HSG B
11,470	55	Woods, Good, HSG B
1,904	74	>75% Grass cover, Good, HSG C
632	70	Woods, Good, HSG C
24,497	59	Weighted Average
24,497		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.7	100	0.0550	0.17		Sheet Flow, Segment #1 Grass: Dense n= 0.240 P2= 3.08"
0.1	8	0.0550	1.64		Shallow Concentrated Flow, Segment #2 Short Grass Pasture Kv= 7.0 fps
2.5	165	0.0485	1.10		Shallow Concentrated Flow, Segment #3 Woodland Kv= 5.0 fps
12.3	273	Total			

Subcatchment 70S: Detention Pond #110

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 310S: Subcatchment 10

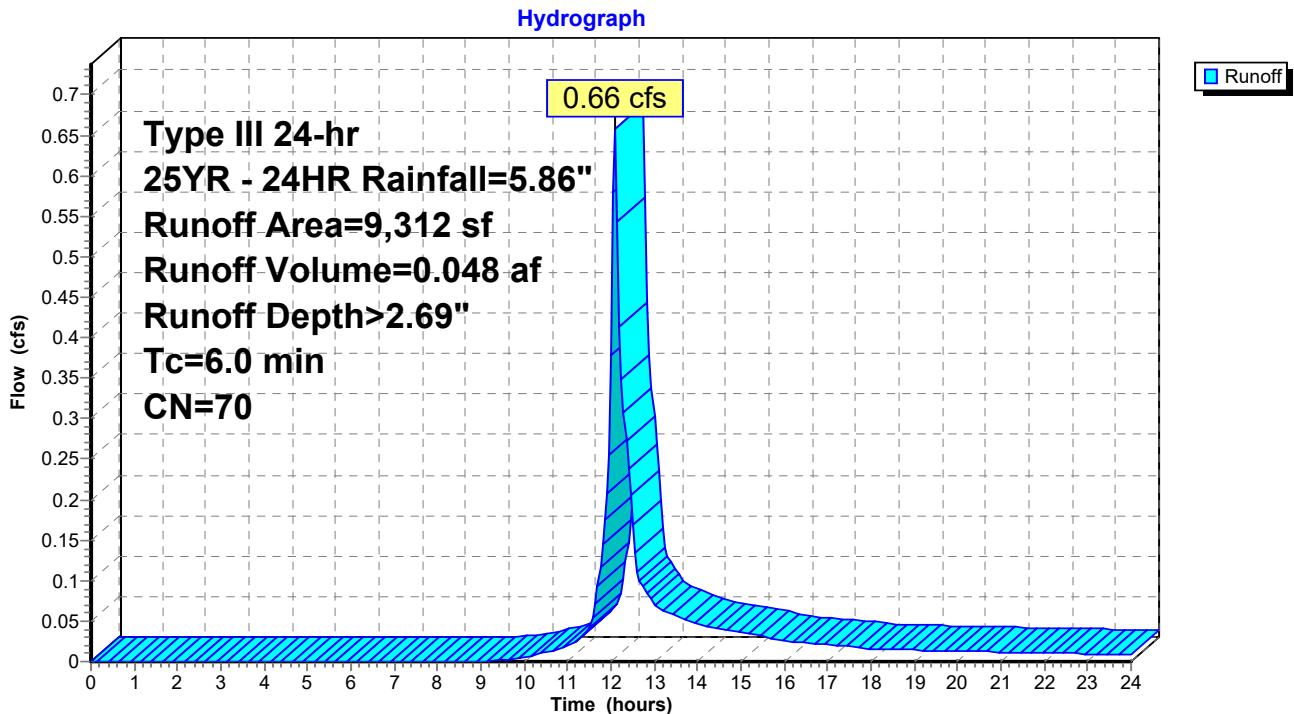
Runoff = 0.66 cfs @ 12.10 hrs, Volume= 0.048 af, Depth> 2.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
746	39	>75% Grass cover, Good, HSG A
2,098	30	Woods, Good, HSG A
2,090	61	>75% Grass cover, Good, HSG B
4,378	98	Paved parking, HSG B
9,312	70	Weighted Average
4,934		52.99% Pervious Area
4,378		47.01% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Segment 1

Subcatchment 310S: Subcatchment 10



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Subcatchment 330S: Subcatchment 30

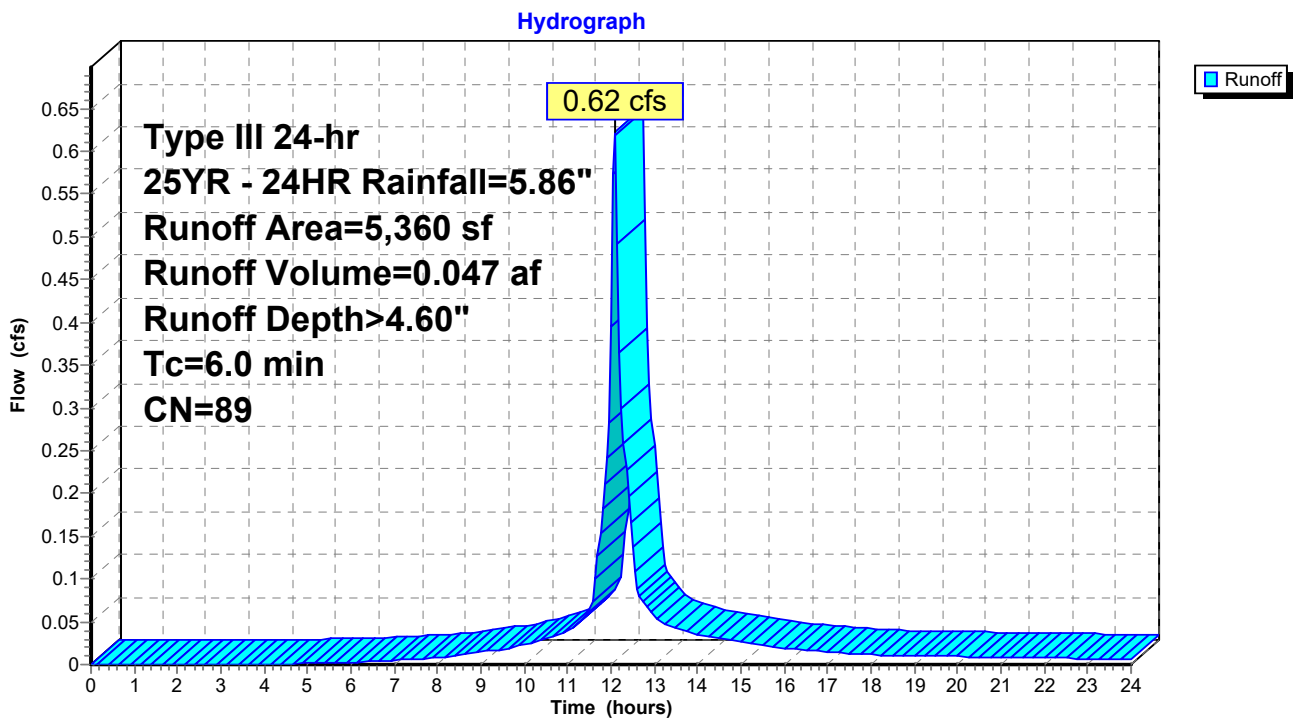
Runoff = 0.62 cfs @ 12.09 hrs, Volume= 0.047 af, Depth> 4.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25YR - 24HR Rainfall=5.86"

Area (sf)	CN	Description
4,128	98	Paved parking, HSG B
1,232	61	>75% Grass cover, Good, HSG B
5,360	89	Weighted Average
1,232		22.99% Pervious Area
4,128		77.01% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Direct Entry

Subcatchment 330S: Subcatchment 30



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Summary for Reach 2R: Reach 2

Inflow Area = 17.551 ac, 0.65% Impervious, Inflow Depth > 1.19" for 25YR - 24HR event
Inflow = 8.18 cfs @ 12.93 hrs, Volume= 1.744 af
Outflow = 8.18 cfs @ 12.94 hrs, Volume= 1.742 af, Atten= 0%, Lag= 0.7 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 3.59 fps, Min. Travel Time= 1.0 min
Avg. Velocity = 1.95 fps, Avg. Travel Time= 1.9 min

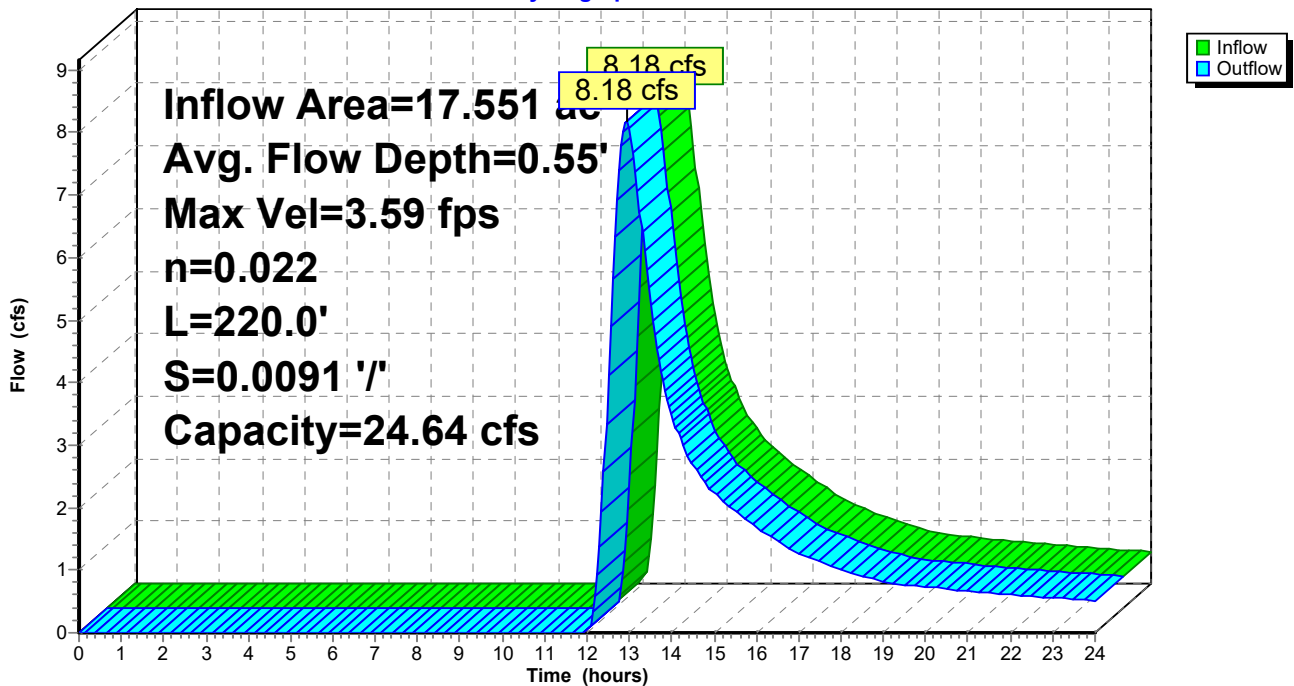
Peak Storage= 501 cf @ 12.94 hrs
Average Depth at Peak Storage= 0.55'
Bank-Full Depth= 1.00' Flow Area= 5.0 sf, Capacity= 24.64 cfs

3.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight
Side Slope Z-value= 2.0 '/' Top Width= 7.00'
Length= 220.0' Slope= 0.0091 '/'
Inlet Invert= 202.00', Outlet Invert= 200.00'



Reach 2R: Reach 2

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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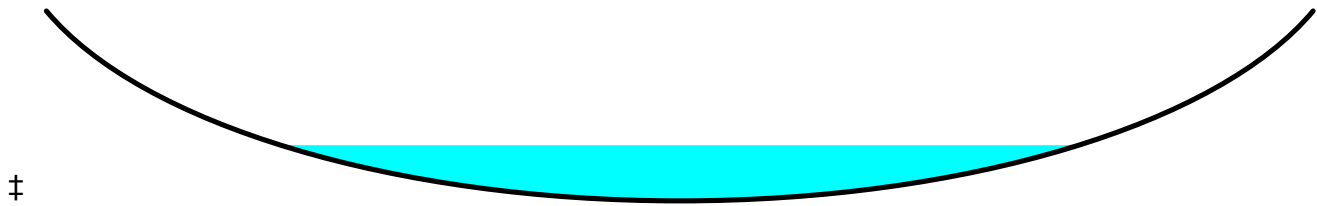
Summary for Reach 11R: Flow Through 8

Inflow Area = 1.933 ac, 13.93% Impervious, Inflow Depth > 0.68" for 25YR - 24HR event
Inflow = 0.54 cfs @ 12.59 hrs, Volume= 0.109 af
Outflow = 0.54 cfs @ 12.60 hrs, Volume= 0.109 af, Atten= 0%, Lag= 0.9 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 1.03 fps, Min. Travel Time= 1.2 min
Avg. Velocity = 0.59 fps, Avg. Travel Time= 2.1 min

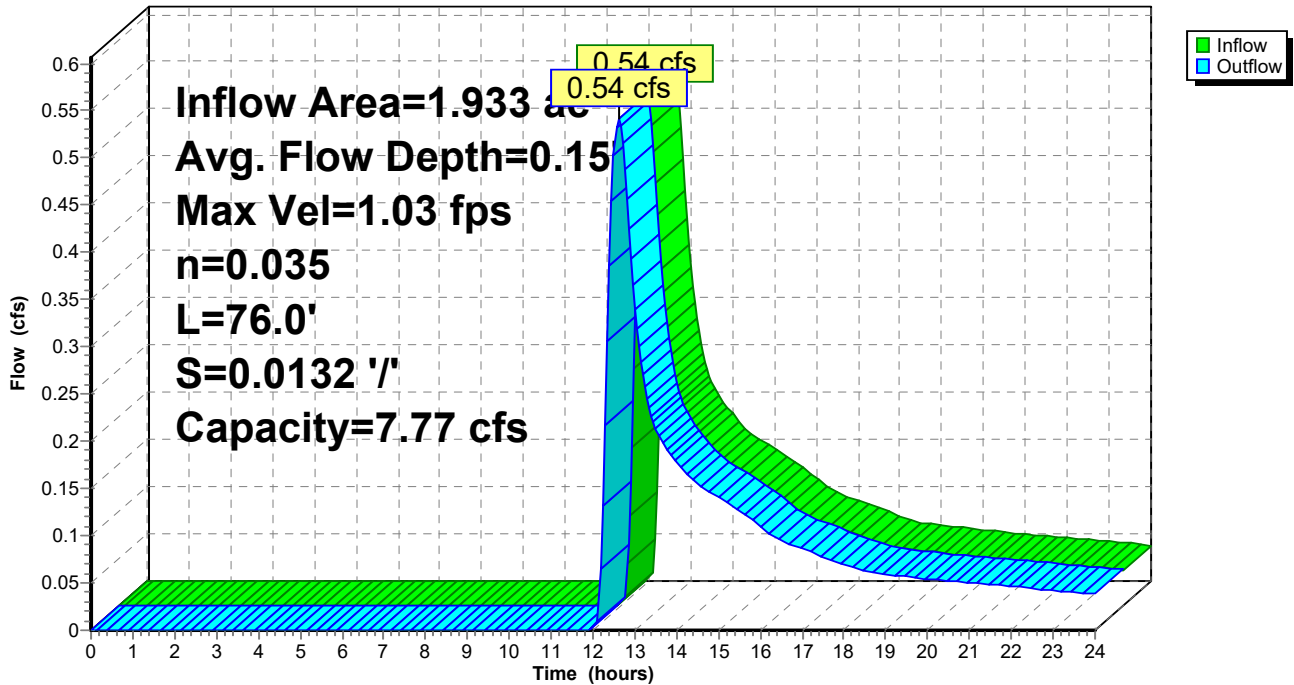
Peak Storage= 40 cf @ 12.60 hrs
Average Depth at Peak Storage= 0.15'
Bank-Full Depth= 0.50' Flow Area= 3.3 sf, Capacity= 7.77 cfs

10.00' x 0.50' deep Parabolic Channel, n= 0.035
Length= 76.0' Slope= 0.0132 '/'
Inlet Invert= 199.00', Outlet Invert= 198.00'



Reach 11R: Flow Through 8

Hydrograph



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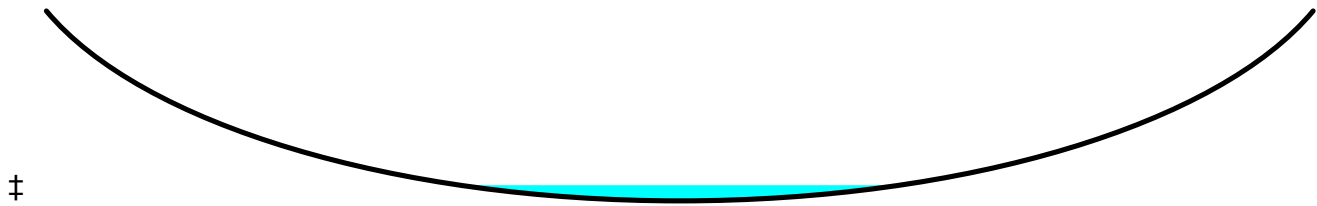
Summary for Reach 50R: Overland flow

Inflow Area = 1.808 ac, 20.57% Impervious, Inflow Depth > 2.01" for 25YR - 24HR event
Inflow = 0.83 cfs @ 12.27 hrs, Volume= 0.303 af
Outflow = 0.83 cfs @ 12.27 hrs, Volume= 0.303 af, Atten= 0%, Lag= 0.1 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 1.80 fps, Min. Travel Time= 0.4 min
Avg. Velocity = 1.11 fps, Avg. Travel Time= 0.6 min

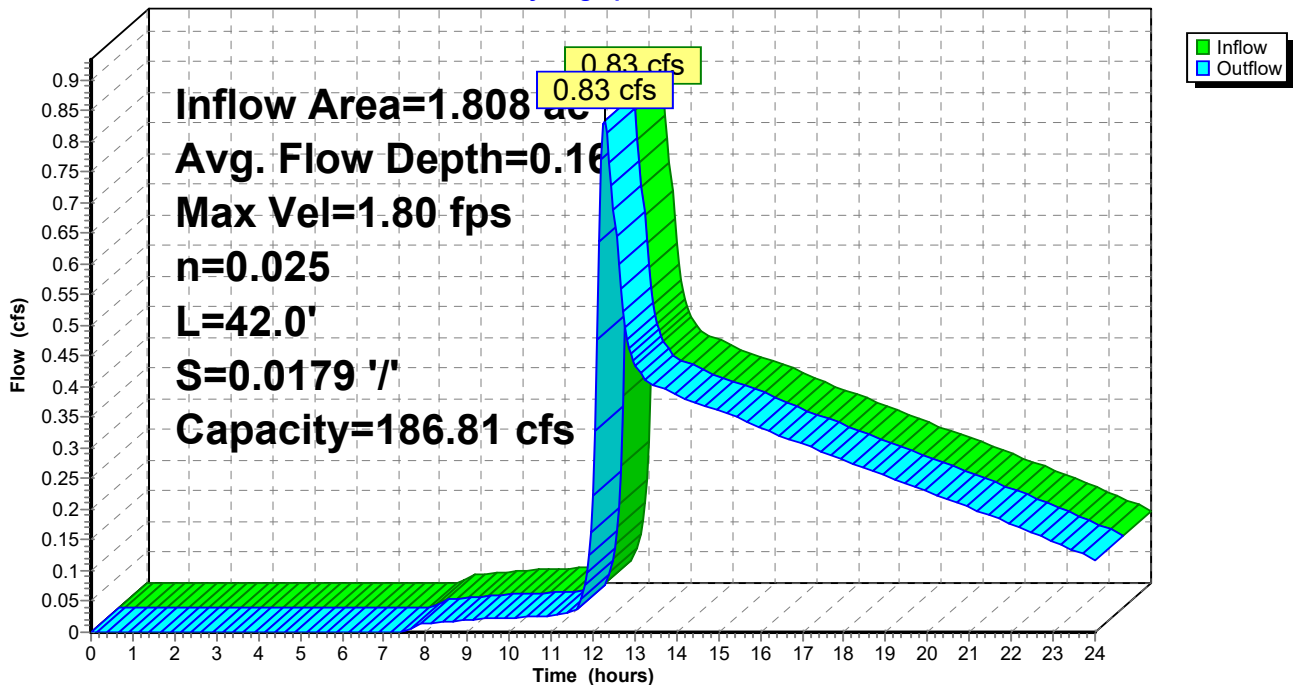
Peak Storage= 19 cf @ 12.27 hrs
Average Depth at Peak Storage= 0.16'
Bank-Full Depth= 2.00' Flow Area= 20.0 sf, Capacity= 186.81 cfs

15.00' x 2.00' deep Parabolic Channel, n= 0.025 Earth, grassed & winding
Length= 42.0' Slope= 0.0179 '/'
Inlet Invert= 203.00', Outlet Invert= 202.25'



Reach 50R: Overland flow

Hydrograph



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Summary for Reach 52R: Wetland Flow

[62] Hint: Exceeded Reach 70R OUTLET depth by 0.18' @ 12.40 hrs

Inflow Area = 8.733 ac, 0.22% Impervious, Inflow Depth > 1.46" for 25YR - 24HR event
Inflow = 5.25 cfs @ 12.45 hrs, Volume= 1.063 af
Outflow = 5.25 cfs @ 12.46 hrs, Volume= 1.062 af, Atten= 0%, Lag= 0.8 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Max. Velocity= 1.84 fps, Min. Travel Time= 1.1 min

Avg. Velocity = 1.03 fps, Avg. Travel Time= 2.0 min

Peak Storage= 351 cf @ 12.46 hrs

Average Depth at Peak Storage= 0.28'

Bank-Full Depth= 0.50' Flow Area= 6.7 sf, Capacity= 17.83 cfs

20.00' x 0.50' deep Parabolic Channel, n= 0.045

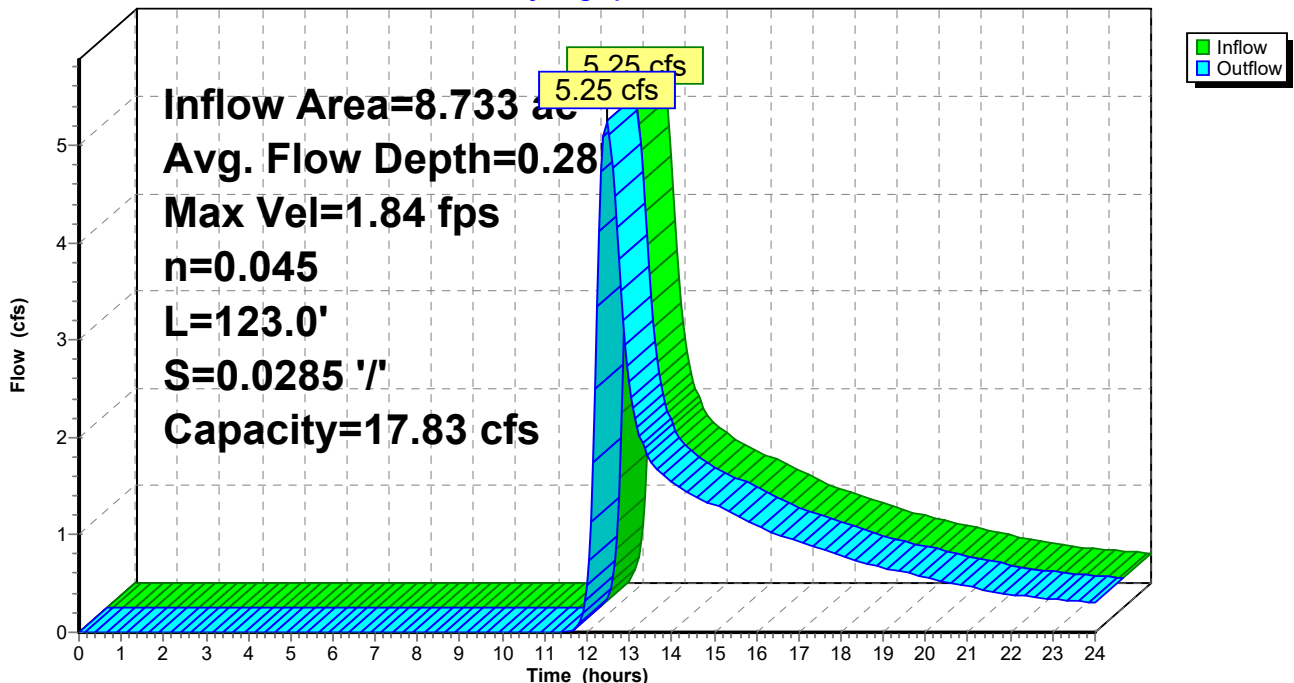
Length= 123.0' Slope= 0.0285 '/'

Inlet Invert= 212.50', Outlet Invert= 209.00'



Reach 52R: Wetland Flow

Hydrograph



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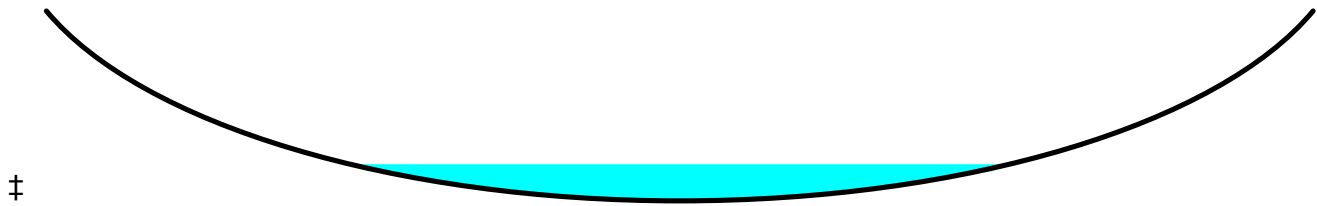
Summary for Reach 53R: Wetland Flow

Inflow Area = 0.542 ac, 0.00% Impervious, Inflow Depth > 1.51" for 25YR - 24HR event
Inflow = 0.57 cfs @ 12.33 hrs, Volume= 0.068 af
Outflow = 0.56 cfs @ 12.36 hrs, Volume= 0.068 af, Atten= 1%, Lag= 1.8 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 1.01 fps, Min. Travel Time= 2.2 min
Avg. Velocity = 0.46 fps, Avg. Travel Time= 4.9 min

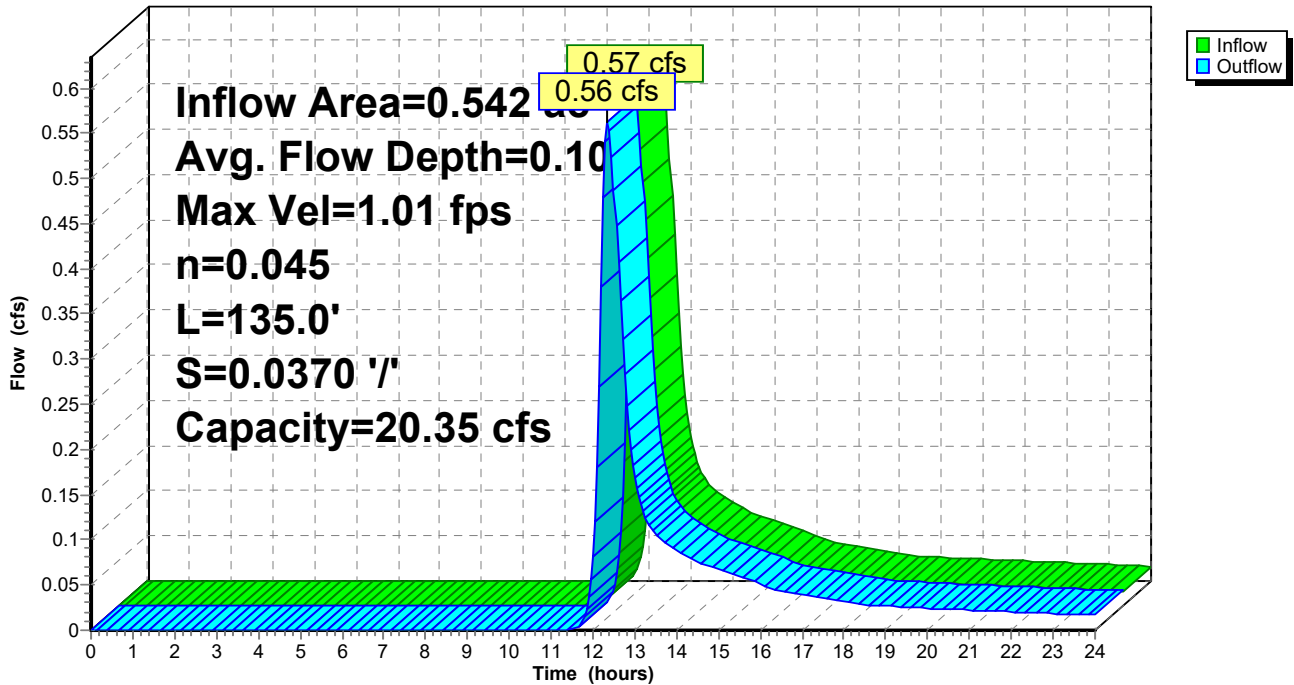
Peak Storage= 75 cf @ 12.36 hrs
Average Depth at Peak Storage= 0.10'
Bank-Full Depth= 0.50' Flow Area= 6.7 sf, Capacity= 20.35 cfs

20.00' x 0.50' deep Parabolic Channel, n= 0.045
Length= 135.0' Slope= 0.0370 '/'
Inlet Invert= 214.00', Outlet Invert= 209.00'



Reach 53R: Wetland Flow

Hydrograph



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Summary for Reach 54R: Combined Wetland Flow

[62] Hint: Exceeded Reach 52R OUTLET depth by 0.04' @ 12.45 hrs

[62] Hint: Exceeded Reach 53R OUTLET depth by 0.24' @ 12.50 hrs

Inflow Area = 9.274 ac, 0.21% Impervious, Inflow Depth > 1.46" for 25YR - 24HR event
Inflow = 5.76 cfs @ 12.46 hrs, Volume= 1.130 af
Outflow = 5.76 cfs @ 12.46 hrs, Volume= 1.130 af, Atten= 0%, Lag= 0.2 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Max. Velocity= 5.20 fps, Min. Travel Time= 0.3 min

Avg. Velocity= 2.68 fps, Avg. Travel Time= 0.5 min

Peak Storage= 96 cf @ 12.46 hrs

Average Depth at Peak Storage= 0.33'

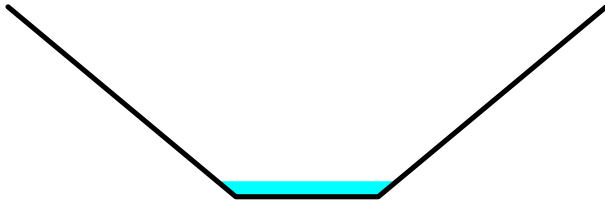
Bank-Full Depth= 4.00' Flow Area= 31.2 sf, Capacity= 610.11 cfs

3.00' x 4.00' deep channel, n= 0.045

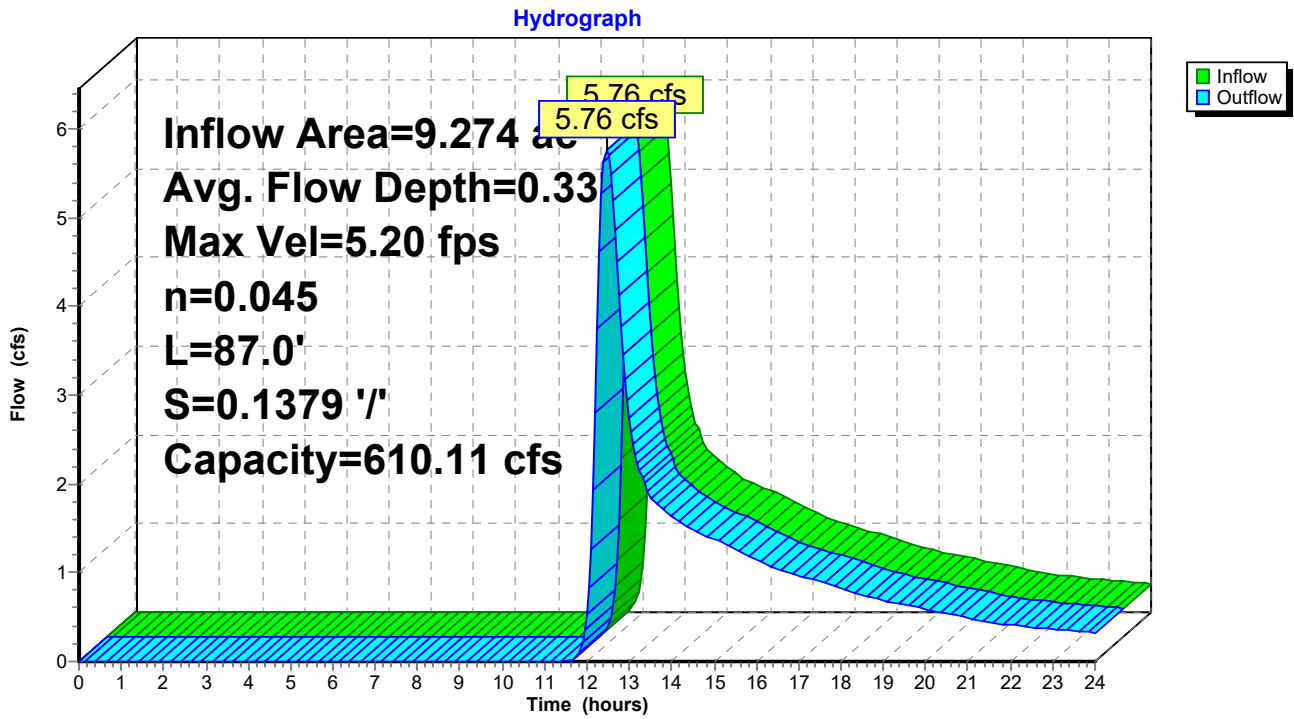
Side Slope Z-value= 1.2 '/' Top Width= 12.60'

Length= 87.0' Slope= 0.1379 '/'

Inlet Invert= 209.00', Outlet Invert= 197.00'



Reach 54R: Combined Wetland Flow



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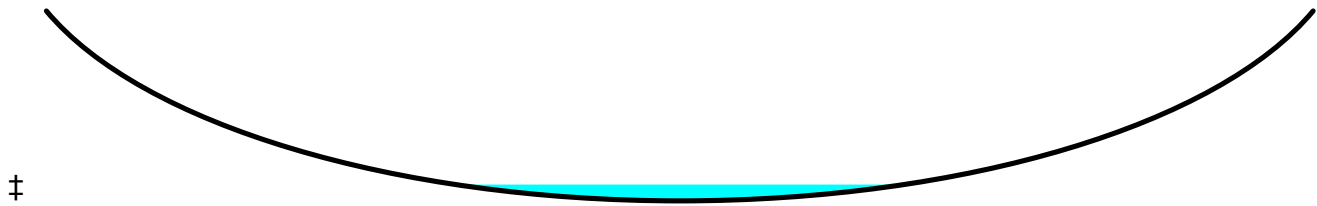
Summary for Reach 63R: Overland Flow

Inflow Area = 0.567 ac, 57.16% Impervious, Inflow Depth > 2.51" for 25YR - 24HR event
Inflow = 0.20 cfs @ 13.18 hrs, Volume= 0.119 af
Outflow = 0.20 cfs @ 13.21 hrs, Volume= 0.119 af, Atten= 0%, Lag= 1.6 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 1.00 fps, Min. Travel Time= 2.1 min
Avg. Velocity = 0.60 fps, Avg. Travel Time= 3.5 min

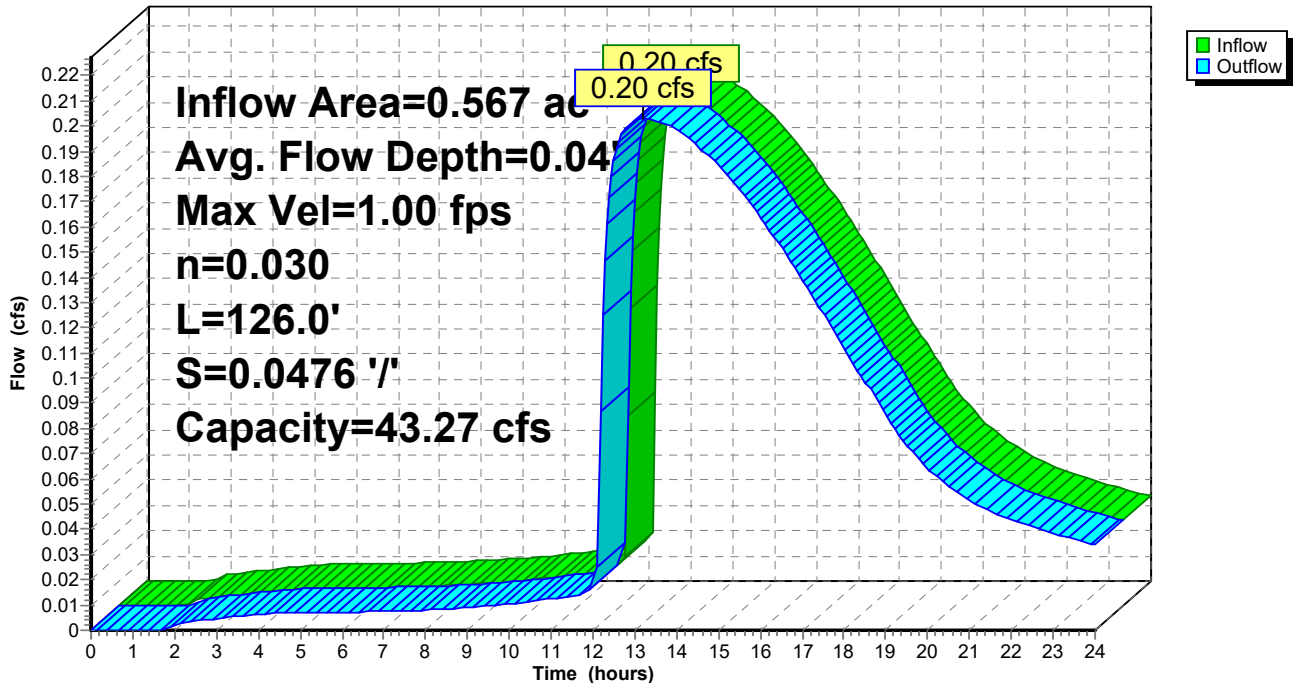
Peak Storage= 26 cf @ 13.21 hrs
Average Depth at Peak Storage= 0.04'
Bank-Full Depth= 0.50' Flow Area= 8.3 sf, Capacity= 43.27 cfs

25.00' x 0.50' deep Parabolic Channel, n= 0.030 Earth, grassed & winding
Length= 126.0' Slope= 0.0476 '/'
Inlet Invert= 211.00', Outlet Invert= 205.00'



Reach 63R: Overland Flow

Hydrograph



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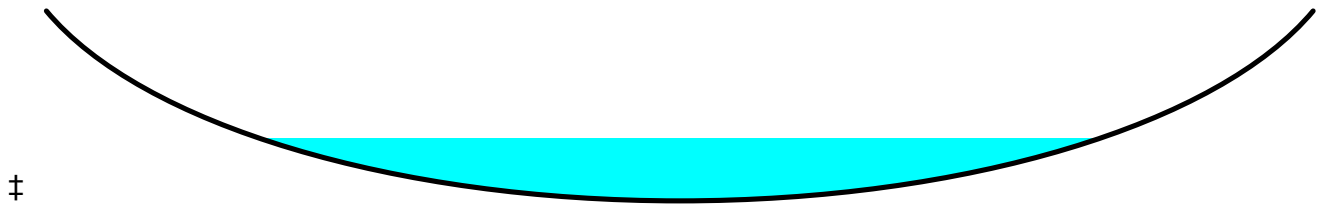
Summary for Reach 65R: Overland Flow

Inflow Area = 2.026 ac, 60.48% Impervious, Inflow Depth > 2.79" for 25YR - 24HR event
Inflow = 2.24 cfs @ 12.42 hrs, Volume= 0.471 af
Outflow = 2.02 cfs @ 12.53 hrs, Volume= 0.469 af, Atten= 10%, Lag= 6.9 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 1.60 fps, Min. Travel Time= 3.6 min
Avg. Velocity = 0.82 fps, Avg. Travel Time= 6.9 min

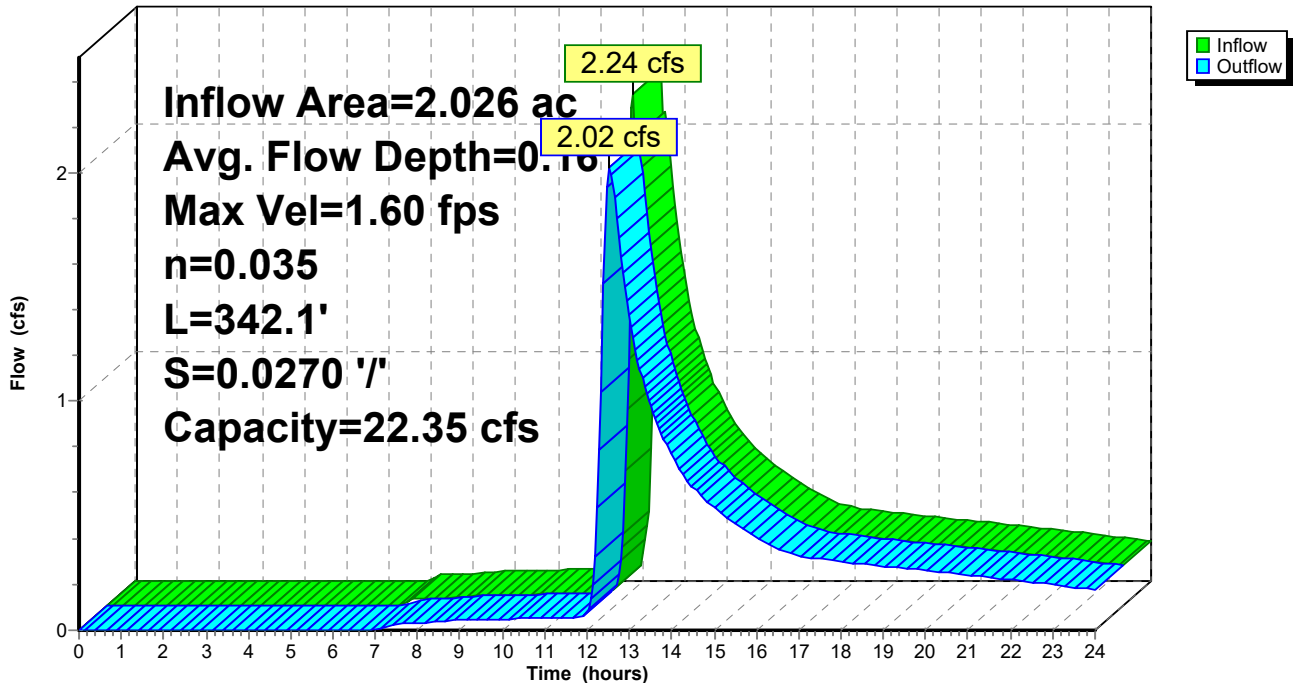
Peak Storage= 432 cf @ 12.53 hrs
Average Depth at Peak Storage= 0.16'
Bank-Full Depth= 0.50' Flow Area= 6.7 sf, Capacity= 22.35 cfs

20.00' x 0.50' deep Parabolic Channel, n= 0.035 Earth, dense weeds
Length= 342.1' Slope= 0.0270 '/'
Inlet Invert= 212.50', Outlet Invert= 203.25'



Reach 65R: Overland Flow

Hydrograph



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Summary for Reach 66R: Overland Flow

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=1)

Inflow Area = 1.231 ac, 30.22% Impervious, Inflow Depth > 2.25" for 25YR - 24HR event
Inflow = 0.30 cfs @ 13.96 hrs, Volume= 0.231 af
Outflow = 0.30 cfs @ 13.96 hrs, Volume= 0.231 af, Atten= 0%, Lag= 0.3 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 1.90 fps, Min. Travel Time= 0.4 min
Avg. Velocity = 1.49 fps, Avg. Travel Time= 0.5 min

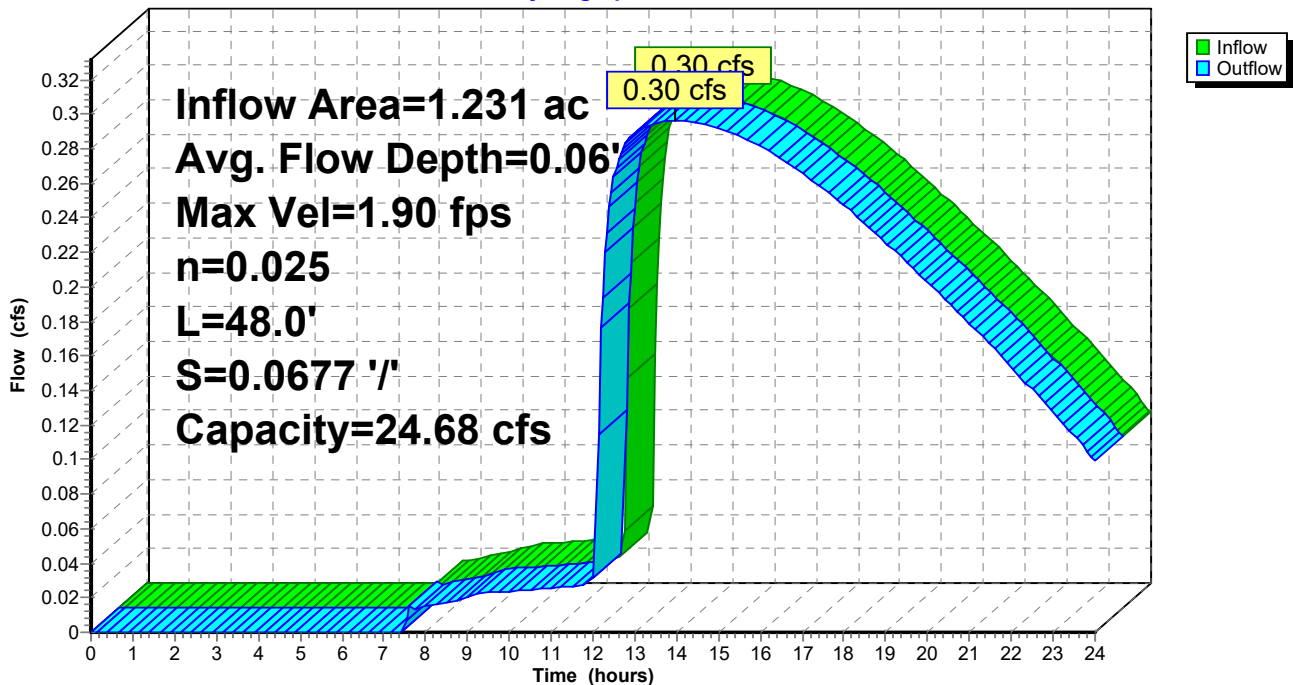
Peak Storage= 7 cf @ 13.96 hrs
Average Depth at Peak Storage= 0.06'
Bank-Full Depth= 0.50' Flow Area= 3.3 sf, Capacity= 24.68 cfs

10.00' x 0.50' deep Parabolic Channel, n= 0.025 Earth, grassed & winding
Length= 48.0' Slope= 0.0677 '/'
Inlet Invert= 211.00', Outlet Invert= 207.75'



Reach 66R: Overland Flow

Hydrograph



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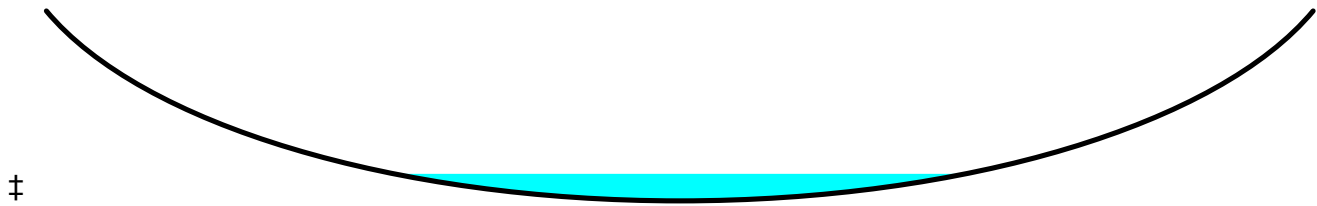
Summary for Reach 67R: Overland flow

Inflow Area = 4.467 ac, 17.16% Impervious, Inflow Depth > 1.30" for 25YR - 24HR event
Inflow = 0.58 cfs @ 15.42 hrs, Volume= 0.483 af
Outflow = 0.58 cfs @ 15.44 hrs, Volume= 0.482 af, Atten= 0%, Lag= 1.3 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 1.62 fps, Min. Travel Time= 1.8 min
Avg. Velocity = 1.54 fps, Avg. Travel Time= 2.0 min

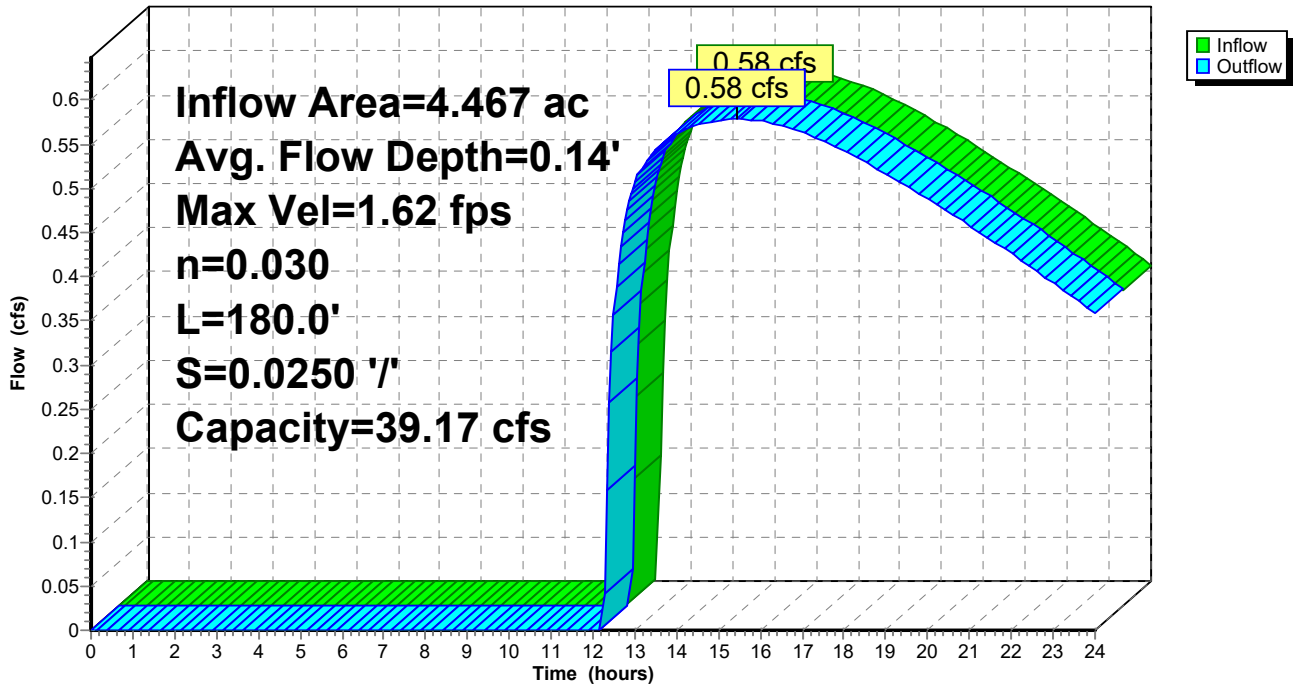
Peak Storage= 64 cf @ 15.44 hrs
Average Depth at Peak Storage= 0.14'
Bank-Full Depth= 1.00' Flow Area= 6.7 sf, Capacity= 39.17 cfs

10.00' x 1.00' deep Parabolic Channel, n= 0.030 Earth, grassed & winding
Length= 180.0' Slope= 0.0250 '/'
Inlet Invert= 223.00', Outlet Invert= 218.50'



Reach 67R: Overland flow

Hydrograph



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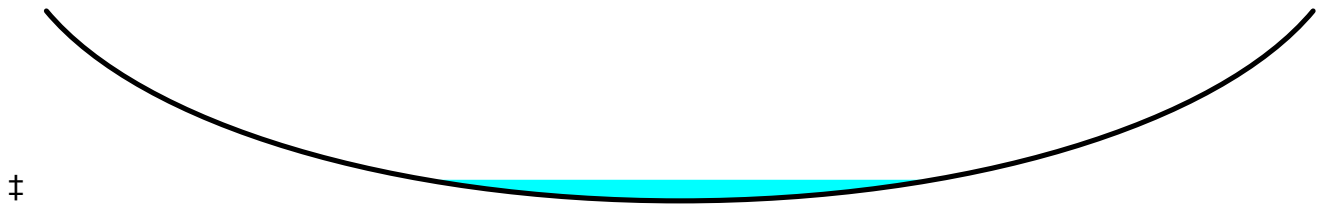
Summary for Reach 69R: Overland Flow

Inflow Area = 6.279 ac, 12.21% Impervious, Inflow Depth > 1.19" for 25YR - 24HR event
Inflow = 0.94 cfs @ 13.50 hrs, Volume= 0.624 af
Outflow = 0.94 cfs @ 13.51 hrs, Volume= 0.624 af, Atten= 0%, Lag= 0.5 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 1.54 fps, Min. Travel Time= 0.8 min
Avg. Velocity = 1.33 fps, Avg. Travel Time= 0.9 min

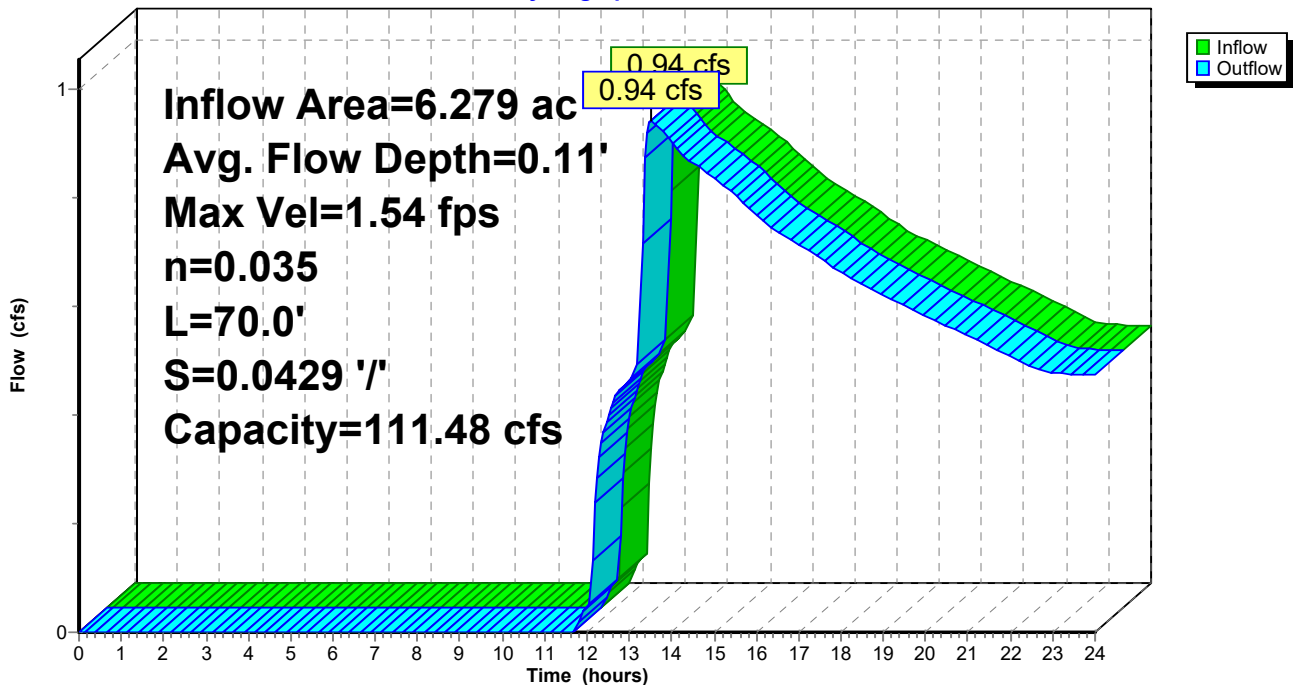
Peak Storage= 43 cf @ 13.51 hrs
Average Depth at Peak Storage= 0.11'
Bank-Full Depth= 1.00' Flow Area= 16.7 sf, Capacity= 111.48 cfs

25.00' x 1.00' deep Parabolic Channel, n= 0.035
Length= 70.0' Slope= 0.0429 '/'
Inlet Invert= 208.00', Outlet Invert= 205.00'



Reach 69R: Overland Flow

Hydrograph



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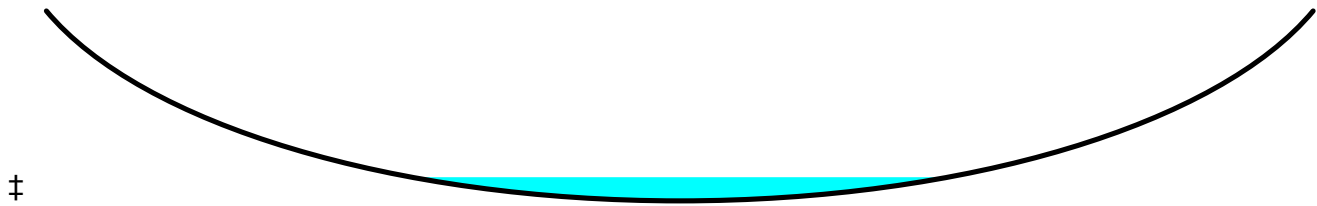
Summary for Reach 70R: Overland Flow From Det #110

Inflow Area = 3.275 ac, 0.59% Impervious, Inflow Depth > 1.52" for 25YR - 24HR event
Inflow = 0.66 cfs @ 13.66 hrs, Volume= 0.415 af
Outflow = 0.66 cfs @ 13.67 hrs, Volume= 0.415 af, Atten= 0%, Lag= 0.3 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Max. Velocity= 2.29 fps, Min. Travel Time= 0.4 min
Avg. Velocity = 1.94 fps, Avg. Travel Time= 0.5 min

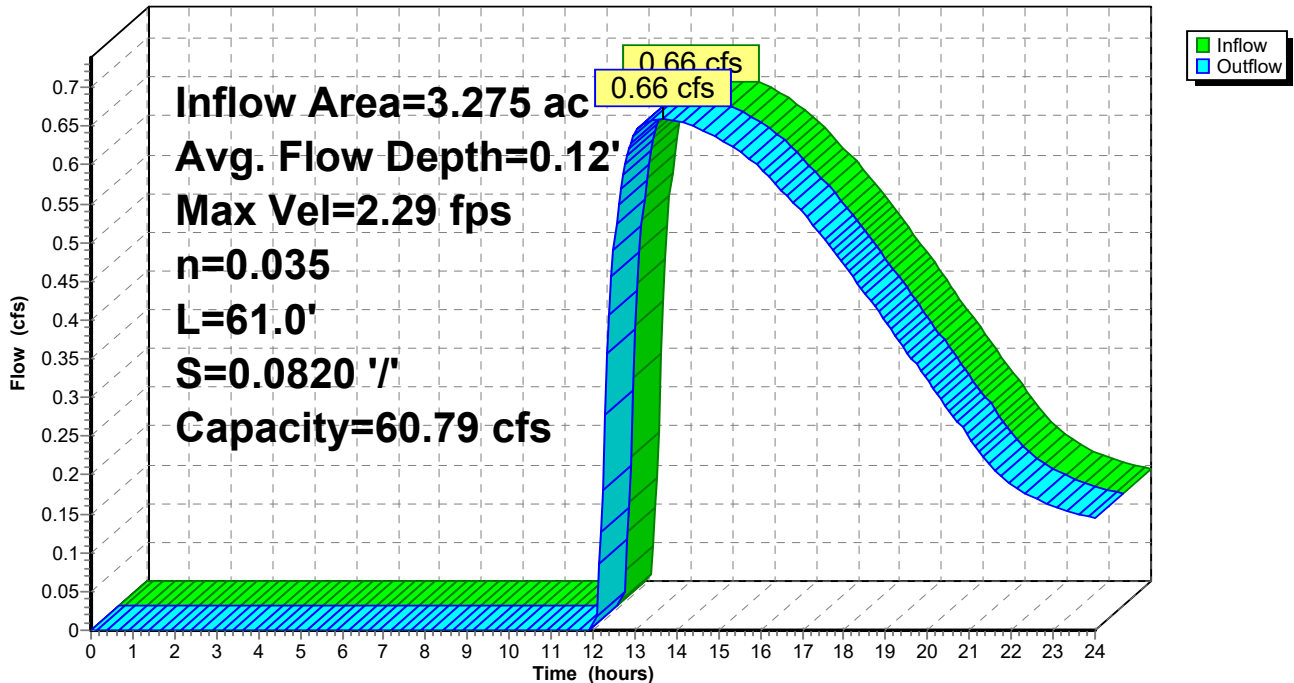
Peak Storage= 18 cf @ 13.67 hrs
Average Depth at Peak Storage= 0.12'
Bank-Full Depth= 1.00' Flow Area= 6.7 sf, Capacity= 60.79 cfs

10.00' x 1.00' deep Parabolic Channel, n= 0.035 Earth, dense weeds
Length= 61.0' Slope= 0.0820 '/'
Inlet Invert= 217.50', Outlet Invert= 212.50'



Reach 70R: Overland Flow From Det #110

Hydrograph



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Summary for Reach 100R: Reach 100

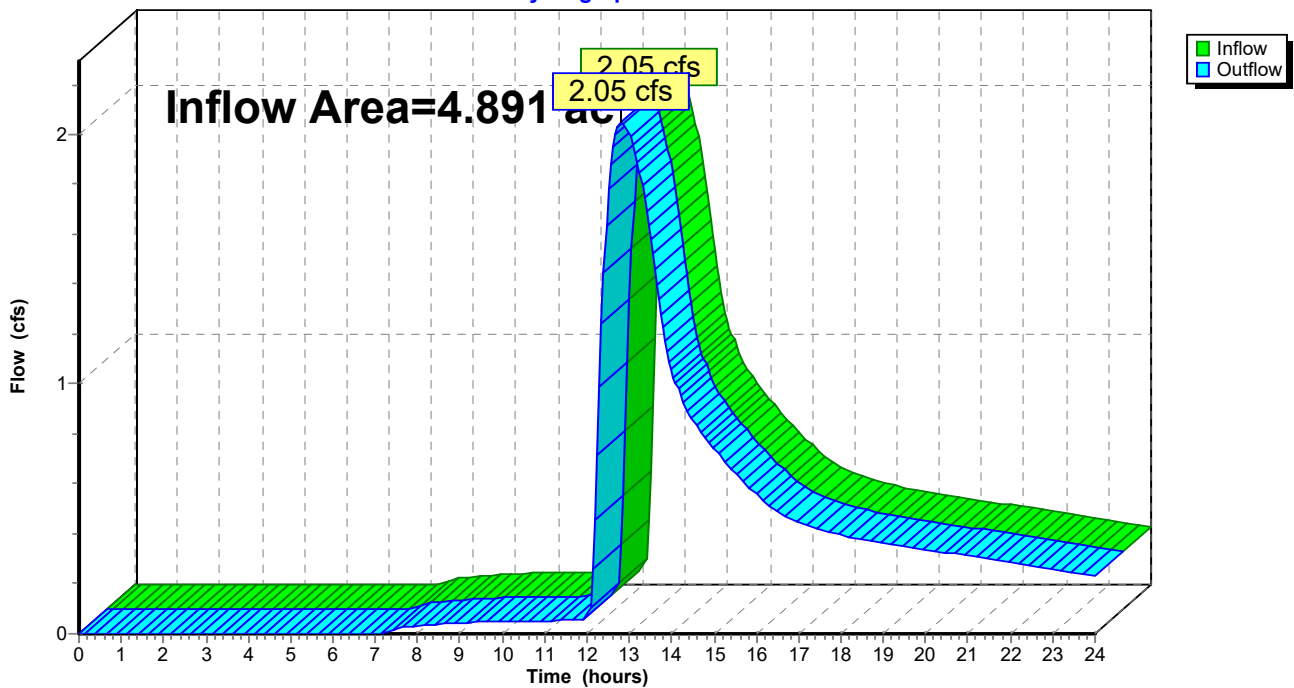
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 4.891 ac, 26.20% Impervious, Inflow Depth > 1.51" for 25YR - 24HR event
Inflow = 2.05 cfs @ 12.81 hrs, Volume= 0.617 af
Outflow = 2.05 cfs @ 12.81 hrs, Volume= 0.617 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Reach 100R: Reach 100

Hydrograph



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Summary for Reach 200R: Reach 200

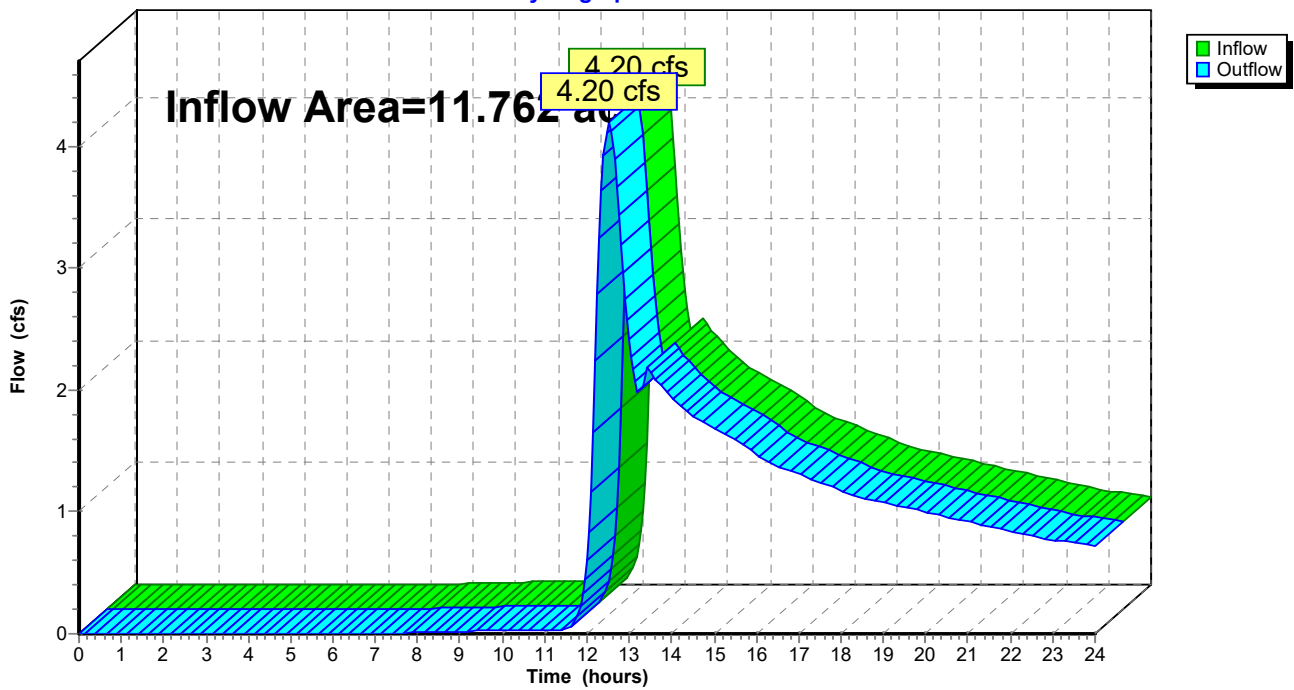
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 11.762 ac, 10.97% Impervious, Inflow Depth > 1.42" for 25YR - 24HR event
Inflow = 4.20 cfs @ 12.52 hrs, Volume= 1.391 af
Outflow = 4.20 cfs @ 12.52 hrs, Volume= 1.391 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Reach 200R: Reach 200

Hydrograph



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Summary for Reach 300R: Reach 300

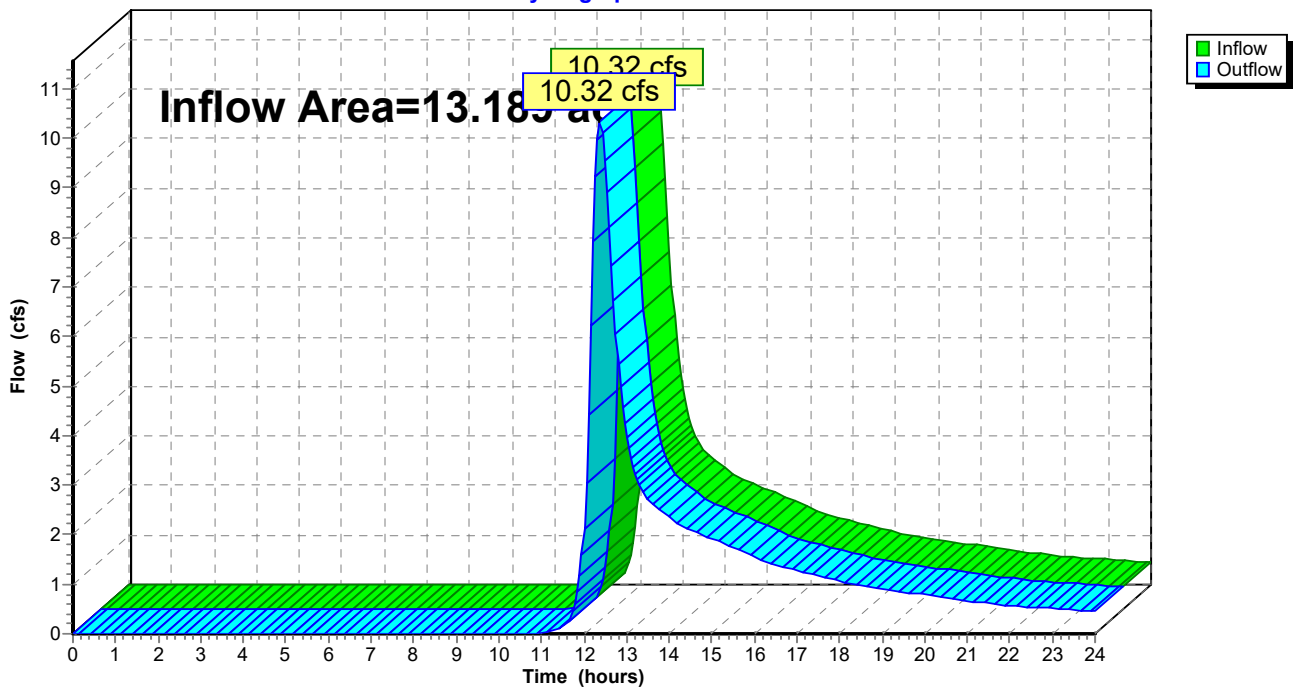
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 13.189 ac, 0.33% Impervious, Inflow Depth > 1.57" for 25YR - 24HR event
Inflow = 10.32 cfs @ 12.37 hrs, Volume= 1.724 af
Outflow = 10.32 cfs @ 12.37 hrs, Volume= 1.724 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Reach 300R: Reach 300

Hydrograph



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Summary for Reach 400R: Reach 400

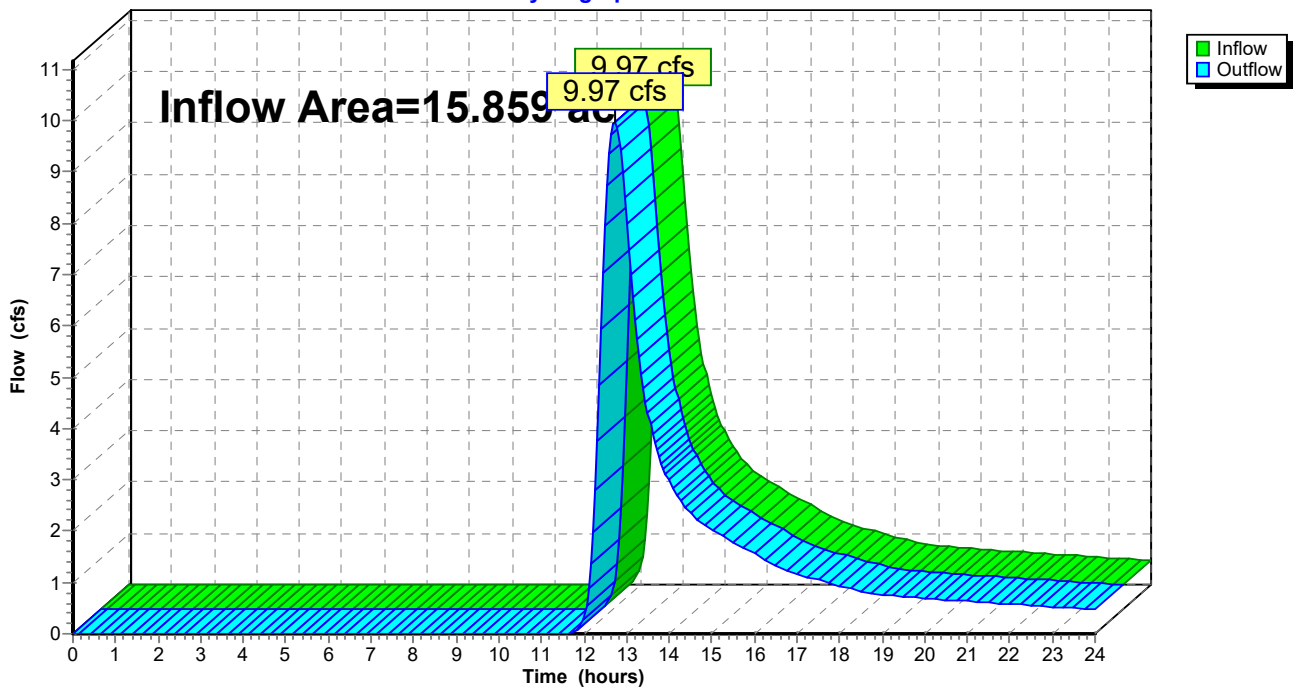
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 15.859 ac, 0.00% Impervious, Inflow Depth > 1.34" for 25YR - 24HR event
Inflow = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af
Outflow = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Reach 400R: Reach 400

Hydrograph



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Summary for Reach 800R: Svenson Pond

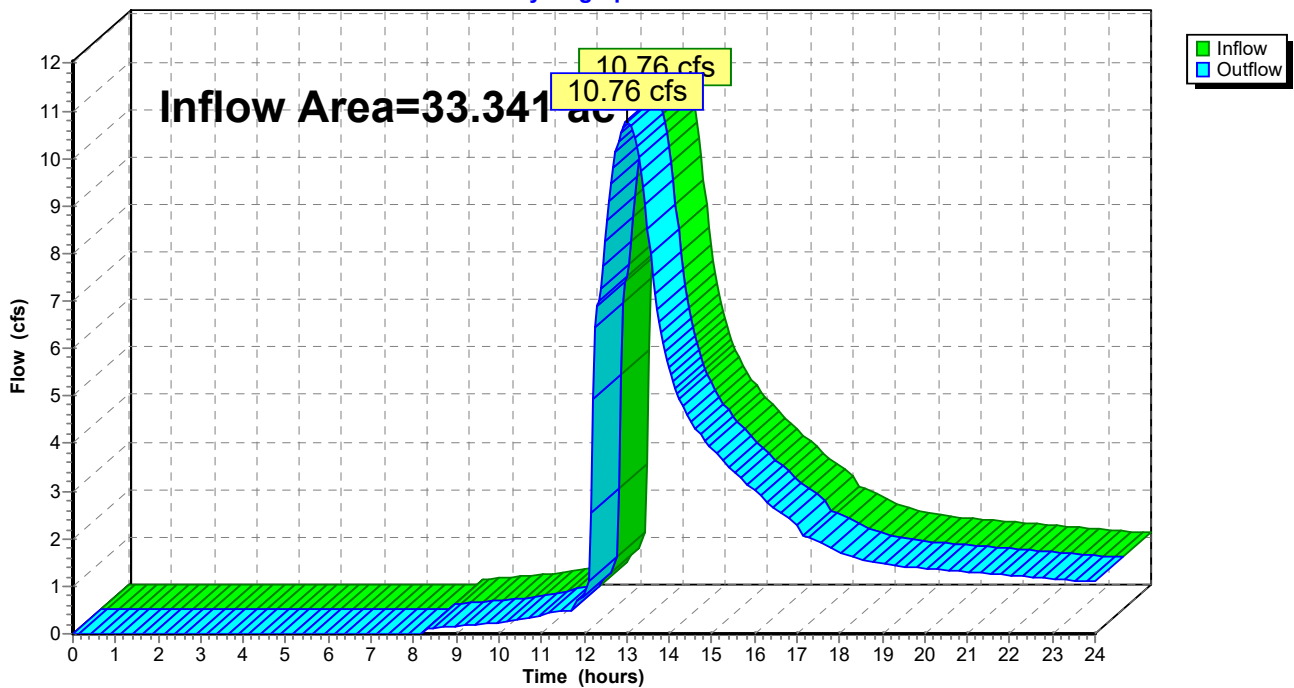
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 33.341 ac, 8.39% Impervious, Inflow Depth > 1.11" for 25YR - 24HR event
Inflow = 10.76 cfs @ 13.01 hrs, Volume= 3.096 af
Outflow = 10.76 cfs @ 13.01 hrs, Volume= 3.096 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2

Reach 800R: Svenson Pond

Hydrograph



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Summary for Pond 1P: Drop Inlet

[42] Hint: Gap in defined storage above volume #1 at 204.50'

Inflow Area = 6.480 ac, 5.37% Impervious, Inflow Depth > 0.78" for 25YR - 24HR event
 Inflow = 1.56 cfs @ 12.66 hrs, Volume= 0.422 af
 Outflow = 1.55 cfs @ 12.66 hrs, Volume= 0.422 af, Atten= 0%, Lag= 0.2 min
 Primary = 1.55 cfs @ 12.66 hrs, Volume= 0.422 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 201.47' @ 12.63 hrs Surf.Area= 3 sf Storage= 2 cf
 Flood Elev= 205.00' Surf.Area= 31 sf Storage= 16 cf

Plug-Flow detention time= 0.0 min calculated for 0.421 af (100% of inflow)
 Center-of-Mass det. time= 0.0 min (950.4 - 950.3)

Volume	Invert	Avail.Storage	Storage Description
#1	200.75'	12 cf	2.00'D x 3.75'H 2' Drop Inlet
#2	204.75'	4 cf	Ponding Area (Irregular) Listed below (Recalc)
		16 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
204.75	7	9.5	0	0	7
205.00	28	18.7	4	4	28

Device	Routing	Invert	Outlet Devices
#1	Primary	200.75'	15.0" Round 15" HDPE N-12 L= 11.5' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 200.75' / 200.40' S= 0.0304 '/' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 1.23 sf
#2	Secondary	204.75'	15.0' long x 4.0' breadth Ponding Outlet Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.67 2.65 2.66 2.66 2.68 2.72 2.73 2.76 2.79 2.88 3.07 3.32

Primary OutFlow Max=1.55 cfs @ 12.66 hrs HW=201.46' TW=201.17' (Dynamic Tailwater)
 ↖1=15" HDPE N-12 (Outlet Controls 1.55 cfs @ 3.10 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=200.75' TW=200.30' (Dynamic Tailwater)
 ↖2=Ponding Outlet (Controls 0.00 cfs)

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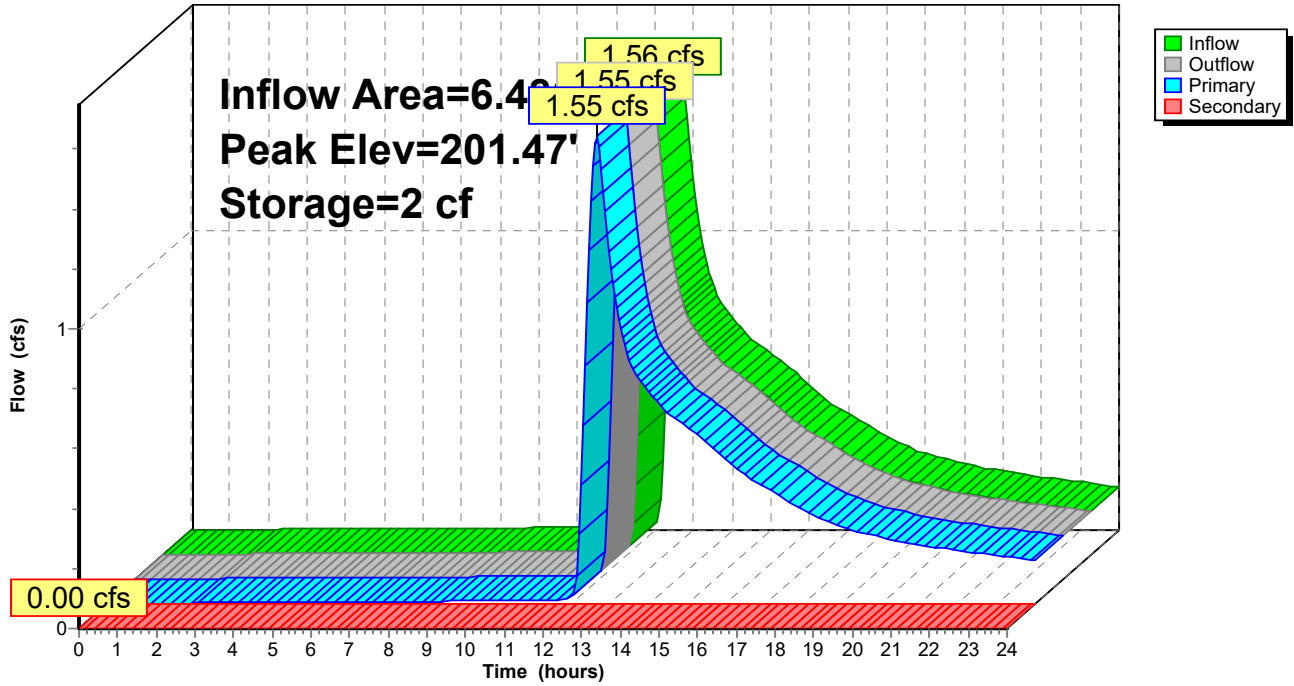
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Pond 1P: Drop Inlet

Hydrograph



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Summary for Pond 2P: Prop. 18" Cross Culvert

Inflow Area = 21.541 ac, 3.27% Impervious, Inflow Depth > 1.10" for 25YR - 24HR event
 Inflow = 8.76 cfs @ 12.94 hrs, Volume= 1.976 af
 Outflow = 8.33 cfs @ 13.08 hrs, Volume= 1.976 af, Atten= 5%, Lag= 8.8 min
 Primary = 8.33 cfs @ 13.08 hrs, Volume= 1.976 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 199.81' @ 13.08 hrs Surf.Area= 3,707 sf Storage= 1,414 cf
 Flood Elev= 201.00' Surf.Area= 5,130 sf Storage= 7,383 cf

Plug-Flow detention time= 0.9 min calculated for 1.976 af (100% of inflow)
 Center-of-Mass det. time= 0.9 min (928.9 - 928.1)

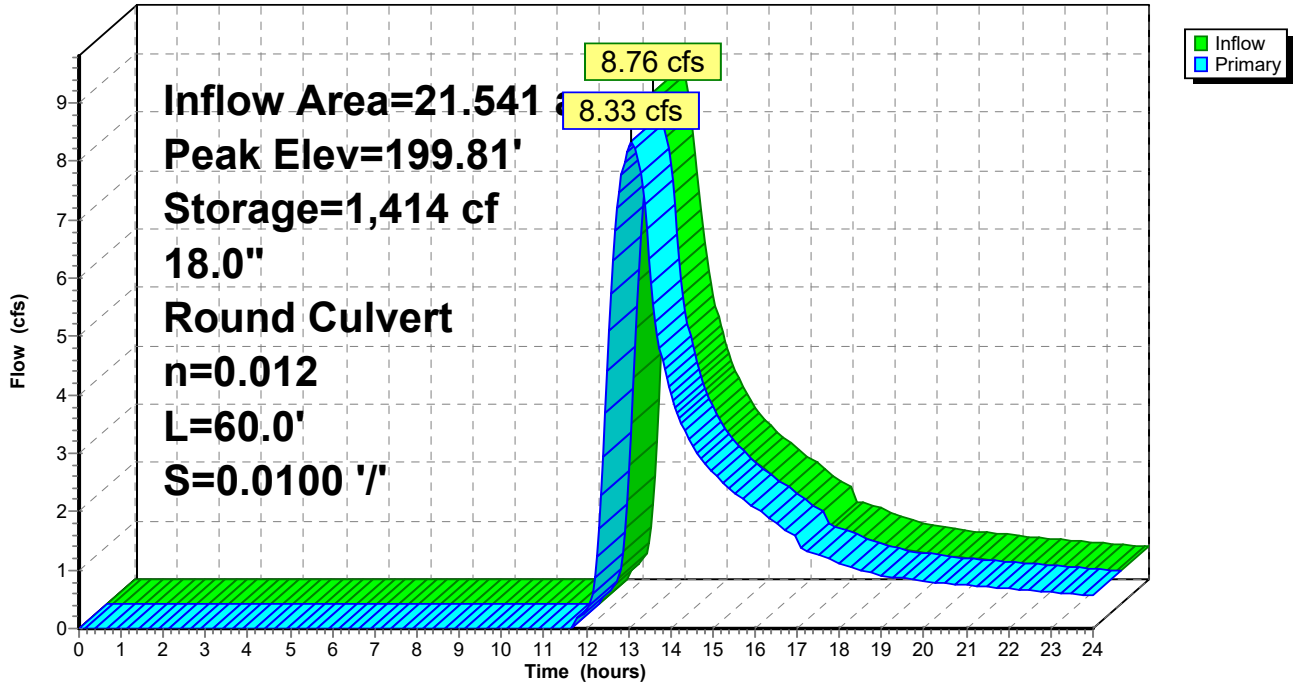
Volume	Invert	Avail.Storage	Storage Description			
#1	198.10'	7,383 cf	Open Water Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
198.10	8	15.0	0	0	8	
198.50	98	58.0	18	18	258	
199.00	235	80.0	81	99	502	
200.00	5,130	630.0	2,154	2,253	31,579	
201.00	5,130	630.0	5,130	7,383	32,209	

Device	Routing	Invert	Outlet Devices
#1	Primary	198.10'	18.0" Round 18" HDPE N-12 L= 60.0' Ke= 0.500 Inlet / Outlet Invert= 198.10' / 197.50' S= 0.0100 ' S Cc= 0.900 n= 0.012, Flow Area= 1.77 sf

Primary OutFlow Max=8.33 cfs @ 13.08 hrs HW=199.81' TW=198.37' (Dynamic Tailwater)
 ↑1=18" HDPE N-12 (Inlet Controls 8.33 cfs @ 4.71 fps)

Pond 2P: Prop. 18" Cross Culvert

Hydrograph



20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 4P: Prop. CB#3

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[80] Warning: Exceeded Pond 10P by 0.02' @ 12.05 hrs (0.33 cfs 0.001 af)

Inflow Area = 7.611 ac, 16.39% Impervious, Inflow Depth > 1.32" for 25YR - 24HR event
 Inflow = 4.46 cfs @ 12.08 hrs, Volume= 0.839 af
 Outflow = 4.46 cfs @ 12.08 hrs, Volume= 0.839 af, Atten= 0%, Lag= 0.3 min
 Primary = 4.46 cfs @ 12.08 hrs, Volume= 0.839 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 201.27' @ 12.20 hrs Surf.Area= 0.000 ac Storage= 0.001 af
 Flood Elev= 202.53' Surf.Area= 0.000 ac Storage= 0.001 af

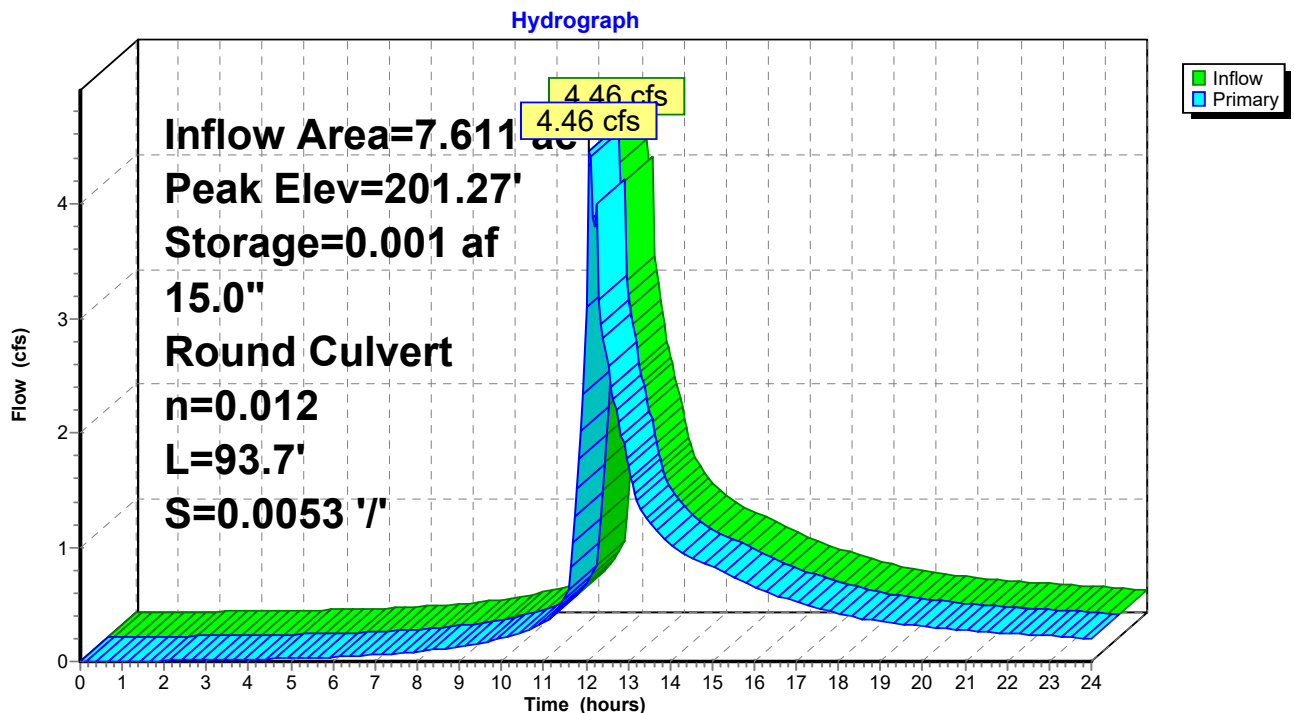
Plug-Flow detention time= 0.2 min calculated for 0.837 af (100% of inflow)
 Center-of-Mass det. time= 0.2 min (869.0 - 868.8)

Volume	Invert	Avail.Storage	Storage Description
#1	199.20'	0.001 af	4.00'D x 3.33'H Basin

Device	Routing	Invert	Outlet Devices
#1	Primary	199.20'	15.0" Round 15" HDPE N-12 L= 93.7' Ke= 0.500 Inlet / Outlet Invert= 199.20' / 198.70' S= 0.0053 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=4.07 cfs @ 12.08 hrs HW=201.05' TW=200.47' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Outlet Controls 4.07 cfs @ 3.32 fps)

Pond 4P: Prop. CB#3



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 6P: Inlet Depression

Inflow Area = 0.586 ac, 84.67% Impervious, Inflow Depth > 4.60" for 25YR - 24HR event
 Inflow = 2.97 cfs @ 12.09 hrs, Volume= 0.224 af
 Outflow = 2.43 cfs @ 12.24 hrs, Volume= 0.224 af, Atten= 18%, Lag= 8.9 min
 Primary = 2.43 cfs @ 12.24 hrs, Volume= 0.224 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 201.51' @ 12.18 hrs Surf.Area= 650 sf Storage= 516 cf

Plug-Flow detention time= 4.0 min calculated for 0.224 af (100% of inflow)
 Center-of-Mass det. time= 3.2 min (791.7 - 788.5)

Volume	Invert	Avail.Storage	Storage Description			
#1	200.00'	915 cf	Open Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
200.00	151	124.0	0	0	151	
201.00	381	173.0	257	257	1,319	
202.00	981	162.0	658	915	1,656	

Device	Routing	Invert	Outlet Devices	
#1	Primary	200.00'	15.0" Round 15" HDPE N-12 L= 30.0' Ke= 0.500 Inlet / Outlet Invert= 200.00' / 199.30' S= 0.0233 ' S Cc= 0.900 n= 0.012, Flow Area= 1.23 sf	

Primary OutFlow Max=2.28 cfs @ 12.24 hrs HW=201.33' TW=201.18' (Dynamic Tailwater)
 ↑1=15" HDPE N-12 (Inlet Controls 2.28 cfs @ 1.85 fps)

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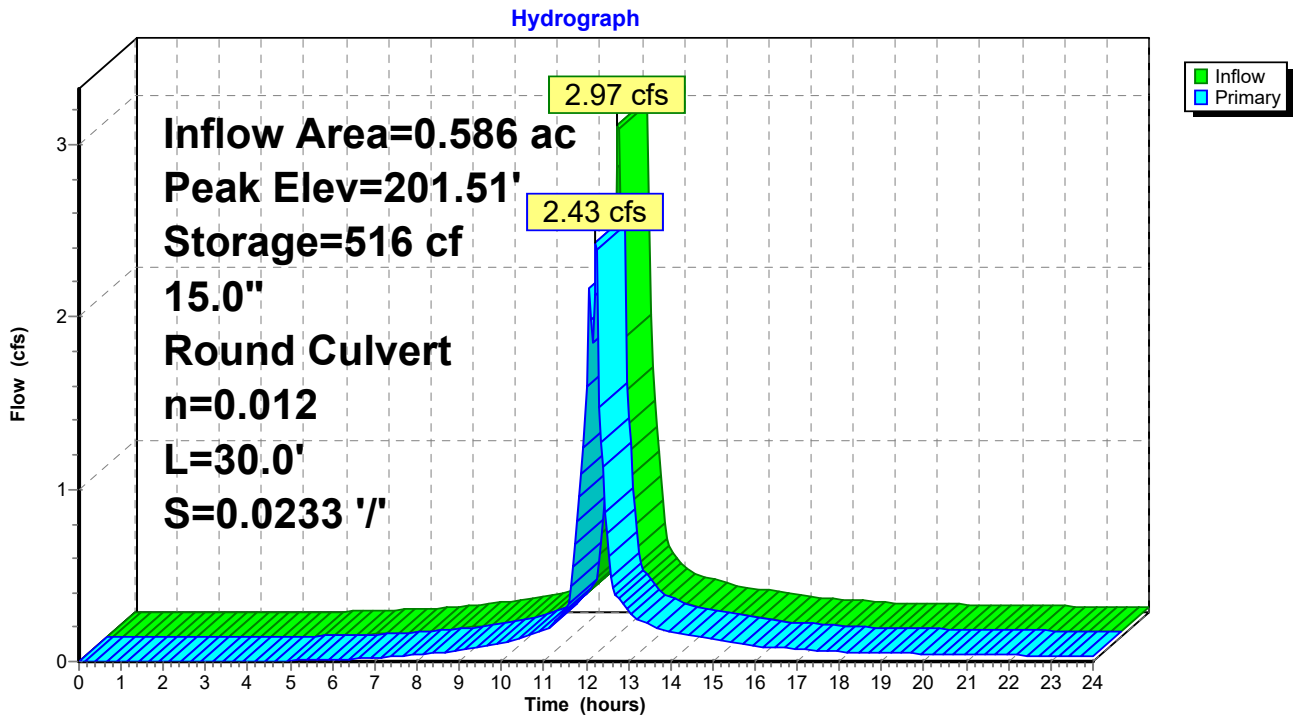
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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Pond 6P: Inlet Depression



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 8P: 24" Cross Culvert

[62] Hint: Exceeded Reach 11R OUTLET depth by 0.26' @ 13.05 hrs

Inflow Area = 32.293 ac, 8.29% Impervious, Inflow Depth > 1.13" for 25YR - 24HR event
 Inflow = 10.68 cfs @ 12.96 hrs, Volume= 3.048 af
 Outflow = 10.66 cfs @ 13.01 hrs, Volume= 3.047 af, Atten= 0%, Lag= 3.4 min
 Primary = 10.66 cfs @ 13.01 hrs, Volume= 3.047 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 198.37' @ 13.01 hrs Surf.Area= 1,794 sf Storage= 1,119 cf
 Flood Elev= 199.55' Surf.Area= 3,482 sf Storage= 4,655 cf

Plug-Flow detention time= 1.1 min calculated for 3.047 af (100% of inflow)
 Center-of-Mass det. time= 1.0 min (929.8 - 928.8)

Volume	Invert	Avail.Storage	Storage Description			
#1	196.55'	6,222 cf	Open Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
196.55	10	10.0	0	0	10	
197.00	184	97.0	36	36	751	
198.00	1,049	166.0	557	593	2,201	
199.00	3,482	329.0	2,147	2,740	8,627	
200.00	3,482	329.0	3,482	6,222	8,956	

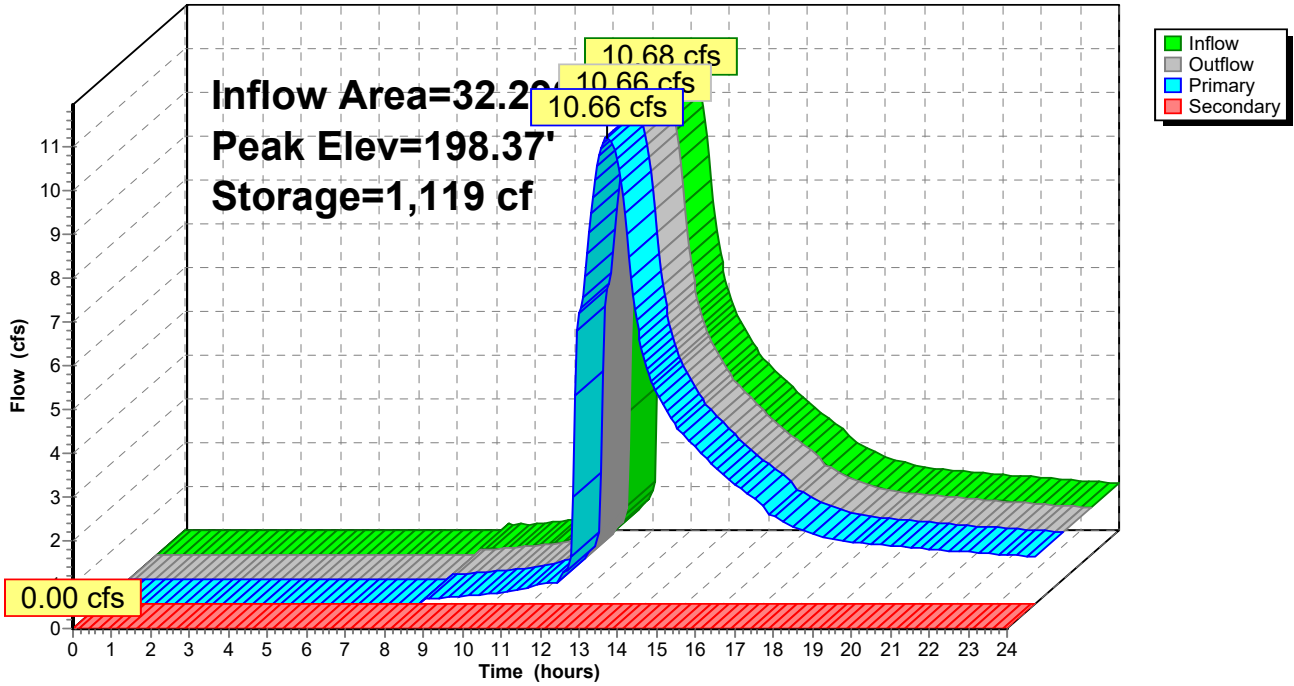
Device	Routing	Invert	Outlet Devices							
#1	Primary	196.55'	24.0" Round 24" HDPE N-12 L= 21.6' Ke= 0.500 Inlet / Outlet Invert= 196.55' / 196.44' S= 0.0051 '/' Cc= 0.900 n= 0.012, Flow Area= 3.14 sf							
#2	Secondary	199.55'	100.0' long x 10.0' breadth Flow Over The Driveway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64							

Primary OutFlow Max=10.65 cfs @ 13.01 hrs HW=198.37' TW=0.00' (Dynamic Tailwater)
 ↗1=24" HDPE N-12 (Barrel Controls 10.65 cfs @ 4.65 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=196.55' TW=0.00' (Dynamic Tailwater)
 ↗2=Flow Over The Driveway (Controls 0.00 cfs)

Pond 8P: 24" Cross Culvert

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 10P: EX. CB#10

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[80] Warning: Exceeded Pond C30P by 0.18' @ 12.15 hrs (2.21 cfs 0.024 af)

Inflow Area = 6.817 ac, 7.97% Impervious, Inflow Depth > 0.91" for 25YR - 24HR event
 Inflow = 1.74 cfs @ 12.64 hrs, Volume= 0.517 af
 Outflow = 1.75 cfs @ 12.64 hrs, Volume= 0.517 af, Atten= 0%, Lag= 0.5 min
 Primary = 1.75 cfs @ 12.64 hrs, Volume= 0.517 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 201.46' @ 12.17 hrs Surf.Area= 13 sf Storage= 17 cf
 Flood Elev= 204.00' Surf.Area= 250 sf Storage= 73 cf

Plug-Flow detention time= 0.2 min calculated for 0.517 af (100% of inflow)
 Center-of-Mass det. time= 0.1 min (925.5 - 925.4)

Volume	Invert	Avail.Storage	Storage Description
#1	200.07'	46 cf	4.00'D x 3.68'H Basin
#2	203.75'	264 cf	Open Storage (Irregular) Listed below (Recalc)
		310 cf	Total Available Storage

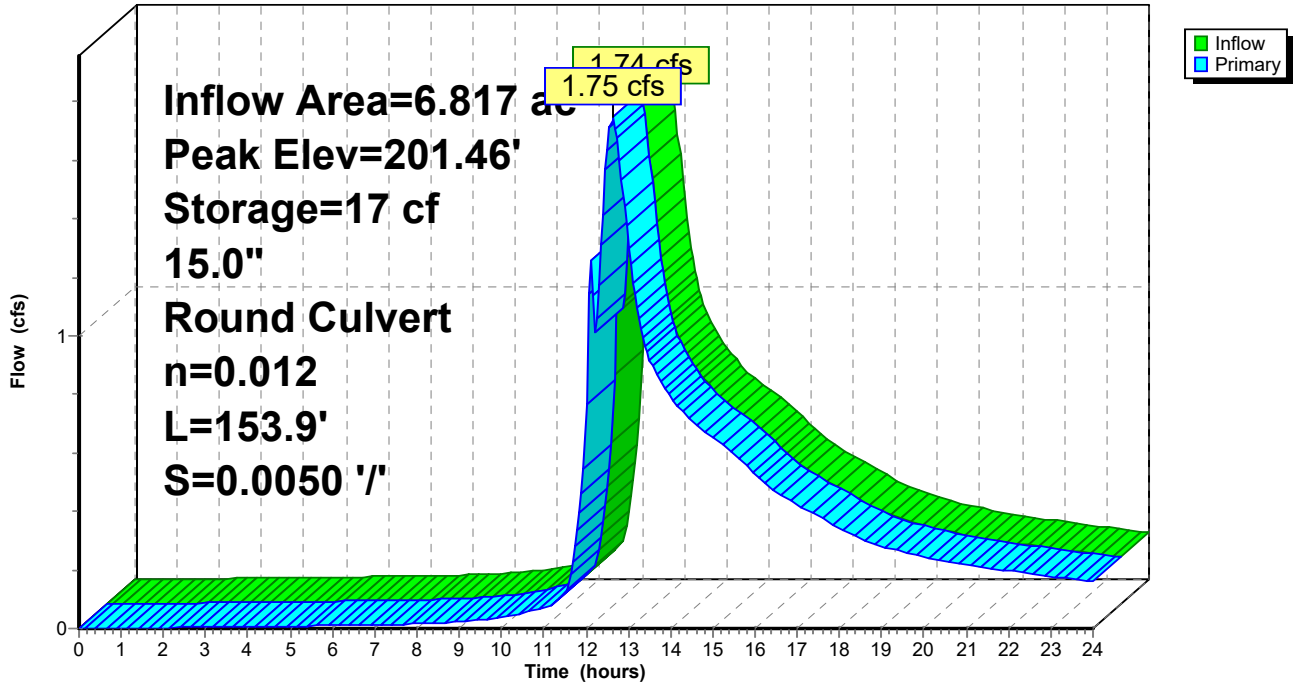
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
203.75	20	20.0	0	0	20
204.00	237	94.0	27	27	691
205.00	237	94.0	237	264	785

Device	Routing	Invert	Outlet Devices
#1	Primary	200.07'	15.0" Round 15" HDPE N-12 L= 153.9' Ke= 0.500 Inlet / Outlet Invert= 200.07' / 199.30' S= 0.0050 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=1.77 cfs @ 12.64 hrs HW=200.97' TW=200.52' (Dynamic Tailwater)
 ←1=15" HDPE N-12 (Outlet Controls 1.77 cfs @ 2.60 fps)

Pond 10P: EX. CB#10

Hydrograph



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Summary for Pond 12P: Ex. CB#2

Inflow Area = 7.712 ac, 17.48% Impervious, Inflow Depth > 1.38" for 25YR - 24HR event
 Inflow = 5.03 cfs @ 12.08 hrs, Volume= 0.886 af
 Outflow = 5.01 cfs @ 12.08 hrs, Volume= 0.886 af, Atten= 0%, Lag= 0.1 min
 Primary = 5.01 cfs @ 12.08 hrs, Volume= 0.886 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 200.74' @ 12.23 hrs Surf.Area= 0.000 ac Storage= 0.001 af
 Flood Elev= 203.38' Surf.Area= 0.000 ac Storage= 0.001 af

Plug-Flow detention time= 0.3 min calculated for 0.884 af (100% of inflow)
 Center-of-Mass det. time= 0.3 min (862.7 - 862.4)

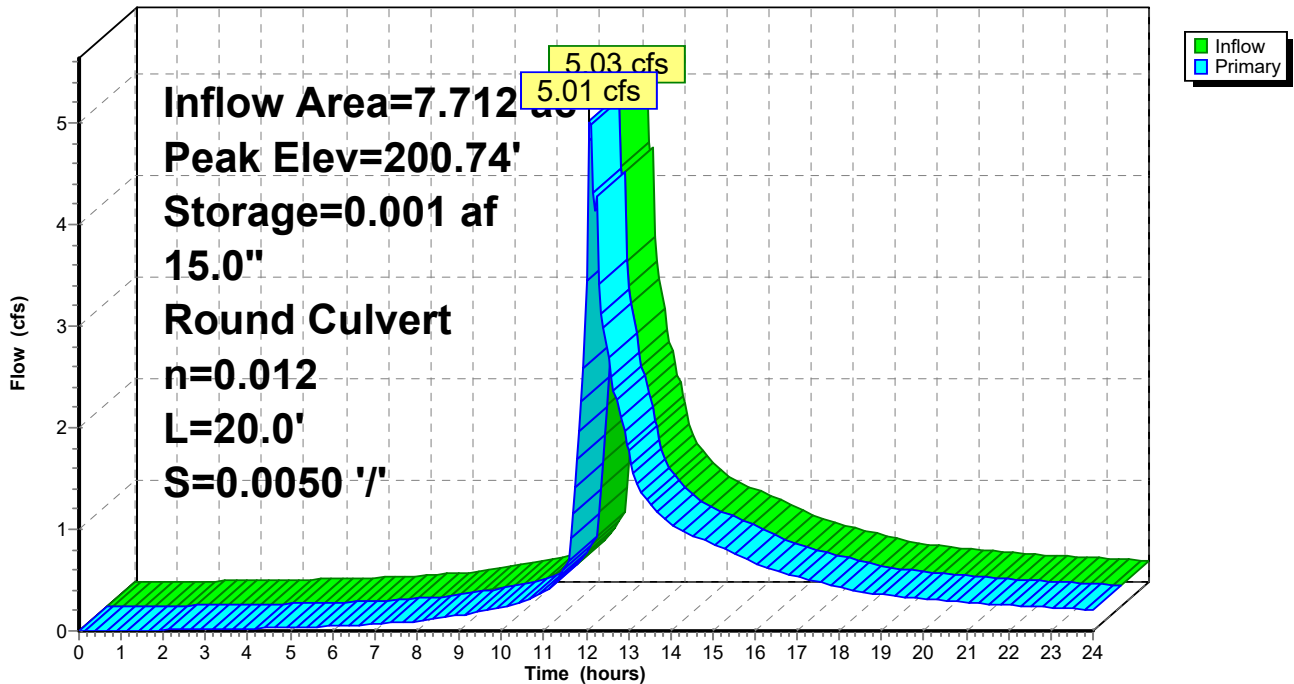
Volume	Invert	Avail.Storage	Storage Description
#1	198.60'	0.001 af	4.00'D x 4.78'H Basin

Device	Routing	Invert	Outlet Devices
#1	Primary	198.60'	15.0" Round 15" HDPE N-12 L= 20.0' Ke= 0.500 Inlet / Outlet Invert= 198.60' / 198.50' S= 0.0050 1/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=4.98 cfs @ 12.08 hrs HW=200.50' TW=199.79' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Inlet Controls 4.98 cfs @ 4.05 fps)

Pond 12P: Ex. CB#2

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 13P: Infiltration Pond

Inflow Area = 0.684 ac, 30.66% Impervious, Inflow Depth > 1.59" for 25YR - 24HR event
 Inflow = 0.92 cfs @ 12.20 hrs, Volume= 0.090 af
 Outflow = 0.31 cfs @ 12.64 hrs, Volume= 0.081 af, Atten= 66%, Lag= 26.8 min
 Discarded = 0.07 cfs @ 12.64 hrs, Volume= 0.058 af
 Primary = 0.24 cfs @ 12.64 hrs, Volume= 0.023 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 203.42' @ 12.64 hrs Surf.Area= 4,162 sf Storage= 1,247 cf
 Flood Elev= 203.50' Surf.Area= 4,691 sf Storage= 1,606 cf

Plug-Flow detention time= 155.0 min calculated for 0.081 af (90% of inflow)
 Center-of-Mass det. time= 107.0 min (984.0 - 876.9)

Volume	Invert	Avail.Storage	Storage Description			
#1	203.00'	3,001 cf	Open Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
203.00	1,934	235.0	0	0	1,934	
203.75	6,520	429.0	3,001	3,001	12,188	

Device	Routing	Invert	Outlet Devices										
#1	Discarded	203.00'	0.710 in/hr Exfiltration over Surface area										
#2	Primary	203.35'	5.0' long x 1.0' breadth Broad-Crested Rectangular Weir										
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00										
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32										

Discarded OutFlow Max=0.07 cfs @ 12.64 hrs HW=203.42' (Free Discharge)
 ↑1=Exfiltration (Exfiltration Controls 0.07 cfs)

Primary OutFlow Max=0.24 cfs @ 12.64 hrs HW=203.42' TW=202.09' (Dynamic Tailwater)
 ↑2=Broad-Crested Rectangular Weir (Weir Controls 0.24 cfs @ 0.71 fps)

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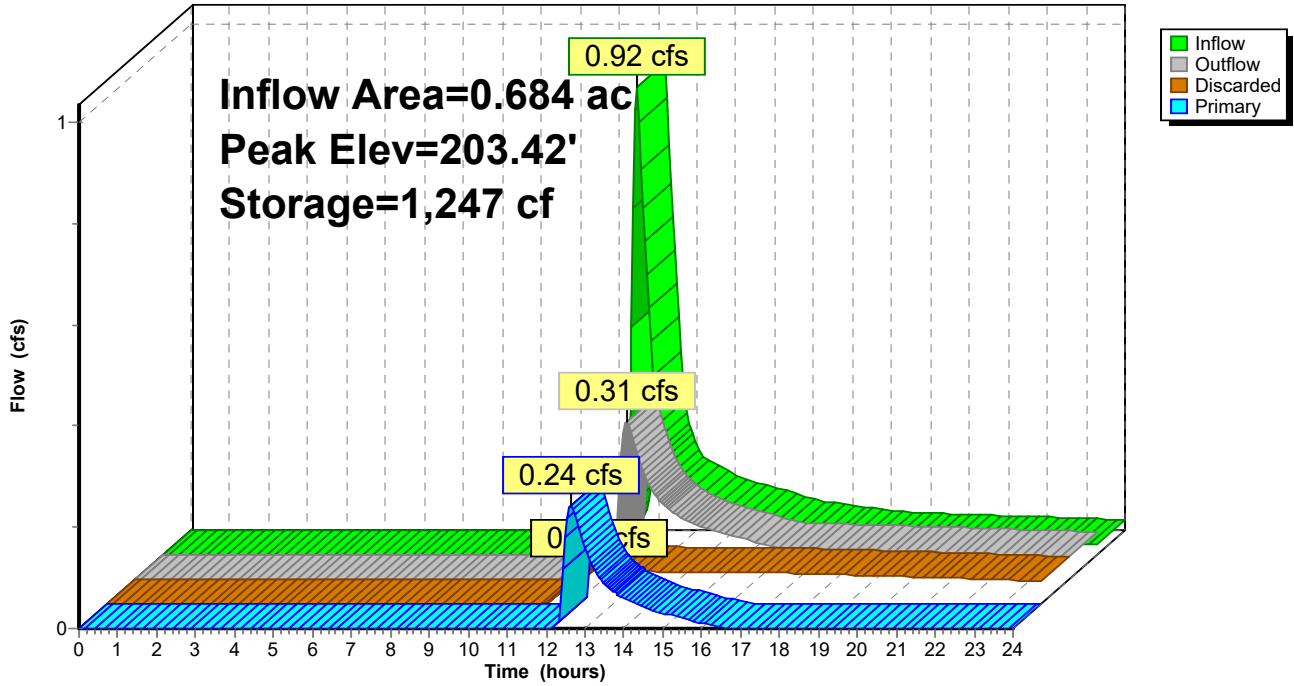
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Pond 13P: Infiltration Pond

Hydrograph



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Summary for Pond 14P: Ex. 15" Cross Culvert

Inflow Area = 0.861 ac, 36.57% Impervious, Inflow Depth > 0.95" for 25YR - 24HR event
 Inflow = 0.62 cfs @ 12.09 hrs, Volume= 0.068 af
 Outflow = 0.30 cfs @ 12.11 hrs, Volume= 0.068 af, Atten= 52%, Lag= 1.2 min
 Discarded = 0.02 cfs @ 12.93 hrs, Volume= 0.015 af
 Primary = 0.28 cfs @ 12.11 hrs, Volume= 0.053 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 202.12' @ 12.93 hrs Surf.Area= 1,485 sf Storage= 651 cf
 Flood Elev= 203.00' Surf.Area= 1,948 sf Storage= 2,162 cf

Plug-Flow detention time= 35.5 min calculated for 0.068 af (100% of inflow)
 Center-of-Mass det. time= 35.5 min (857.4 - 822.0)

Volume	Invert	Avail.Storage	Storage Description		
#1	201.50'	2,162 cf	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
201.50	560	120.0	0	0	560
202.00	1,428	163.0	480	480	1,531
203.00	1,948	182.0	1,681	2,162	2,080

Device	Routing	Invert	Outlet Devices
#1	Primary	201.50'	15.0" Round 15" HDPE N-12 L= 50.0' Ke= 0.500 Inlet / Outlet Invert= 201.50' / 201.00' S= 0.0100 ' / ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Discarded	201.50'	0.710 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.02 cfs @ 12.93 hrs HW=202.12' (Free Discharge)
 ↳ **2=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.29 cfs @ 12.11 hrs HW=201.82' TW=201.62' (Dynamic Tailwater)
 ↳ **1=15" HDPE N-12** (Outlet Controls 0.29 cfs @ 1.74 fps)

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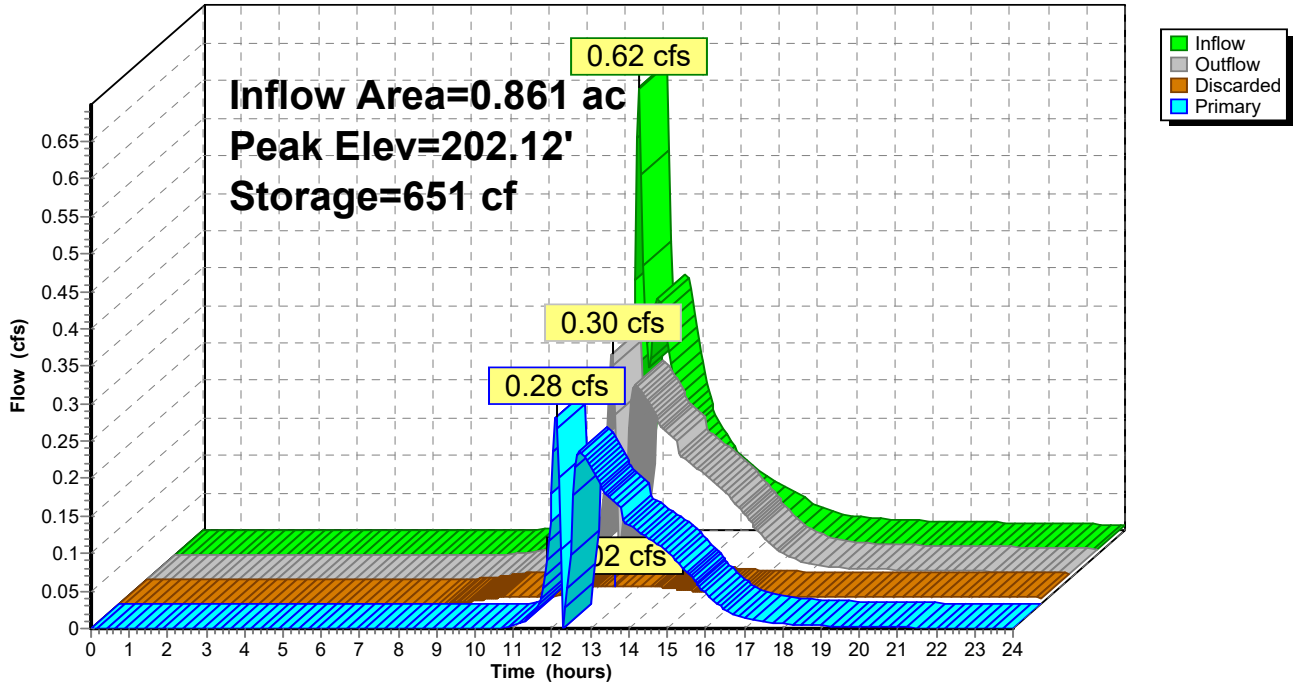
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Pond 14P: Ex. 15" Cross Culvert

Hydrograph



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Summary for Pond 16P: Ex. 12" CMP

[62] Hint: Exceeded Reach 65R OUTLET depth by 0.98' @ 12.85 hrs

Inflow Area = 4.891 ac, 26.20% Impervious, Inflow Depth > 1.52" for 25YR - 24HR event
 Inflow = 2.80 cfs @ 12.50 hrs, Volume= 0.618 af
 Outflow = 2.05 cfs @ 12.81 hrs, Volume= 0.617 af, Atten= 27%, Lag= 18.5 min
 Primary = 2.05 cfs @ 12.81 hrs, Volume= 0.617 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 204.38' @ 12.81 hrs Surf.Area= 5,490 sf Storage= 1,402 cf

Plug-Flow detention time= 5.5 min calculated for 0.617 af (100% of inflow)
 Center-of-Mass det. time= 4.6 min (945.6 - 941.0)

Volume	Invert	Avail.Storage	Storage Description			
#1	203.25'	9,229 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
203.25	50	30.0	0	0	50	
204.00	962	127.1	308	308	1,265	
205.00	21,278	680.9	8,921	9,229	36,876	

Device	Routing	Invert	Outlet Devices									
#1	Primary	204.75'	50.0' long x 15.0' breadth Broad-Crested Rectangular Weir									
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60									
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63									
#2	Primary	203.25'	12.0" Round 12" CMP									
			L= 20.0' CMP, projecting, no headwall, Ke= 0.900									
			Inlet / Outlet Invert= 203.25' / 203.05' S= 0.0100 1/ S= 0.0100 1/ Cc= 0.900									
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf									

Primary OutFlow Max=2.05 cfs @ 12.81 hrs HW=204.37' TW=0.00' (Dynamic Tailwater)

- 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)
- 2=12" CMP (Barrel Controls 2.05 cfs @ 2.90 fps)

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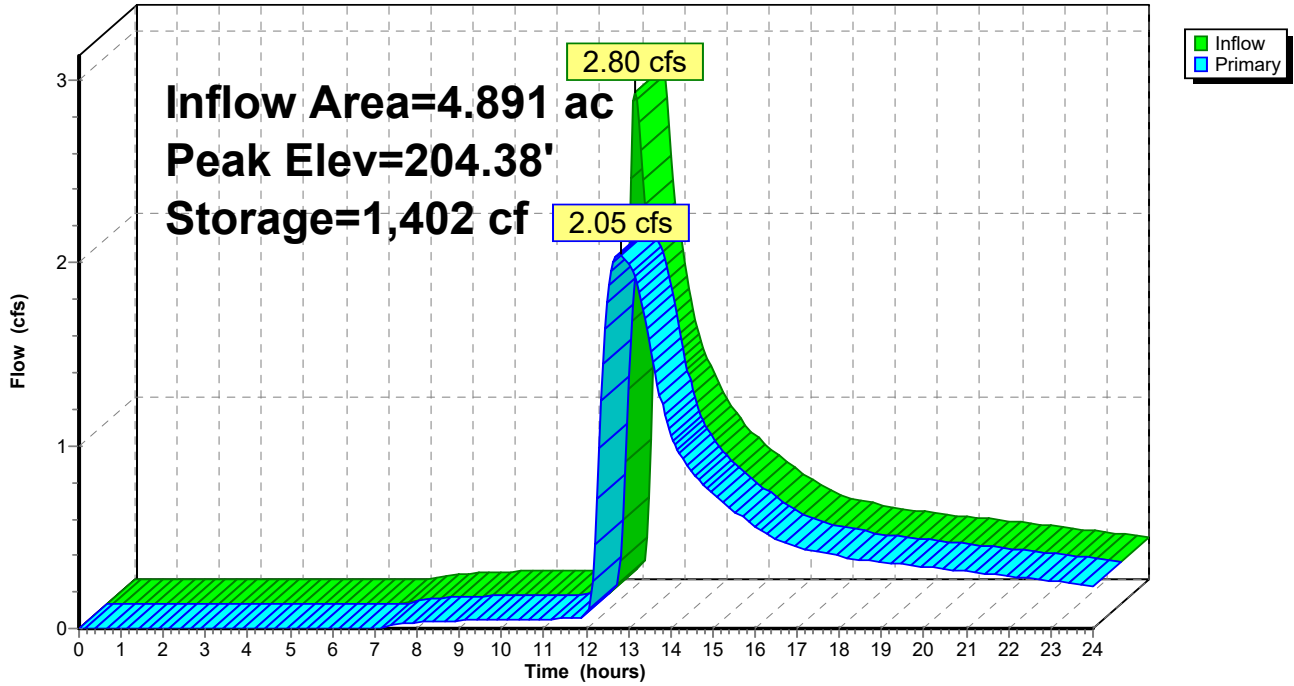
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Pond 16P: Ex. 12" CMP

Hydrograph



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Summary for Pond 17P: Ex. 18" HDPE N-12

[63] Warning: Exceeded Reach 50R INLET depth by 0.29' @ 12.55 hrs

Inflow Area = 11.762 ac, 10.97% Impervious, Inflow Depth > 1.42" for 25YR - 24HR event
 Inflow = 4.24 cfs @ 12.47 hrs, Volume= 1.392 af
 Outflow = 4.20 cfs @ 12.52 hrs, Volume= 1.391 af, Atten= 1%, Lag= 2.7 min
 Primary = 4.20 cfs @ 12.52 hrs, Volume= 1.391 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 203.44' @ 12.52 hrs Surf.Area= 914 sf Storage= 402 cf
 Flood Elev= 206.00' Surf.Area= 3,976 sf Storage= 4,672 cf

Plug-Flow detention time= 1.2 min calculated for 1.391 af (100% of inflow)
 Center-of-Mass det. time= 0.8 min (992.4 - 991.6)

Volume	Invert	Avail.Storage	Storage Description
#1	202.25'	4,672 cf	Open Water Storage (Irregular) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
202.25	58	31.0	0	0	58
203.00	344	126.0	136	136	1,246
204.00	2,035	75.0	1,072	1,208	2,068
204.50	3,976	367.9	1,476	2,684	12,392
205.00	3,976	367.9	1,988	4,672	12,576

Device	Routing	Invert	Outlet Devices
#1	Secondary	204.50'	15.0' long x 14.0' breadth Flow Over Roadway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.64 2.67 2.70 2.65 2.64 2.65 2.65 2.63
#2	Primary	202.25'	18.0" Round 18" HDPE N-12 L= 37.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 202.25' / 202.00' S= 0.0068 1' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 1.77 sf

Primary OutFlow Max=4.18 cfs @ 12.52 hrs HW=203.44' TW=0.00' (Dynamic Tailwater)
 ↳2=18" HDPE N-12 (Barrel Controls 4.18 cfs @ 3.83 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=202.25' TW=0.00' (Dynamic Tailwater)
 ↳1=Flow Over Roadway (Controls 0.00 cfs)

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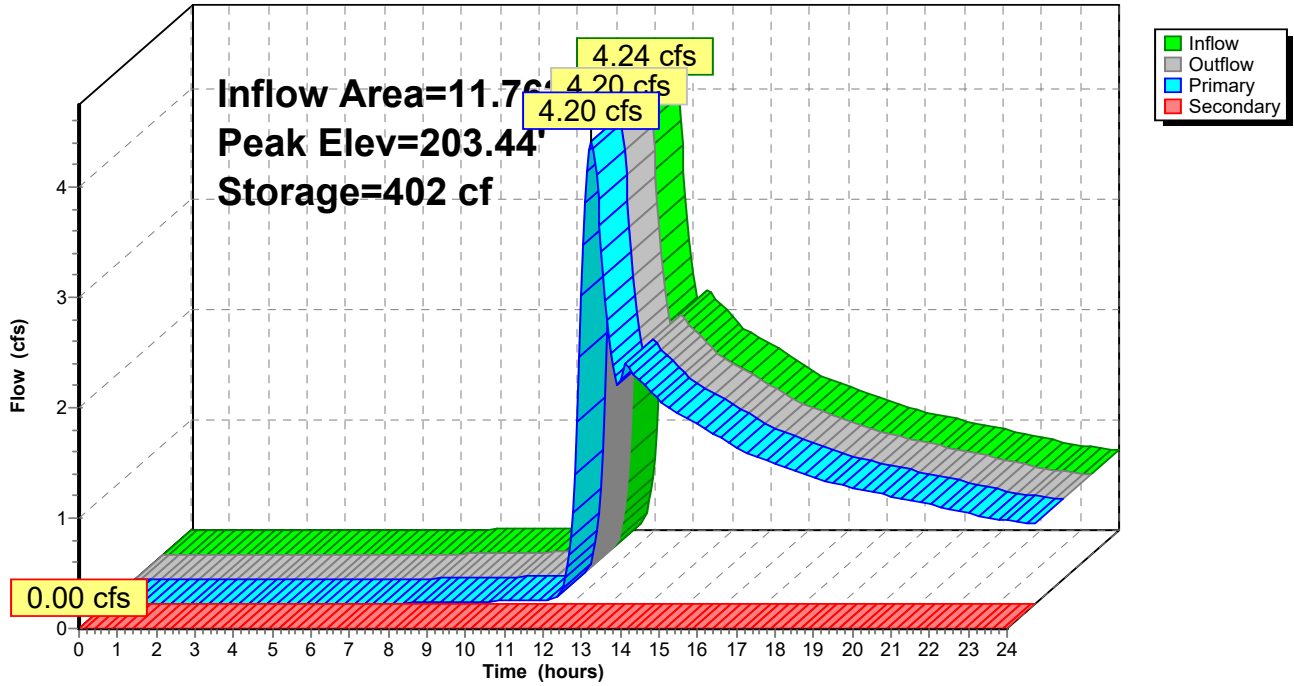
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Pond 17P: Ex. 18" HDPE N-12

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 18P: Box Culvert

Inflow Area = 13.189 ac, 0.33% Impervious, Inflow Depth > 1.57" for 25YR - 24HR event
 Inflow = 10.32 cfs @ 12.36 hrs, Volume= 1.724 af
 Outflow = 10.32 cfs @ 12.37 hrs, Volume= 1.724 af, Atten= 0%, Lag= 0.5 min
 Primary = 10.32 cfs @ 12.37 hrs, Volume= 1.724 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 191.50' @ 12.37 hrs Surf.Area= 377 sf Storage= 148 cf

Plug-Flow detention time= 0.2 min calculated for 1.721 af (100% of inflow)
 Center-of-Mass det. time= 0.2 min (914.2 - 914.0)

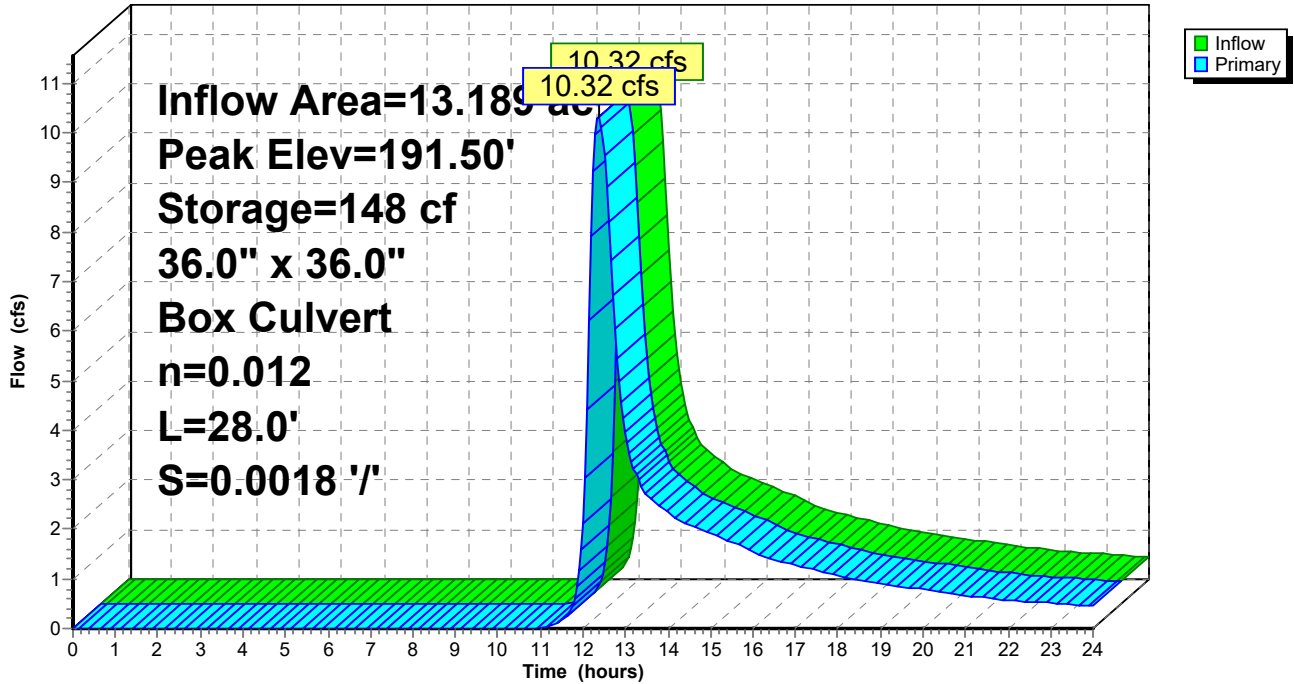
Volume	Invert	Avail.Storage	Storage Description		
#1	190.25'	56,817 cf	Open Water Storage (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
190.25	50	30.0	0	0	50
191.00	72	54.2	46	46	215
192.00	912	215.6	413	459	3,683
193.00	2,290	273.4	1,549	2,008	5,946
194.00	4,070	334.6	3,138	5,146	8,922
195.00	6,222	483.3	5,108	10,254	18,609
196.00	8,396	606.1	7,282	17,536	29,269
197.00	11,534	890.2	9,924	27,459	63,105
198.00	15,764	977.3	13,594	41,053	76,083
199.00	15,764	977.3	15,764	56,817	77,060

Device	Routing	Invert	Outlet Devices
#1	Primary	190.25'	36.0" W x 36.0" H Box Box Culvert N-12 L= 28.0' Ke= 0.500 Inlet / Outlet Invert= 190.25' / 190.20' S= 0.0018 '/' Cc= 0.900 n= 0.012, Flow Area= 9.00 sf

Primary OutFlow Max=10.28 cfs @ 12.37 hrs HW=191.50' TW=0.00' (Dynamic Tailwater)
 ↑**1=Box Culvert N-12** (Barrel Controls 10.28 cfs @ 3.66 fps)

Pond 18P: Box Culvert

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 19P: Box Culvert

Inflow Area = 15.859 ac, 0.00% Impervious, Inflow Depth > 1.34" for 25YR - 24HR event
 Inflow = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af
 Outflow = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af, Atten= 0%, Lag= 0.1 min
 Primary = 9.97 cfs @ 12.72 hrs, Volume= 1.775 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 184.15' @ 12.72 hrs Surf.Area= 49 sf Storage= 24 cf

Plug-Flow detention time= 0.0 min calculated for 1.771 af (100% of inflow)
 Center-of-Mass det. time= 0.0 min (911.5 - 911.4)

Volume	Invert	Avail.Storage	Storage Description			
#1	182.69'	612 cf	Open Water Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
182.69	1	5.1	0	0	1	
184.00	33	33.5	17	17	92	
185.00	195	111.6	103	120	997	
186.00	870	252.1	492	612	5,067	

Device	Routing	Invert	Outlet Devices			
#1	Primary	183.13'	36.0" W x 36.0" H Box Box Culvert N-12 L= 52.0' Ke= 0.500 Inlet / Outlet Invert= 182.69' / 183.13' S= -0.0085 '/' Cc= 0.900 n= 0.012, Flow Area= 9.00 sf			

Primary OutFlow Max=9.94 cfs @ 12.72 hrs HW=184.15' TW=0.00' (Dynamic Tailwater)
 ↑1=Box Culvert N-12 (Inlet Controls 9.94 cfs @ 3.24 fps)

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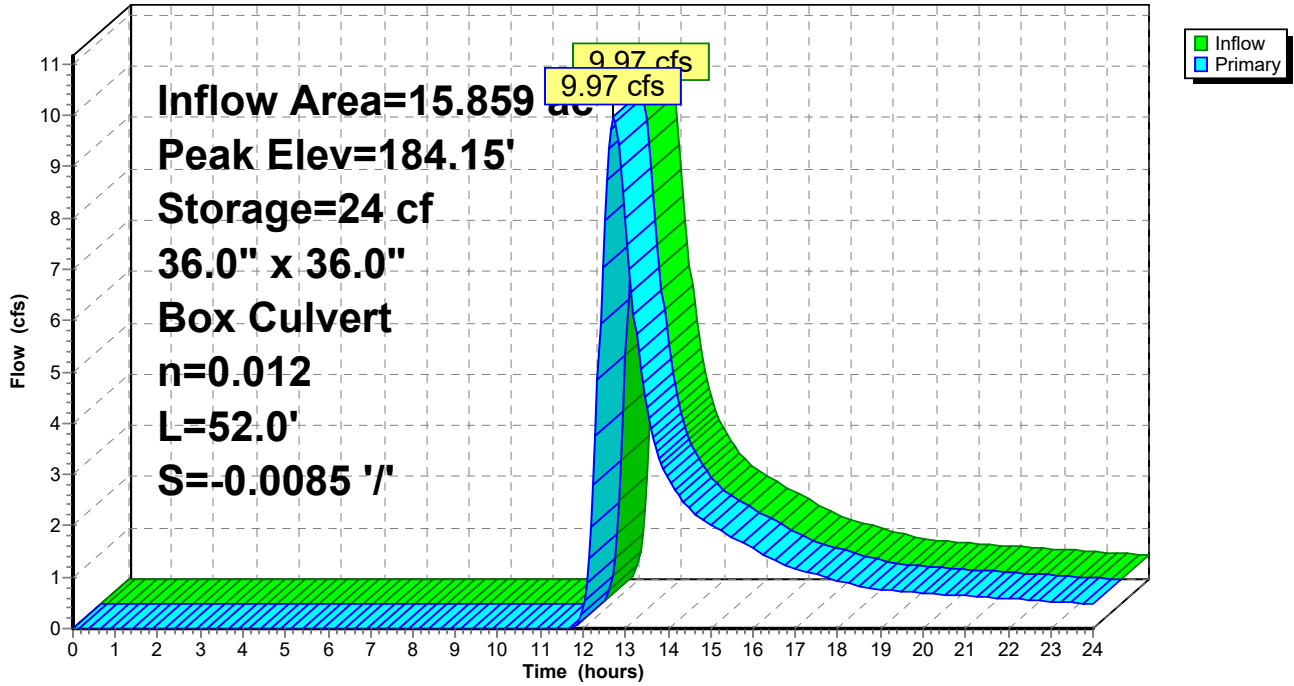
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Pond 19P: Box Culvert

Hydrograph



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Summary for Pond 47P: Inlet Sump High Point Drive

Inflow Area = 2.193 ac, 3.02% Impervious, Inflow Depth > 1.43" for 25YR - 24HR event
 Inflow = 1.95 cfs @ 12.42 hrs, Volume= 0.261 af
 Outflow = 1.95 cfs @ 12.43 hrs, Volume= 0.261 af, Atten= 0%, Lag= 0.7 min
 Primary = 1.95 cfs @ 12.43 hrs, Volume= 0.261 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 237.44' @ 12.43 hrs Surf.Area= 195 sf Storage= 64 cf
 Flood Elev= 238.50' Surf.Area= 831 sf Storage= 571 cf

Plug-Flow detention time= 0.6 min calculated for 0.260 af (100% of inflow)
 Center-of-Mass det. time= 0.4 min (893.8 - 893.4)

Volume	Invert	Avail.Storage	Storage Description			
#1	236.75'	571 cf	Ponding Area (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
236.75	27	29.5	0	0	27	
237.00	61	36.0	11	11	62	
238.00	479	219.3	237	248	3,788	
238.50	831	239.3	323	571	4,527	

Device	Routing	Invert	Outlet Devices
#1	Primary	236.75'	15.0" Round 15" HDPE N-12 L= 23.0' Ke= 0.500 Inlet / Outlet Invert= 236.75' / 235.35' S= 0.0609 ' S= 0.0609 ' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=1.94 cfs @ 12.43 hrs HW=237.43' TW=235.99' (Dynamic Tailwater)
 ↑1=15" HDPE N-12 (Inlet Controls 1.94 cfs @ 2.82 fps)

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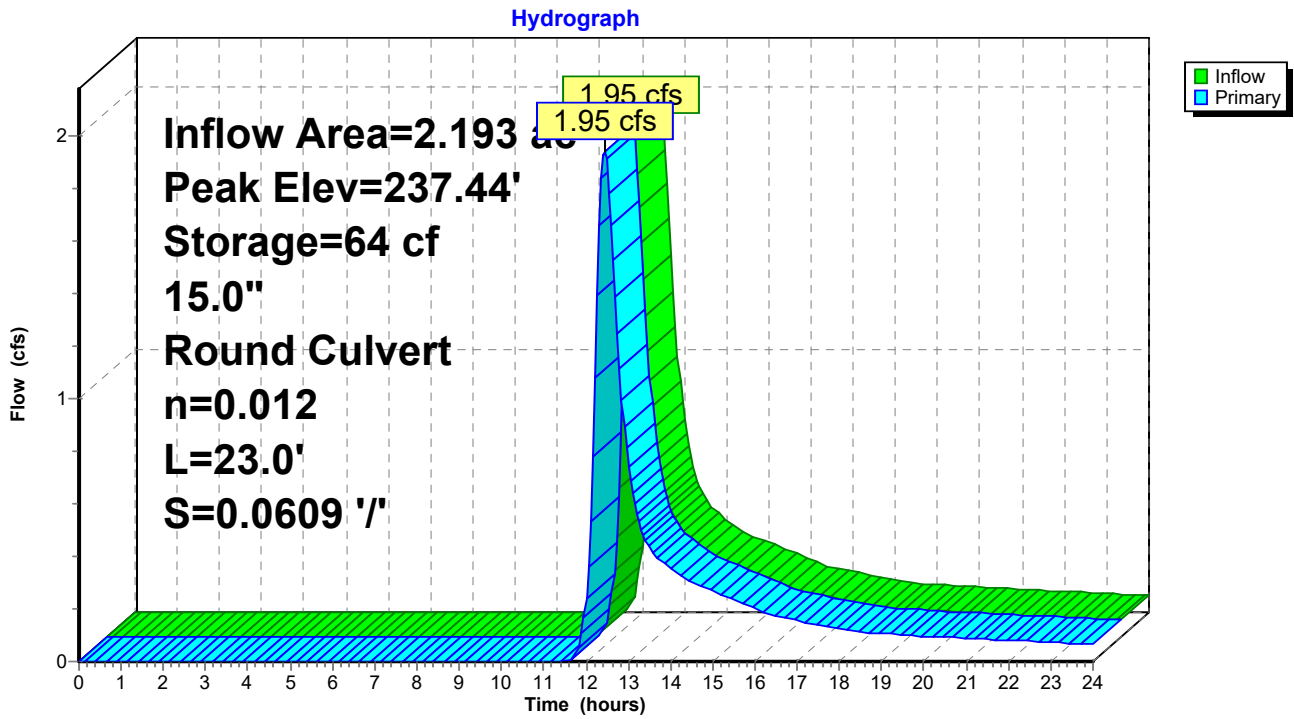
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Pond 47P: Inlet Sump High Point Drive



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 48P: High Point Drive Cul-de Sac

Inflow Area = 0.173 ac, 77.93% Impervious, Inflow Depth > 4.82" for 25YR - 24HR event
 Inflow = 0.90 cfs @ 12.09 hrs, Volume= 0.069 af
 Outflow = 0.84 cfs @ 12.12 hrs, Volume= 0.069 af, Atten= 7%, Lag= 2.0 min
 Primary = 0.84 cfs @ 12.12 hrs, Volume= 0.069 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 236.43' @ 12.12 hrs Surf.Area= 466 sf Storage= 180 cf
 Flood Elev= 239.00' Surf.Area= 1,432 sf Storage= 2,384 cf

Plug-Flow detention time= 11.1 min calculated for 0.069 af (99% of inflow)
 Center-of-Mass det. time= 7.8 min (789.1 - 781.3)

Volume	Invert	Avail.Storage	Storage Description			
#1	236.00'	2,384 cf	Ponding Area (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
236.00	372	68.2	0	0	372	
237.00	606	87.2	484	484	619	
238.00	896	106.2	746	1,231	927	
239.00	1,432	134.5	1,154	2,384	1,483	

Device	Routing	Invert	Outlet Devices
#1	Primary	236.00'	15.0" Round 15" HDPE N-12 L= 50.0' Ke= 0.500 Inlet / Outlet Invert= 236.00' / 235.35' S= 0.0130 ' /' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.82 cfs @ 12.12 hrs HW=236.42' TW=228.76' (Dynamic Tailwater)
 ↑1=15" HDPE N-12 (Inlet Controls 0.82 cfs @ 2.22 fps)

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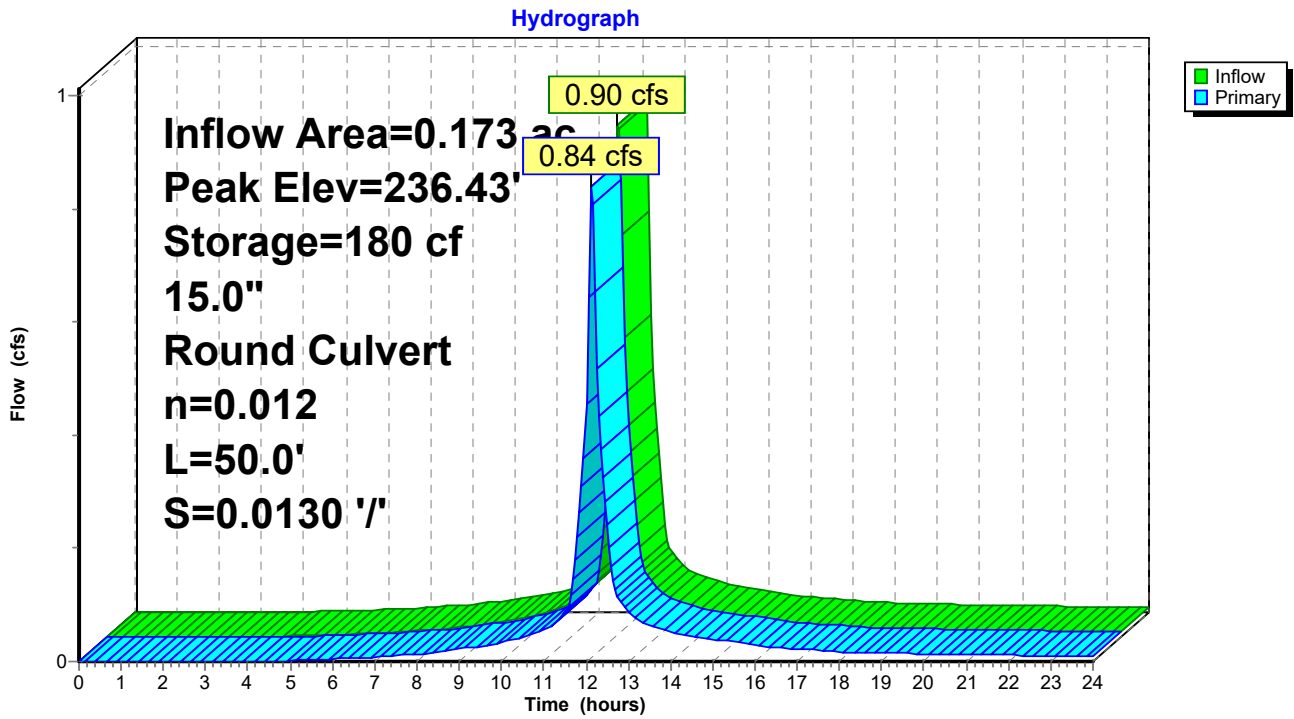
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Pond 48P: High Point Drive Cul-de Sac



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 49P: Community Drive Cul-de Sac

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=10)

Inflow Area = 0.250 ac, 69.81% Impervious, Inflow Depth > 4.49" for 25YR - 24HR event
 Inflow = 1.24 cfs @ 12.09 hrs, Volume= 0.093 af
 Outflow = 0.99 cfs @ 12.09 hrs, Volume= 0.089 af, Atten= 21%, Lag= 0.2 min
 Primary = 0.99 cfs @ 12.09 hrs, Volume= 0.089 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 218.85' @ 14.00 hrs Surf.Area= 499 sf Storage= 636 cf
 Flood Elev= 220.00' Surf.Area= 990 sf Storage= 1,461 cf

Plug-Flow detention time= 74.5 min calculated for 0.089 af (95% of inflow)
 Center-of-Mass det. time= 46.2 min (838.1 - 791.8)

Volume	Invert	Avail.Storage	Storage Description			
#1	216.50'	1,461 cf	Ponding Area (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
216.50	93	35.2	0	0	93	
217.00	153	44.0	61	61	152	
218.00	316	63.5	230	291	327	
219.00	534	82.4	420	711	558	
220.00	990	120.6	750	1,461	1,184	

Device	Routing	Invert	Outlet Devices
#1	Primary	216.50'	15.0" Round 15" HDPE N-12 L= 53.5' Ke= 0.500 Inlet / Outlet Invert= 216.50' / 215.85' S= 0.0121 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=217.48' TW=217.66' (Dynamic Tailwater)
 ↑1=15" HDPE N-12 (Controls 0.00 cfs)

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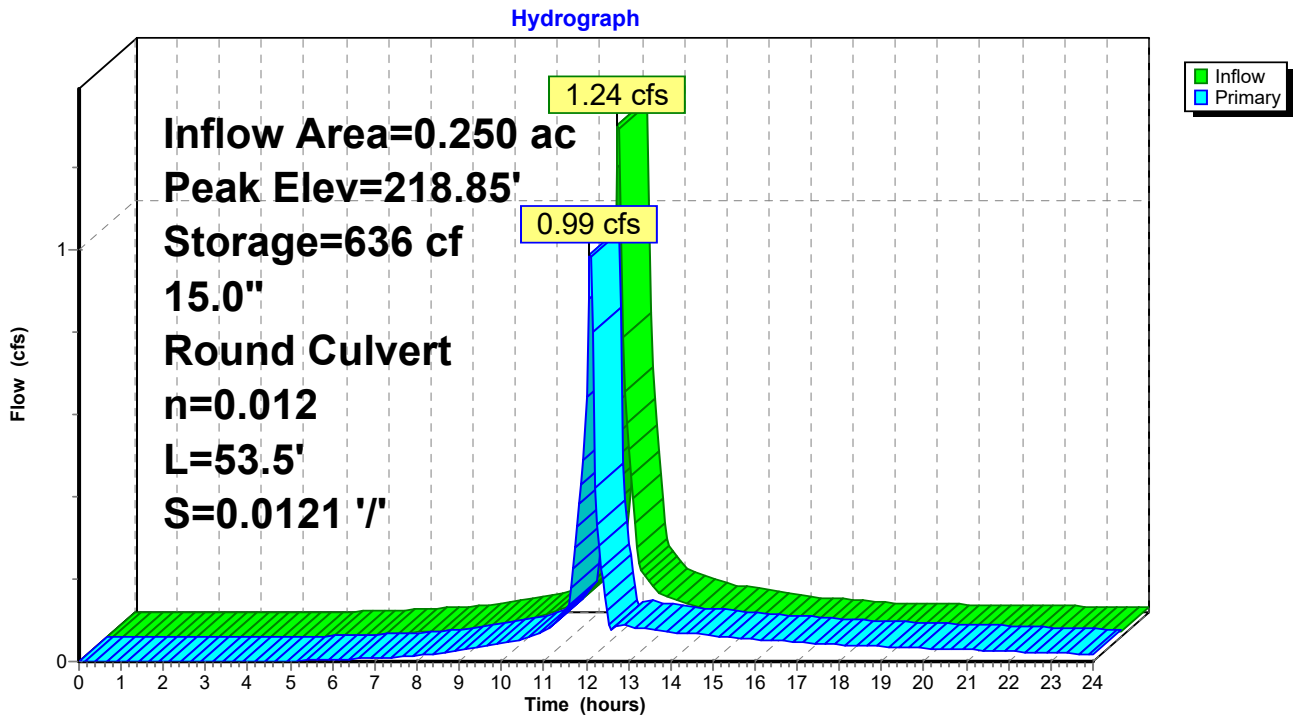
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Pond 49P: Community Drive Cul-de Sac



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond 50P: 15" HDPE (Access Road)

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

Inflow Area = 1.808 ac, 20.57% Impervious, Inflow Depth > 2.02" for 25YR - 24HR event
 Inflow = 0.83 cfs @ 12.26 hrs, Volume= 0.304 af
 Outflow = 0.83 cfs @ 12.27 hrs, Volume= 0.303 af, Atten= 0%, Lag= 0.5 min
 Primary = 0.83 cfs @ 12.27 hrs, Volume= 0.303 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 203.75' @ 12.27 hrs Surf.Area= 157 sf Storage= 60 cf
 Flood Elev= 206.00' Surf.Area= 400 sf Storage= 399 cf

Plug-Flow detention time= 1.8 min calculated for 0.303 af (100% of inflow)
 Center-of-Mass det. time= 1.2 min (986.8 - 985.6)

Volume	Invert	Avail.Storage	Storage Description			
#1	203.25'	399 cf	Open Water Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
203.25	88	38.0	0	0	88	
204.00	200	60.0	105	105	263	
205.00	400	100.0	294	399	779	

Device	Routing	Invert	Outlet Devices
#1	Primary	203.25'	15.0" Round 15" HDPE N-12 L= 42.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 203.25' / 203.00' S= 0.0060 ' / ' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=0.83 cfs @ 12.27 hrs HW=203.75' TW=203.16' (Dynamic Tailwater)
 ↑1=15" HDPE N-12 (Barrel Controls 0.83 cfs @ 2.70 fps)

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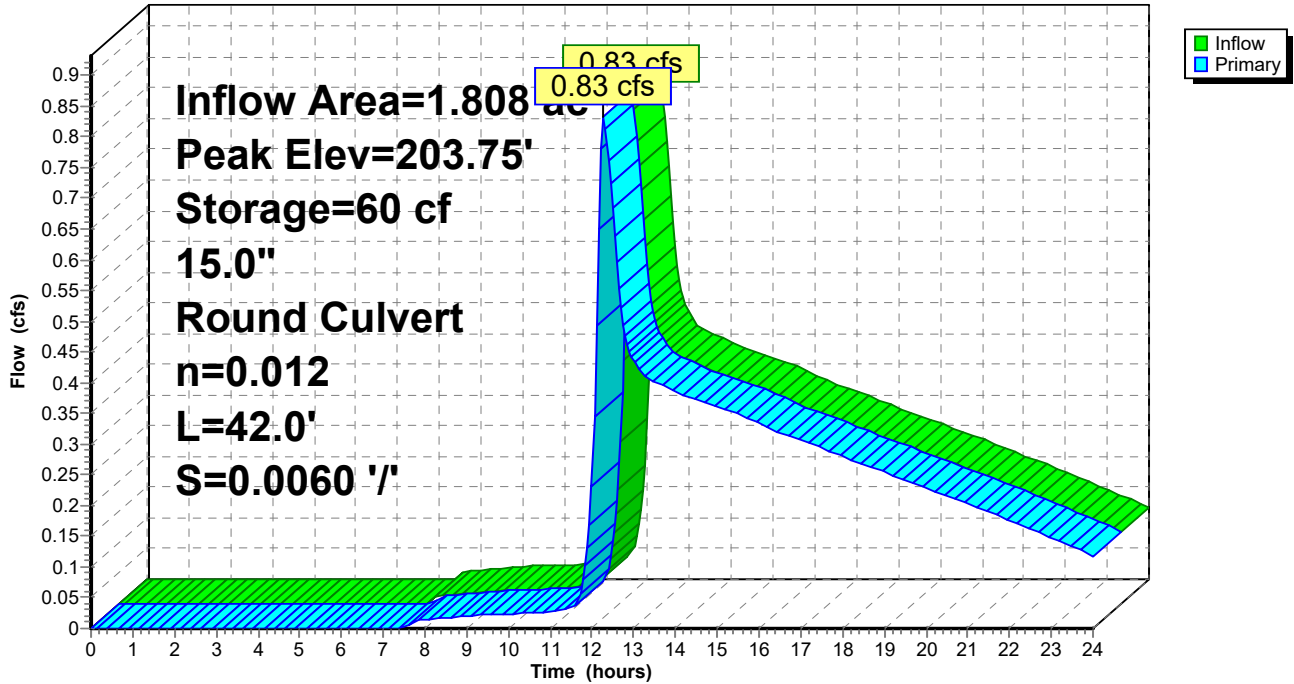
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Pond 50P: 15" HDPE (Access Road)

Hydrograph



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Summary for Pond 51P: Outlet Pond

Inflow Area = 0.397 ac, 48.01% Impervious, Inflow Depth > 2.63" for 25YR - 24HR event
 Inflow = 0.87 cfs @ 12.23 hrs, Volume= 0.087 af
 Outflow = 0.83 cfs @ 12.41 hrs, Volume= 0.066 af, Atten= 5%, Lag= 11.1 min
 Primary = 0.83 cfs @ 12.41 hrs, Volume= 0.066 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 214.07' @ 12.42 hrs Surf.Area= 875 sf Storage= 949 cf
 Flood Elev= 215.00' Surf.Area= 875 sf Storage= 1,767 cf

Plug-Flow detention time= 140.0 min calculated for 0.066 af (76% of inflow)
 Center-of-Mass det. time= 51.3 min (918.4 - 867.1)

Volume	Invert	Avail.Storage	Storage Description			
#1	212.00'	1,767 cf	Ponding Area (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
212.00	75	42.5	0	0	75	
213.00	455	174.0	238	238	2,343	
214.00	875	185.8	654	892	2,726	
215.00	875	185.8	875	1,767	2,912	

Device	Routing	Invert	Outlet Devices										
#1	Primary	214.00'	20.0' long x 2.0' breadth Level Spreader										
			Head (feet)	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60	1.80	2.00
				2.50	3.00	3.50							
			Coef. (English)	2.54	2.61	2.61	2.60	2.66	2.70	2.77	2.89	2.88	
				2.85	3.07	3.20	3.32						

Primary OutFlow Max=0.73 cfs @ 12.41 hrs HW=214.06' TW=212.65' (Dynamic Tailwater)
 ↑1=Level Spreader (Weir Controls 0.73 cfs @ 0.62 fps)

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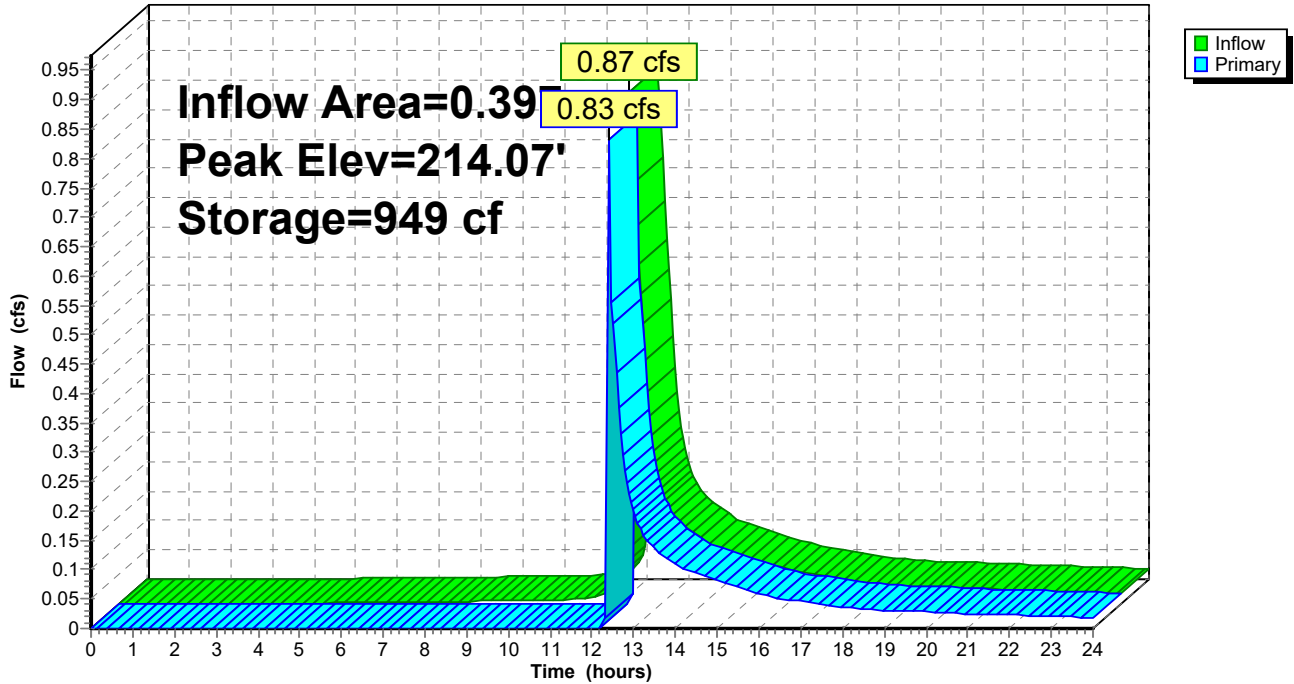
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Pond 51P: Outlet Pond

Hydrograph



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Summary for Pond 52P: S Wetland Crossing 24" HDPE N-12

Inflow Area = 5.458 ac, 0.00% Impervious, Inflow Depth > 1.43" for 25YR - 24HR event
 Inflow = 4.80 cfs @ 12.43 hrs, Volume= 0.649 af
 Outflow = 4.80 cfs @ 12.44 hrs, Volume= 0.649 af, Atten= 0%, Lag= 0.5 min
 Primary = 4.80 cfs @ 12.44 hrs, Volume= 0.649 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 214.35' @ 12.44 hrs Surf.Area= 255 sf Storage= 86 cf
 Flood Elev= 217.00' Surf.Area= 5,218 sf Storage= 7,230 cf

Plug-Flow detention time= 0.2 min calculated for 0.649 af (100% of inflow)
 Center-of-Mass det. time= 0.2 min (894.0 - 893.8)

Volume	Invert	Avail.Storage	Storage Description		
#1	213.50'	9,839 cf	Ponding Area (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
213.50	22	26.8	0	0	22
214.00	97	51.8	28	28	180
215.00	761	152.6	377	404	1,822
216.00	3,629	290.4	2,017	2,421	6,685
216.50	5,218	306.3	2,200	4,621	7,455
217.50	5,218	306.3	5,218	9,839	7,761

Device	Routing	Invert	Outlet Devices
#1	Primary	213.50'	24.0" Round 24" HDPE N-12 6" Bury w/ 6.0" inside fill L= 36.0' Ke= 0.500 Inlet / Outlet Invert= 213.00' / 212.00' S= 0.0278 ' Cc= 0.900 n= 0.024, Flow Area= 2.53 sf

Primary OutFlow Max=4.78 cfs @ 12.44 hrs HW=214.34' TW=212.78' (Dynamic Tailwater)
 ↑1=24" HDPE N-12 6" Bury (Inlet Controls 4.78 cfs @ 2.93 fps)

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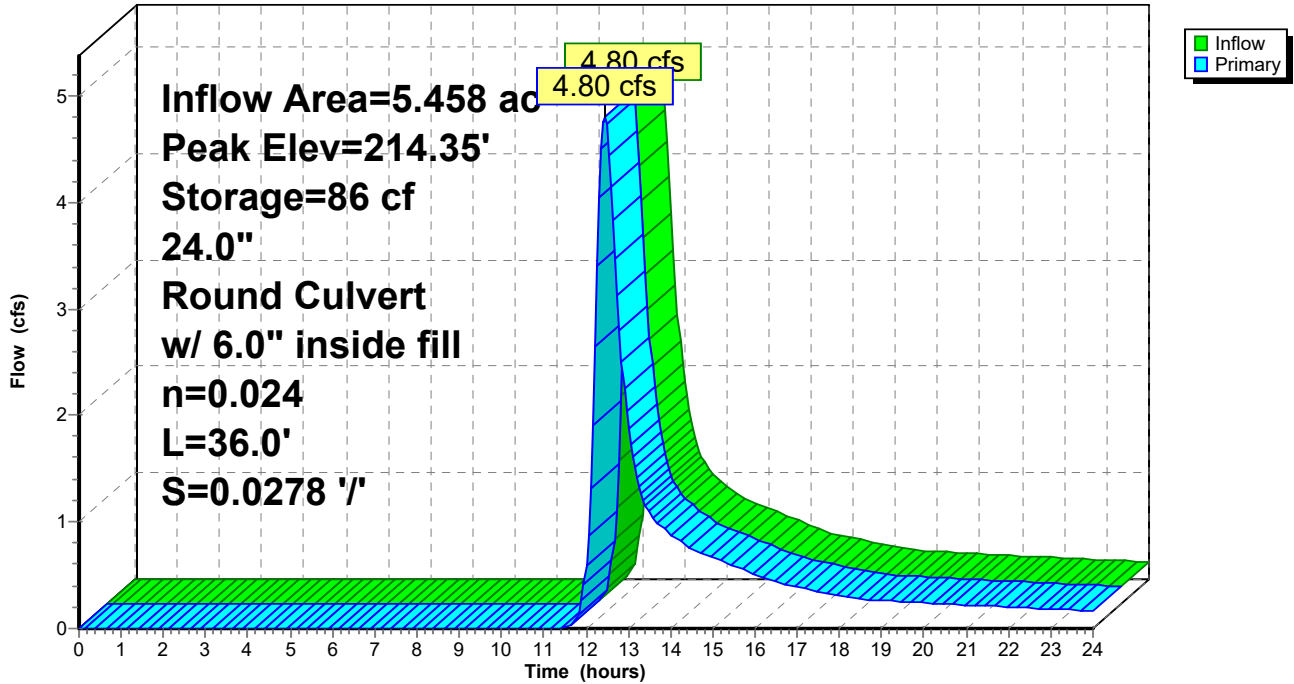
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Pond 52P: S Wetland Crossing 24" HDPE N-12

Hydrograph



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Summary for Pond 53P: N Wetland Crossing 24" HDPE N-12

Inflow Area = 0.542 ac, 0.00% Impervious, Inflow Depth > 1.51" for 25YR - 24HR event
 Inflow = 0.57 cfs @ 12.32 hrs, Volume= 0.068 af
 Outflow = 0.57 cfs @ 12.33 hrs, Volume= 0.068 af, Atten= 0%, Lag= 0.2 min
 Primary = 0.57 cfs @ 12.33 hrs, Volume= 0.068 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 215.71' @ 12.33 hrs Surf.Area= 43 sf Storage= 6 cf

Plug-Flow detention time= 0.3 min calculated for 0.068 af (100% of inflow)
 Center-of-Mass det. time= 0.2 min (886.3 - 886.1)

Volume	Invert	Avail.Storage	Storage Description			
#1	215.50'	1,811 cf	Ponding Area (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
215.50	20	22.1	0	0	20	
216.00	88	44.4	25	25	139	
216.50	1,467	201.6	319	344	3,217	
217.50	1,467	201.6	1,467	1,811	3,419	

Device	Routing	Invert	Outlet Devices	
#1	Primary	215.50'	24.0" Round 24" HDPE N-12 6" Bury w/ 6.0" inside fill L= 25.0' Ke= 0.500 Inlet / Outlet Invert= 215.00' / 213.50' S= 0.0600 ' Cc= 0.900 n= 0.024, Flow Area= 2.53 sf	

Primary OutFlow Max=0.56 cfs @ 12.33 hrs HW=215.71' TW=214.09' (Dynamic Tailwater)
 ↳1=24" HDPE N-12 6" Bury (Inlet Controls 0.56 cfs @ 1.46 fps)

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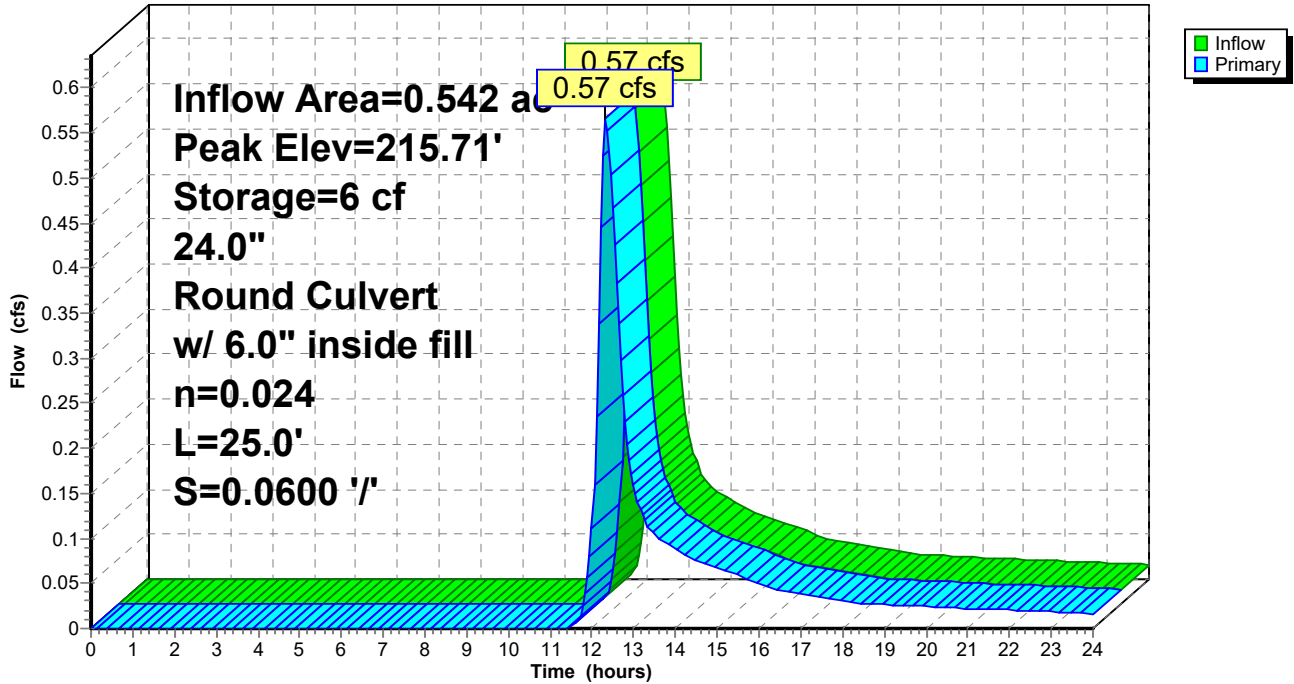
Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Pond 53P: N Wetland Crossing 24" HDPE N-12

Hydrograph



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Summary for Pond 54P: Inlet Sump Detention Pond #110

Inflow Area = 2.712 ac, 0.71% Impervious, Inflow Depth > 1.66" for 25YR - 24HR event
 Inflow = 2.93 cfs @ 12.40 hrs, Volume= 0.375 af
 Outflow = 2.93 cfs @ 12.41 hrs, Volume= 0.375 af, Atten= 0%, Lag= 0.4 min
 Primary = 2.93 cfs @ 12.41 hrs, Volume= 0.375 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 222.88' @ 12.41 hrs Surf.Area= 124 sf Storage= 79 cf
 Flood Elev= 223.00' Surf.Area= 135 sf Storage= 94 cf

Plug-Flow detention time= 0.8 min calculated for 0.374 af (100% of inflow)
 Center-of-Mass det. time= 0.5 min (884.8 - 884.3)

Volume	Invert	Avail.Storage	Storage Description			
#1	222.00'	94 cf	Ponding Area (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
222.00	59	30.2	0	0	59	
223.00	135	45.5	94	94	159	

Device	Routing	Invert	Outlet Devices	
#1	Primary	222.00'	15.0" Round 15" HDPE N-12 L= 35.0' Ke= 0.500 Inlet / Outlet Invert= 222.00' / 220.00' S= 0.0571 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf	

Primary OutFlow Max=2.92 cfs @ 12.41 hrs HW=222.88' TW=219.20' (Dynamic Tailwater)
 ↳ **1=15" HDPE N-12** (Inlet Controls 2.92 cfs @ 3.19 fps)

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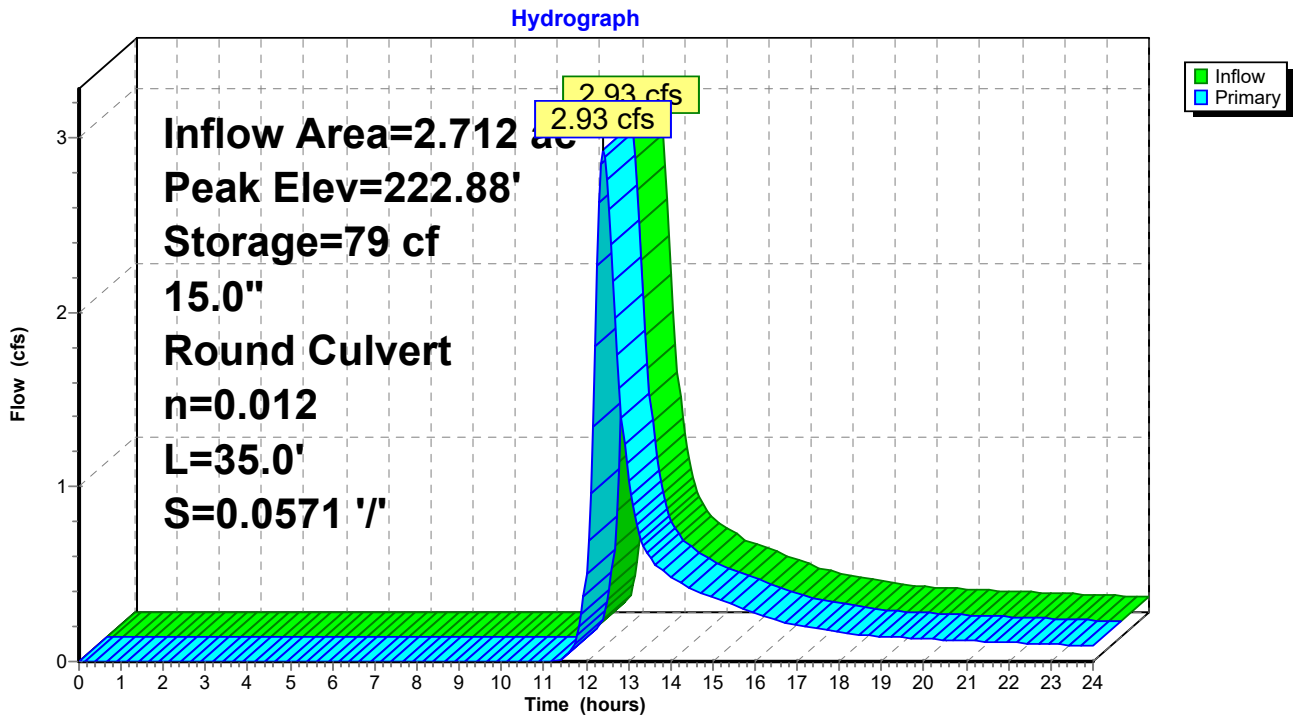
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Pond 54P: Inlet Sump Detention Pond #110



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Summary for Pond 55P: Drop Inlet #55

Inflow Area = 1.332 ac, 27.93% Impervious, Inflow Depth > 2.22" for 25YR - 24HR event
Inflow = 0.33 cfs @ 12.40 hrs, Volume= 0.247 af
Outflow = 0.33 cfs @ 12.40 hrs, Volume= 0.247 af, Atten= 0%, Lag= 0.0 min
Primary = 0.33 cfs @ 12.40 hrs, Volume= 0.247 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Peak Elev= 204.09' @ 12.31 hrs Surf.Area= 0.000 ac Storage= 0.000 af
Flood Elev= 207.75' Surf.Area= 0.000 ac Storage= 0.000 af

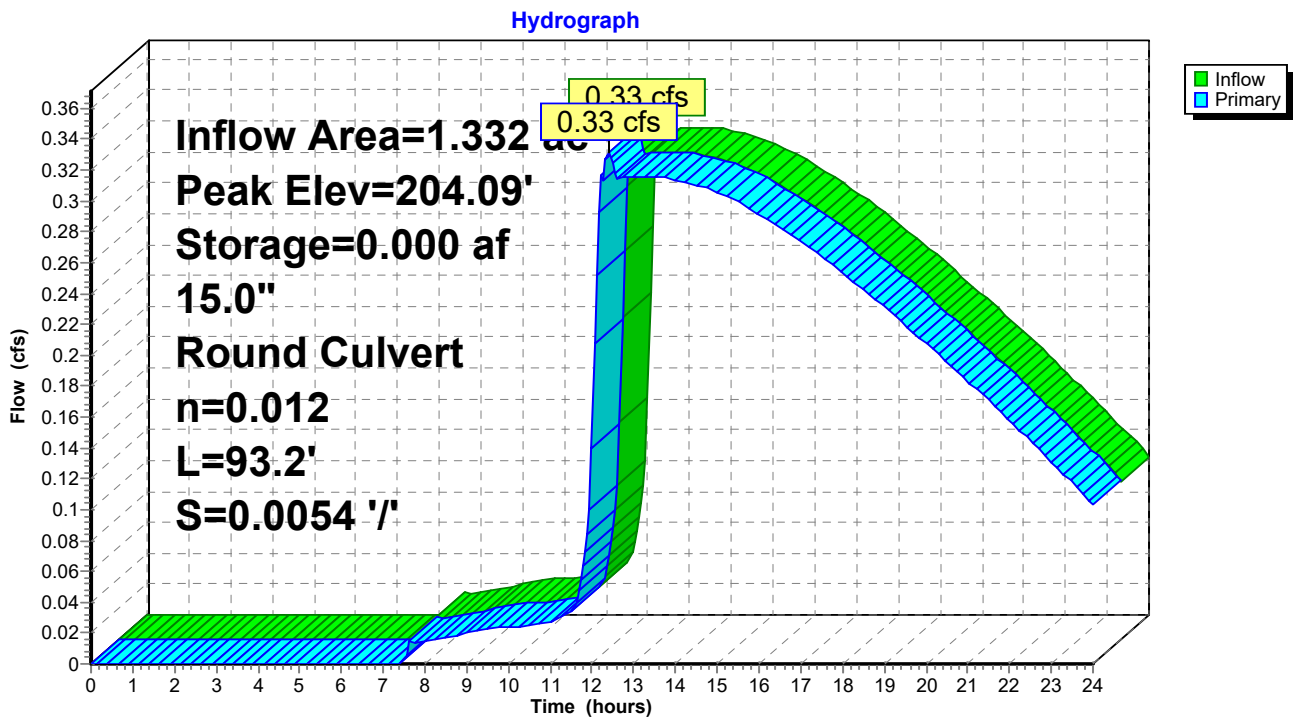
Plug-Flow detention time= 0.1 min calculated for 0.247 af (100% of inflow)
Center-of-Mass det. time= 0.0 min (1,008.7 - 1,008.6)

Volume	Invert	Avail.Storage	Storage Description
#1	203.75'	0.000 af	2.00'D x 4.00'H 2' Drop Inlet

Device	Routing	Invert	Outlet Devices
#1	Primary	203.75'	15.0" Round 15" HDPE N-12 L= 93.2' Ke= 0.500 Inlet / Outlet Invert= 203.75' / 203.25' S= 0.0054 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.33 cfs @ 12.40 hrs HW=204.08' TW=203.72' (Dynamic Tailwater)
←1=15" HDPE N-12 (Outlet Controls 0.33 cfs @ 1.90 fps)

Pond 55P: Drop Inlet #55



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Summary for Pond 101P: Ex. Rain Garden #101

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=34)

Inflow Area = 1.269 ac, 46.37% Impervious, Inflow Depth > 1.64" for 25YR - 24HR event
 Inflow = 1.94 cfs @ 12.09 hrs, Volume= 0.174 af
 Outflow = 0.39 cfs @ 12.96 hrs, Volume= 0.155 af, Atten= 80%, Lag= 52.2 min
 Primary = 0.39 cfs @ 12.96 hrs, Volume= 0.155 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 202.10' @ 12.96 hrs Surf.Area= 1,677 sf Storage= 2,682 cf
 Flood Elev= 203.00' Surf.Area= 3,677 sf Storage= 5,022 cf

Plug-Flow detention time= 118.3 min calculated for 0.154 af (89% of inflow)
 Center-of-Mass det. time= 74.7 min (895.3 - 820.5)

Volume	Invert	Avail.Storage	Storage Description
#1	198.50'	384 cf	Stone Bed (Irregular) Listed below (Recalc) -Impervious 959 cf Overall x 40.0% Voids
#2	199.50'	288 cf	Bio Media (Irregular) Listed below -Impervious 1,439 cf Overall x 20.0% Voids
#3	201.00'	3,722 cf	Open Storage (Irregular) Listed below (Recalc)
#4	200.00'	629 cf	Forebay (Irregular) Listed below (Recalc) -Impervious
		5,022 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
198.50	959	250.0	0	0	959
199.50	959	250.0	959	959	1,209

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
199.50	959	250.0	0	0	959
201.00	959	250.0	1,439	1,439	1,334

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
201.00	959	250.0	0	0	959
202.00	1,494	284.0	1,217	1,217	2,428
203.00	3,677	596.0	2,505	3,722	24,281

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
200.00	55	35.0	0	0	55
201.00	281	320.0	153	153	8,108
202.00	702	445.0	476	629	15,727

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Device	Routing	Invert	Outlet Devices
#1	Secondary	202.50'	20.0' long x 4.0' breadth E-Spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.67 2.65 2.66 2.66 2.68 2.72 2.73 2.76 2.79 2.88 3.07 3.32
#2	Primary	198.50'	6.0" Round 6" U.D. L= 20.0' Ke= 0.500 Inlet / Outlet Invert= 198.50' / 198.30' S= 0.0100 '/' Cc= 0.900 n= 0.012, Flow Area= 0.20 sf
#3	Device 2	201.00'	10.000 in/hr Exfiltration over Surface area

Primary OutFlow Max=0.39 cfs @ 12.96 hrs HW=202.10' TW=199.77' (Dynamic Tailwater)

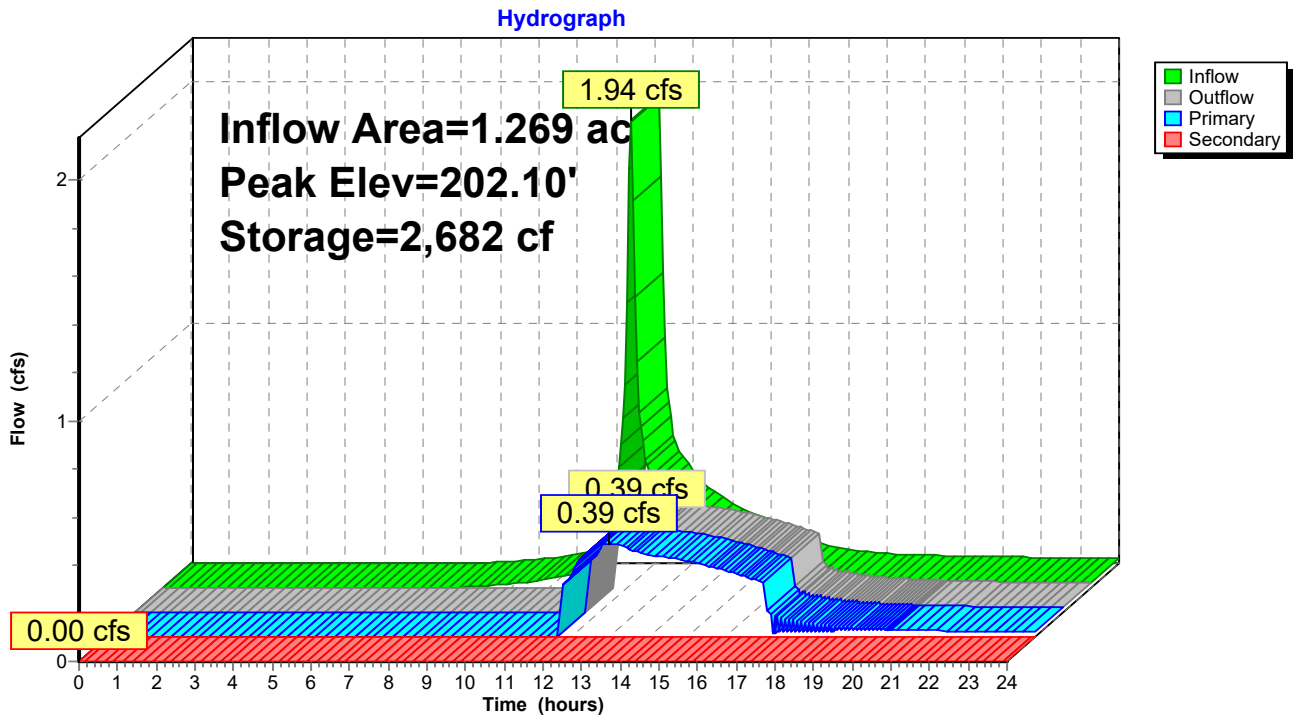
↳ **2=6" U.D.** (Passes 0.39 cfs of 1.43 cfs potential flow)

↳ **3=Exfiltration** (Exfiltration Controls 0.39 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=198.50' TW=198.10' (Dynamic Tailwater)

↳ **1=E-Spillway** (Controls 0.00 cfs)

Pond 101P: Ex. Rain Garden #101



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Summary for Pond 102P: Ex. Rain Garden #102

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=27)

Inflow Area = 8.228 ac, 18.90% Impervious, Inflow Depth > 1.42" for 25YR - 24HR event
 Inflow = 6.14 cfs @ 12.09 hrs, Volume= 0.975 af
 Outflow = 4.96 cfs @ 12.24 hrs, Volume= 0.920 af, Atten= 19%, Lag= 9.0 min
 Primary = 0.46 cfs @ 11.95 hrs, Volume= 0.545 af
 Secondary = 4.50 cfs @ 12.24 hrs, Volume= 0.375 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 200.21' @ 12.24 hrs Surf.Area= 1,994 sf Storage= 6,276 cf
 Flood Elev= 200.50' Surf.Area= 1,994 sf Storage= 7,317 cf

Plug-Flow detention time= 95.1 min calculated for 0.920 af (94% of inflow)
 Center-of-Mass det. time= 65.5 min (927.6 - 862.1)

Volume	Invert	Avail.Storage	Storage Description
#1	196.50'	798 cf	Stone Base (Irregular) Listed below (Recalc) -Impervious 1,994 cf Overall x 40.0% Voids
#2	197.50'	598 cf	Bio Media (Irregular) Listed below (Recalc) 2,991 cf Overall x 20.0% Voids
#3	199.00'	4,816 cf	Open Storage (Irregular) Listed below (Recalc) -Impervious
#4	197.00'	1,106 cf	Forebay (Irregular) Listed below (Recalc) -Impervious
		7,317 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
196.50	1,994	198.7	0	0	1,994
197.50	1,994	198.7	1,994	1,994	2,193

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
197.50	1,994	198.7	0	0	1,994
199.00	1,994	198.7	2,991	2,991	2,292

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
199.00	2,793	272.2	0	0	2,793
200.00	3,352	285.2	3,068	3,068	3,433
200.50	3,640	291.5	1,748	4,816	3,757

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
197.00	336	93.0	0	0	336
198.00	547	108.0	437	437	596
199.00	798	127.0	669	1,106	970

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Device	Routing	Invert	Outlet Devices
#1	Primary	196.50'	6.0" Round 6" U.D. L= 20.0' Ke= 0.500 Inlet / Outlet Invert= 196.50' / 196.40' S= 0.0050 '/' Cc= 0.900 n= 0.012, Flow Area= 0.20 sf
#2	Device 1	197.50'	10.000 in/hr Exfil. To UD over Surface area 20.0' long x 4.0' breadth E-Spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.67 2.65 2.66 2.66 2.68 2.72 2.73 2.76 2.79 2.88 3.07 3.32
#3	Secondary	200.00'	

Primary OutFlow Max=0.46 cfs @ 11.95 hrs HW=199.12' TW=196.95' (Dynamic Tailwater)

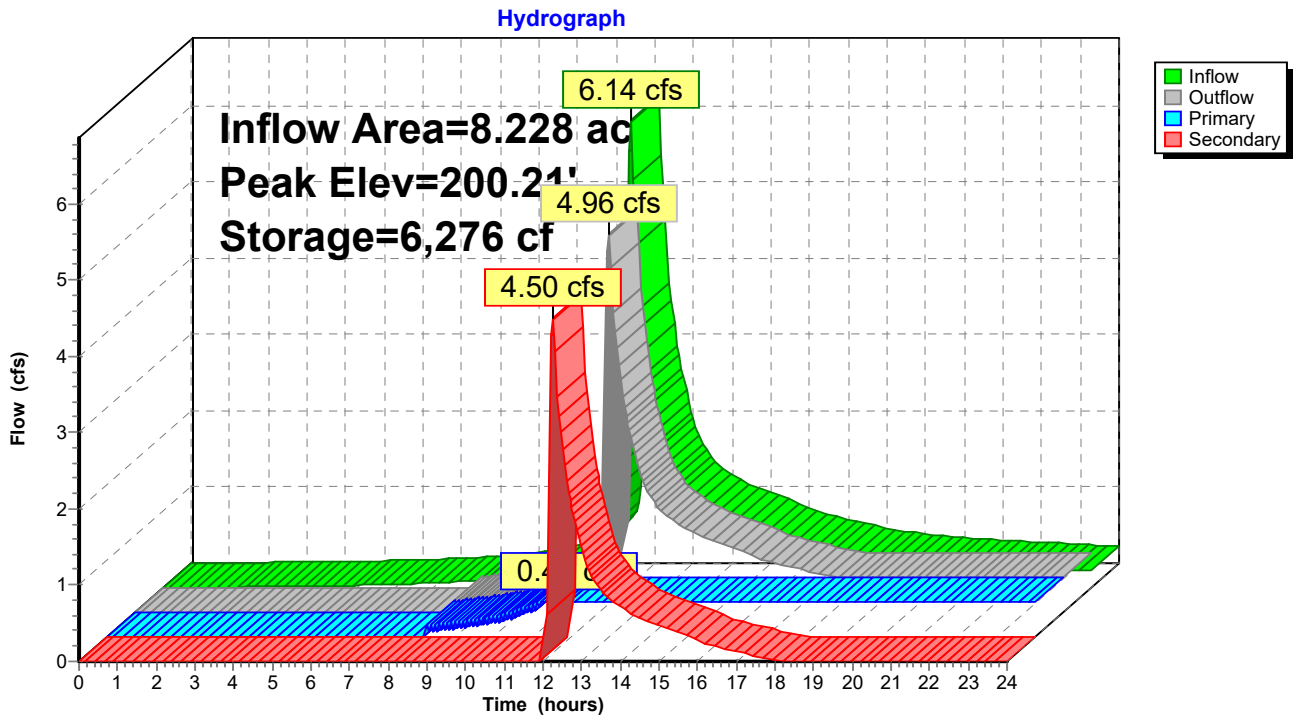
↑1=6" U.D. (Passes 0.46 cfs of 1.38 cfs potential flow)

↑2=Exfil. To UD (Exfiltration Controls 0.46 cfs)

Secondary OutFlow Max=4.45 cfs @ 12.24 hrs HW=200.21' TW=197.83' (Dynamic Tailwater)

↑3=E-Spillway (Weir Controls 4.45 cfs @ 1.08 fps)

Pond 102P: Ex. Rain Garden #102



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Summary for Pond 103P: Gravel Wetland #103

[80] Warning: Exceeded Pond D01P by 0.01' @ 22.00 hrs (0.71 cfs 0.042 af)

Inflow Area = 0.567 ac, 57.16% Impervious, Inflow Depth > 3.95" for 25YR - 24HR event
 Inflow = 2.43 cfs @ 12.09 hrs, Volume= 0.187 af
 Outflow = 0.20 cfs @ 13.18 hrs, Volume= 0.119 af, Atten= 92%, Lag= 65.4 min
 Primary = 0.20 cfs @ 13.18 hrs, Volume= 0.119 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 214.46' @ 13.18 hrs Surf.Area= 4,356 sf Storage= 4,554 cf
 Flood Elev= 216.00' Surf.Area= 5,371 sf Storage= 9,385 cf

Plug-Flow detention time= 260.0 min calculated for 0.119 af (64% of inflow)
 Center-of-Mass det. time= 155.3 min (948.4 - 793.1)

Volume	Invert	Avail.Storage	Storage Description
#1	211.67'	32 cf	4.00'D x 2.57'H 4' Outlet Structure
#2	212.00'	561 cf	Cell 1 (Irregular) Listed below (Recalc)
#3	212.00'	555 cf	Cell 2 (Irregular) Listed below (Recalc)
#4	213.00'	7,925 cf	Open Water Storage (Irregular) Listed below (Recalc)
#5	212.00'	311 cf	Sediment Forebay (Irregular) Listed below (Recalc)
		9,385 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
212.00	434	78.7	0	0	434
213.00	698	97.5	561	561	712

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
212.00	426	79.3	0	0	426
213.00	695	98.2	555	555	707

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
213.00	1,515	153.7	0	0	1,515
214.00	2,373	196.6	1,928	1,928	2,724
215.00	2,990	215.5	2,676	4,604	3,377
216.00	3,665	234.3	3,322	7,925	4,086

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
212.00	47	26.8	0	0	47
213.00	147	45.3	92	92	159
214.00	300	63.8	219	311	329

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Device	Routing	Invert	Outlet Devices
#1	Primary	211.67'	15.0" Round 15" N-12 HDPE L= 20.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 211.67' / 211.00' S= 0.0335 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	211.67'	0.7" Vert. 0.75" Orifice Goose Neck C= 0.600
#3	Device 1	213.75'	3.0" Vert. 3" Orifice C= 0.600
#4	Device 1	215.45'	48.0" Horiz. 48" Structure C= 0.600 Limited to weir flow at low heads
#5	Secondary	215.50'	5.0' long x 7.0' breadth 5' Emergency Spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65 2.65 2.66 2.65 2.66 2.68 2.70 2.73 2.78

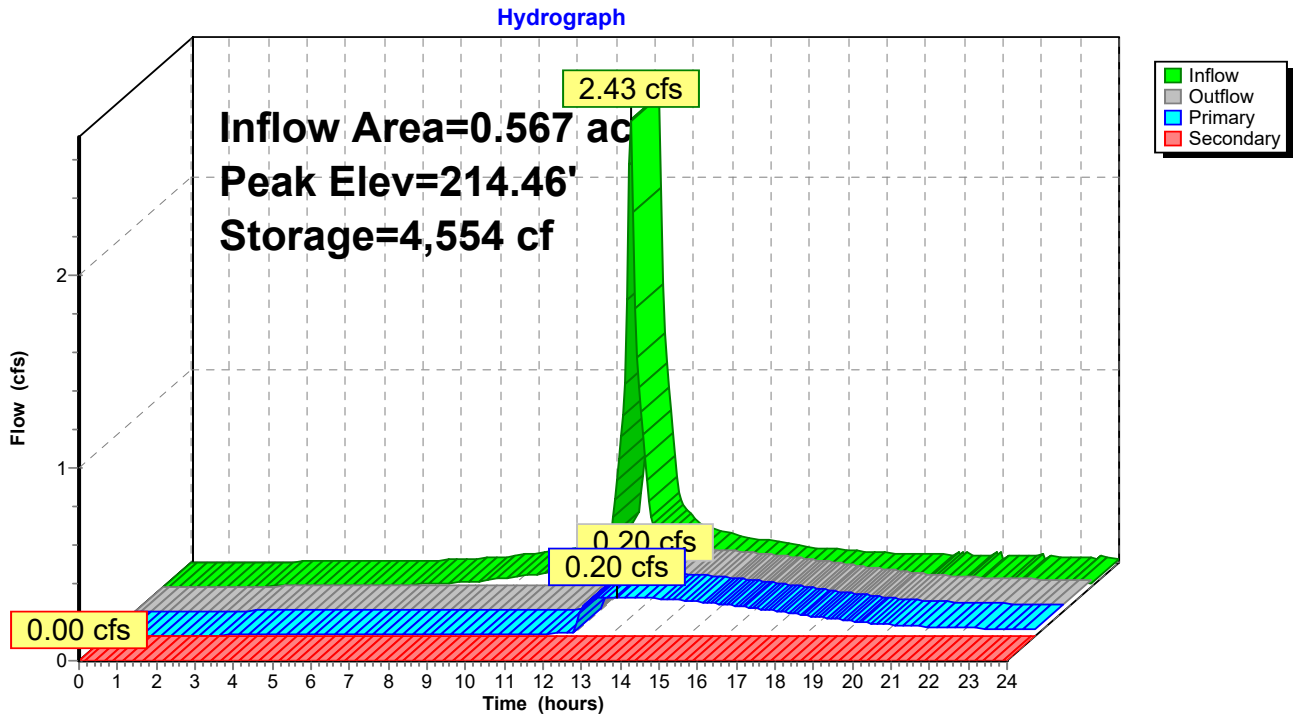
Primary OutFlow Max=0.20 cfs @ 13.18 hrs HW=214.46' TW=211.04' (Dynamic Tailwater)

- 1=15" N-12 HDPE (Passes 0.20 cfs of 8.70 cfs potential flow)
- 2=0.75" Orifice Goose Neck (Orifice Controls 0.02 cfs @ 8.01 fps)
- 3=3" Orifice (Orifice Controls 0.18 cfs @ 3.70 fps)
- 4=48" Structure (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=211.67' TW=211.00' (Dynamic Tailwater)

- 5=5' Emergency Spillway (Controls 0.00 cfs)

Pond 103P: Gravel Wetland #103



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Summary for Pond 104P: Gravel Wetland #104

[80] Warning: Exceeded Pond C31P by 0.02' @ 21.90 hrs (0.76 cfs 0.102 af)

Inflow Area = 0.331 ac, 57.47% Impervious, Inflow Depth > 3.99" for 25YR - 24HR event
 Inflow = 1.46 cfs @ 12.09 hrs, Volume= 0.110 af
 Outflow = 0.79 cfs @ 12.24 hrs, Volume= 0.076 af, Atten= 46%, Lag= 8.7 min
 Primary = 0.79 cfs @ 12.24 hrs, Volume= 0.076 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 216.47' @ 12.24 hrs Surf.Area= 2,243 sf Storage= 1,882 cf
 Flood Elev= 217.00' Surf.Area= 2,431 sf Storage= 2,575 cf

Plug-Flow detention time= 162.5 min calculated for 0.076 af (69% of inflow)
 Center-of-Mass det. time= 67.4 min (868.0 - 800.5)

Volume	Invert	Avail.Storage	Storage Description
#1	213.67'	34 cf	4.00'D x 2.73'H 4' Outlet Structure
#2	214.00'	1,004 cf	Single Cell (Irregular) Listed below (Recalc)
#3	214.00'	311 cf	Sediment Forebay (Irregular) Listed below (Recalc)
#4	216.00'	1,226 cf	Open Water Storage (Irregular) Listed below (Recalc)
		2,575 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
214.00	305	87.3	0	0	305
215.00	496	101.5	397	397	538
216.00	725	117.0	607	1,004	829

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
214.00	40	24.5	0	0	40
215.00	155	57.8	91	91	262
216.00	291	73.5	219	311	439

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
216.00	1,059	165.1	0	0	1,059
217.00	1,402	177.7	1,226	1,226	1,443

Device	Routing	Invert	Outlet Devices
#1	Primary	213.67'	15.0" Round 15" N-12 HDPE L= 20.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 213.67' / 213.00' S= 0.0335 '/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	213.67'	0.5" Vert. 0.50" Orifice Goose Neck C= 0.600
#3	Device 1	216.10'	12.0" W x 3.0" H Vert. 3" X 12" Box Orifice C= 0.600
#4	Device 1	216.40'	12.0" Horiz. 12" Horizontal Orifice C= 0.600 Limited to weir flow at low heads
#5	Secondary	216.50'	5.0' long x 7.0' breadth E-Spillway

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Head (feet)	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60	1.80	2.00
	2.50	3.00	3.50	4.00	4.50	5.00	5.50			
Coef. (English)	2.40	2.52	2.70	2.68	2.68	2.67	2.66	2.65	2.65	
	2.65	2.66	2.65	2.66	2.68	2.70	2.73	2.78		

Primary OutFlow Max=0.78 cfs @ 12.24 hrs HW=216.47' TW=213.59' (Dynamic Tailwater)

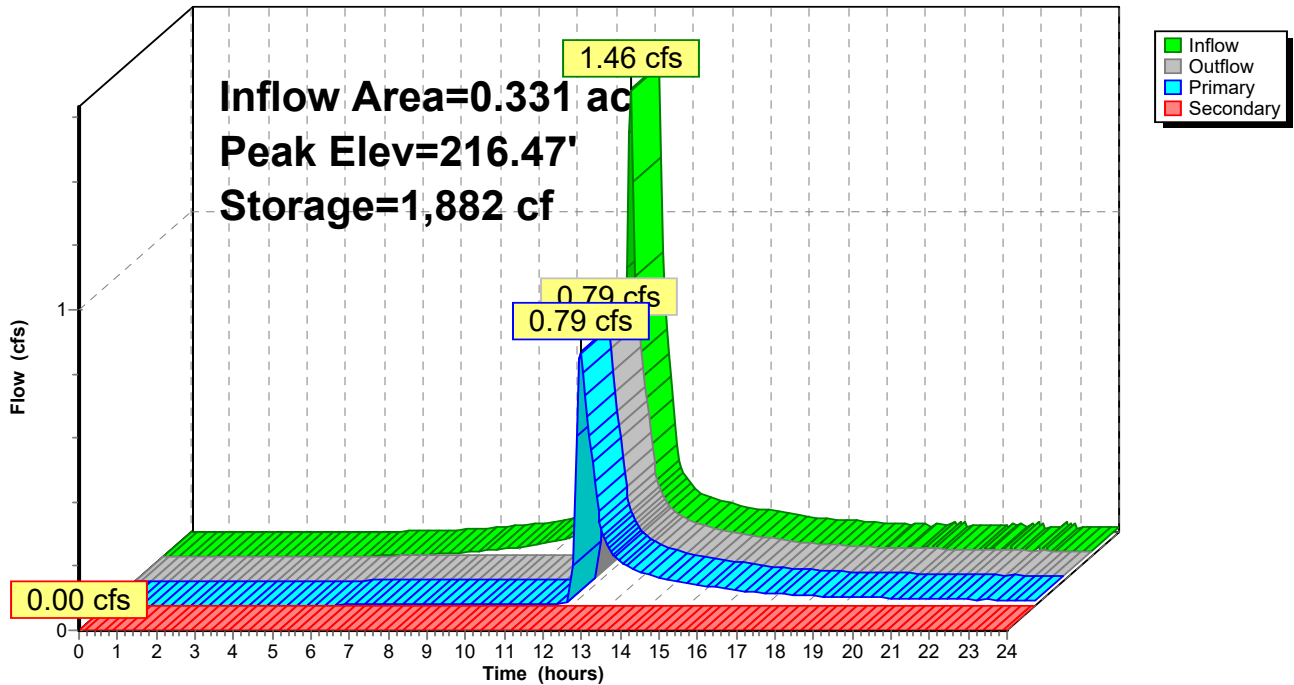
- 1=15" N-12 HDPE (Passes 0.78 cfs of 8.71 cfs potential flow)
- 2=0.50" Orifice Goose Neck (Orifice Controls 0.01 cfs @ 8.02 fps)
- 3=3" X 12" Box Orifice (Orifice Controls 0.59 cfs @ 2.35 fps)
- 4=12" Horizontal Orifice (Weir Controls 0.18 cfs @ 0.85 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=213.67' TW=212.00' (Dynamic Tailwater)

- 5=E-Spillway (Controls 0.00 cfs)

Pond 104P: Gravel Wetland #104

Hydrograph



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Summary for Pond 105P: Rain Garden #105

[80] Warning: Exceeded Pond C35P by 0.02' @ 22.85 hrs (0.80 cfs 0.186 af)

[80] Warning: Exceeded Pond C39P by 0.02' @ 20.75 hrs (0.86 cfs 0.084 af)

Inflow Area = 1.629 ac, 63.51% Impervious, Inflow Depth > 4.29" for 25YR - 24HR event
 Inflow = 7.52 cfs @ 12.09 hrs, Volume= 0.582 af
 Outflow = 1.51 cfs @ 12.53 hrs, Volume= 0.405 af, Atten= 80%, Lag= 26.3 min
 Primary = 1.51 cfs @ 12.53 hrs, Volume= 0.405 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 219.61' @ 12.53 hrs Surf.Area= 1,331 sf Storage= 13,225 cf
 Flood Elev= 220.50' Surf.Area= 1,331 sf Storage= 18,035 cf

Plug-Flow detention time= 248.8 min calculated for 0.404 af (69% of inflow)
 Center-of-Mass det. time= 154.6 min (941.2 - 786.6)

Volume	Invert	Avail.Storage	Storage Description
#1	212.75'	532 cf	Stone (Irregular) Listed below (Recalc) -Impervious 1,331 cf Overall x 40.0% Voids
#2	213.75'	532 cf	Bio-media (Irregular) Listed below (Recalc) 2,662 cf Overall x 20.0% Voids
#3	216.00'	3,584 cf	RG Cell (Irregular) Listed below (Recalc) -Impervious
#4	218.00'	11,794 cf	Open Water Storage (Irregular) Listed below (Recalc) -Impervious
#5	215.75'	89 cf	Loam (Irregular) Listed below (Recalc) -Impervious 447 cf Overall x 20.0% Voids
#6	216.00'	745 cf	Sediment Forebay #1 (Irregular) Listed below (Recalc) -Impervious
#7	216.00'	758 cf	Sediment Forebay #2 (Irregular) Listed below (Recalc) -Impervious
		18,035 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
212.75	1,331	159.0	0	0	1,331
213.75	1,331	159.0	1,331	1,331	1,490

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
213.75	1,331	159.0	0	0	1,331
215.75	1,331	159.0	2,662	2,662	1,649

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
216.00	1,331	159.0	0	0	1,331
217.00	1,787	175.8	1,553	1,553	1,809
218.00	2,285	192.8	2,031	3,584	2,340

20-097 Proposed Analysis

Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
218.00	3,654	268.0	0	0	3,654
219.00	4,485	286.8	4,062	4,062	4,529
220.00	5,380	306.3	4,926	8,988	5,496
220.50	5,846	315.7	2,806	11,794	5,987

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
215.75	1,787	176.7	0	0	1,787
216.00	1,787	176.7	447	447	1,831

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
216.00	185	59.4	0	0	185
217.00	365	77.2	270	270	390
218.00	595	94.9	475	745	647

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
216.00	188	82.9	0	0	188
217.00	367	77.3	273	273	295
218.00	614	97.7	485	758	593

Device	Routing	Invert	Outlet Devices
#1	Primary	212.75'	18.0" Round 18" HDPE N-12 L= 85.0' Ke= 0.500 Inlet / Outlet Invert= 212.75' / 212.00' S= 0.0088 ' S= 0.0088 ' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	212.75'	1.0" Vert. 1" Orifice C= 0.600
#3	Device 2	213.75'	10.000 in/hr Exfiltration over Surface area
#4	Device 1	220.00'	15.0" Horiz. 15" Horizontal Orifice C= 0.600 Limited to weir flow at low heads
#5	Device 1	218.10'	3.0" Vert. 3" Orifice C= 0.600
#6	Device 1	219.00'	9.0" W x 12.0" H Vert. 12" X 12" Box Orifice C= 0.600

Primary OutFlow Max=1.50 cfs @ 12.53 hrs HW=219.61' TW=212.66' (Dynamic Tailwater)

- 1=18" HDPE N-12 (Passes 1.50 cfs of 20.86 cfs potential flow)
- 2=1" Orifice (Orifice Controls 0.07 cfs @ 12.58 fps)
- 3=Exfiltration (Passes 0.07 cfs of 0.31 cfs potential flow)
- 4=15" Horizontal Orifice (Controls 0.00 cfs)
- 5=3" Orifice (Orifice Controls 0.28 cfs @ 5.67 fps)
- 6=12" X 12" Box Orifice (Orifice Controls 1.16 cfs @ 2.51 fps)

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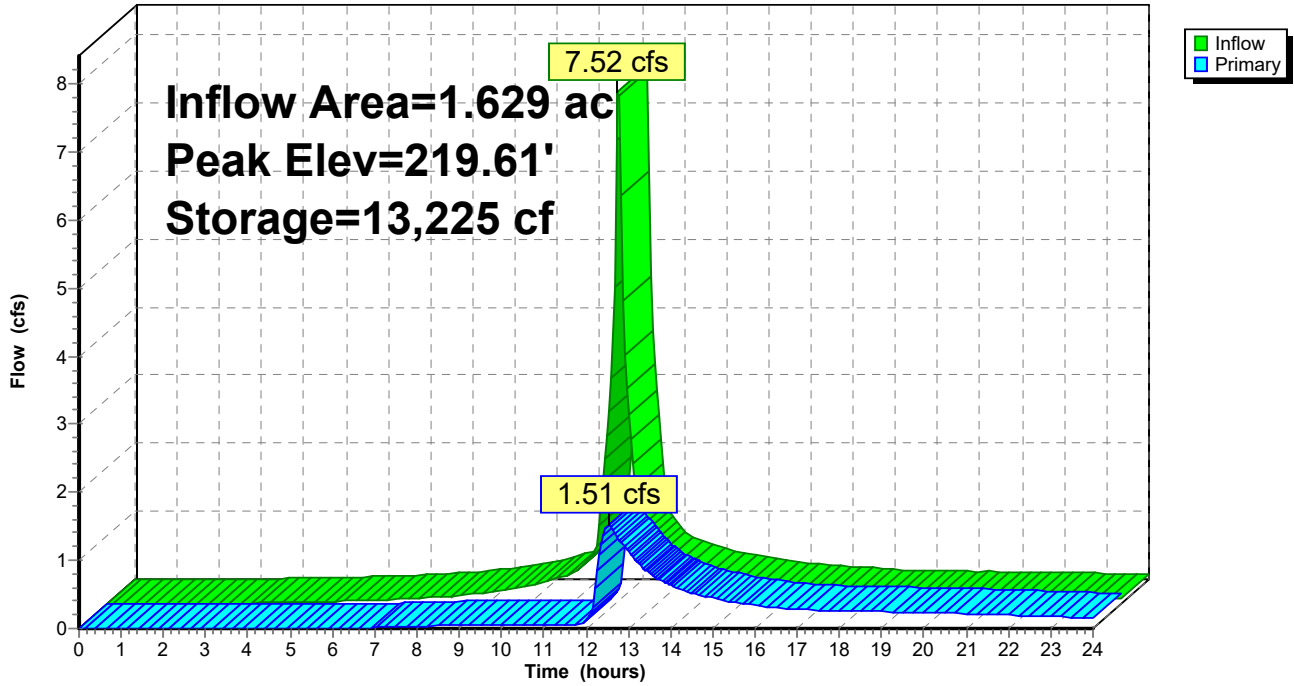
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Pond 105P: Rain Garden #105

Hydrograph



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Summary for Pond 106P: Rain Garden #106

Inflow Area = 1.231 ac, 30.22% Impervious, Inflow Depth > 3.07" for 25YR - 24HR event
 Inflow = 3.02 cfs @ 12.12 hrs, Volume= 0.315 af
 Outflow = 0.30 cfs @ 13.96 hrs, Volume= 0.231 af, Atten= 90%, Lag= 110.3 min
 Primary = 0.30 cfs @ 13.96 hrs, Volume= 0.231 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 218.85' @ 13.96 hrs Surf.Area= 391 sf Storage= 7,015 cf
 Flood Elev= 220.00' Surf.Area= 391 sf Storage= 11,576 cf

Plug-Flow detention time= 285.3 min calculated for 0.230 af (73% of inflow)
 Center-of-Mass det. time= 186.2 min (1,018.5 - 832.3)

Volume	Invert	Avail.Storage	Storage Description
#1	211.75'	156 cf	Stone (Irregular) Listed below (Recalc) -Impervious 391 cf Overall x 40.0% Voids
#2	212.75'	156 cf	Bio-media (Irregular) Listed below (Recalc) 782 cf Overall x 20.0% Voids
#3	215.00'	10,744 cf	Open Water Storage (Irregular) Listed below (Recalc) -Impervious
#4	214.75'	20 cf	Loam (Irregular) Listed below (Recalc) -Impervious 98 cf Overall x 20.0% Voids
#5	215.00'	500 cf	Sediment Forebay (Irregular) Listed below (Recalc) -Impervious
		11,576 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
211.75	391	90.7	0	0	391
212.75	391	90.7	391	391	482

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
212.75	391	90.7	0	0	391
214.75	391	90.7	782	782	572

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
215.00	391	90.7	0	0	391
216.00	680	109.0	529	529	698
217.00	1,404	149.4	1,020	1,549	1,539
218.00	2,730	229.3	2,031	3,580	3,955
219.00	3,498	255.5	3,106	6,686	4,994
220.00	4,645	388.2	4,058	10,744	11,799

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
214.75	391	90.7	0	0	391
215.00	391	90.7	98	98	414

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Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
215.00	104	39.3	0	0	104
216.00	238	57.1	166	166	249
217.00	439	77.5	333	500	477

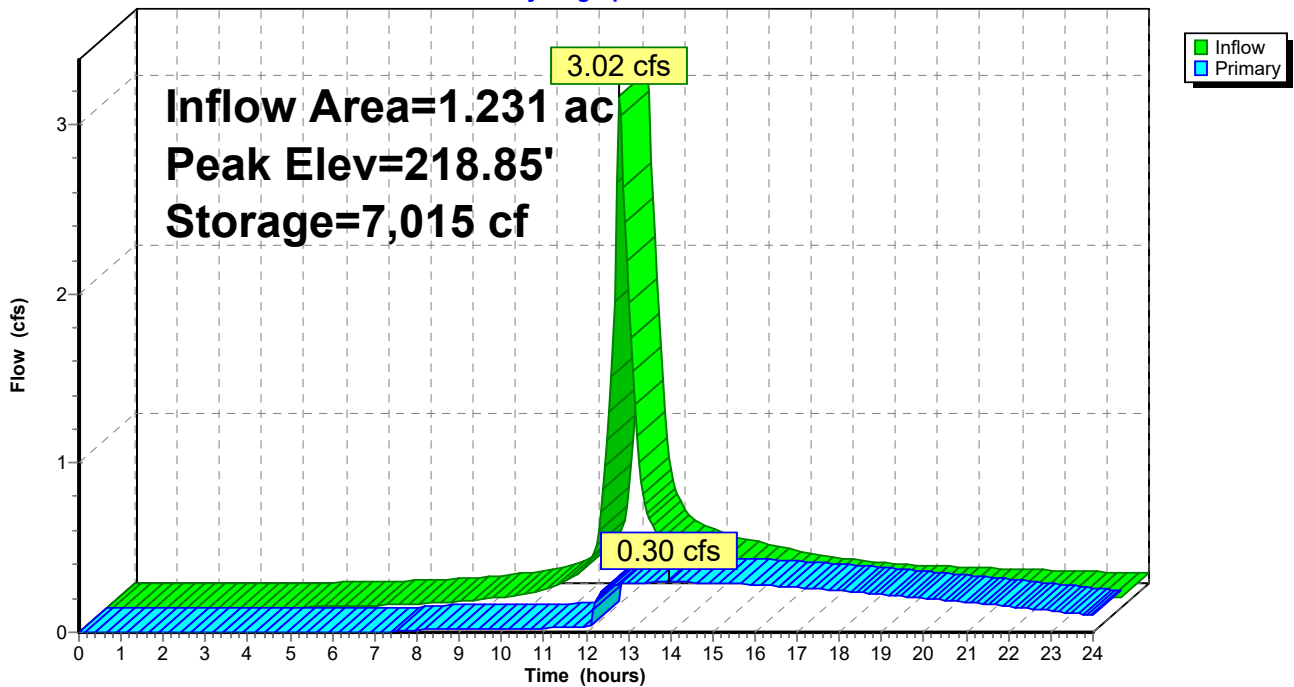
Device	Routing	Invert	Outlet Devices
#1	Primary	211.75'	15.0" Round 15" HDPE N-12 L= 95.0' Ke= 0.500 Inlet / Outlet Invert= 211.75' / 211.00' S= 0.0079 ' /' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	211.75'	0.7" Vert. 0.75" Orifice C= 0.600
#3	Device 2	212.75'	10.000 in/hr Exfiltration over Surface area
#4	Device 1	217.50'	3.0" Vert. 3" Orifice C= 0.600
#5	Device 1	219.00'	48.0" Horiz. 48" Top Structure C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=0.30 cfs @ 13.96 hrs HW=218.85' TW=211.06' (Dynamic Tailwater)

- 1=15" HDPE N-12 (Passes 0.30 cfs of 13.75 cfs potential flow)
- 2=0.75" Orifice (Orifice Controls 0.03 cfs @ 12.81 fps)
- 3=Exfiltration (Passes 0.03 cfs of 0.09 cfs potential flow)
- 4=3" Orifice (Orifice Controls 0.26 cfs @ 5.34 fps)
- 5=48" Top Structure (Controls 0.00 cfs)

Pond 106P: Rain Garden #106

Hydrograph



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Summary for Pond 107P: Rain Garden #107

Inflow Area = 4.467 ac, 17.16% Impervious, Inflow Depth > 2.18" for 25YR - 24HR event
 Inflow = 6.78 cfs @ 12.17 hrs, Volume= 0.812 af
 Outflow = 0.59 cfs @ 15.42 hrs, Volume= 0.500 af, Atten= 91%, Lag= 194.9 min
 Discarded = 0.01 cfs @ 10.10 hrs, Volume= 0.017 af
 Primary = 0.58 cfs @ 15.42 hrs, Volume= 0.483 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 229.12' @ 15.42 hrs Surf.Area= 2,135 sf Storage= 20,541 cf
 Flood Elev= 230.00' Surf.Area= 2,135 sf Storage= 28,192 cf

Plug-Flow detention time= 337.0 min calculated for 0.499 af (61% of inflow)
 Center-of-Mass det. time= 221.6 min (1,069.4 - 847.7)

Volume	Invert	Avail.Storage	Storage Description
#1	222.75'	854 cf	Stone (Irregular) Listed below (Recalc) -Impervious 2,135 cf Overall x 40.0% Voids
#2	223.75'	854 cf	Bio-media (Irregular) Listed below (Recalc) 4,270 cf Overall x 20.0% Voids
#3	225.75'	107 cf	Loam (Irregular) Listed below (Recalc) -Impervious 534 cf Overall x 20.0% Voids
#4	226.00'	16,356 cf	Infiltration Cell Storage (Irregular) Listed below (Recalc) -Impervious
#5	229.00'	8,667 cf	Open Water Storage (Irregular) Listed below (Recalc) -Impervious
#6	227.00'	641 cf	Sediment Forebay #1 (Irregular) Listed below (Recalc) -Impervious
#7	227.00'	714 cf	Sediment Forebay #2 (Irregular) Listed below (Recalc) -Impervious
		28,192 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
222.75	2,135	177.0	0	0	2,135
223.75	2,135	177.0	2,135	2,135	2,312

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
223.75	2,135	177.0	0	0	2,135
225.75	2,135	177.0	4,270	4,270	2,489

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
225.75	2,135	177.0	0	0	2,135
226.00	2,135	177.0	534	534	2,179

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
226.00	3,961	245.8	0	0	3,961
227.00	5,137	273.0	4,536	4,536	5,114
228.00	5,903	291.7	5,516	10,052	6,000
229.00	6,715	310.3	6,305	16,356	6,941

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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
229.00	8,122	357.5	0	0	8,122
230.00	9,223	376.4	8,667	8,667	9,285

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
227.00	115	41.3	0	0	115
228.00	312	74.3	205	205	424
229.00	571	103.5	435	641	847

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
227.00	144	49.8	0	0	144
228.00	345	81.0	237	237	475
229.00	622	111.6	477	714	954

Device	Routing	Invert	Outlet Devices
#1	Primary	223.50'	15.0" Round 15" HDPE N-12 L= 20.0' Ke= 0.500 Inlet / Outlet Invert= 223.50' / 223.00' S= 0.0250 1/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Discarded	223.75'	0.300 in/hr Exfiltration over Surface area
#3	Device 1	227.50'	3.0" Vert. 3" Orifice X 2.00 C= 0.600
#4	Device 1	229.40'	15.0" Horiz. 15" Horizontal Orifice C= 0.600 Limited to weir flow at low heads
#5	Secondary	229.50'	10.0' long x 7.0' breadth 10' Emergency Spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65 2.65 2.66 2.65 2.66 2.68 2.70 2.73 2.78

Discarded OutFlow Max=0.01 cfs @ 10.10 hrs HW=223.76' (Free Discharge)

↑**2=Exfiltration** (Exfiltration Controls 0.01 cfs)

Primary OutFlow Max=0.58 cfs @ 15.42 hrs HW=229.12' TW=223.14' (Dynamic Tailwater)

↑**1=15" HDPE N-12** (Passes 0.58 cfs of 13.21 cfs potential flow)

↑**3=3" Orifice** (Orifice Controls 0.58 cfs @ 5.90 fps)

↑**4=15" Horizontal Orifice** (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=222.75' TW=223.00' (Dynamic Tailwater)

↑**5=10' Emergency Spillway** (Controls 0.00 cfs)

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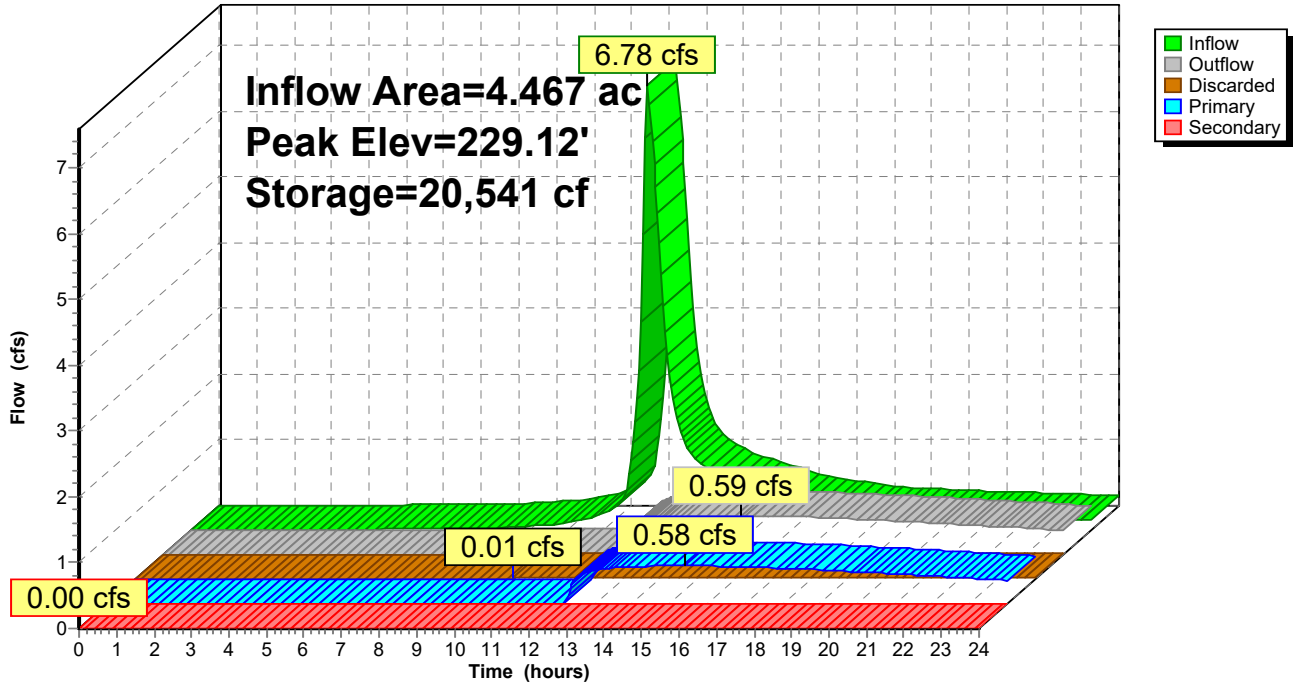
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Pond 107P: Rain Garden #107

Hydrograph



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Summary for Pond 108P: Rain Garden #108

Inflow Area = 0.171 ac, 45.91% Impervious, Inflow Depth > 3.45" for 25YR - 24HR event
 Inflow = 0.68 cfs @ 12.09 hrs, Volume= 0.049 af
 Outflow = 0.05 cfs @ 13.86 hrs, Volume= 0.027 af, Atten= 93%, Lag= 106.2 min
 Primary = 0.02 cfs @ 18.39 hrs, Volume= 0.025 af
 Secondary = 0.02 cfs @ 13.86 hrs, Volume= 0.002 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 206.51' @ 13.86 hrs Surf.Area= 530 sf Storage= 1,314 cf
 Flood Elev= 207.00' Surf.Area= 530 sf Storage= 2,072 cf

Plug-Flow detention time= 346.4 min calculated for 0.027 af (55% of inflow)
 Center-of-Mass det. time= 237.1 min (1,056.7 - 819.6)

Volume	Invert	Avail.Storage	Storage Description
#1	202.50'	212 cf	Stone (Irregular) Listed below (Recalc) -Impervious 530 cf Overall x 40.0% Voids
#2	203.50'	212 cf	Bio-media (Irregular) Listed below (Recalc) 1,060 cf Overall x 20.0% Voids
#3	205.50'	27 cf	Loam (Irregular) Listed below (Recalc) -Impervious 133 cf Overall x 20.0% Voids
#4	205.75'	1,550 cf	Open Water Storage (Irregular) Listed below (Recalc) -Impervious
#5	205.75'	72 cf	Forebay (Irregular) Listed below (Recalc) -Impervious
		2,072 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
202.50	530	89.7	0	0	530
203.50	530	89.7	530	530	620

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
203.50	530	89.7	0	0	530
205.50	530	89.7	1,060	1,060	709

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
205.50	530	89.7	0	0	530
205.75	530	89.7	133	133	552

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
205.75	530	89.7	0	0	530
206.00	1,050	140.4	194	194	1,459
206.50	1,297	161.2	586	779	1,964
207.00	1,800	205.6	771	1,550	3,263

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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
205.75	62	28.3	0	0	62
206.00	83	32.5	18	18	84
206.50	133	41.4	54	72	139

Device	Routing	Invert	Outlet Devices
#1	Primary	202.50'	6.0" Round 6" HDPE N-12 UD L= 22.5' Ke= 0.500 Inlet / Outlet Invert= 202.50' / 202.25' S= 0.0111 '/' Cc= 0.900 n= 0.012, Flow Area= 0.20 sf
#2	Device 1	202.50'	0.7" Vert. 0.75" Orifice C= 0.600
#3	Device 2	203.50'	10.000 in/hr Exfiltration over Surface area
#4	Device 2	206.40'	24.0" Horiz. 24" Drop Inlet C= 0.600 Limited to weir flow at low heads
#5	Secondary	206.50'	10.0' long x 7.0' breadth 10' Emergency spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65 2.65 2.66 2.65 2.66 2.68 2.70 2.73 2.78

Primary OutFlow Max=0.02 cfs @ 18.39 hrs HW=206.46' TW=202.79' (Dynamic Tailwater)

↑ **1=6" HDPE N-12 UD** (Passes 0.02 cfs of 1.74 cfs potential flow)

↑ **2=0.75" Orifice** (Orifice Controls 0.02 cfs @ 9.22 fps)

↑ **3=Exfiltration** (Passes < 0.12 cfs potential flow)

↑ **4=24" Drop Inlet** (Passes < 0.30 cfs potential flow)

Secondary OutFlow Max=0.02 cfs @ 13.86 hrs HW=206.51' TW=203.01' (Dynamic Tailwater)

↑ **5=10' Emergency spillway** (Weir Controls 0.02 cfs @ 0.23 fps)

20-097 Proposed Analysis

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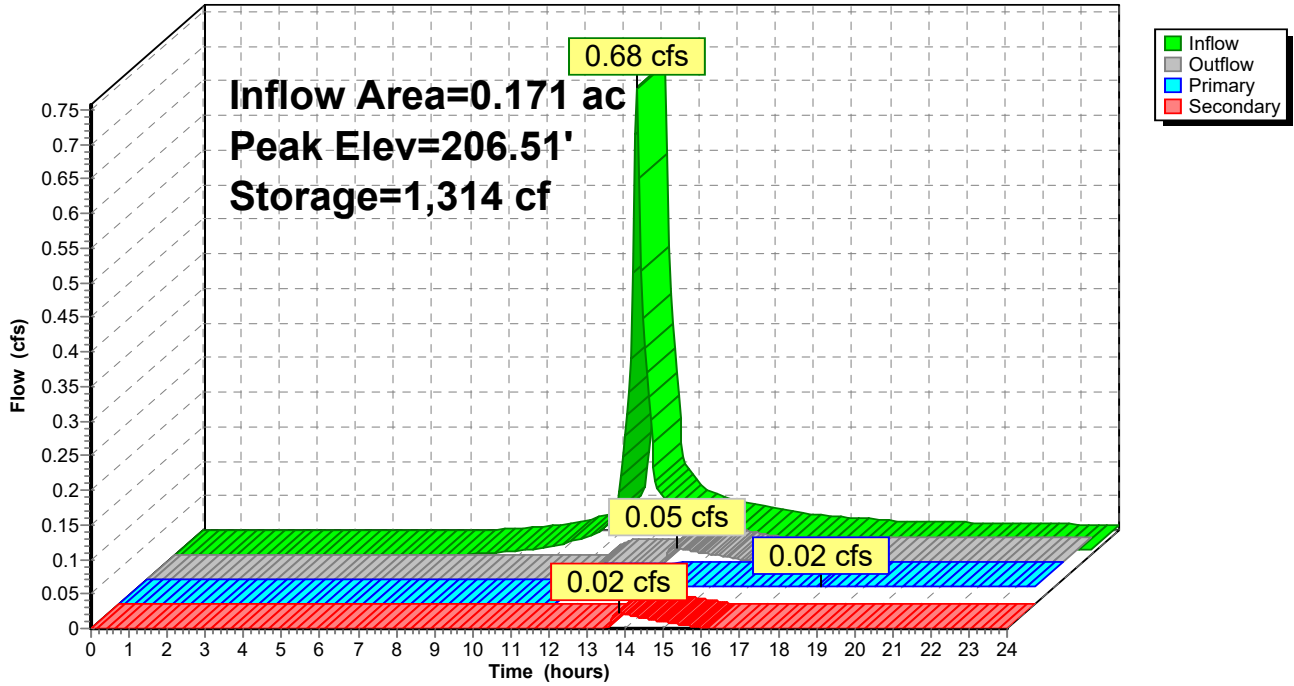
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Pond 108P: Rain Garden #108

Hydrograph



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Summary for Pond 109P: Rain Garden #109

Inflow Area = 6.279 ac, 12.21% Impervious, Inflow Depth > 1.47" for 25YR - 24HR event
 Inflow = 2.93 cfs @ 12.22 hrs, Volume= 0.770 af
 Outflow = 0.94 cfs @ 13.50 hrs, Volume= 0.624 af, Atten= 68%, Lag= 77.0 min
 Primary = 0.94 cfs @ 13.50 hrs, Volume= 0.624 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 217.80' @ 13.50 hrs Surf.Area= 719 sf Storage= 6,590 cf
 Flood Elev= 218.50' Surf.Area= 719 sf Storage= 8,532 cf

Plug-Flow detention time= 141.2 min calculated for 0.623 af (81% of inflow)
 Center-of-Mass det. time= 63.7 min (1,059.3 - 995.6)

Volume	Invert	Avail.Storage	Storage Description
#1	210.75'	288 cf	Stone (Irregular) Listed below (Recalc) -Impervious 719 cf Overall x 40.0% Voids
#2	211.75'	288 cf	Bio Media (Irregular) Listed below (Recalc) 1,438 cf Overall x 20.0% Voids
#3	213.75'	36 cf	Loam (Irregular) Listed below (Recalc) -Impervious 180 cf Overall x 20.0% Voids
#4	214.00'	7,920 cf	Open Water Storage (Irregular) Listed below (Recalc) -Impervious
		8,532 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
210.75	719	114.5	0	0	719
211.75	719	114.5	719	719	834

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
211.75	719	114.5	0	0	719
213.75	719	114.5	1,438	1,438	948

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
213.75	719	114.5	0	0	719
214.00	719	114.5	180	180	748

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
214.00	719	114.5	0	0	719
215.00	1,126	139.0	915	915	1,229
216.00	1,591	160.5	1,352	2,267	1,763
217.00	2,111	181.1	1,845	4,112	2,349
218.00	2,683	199.5	2,391	6,503	2,937
218.50	2,990	209.1	1,418	7,920	3,266

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Device	Routing	Invert	Outlet Devices
#1	Primary	210.75'	15.0" Round 15" HDPE N-12 L= 33.0' Ke= 0.500 Inlet / Outlet Invert= 210.75' / 209.00' S= 0.0530 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	210.75'	1.0" Vert. 1" Orifice C= 0.600
#3	Device 2	211.75'	10.000 in/hr Exfiltration Through Media over Surface area
#4	Device 1	214.65'	3.0" Vert. 3" Orifice C= 0.600
#5	Device 1	217.75'	48.0" Horiz. 48" Structure C= 0.600 Limited to weir flow at low heads
#6	Secondary	218.00'	10.0' long x 7.0' breadth 10' Emergency Spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65 2.65 2.66 2.65 2.66 2.68 2.70 2.73 2.78

Primary OutFlow Max=0.94 cfs @ 13.50 hrs HW=217.80' TW=208.11' (Dynamic Tailwater)

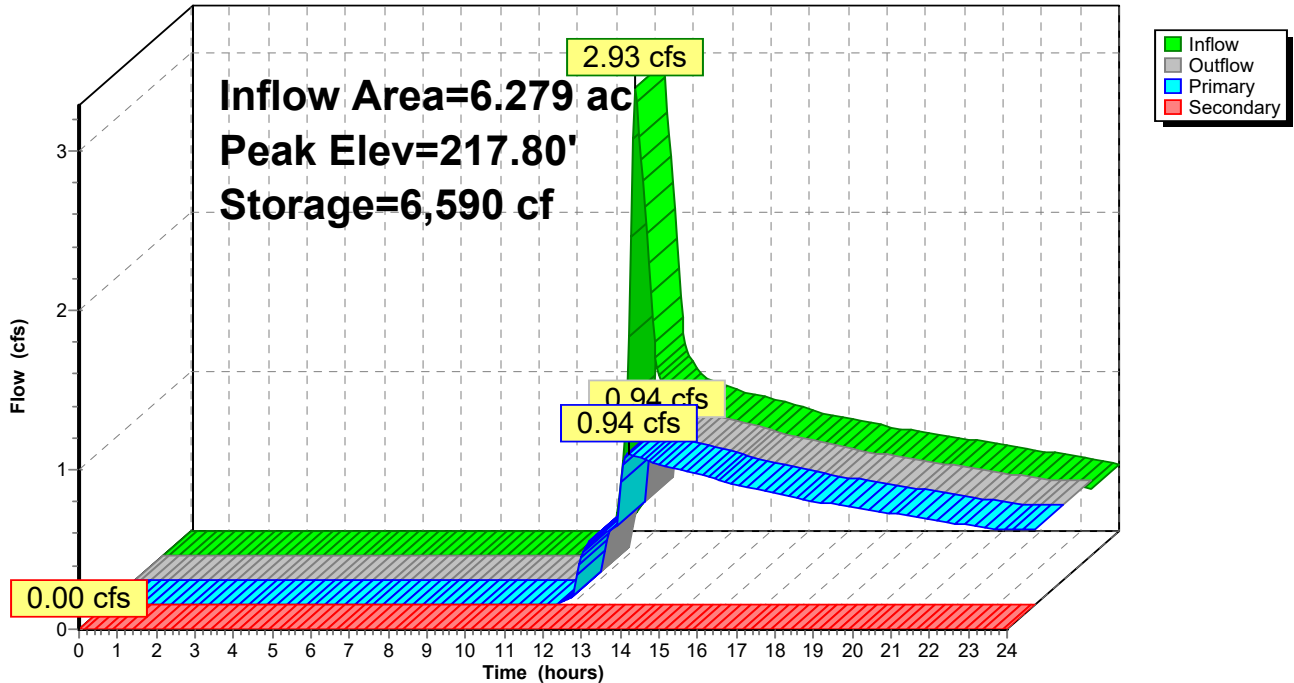
- 1=15" HDPE N-12 (Passes 0.94 cfs of 14.98 cfs potential flow)
- 2=1" Orifice (Orifice Controls 0.07 cfs @ 12.75 fps)
- 3=Exfiltration Through Media (Passes 0.07 cfs of 0.17 cfs potential flow)
- 4=3" Orifice (Orifice Controls 0.41 cfs @ 8.37 fps)
- 5=48" Structure (Weir Controls 0.46 cfs @ 0.73 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=210.75' TW=208.00' (Dynamic Tailwater)

- 6=10' Emergency Spillway (Controls 0.00 cfs)

Pond 109P: Rain Garden #109

Hydrograph



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Summary for Pond 110P: Detention Pond #110

Inflow Area = 3.275 ac, 0.59% Impervious, Inflow Depth > 1.67" for 25YR - 24HR event
 Inflow = 3.50 cfs @ 12.38 hrs, Volume= 0.456 af
 Outflow = 0.66 cfs @ 13.66 hrs, Volume= 0.415 af, Atten= 81%, Lag= 76.9 min
 Primary = 0.66 cfs @ 13.66 hrs, Volume= 0.415 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 220.33' @ 13.66 hrs Surf.Area= 7,637 sf Storage= 7,901 cf
 Flood Elev= 222.00' Surf.Area= 8,493 sf Storage= 15,228 cf

Plug-Flow detention time= 166.6 min calculated for 0.415 af (91% of inflow)
 Center-of-Mass det. time= 122.9 min (1,005.3 - 882.4)

Volume	Invert	Avail.Storage	Storage Description
#1	217.50'	6,174 cf	Detention Area (Irregular) Listed below (Recalc)
#2	218.00'	442 cf	Sediment Forebay (Irregular) Listed below (Recalc)
#3	220.00'	8,611 cf	Open Water Storage (Irregular) Listed below (Recalc)
		15,228 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
217.50	128	39.7	0	0	128
218.00	2,386	203.9	511	511	3,312
219.00	2,825	219.3	2,602	3,114	3,872
220.00	3,303	236.5	3,061	6,174	4,536

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
218.00	103	39.9	0	0	103
219.00	214	54.9	155	155	226
220.00	367	71.7	287	442	406

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
220.00	3,806	241.3	0	0	3,806
221.00	4,302	250.1	4,051	4,051	4,229
222.00	4,823	266.8	4,560	8,611	4,963

Device	Routing	Invert	Outlet Devices
#1	Primary	217.50'	15.0" Round 15" HDPE N-12 L= 12.5' Ke= 0.500 Inlet / Outlet Invert= 217.50' / 217.00' S= 0.0400 1' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	218.00'	3.0" Vert. 3" Orifice C= 0.600
#3	Device 1	218.50'	3.0" Vert. 3" Orifice C= 0.600
#4	Device 1	221.25'	48.0" Horiz. 48" Structure C= 0.600 Limited to weir flow at low heads
#5	Secondary	221.50'	10.0' long x 7.0' breadth 10' Emergency Spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50

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Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65
2.65 2.66 2.65 2.66 2.68 2.70 2.73 2.78

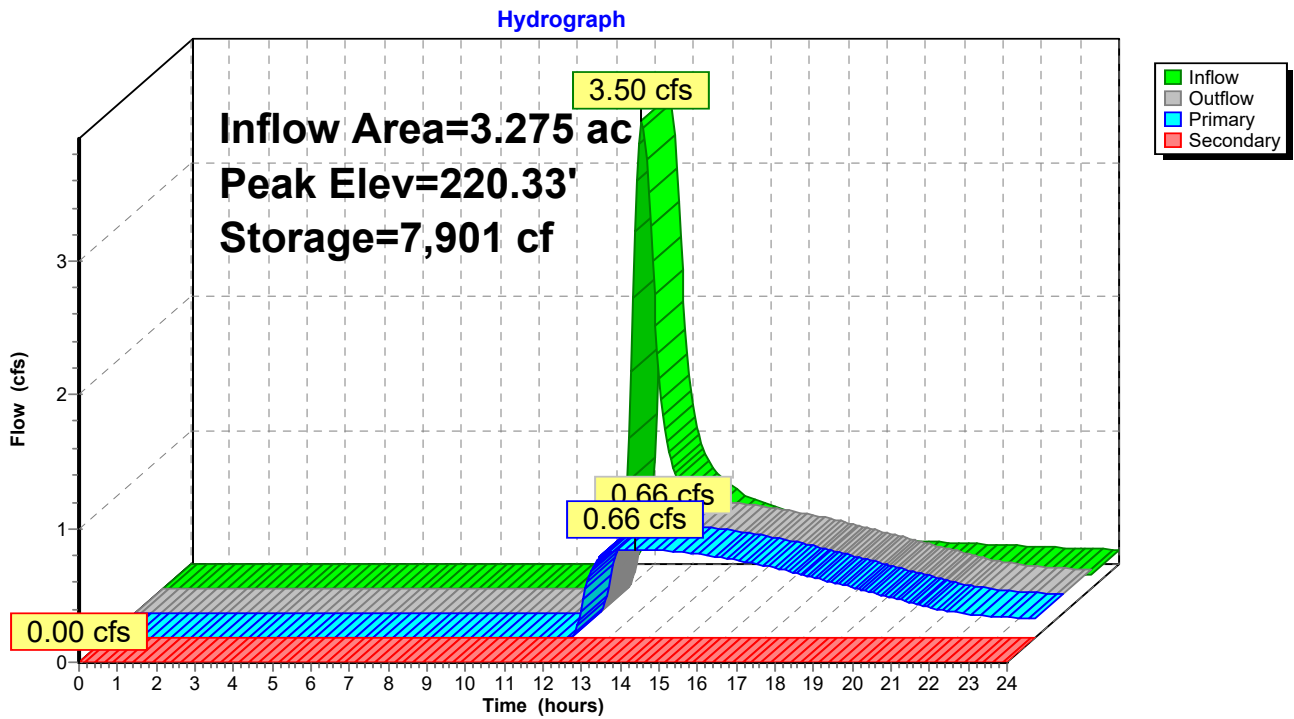
Primary OutFlow Max=0.66 cfs @ 13.66 hrs HW=220.33' TW=217.62' (Dynamic Tailwater)

- 1=15" HDPE N-12 (Passes 0.66 cfs of 8.77 cfs potential flow)
- 2=3" Orifice (Orifice Controls 0.35 cfs @ 7.15 fps)
- 3=3" Orifice (Orifice Controls 0.31 cfs @ 6.29 fps)
- 4=48" Structure (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=217.50' TW=217.50' (Dynamic Tailwater)

- 5=10' Emergency Spillway (Controls 0.00 cfs)

Pond 110P: Detention Pond #110



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Summary for Pond C30P: CB #30

[80] Warning: Exceeded Pond 1P by 0.16' @ 12.10 hrs (0.42 cfs 0.002 af)

Inflow Area = 6.603 ac, 6.70% Impervious, Inflow Depth > 0.85" for 25YR - 24HR event
 Inflow = 1.63 cfs @ 12.65 hrs, Volume= 0.470 af
 Outflow = 1.64 cfs @ 12.65 hrs, Volume= 0.469 af, Atten= 0%, Lag= 0.1 min
 Primary = 1.64 cfs @ 12.65 hrs, Volume= 0.469 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 201.36' @ 12.25 hrs Surf.Area= 13 sf Storage= 13 cf
 Flood Elev= 204.00' Surf.Area= 13 sf Storage= 46 cf

Plug-Flow detention time= 0.2 min calculated for 0.468 af (100% of inflow)
 Center-of-Mass det. time= 0.1 min (934.2 - 934.1)

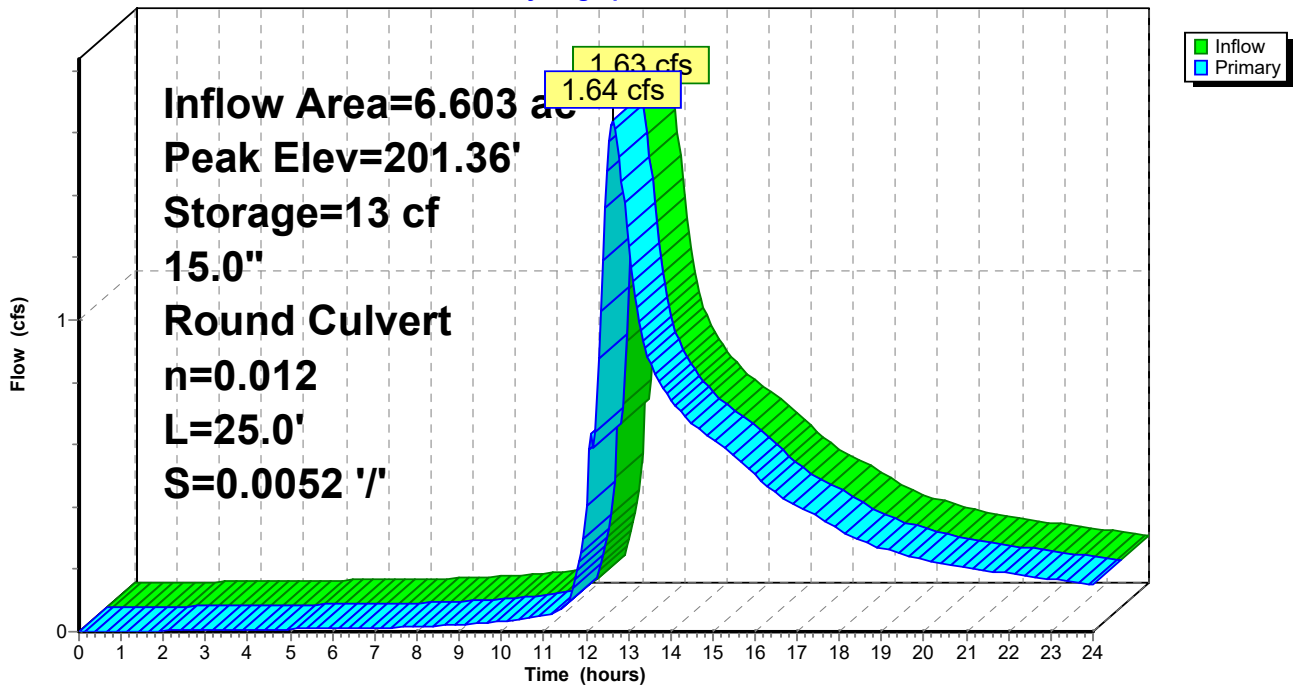
Volume	Invert	Avail.Storage	Storage Description
#1	200.30'	46 cf	4.00'D x 3.70'H Basin

Device	Routing	Invert	Outlet Devices
#1	Primary	200.30'	15.0" Round 15" HDPE N-12 L= 25.0' Ke= 0.500 Inlet / Outlet Invert= 200.30' / 200.17' S= 0.0052 '/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=1.68 cfs @ 12.65 hrs HW=201.18' TW=200.97' (Dynamic Tailwater)
 ←1=15" HDPE N-12 (Outlet Controls 1.68 cfs @ 2.57 fps)

Pond C30P: CB #30

Hydrograph



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Summary for Pond C31P: CB #31

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)

[80] Warning: Exceeded Pond C32P by 0.19' @ 12.10 hrs (2.57 cfs 0.287 af)

Inflow Area = 0.287 ac, 66.40% Impervious, Inflow Depth > 4.34" for 25YR - 24HR event
 Inflow = 1.38 cfs @ 12.09 hrs, Volume= 0.104 af
 Outflow = 1.36 cfs @ 12.09 hrs, Volume= 0.103 af, Atten= 1%, Lag= 0.0 min
 Primary = 1.36 cfs @ 12.09 hrs, Volume= 0.103 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 216.49' @ 12.22 hrs Surf.Area= 13 sf Storage= 29 cf
 Flood Elev= 217.90' Surf.Area= 13 sf Storage= 47 cf

Plug-Flow detention time= 4.2 min calculated for 0.103 af (99% of inflow)
 Center-of-Mass det. time= 0.8 min (796.4 - 795.5)

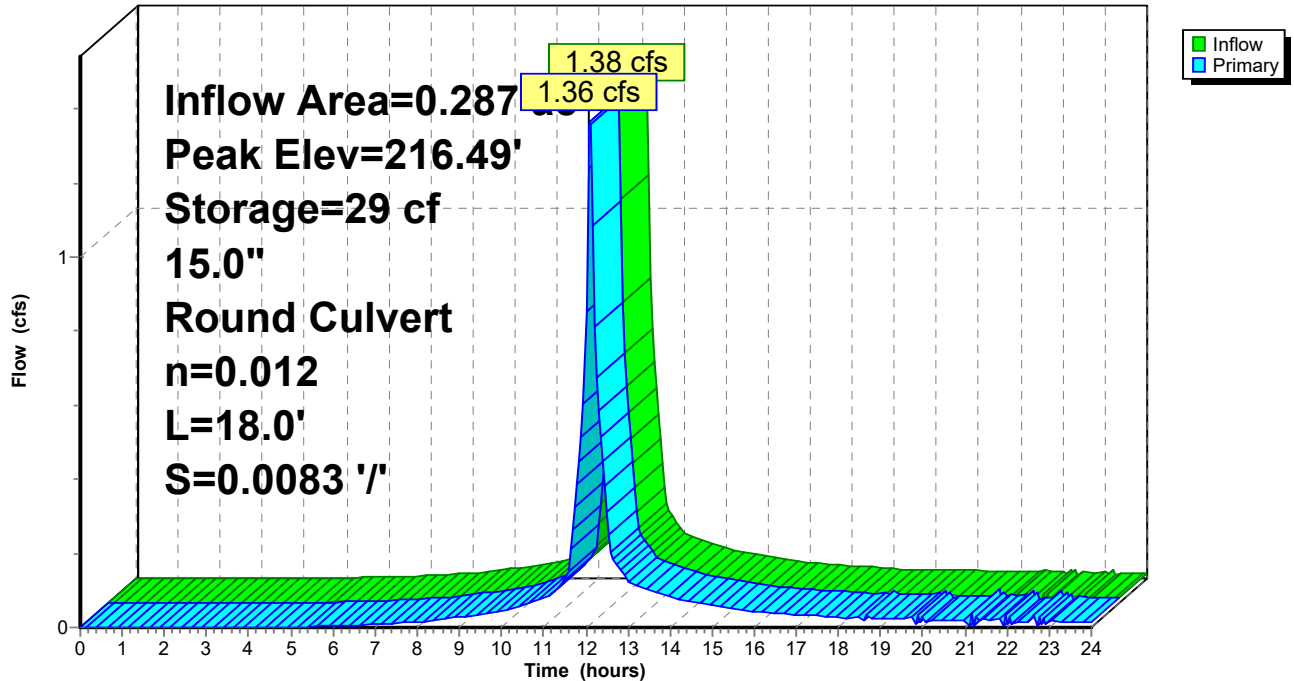
Volume	Invert	Avail.Storage	Storage Description
#1	214.15'	47 cf	4.00'D x 3.75'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	214.15'	15.0" Round 15" HDPE N-12 L= 18.0' Ke= 0.500 Inlet / Outlet Invert= 214.15' / 214.00' S= 0.0083 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=1.36 cfs @ 12.09 hrs HW=216.28' TW=216.23' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Inlet Controls 1.36 cfs @ 1.11 fps)

Pond C31P: CB #31

Hydrograph



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Summary for Pond C32P: CB #32

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=32)

Inflow Area = 0.131 ac, 79.08% Impervious, Inflow Depth > 4.71" for 25YR - 24HR event
 Inflow = 0.67 cfs @ 12.09 hrs, Volume= 0.051 af
 Outflow = 0.66 cfs @ 12.09 hrs, Volume= 0.051 af, Atten= 2%, Lag= 0.0 min
 Primary = 0.66 cfs @ 12.09 hrs, Volume= 0.051 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 216.49' @ 12.27 hrs Surf.Area= 13 sf Storage= 26 cf
 Flood Elev= 217.90' Surf.Area= 13 sf Storage= 44 cf

Plug-Flow detention time= 7.3 min calculated for 0.051 af (99% of inflow)
 Center-of-Mass det. time= 1.3 min (786.3 - 785.0)

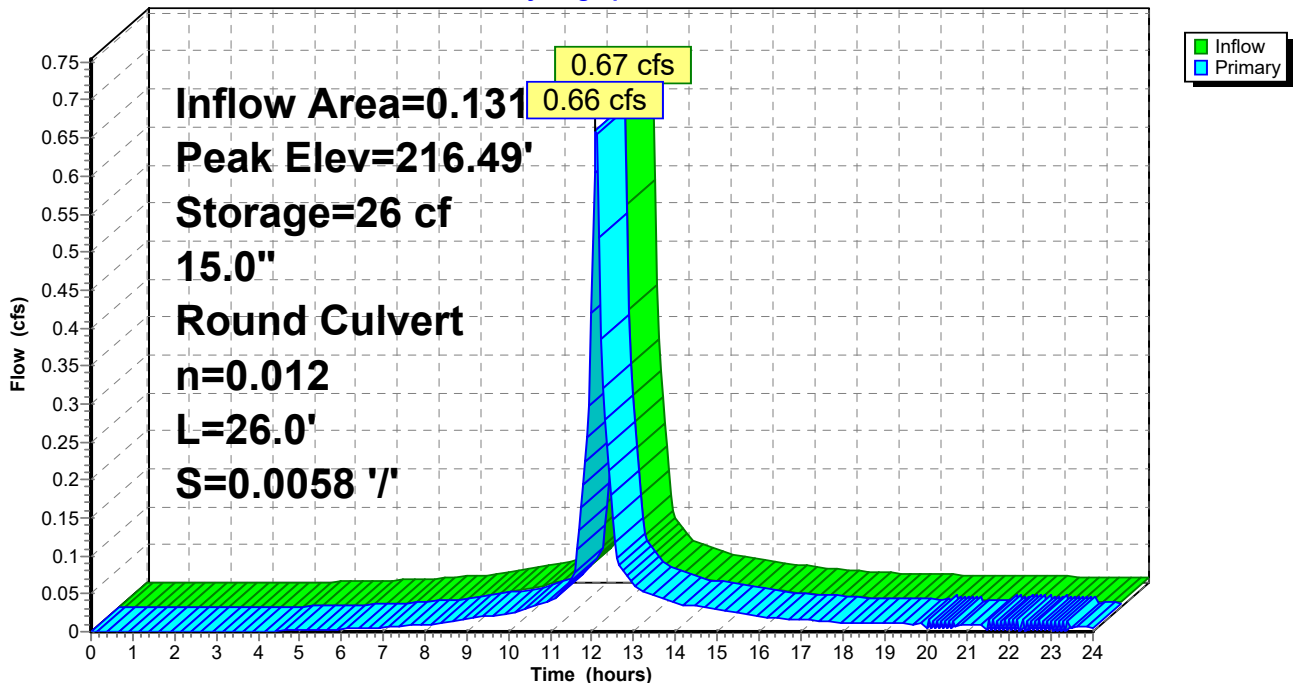
Volume	Invert	Avail.Storage	Storage Description
#1	214.40'	44 cf	4.00'D x 3.50'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	214.40'	15.0" Round 15" HDPE N-12 L= 26.0' Ke= 0.500 Inlet / Outlet Invert= 214.40' / 214.25' S= 0.0058 '/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=216.09' TW=216.28' (Dynamic Tailwater)
 ←1=15" HDPE N-12 (Controls 0.00 cfs)

Pond C32P: CB #32

Hydrograph



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Summary for Pond C33P: CB #33

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=42)

Inflow Area = 0.338 ac, 60.85% Impervious, Inflow Depth > 4.06" for 25YR - 24HR event
 Inflow = 1.56 cfs @ 12.09 hrs, Volume= 0.115 af
 Outflow = 1.55 cfs @ 12.09 hrs, Volume= 0.114 af, Atten= 1%, Lag= 0.0 min
 Primary = 1.55 cfs @ 12.09 hrs, Volume= 0.114 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 214.47' @ 13.23 hrs Surf.Area= 13 sf Storage= 25 cf
 Flood Elev= 216.00' Surf.Area= 13 sf Storage= 44 cf

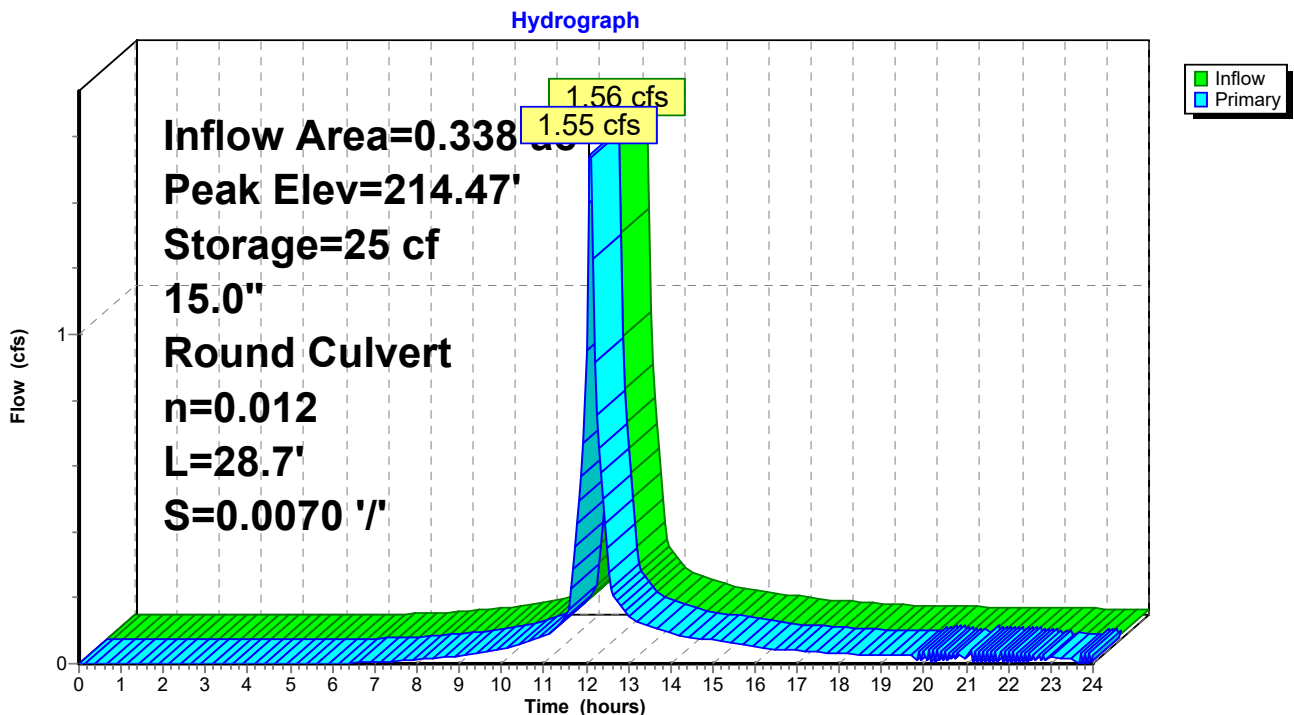
Plug-Flow detention time= 3.1 min calculated for 0.114 af (100% of inflow)
 Center-of-Mass det. time= 0.7 min (804.6 - 803.9)

Volume	Invert	Avail.Storage	Storage Description
#1	212.50'	44 cf	4.00'D x 3.50'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	212.50'	15.0" Round 15" HDPE N-12 L= 28.7' Ke= 0.500 Inlet / Outlet Invert= 212.50' / 212.30' S= 0.0070 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=213.78' TW=213.88' (Dynamic Tailwater)
 ←1=15" HDPE N-12 (Controls 0.00 cfs)

Pond C33P: CB #33



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Summary for Pond C34P: CB #34

Inflow Area = 0.119 ac, 100.00% Impervious, Inflow Depth > 5.62" for 25YR - 24HR event
 Inflow = 0.66 cfs @ 12.09 hrs, Volume= 0.056 af
 Outflow = 0.67 cfs @ 12.09 hrs, Volume= 0.055 af, Atten= 0%, Lag= 0.1 min
 Primary = 0.67 cfs @ 12.09 hrs, Volume= 0.055 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 216.93' @ 12.09 hrs Surf.Area= 13 sf Storage= 9 cf
 Flood Elev= 220.05' Surf.Area= 13 sf Storage= 44 cf

Plug-Flow detention time= 2.5 min calculated for 0.055 af (100% of inflow)
 Center-of-Mass det. time= 1.4 min (746.4 - 745.1)

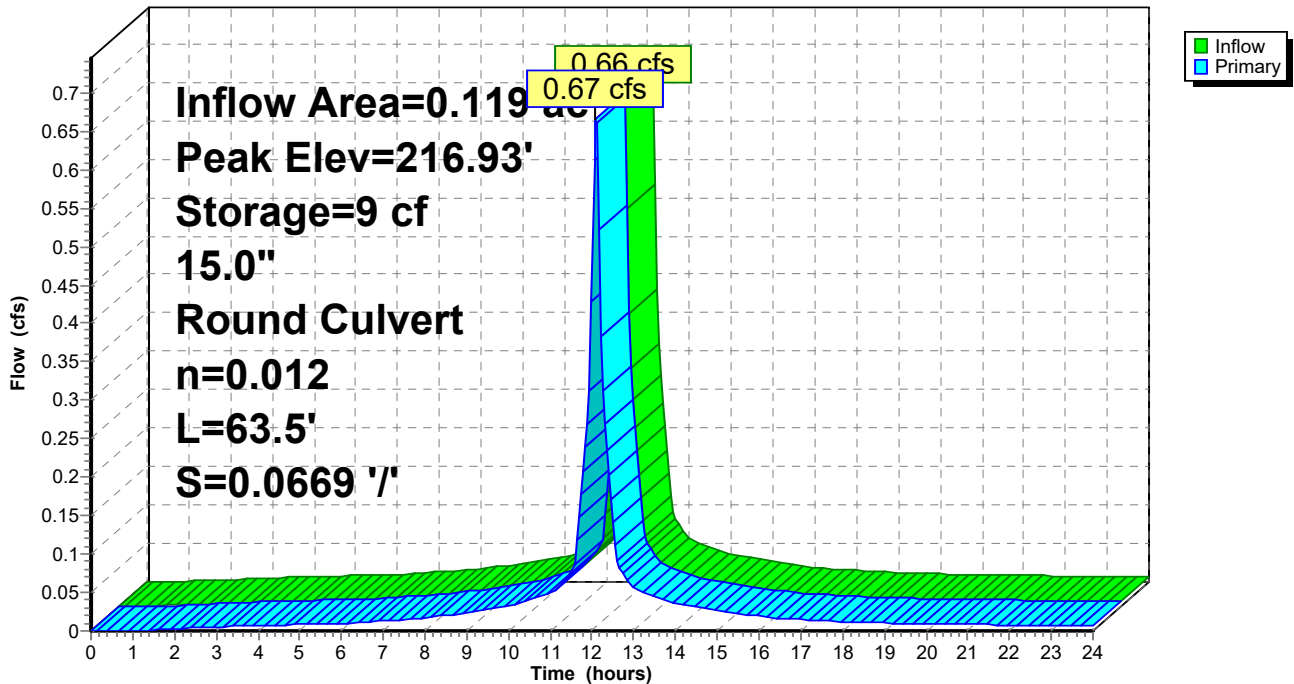
Volume	Invert	Avail.Storage	Storage Description
#1	216.25'	44 cf	4.00'D x 3.50'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	216.55'	15.0" Round 15" HDPE N-12 L= 63.5' Ke= 0.500 Inlet / Outlet Invert= 216.55' / 212.30' S= 0.0669 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.65 cfs @ 12.09 hrs HW=216.93' TW=213.87' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Inlet Controls 0.65 cfs @ 2.09 fps)

Pond C34P: CB #34

Hydrograph



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Summary for Pond C35P: CB #35

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=31)

Inflow Area = 0.146 ac, 67.93% Impervious, Inflow Depth > 4.27" for 25YR - 24HR event
 Inflow = 0.70 cfs @ 12.09 hrs, Volume= 0.052 af
 Outflow = 0.68 cfs @ 12.09 hrs, Volume= 0.051 af, Atten= 3%, Lag= 0.0 min
 Primary = 0.68 cfs @ 12.09 hrs, Volume= 0.051 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 219.62' @ 12.53 hrs Surf.Area= 13 sf Storage= 35 cf
 Flood Elev= 220.30' Surf.Area= 13 sf Storage= 44 cf

Plug-Flow detention time= 9.3 min calculated for 0.051 af (99% of inflow)
 Center-of-Mass det. time= 2.3 min (800.4 - 798.1)

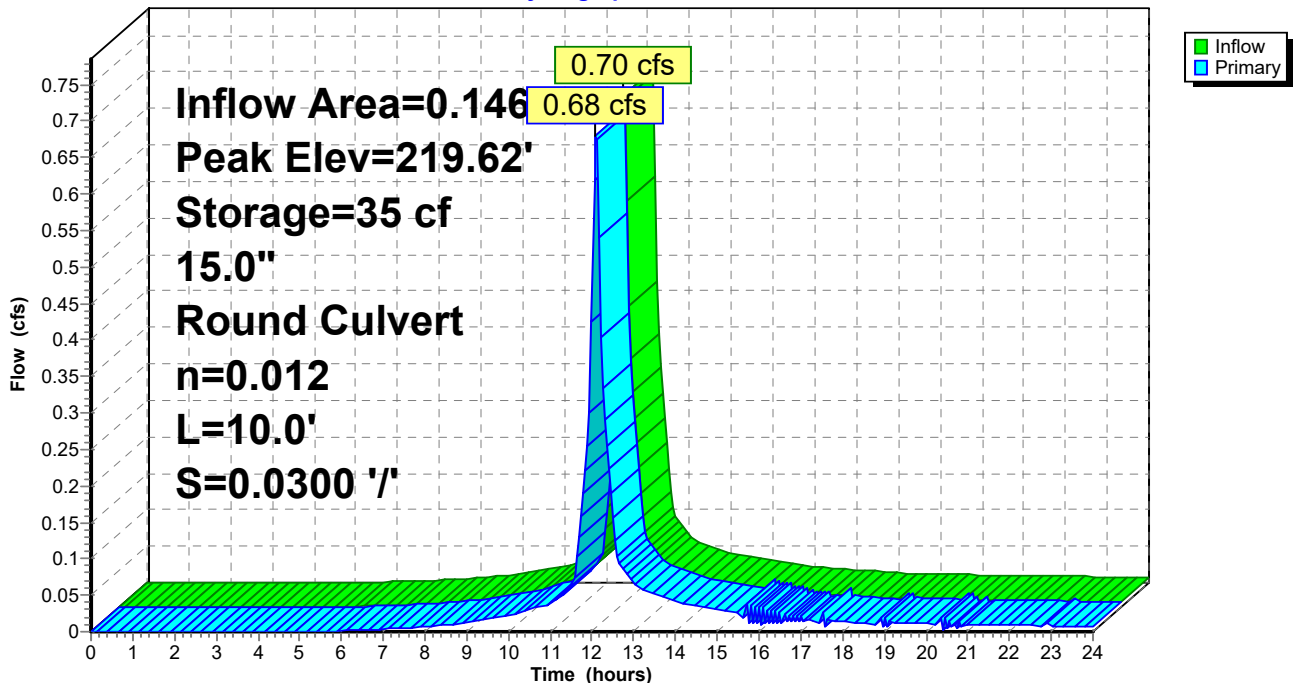
Volume	Invert	Avail.Storage	Storage Description
#1	216.80'	44 cf	4.00'D x 3.50'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	216.80'	15.0" Round 15" HDPE N-12 L= 10.0' Ke= 0.500 Inlet / Outlet Invert= 216.80' / 216.50' S= 0.0300 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.71 cfs @ 12.09 hrs HW=218.74' TW=218.73' (Dynamic Tailwater)
 ←1=15" HDPE N-12 (Inlet Controls 0.71 cfs @ 0.58 fps)

Pond C35P: CB #35

Hydrograph



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Summary for Pond C36P: CB #36

Inflow Area = 0.173 ac, 93.27% Impervious, Inflow Depth > 5.38" for 25YR - 24HR event
 Inflow = 0.96 cfs @ 12.09 hrs, Volume= 0.078 af
 Outflow = 0.96 cfs @ 12.09 hrs, Volume= 0.078 af, Atten= 0%, Lag= 0.1 min
 Primary = 0.96 cfs @ 12.09 hrs, Volume= 0.078 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 225.21' @ 12.09 hrs Surf.Area= 13 sf Storage= 7 cf
 Flood Elev= 228.19' Surf.Area= 13 sf Storage= 44 cf

Plug-Flow detention time= 0.4 min calculated for 0.078 af (100% of inflow)
 Center-of-Mass det. time= 0.3 min (758.6 - 758.3)

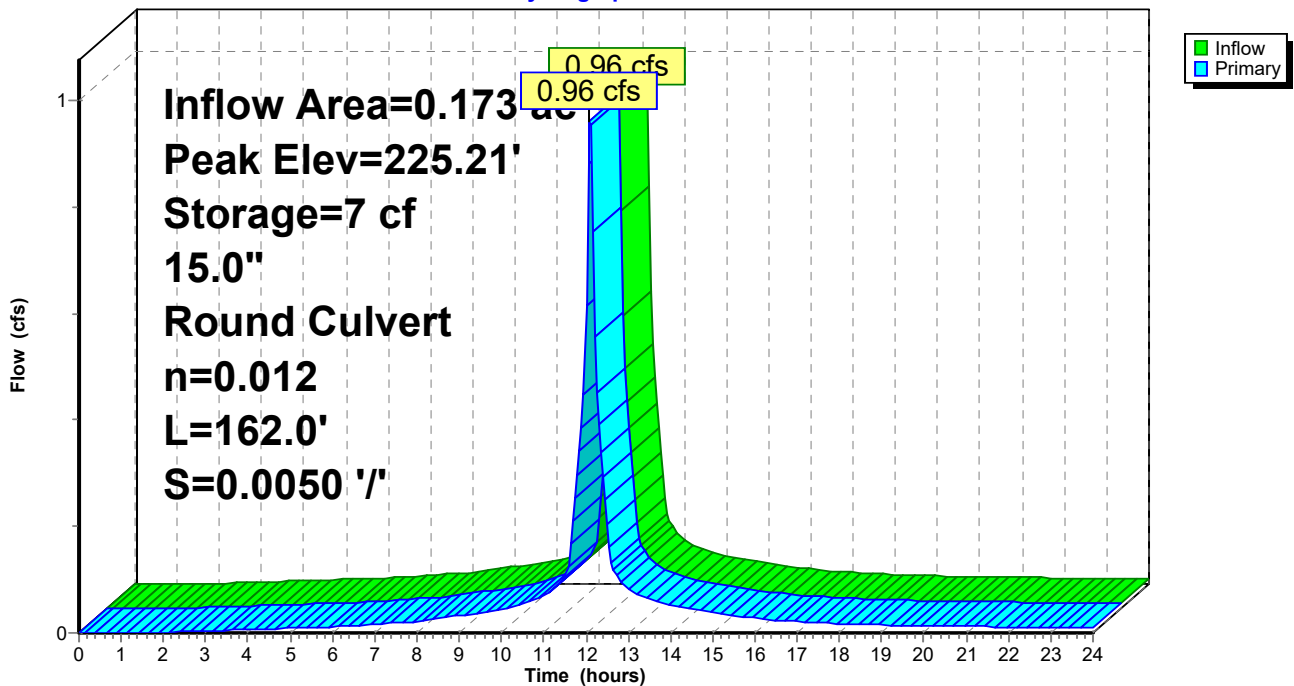
Volume	Invert	Avail.Storage	Storage Description
#1	224.69'	44 cf	4.00'D x 3.50'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	224.69'	15.0" Round 15" HDPE N-12 L= 162.0' Ke= 0.500 Inlet / Outlet Invert= 224.69' / 223.88' S= 0.0050 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.94 cfs @ 12.09 hrs HW=225.21' TW=224.34' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Outlet Controls 0.94 cfs @ 2.90 fps)

Pond C36P: CB #36

Hydrograph



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Summary for Pond C37P: CB #37

Inflow Area = 0.382 ac, 86.35% Impervious, Inflow Depth > 5.07" for 25YR - 24HR event
 Inflow = 2.05 cfs @ 12.09 hrs, Volume= 0.162 af
 Outflow = 2.06 cfs @ 12.09 hrs, Volume= 0.162 af, Atten= 0%, Lag= 0.1 min
 Primary = 2.06 cfs @ 12.09 hrs, Volume= 0.162 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 224.35' @ 12.09 hrs Surf.Area= 13 sf Storage= 9 cf
 Flood Elev= 228.64' Surf.Area= 13 sf Storage= 63 cf

Plug-Flow detention time= 0.3 min calculated for 0.162 af (100% of inflow)
 Center-of-Mass det. time= 0.2 min (770.6 - 770.4)

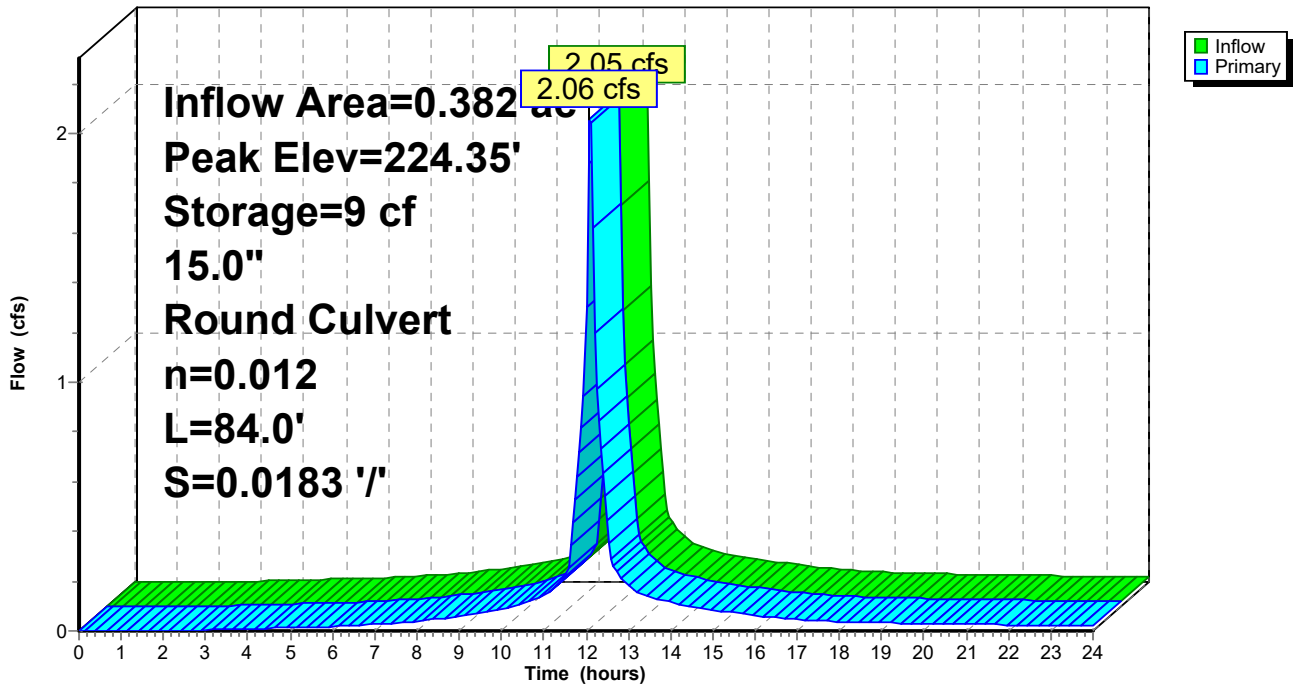
Volume	Invert	Avail.Storage	Storage Description
#1	223.64'	63 cf	4.00'D x 5.00'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	223.64'	15.0" Round 15" HDPE N-12 L= 84.0' Ke= 0.500 Inlet / Outlet Invert= 223.64' / 222.10' S= 0.0183 1/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=2.00 cfs @ 12.09 hrs HW=224.34' TW=223.03' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Inlet Controls 2.00 cfs @ 2.84 fps)

Pond C37P: CB #37

Hydrograph



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Summary for Pond C38P: CB #38

Inflow Area = 0.193 ac, 77.58% Impervious, Inflow Depth > 4.71" for 25YR - 24HR event
 Inflow = 0.99 cfs @ 12.09 hrs, Volume= 0.076 af
 Outflow = 0.99 cfs @ 12.09 hrs, Volume= 0.075 af, Atten= 0%, Lag= 0.1 min
 Primary = 0.99 cfs @ 12.09 hrs, Volume= 0.075 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 219.68' @ 12.09 hrs Surf.Area= 13 sf Storage= 6 cf
 Flood Elev= 222.68' Surf.Area= 13 sf Storage= 44 cf

Plug-Flow detention time= 0.4 min calculated for 0.075 af (100% of inflow)
 Center-of-Mass det. time= 0.3 min (785.3 - 785.0)

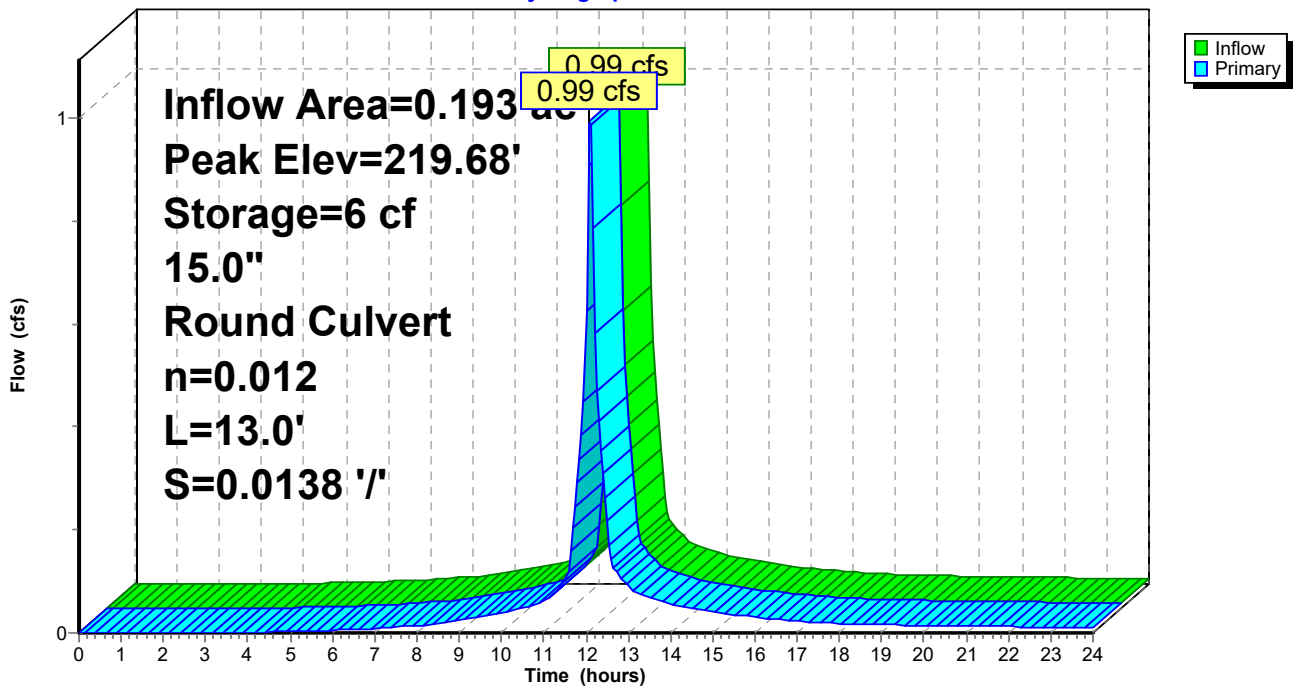
Volume	Invert	Avail.Storage	Storage Description
#1	219.18'	44 cf	4.00'D x 3.50'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	219.18'	15.0" Round 15" HDPE N-12 L= 13.0' Ke= 0.500 Inlet / Outlet Invert= 219.18' / 219.00' S= 0.0138 1/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.97 cfs @ 12.09 hrs HW=219.67' TW=218.72' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Barrel Controls 0.97 cfs @ 3.18 fps)

Pond C38P: CB #38

Hydrograph



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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Summary for Pond C39P: CB #39

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=27)

[80] Warning: Exceeded Pond C40P by 0.29' @ 12.10 hrs (3.20 cfs 0.338 af)

Inflow Area = 0.290 ac, 54.32% Impervious, Inflow Depth > 3.91" for 25YR - 24HR event
 Inflow = 1.23 cfs @ 12.09 hrs, Volume= 0.094 af
 Outflow = 1.20 cfs @ 12.09 hrs, Volume= 0.094 af, Atten= 2%, Lag= 0.0 min
 Primary = 1.20 cfs @ 12.09 hrs, Volume= 0.094 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 219.62' @ 12.52 hrs Surf.Area= 13 sf Storage= 39 cf
 Flood Elev= 220.50' Surf.Area= 13 sf Storage= 50 cf

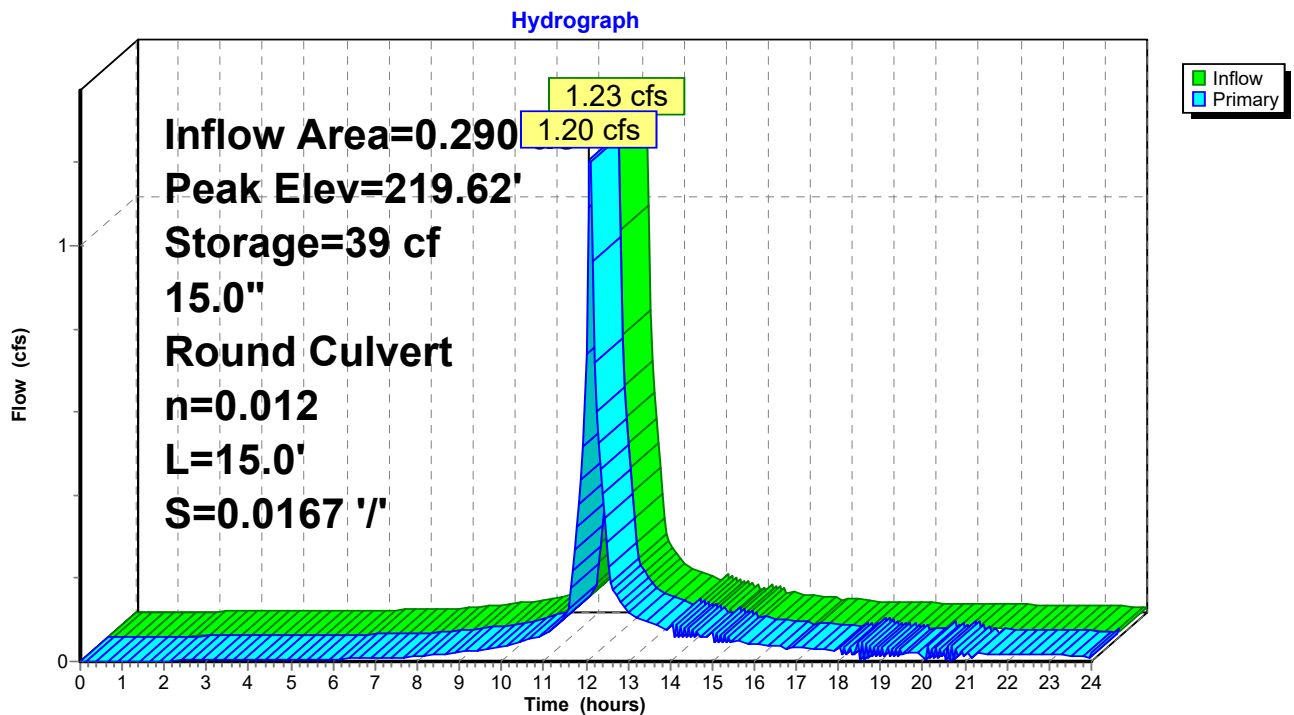
Plug-Flow detention time= 5.8 min calculated for 0.093 af (99% of inflow)
 Center-of-Mass det. time= 1.2 min (796.8 - 795.6)

Volume	Invert	Avail.Storage	Storage Description
#1	216.50'	50 cf	4.00'D x 4.00'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	216.50'	15.0" Round 15" HDPE N-12 L= 15.0' Ke= 0.500 Inlet / Outlet Invert= 216.50' / 216.25' S= 0.0167 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=1.20 cfs @ 12.09 hrs HW=218.77' TW=218.73' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Inlet Controls 1.20 cfs @ 0.98 fps)

Pond C39P: CB #39



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Summary for Pond C40P: CB #40

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=52)

Inflow Area = 0.074 ac, 100.00% Impervious, Inflow Depth > 5.62" for 25YR - 24HR event
 Inflow = 0.41 cfs @ 12.09 hrs, Volume= 0.034 af
 Outflow = 0.39 cfs @ 12.09 hrs, Volume= 0.034 af, Atten= 5%, Lag= 0.0 min
 Primary = 0.39 cfs @ 12.09 hrs, Volume= 0.034 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 219.62' @ 12.58 hrs Surf.Area= 13 sf Storage= 33 cf
 Flood Elev= 220.50' Surf.Area= 13 sf Storage= 44 cf

Plug-Flow detention time= 13.1 min calculated for 0.034 af (98% of inflow)
 Center-of-Mass det. time= 3.2 min (748.3 - 745.1)

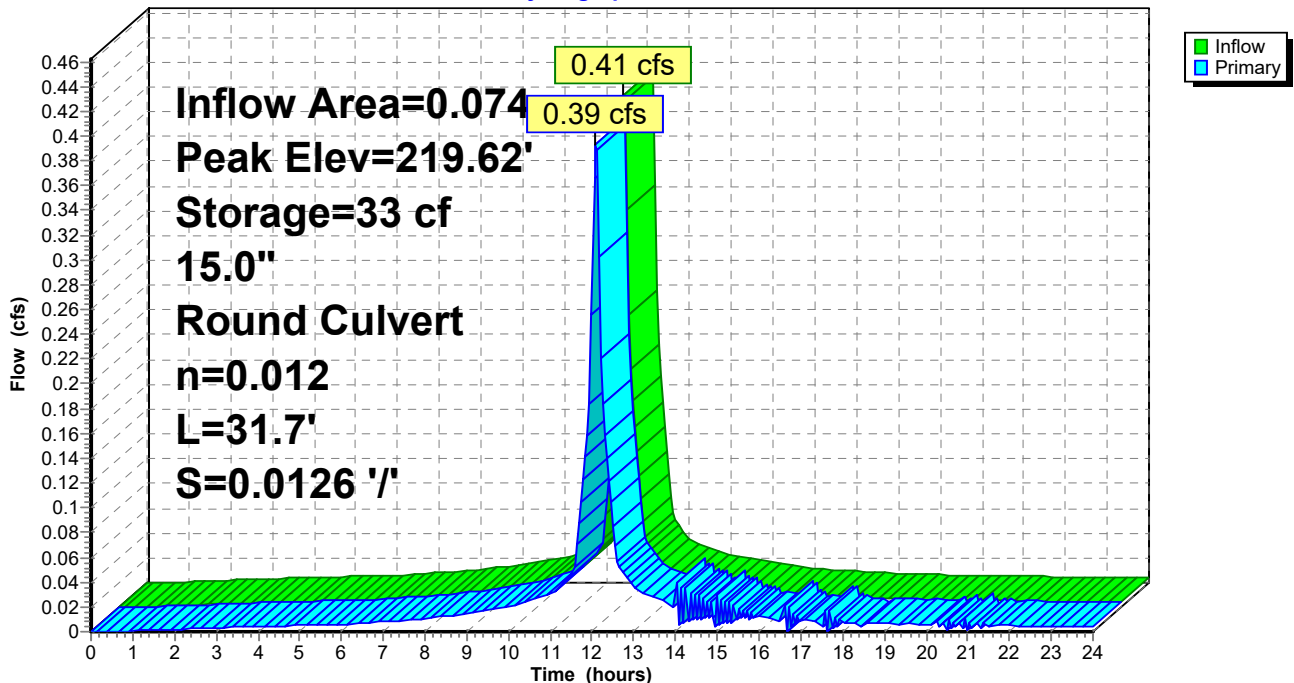
Volume	Invert	Avail.Storage	Storage Description
#1	217.00'	44 cf	4.00'D x 3.50'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	217.00'	15.0" Round 15" HDPE N-12 L= 31.7' Ke= 0.500 Inlet / Outlet Invert= 217.00' / 216.60' S= 0.0126 '/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=218.46' TW=218.74' (Dynamic Tailwater)
 ←1=15" HDPE N-12 (Controls 0.00 cfs)

Pond C40P: CB #40

Hydrograph



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Summary for Pond C41P: CB #41

[80] Warning: Exceeded Pond 49P by 0.20' @ 12.15 hrs (2.57 cfs 0.140 af)

[80] Warning: Exceeded Pond C42P by 0.23' @ 12.10 hrs (2.86 cfs 0.261 af)

Inflow Area = 0.440 ac, 76.05% Impervious, Inflow Depth > 4.58" for 25YR - 24HR event
 Inflow = 1.99 cfs @ 12.09 hrs, Volume= 0.168 af
 Outflow = 1.98 cfs @ 12.09 hrs, Volume= 0.168 af, Atten= 1%, Lag= 0.0 min
 Primary = 1.98 cfs @ 12.09 hrs, Volume= 0.168 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 218.85' @ 13.95 hrs Surf.Area= 13 sf Storage= 39 cf
 Flood Elev= 219.75' Surf.Area= 13 sf Storage= 50 cf

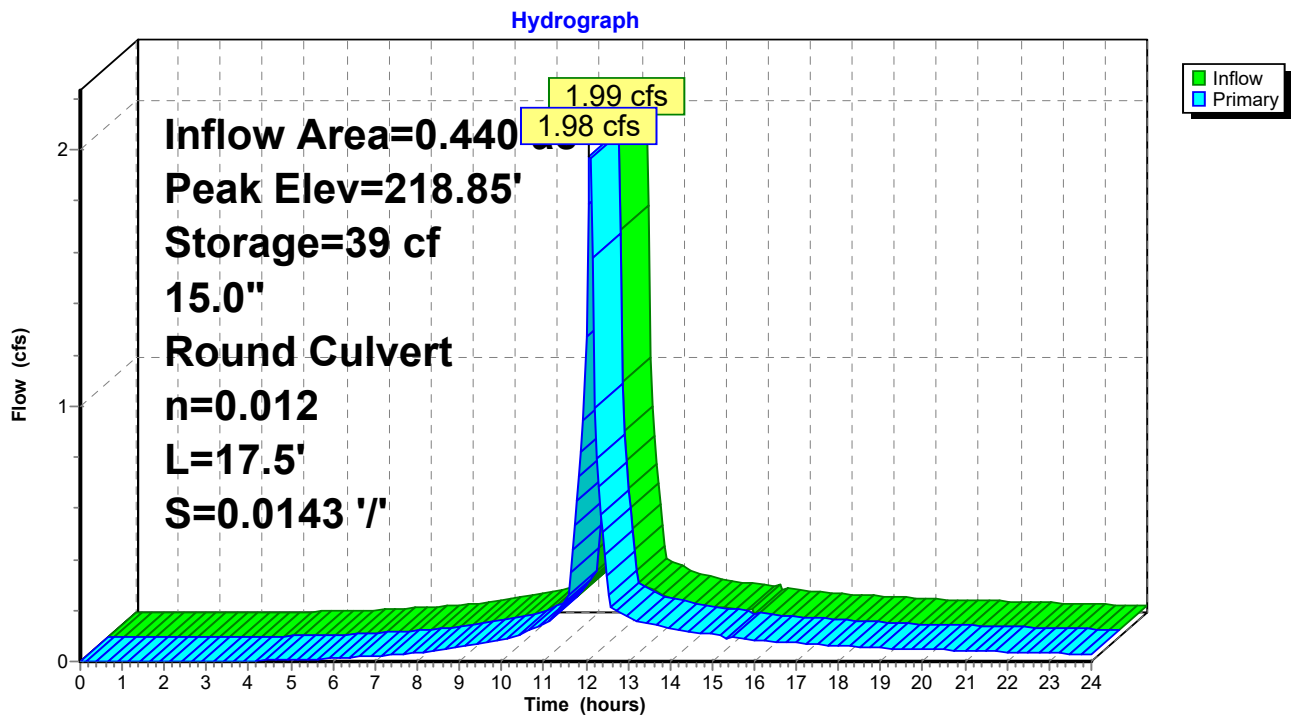
Plug-Flow detention time= 3.3 min calculated for 0.167 af (99% of inflow)
 Center-of-Mass det. time= 1.2 min (809.7 - 808.4)

Volume	Invert	Avail.Storage	Storage Description
#1	215.75'	50 cf	4.00'D x 4.00'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	215.75'	15.0" Round 15" HDPE N-12 L= 17.5' Ke= 0.500 Inlet / Outlet Invert= 215.75' / 215.50' S= 0.0143 '/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=1.97 cfs @ 12.09 hrs HW=217.65' TW=217.54' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Inlet Controls 1.97 cfs @ 1.60 fps)

Pond C41P: CB #41



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Summary for Pond C42P: CB #42

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=30)

Inflow Area = 0.107 ac, 81.42% Impervious, Inflow Depth > 4.93" for 25YR - 24HR event
 Inflow = 0.57 cfs @ 12.09 hrs, Volume= 0.044 af
 Outflow = 0.55 cfs @ 12.09 hrs, Volume= 0.043 af, Atten= 3%, Lag= 0.1 min
 Primary = 0.55 cfs @ 12.09 hrs, Volume= 0.043 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 218.85' @ 14.00 hrs Surf.Area= 13 sf Storage= 33 cf
 Flood Elev= 219.75' Surf.Area= 13 sf Storage= 44 cf

Plug-Flow detention time= 10.0 min calculated for 0.043 af (99% of inflow)
 Center-of-Mass det. time= 3.6 min (781.1 - 777.4)

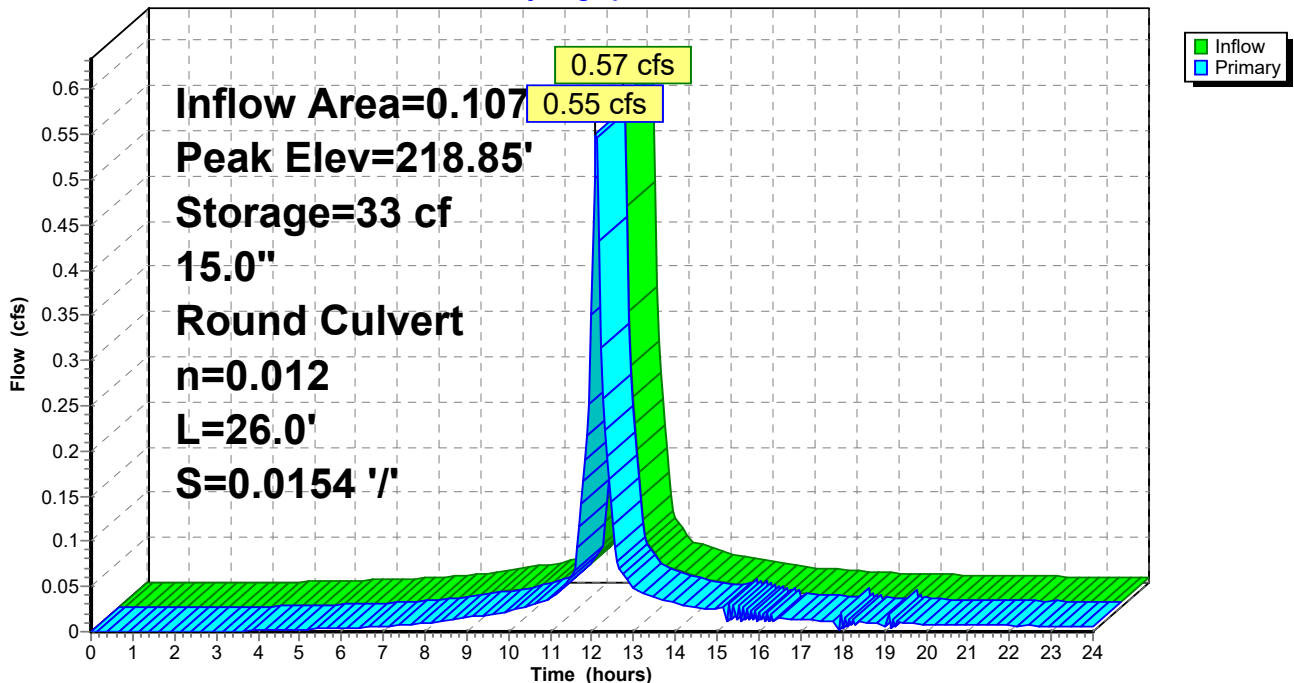
Volume	Invert	Avail.Storage	Storage Description
#1	216.25'	44 cf	4.00'D x 3.50'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	216.25'	15.0" Round 15" HDPE N-12 L= 26.0' Ke= 0.500 Inlet / Outlet Invert= 216.25' / 215.85' S= 0.0154 1/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=217.41' TW=217.64' (Dynamic Tailwater)
 ←1=15" HDPE N-12 (Controls 0.00 cfs)

Pond C42P: CB #42

Hydrograph



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Summary for Pond C43P: CB #43

Inflow Area = 0.328 ac, 87.98% Impervious, Inflow Depth > 5.15" for 25YR - 24HR event
 Inflow = 1.78 cfs @ 12.09 hrs, Volume= 0.141 af
 Outflow = 1.79 cfs @ 12.09 hrs, Volume= 0.141 af, Atten= 0%, Lag= 0.1 min
 Primary = 1.79 cfs @ 12.09 hrs, Volume= 0.141 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 224.53' @ 12.09 hrs Surf.Area= 13 sf Storage= 8 cf
 Flood Elev= 227.38' Surf.Area= 13 sf Storage= 44 cf

Plug-Flow detention time= 0.3 min calculated for 0.141 af (100% of inflow)
 Center-of-Mass det. time= 0.2 min (768.9 - 768.7)

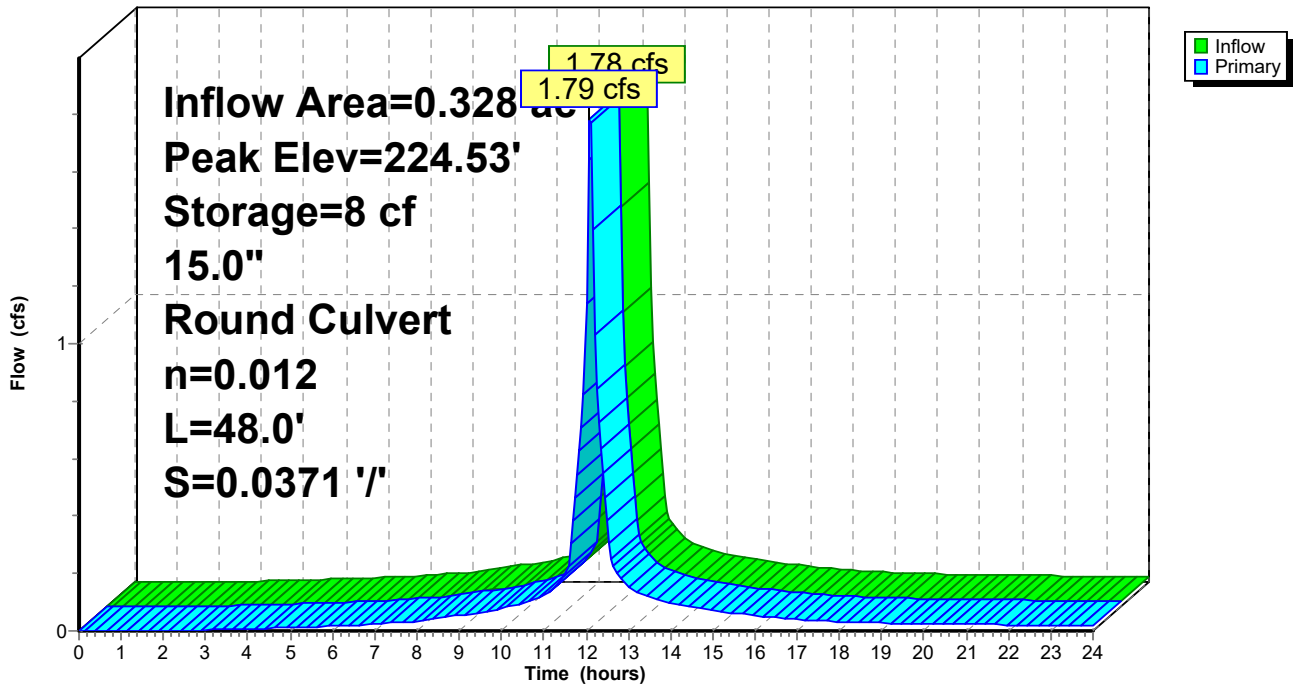
Volume	Invert	Avail.Storage	Storage Description
#1	223.88'	44 cf	4.00'D x 3.50'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	223.88'	15.0" Round 15" HDPE N-12 L= 48.0' Ke= 0.500 Inlet / Outlet Invert= 223.88' / 222.10' S= 0.0371 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=1.74 cfs @ 12.09 hrs HW=224.52' TW=223.03' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Inlet Controls 1.74 cfs @ 2.73 fps)

Pond C43P: CB #43

Hydrograph



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Summary for Pond C44P: CB #44

Inflow Area = 1.417 ac, 28.26% Impervious, Inflow Depth > 2.74" for 25YR - 24HR event
 Inflow = 3.54 cfs @ 12.18 hrs, Volume= 0.323 af
 Outflow = 3.54 cfs @ 12.18 hrs, Volume= 0.323 af, Atten= 0%, Lag= 0.1 min
 Primary = 3.54 cfs @ 12.18 hrs, Volume= 0.323 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 229.62' @ 12.18 hrs Surf.Area= 13 sf Storage= 12 cf
 Flood Elev= 232.13' Surf.Area= 13 sf Storage= 44 cf

Plug-Flow detention time= 0.2 min calculated for 0.323 af (100% of inflow)
 Center-of-Mass det. time= 0.2 min (842.8 - 842.6)

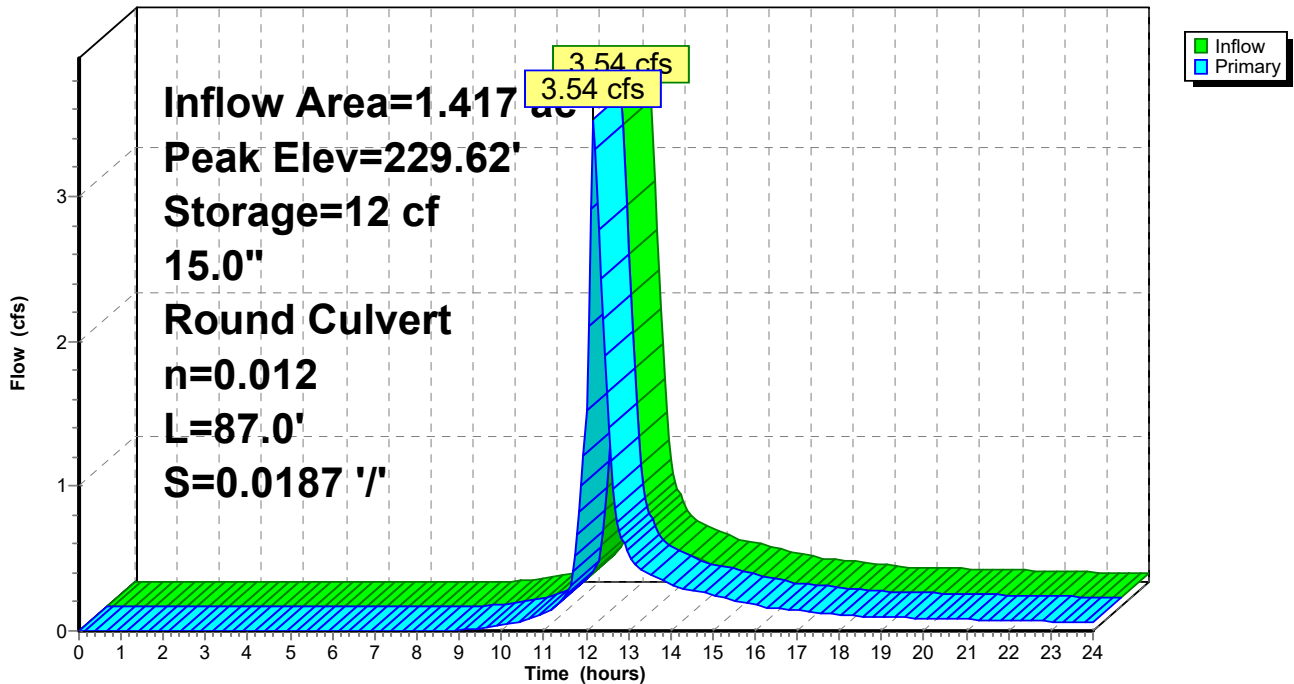
Volume	Invert	Avail.Storage	Storage Description
#1	228.63'	44 cf	4.00'D x 3.50'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	228.63'	15.0" Round 15" HDPE N-12 L= 87.0' Ke= 0.500 Inlet / Outlet Invert= 228.63' / 227.00' S= 0.0187 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=3.49 cfs @ 12.18 hrs HW=229.61' TW=227.25' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Inlet Controls 3.49 cfs @ 3.38 fps)

Pond C44P: CB #44

Hydrograph



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Summary for Pond C45P: CB #45

Inflow Area = 0.711 ac, 18.55% Impervious, Inflow Depth > 2.51" for 25YR - 24HR event
 Inflow = 1.77 cfs @ 12.15 hrs, Volume= 0.149 af
 Outflow = 1.77 cfs @ 12.15 hrs, Volume= 0.149 af, Atten= 0%, Lag= 0.0 min
 Primary = 1.77 cfs @ 12.15 hrs, Volume= 0.149 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 231.15' @ 12.15 hrs Surf.Area= 13 sf Storage= 8 cf
 Flood Elev= 235.00' Surf.Area= 364 sf Storage= 202 cf

Plug-Flow detention time= 0.2 min calculated for 0.148 af (100% of inflow)
 Center-of-Mass det. time= 0.1 min (847.2 - 847.0)

Volume	Invert	Avail.Storage	Storage Description
#1	230.50'	44 cf	4.00'D x 3.50'H 4' Structure
#2	234.00'	158 cf	Ponding Area (Irregular) Listed below (Recalc)
		202 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
234.00	27	30.0	0	0	27
235.00	351	95.9	158	158	690

Device	Routing	Invert	Outlet Devices
#1	Primary	230.50'	15.0" Round 15" HDPE N-12 L= 65.0' Ke= 0.500 Inlet / Outlet Invert= 230.50' / 229.80' S= 0.0108 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=1.75 cfs @ 12.15 hrs HW=231.15' TW=230.35' (Dynamic Tailwater)
 ←1=15" HDPE N-12 (Inlet Controls 1.75 cfs @ 2.74 fps)

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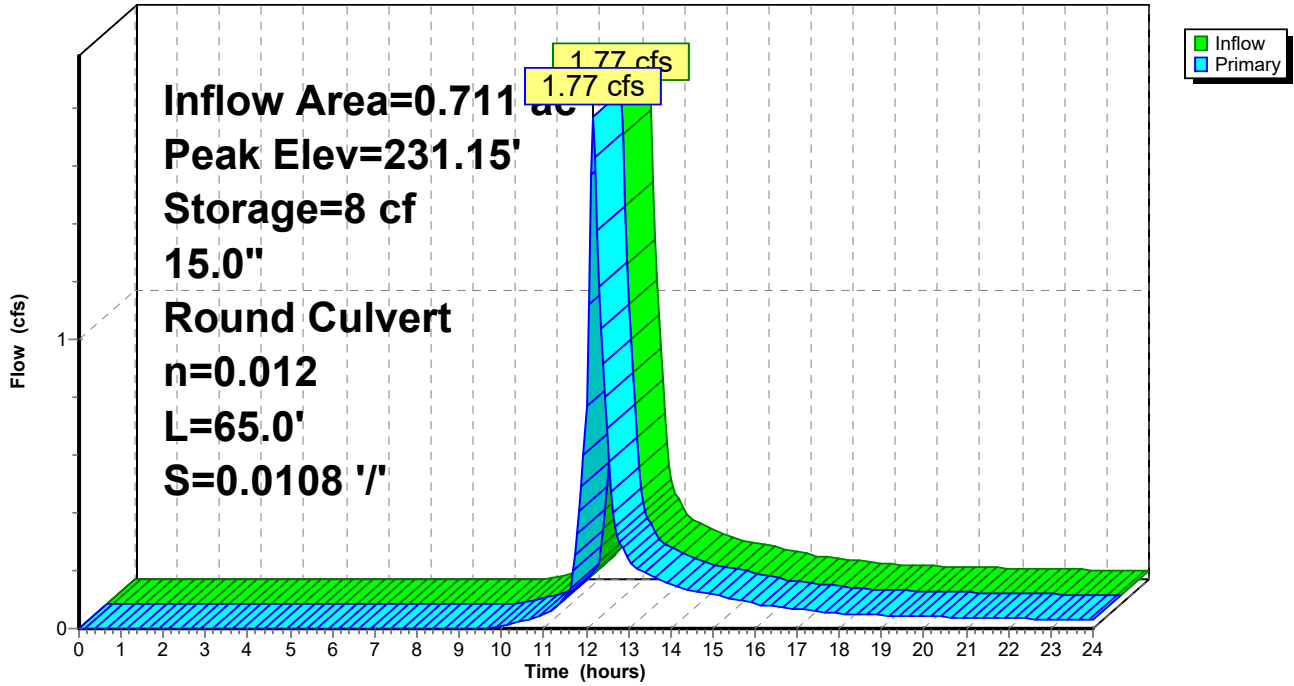
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Pond C45P: CB #45

Hydrograph



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Summary for Pond C46P: CB #46

Inflow Area = 2.359 ac, 9.81% Impervious, Inflow Depth > 1.72" for 25YR - 24HR event
 Inflow = 2.21 cfs @ 12.40 hrs, Volume= 0.338 af
 Outflow = 2.21 cfs @ 12.41 hrs, Volume= 0.338 af, Atten= 0%, Lag= 0.0 min
 Primary = 2.21 cfs @ 12.41 hrs, Volume= 0.338 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 235.99' @ 12.41 hrs Surf.Area= 13 sf Storage= 9 cf
 Flood Elev= 240.25' Surf.Area= 13 sf Storage= 63 cf

Plug-Flow detention time= 0.2 min calculated for 0.337 af (100% of inflow)
 Center-of-Mass det. time= 0.1 min (859.9 - 859.8)

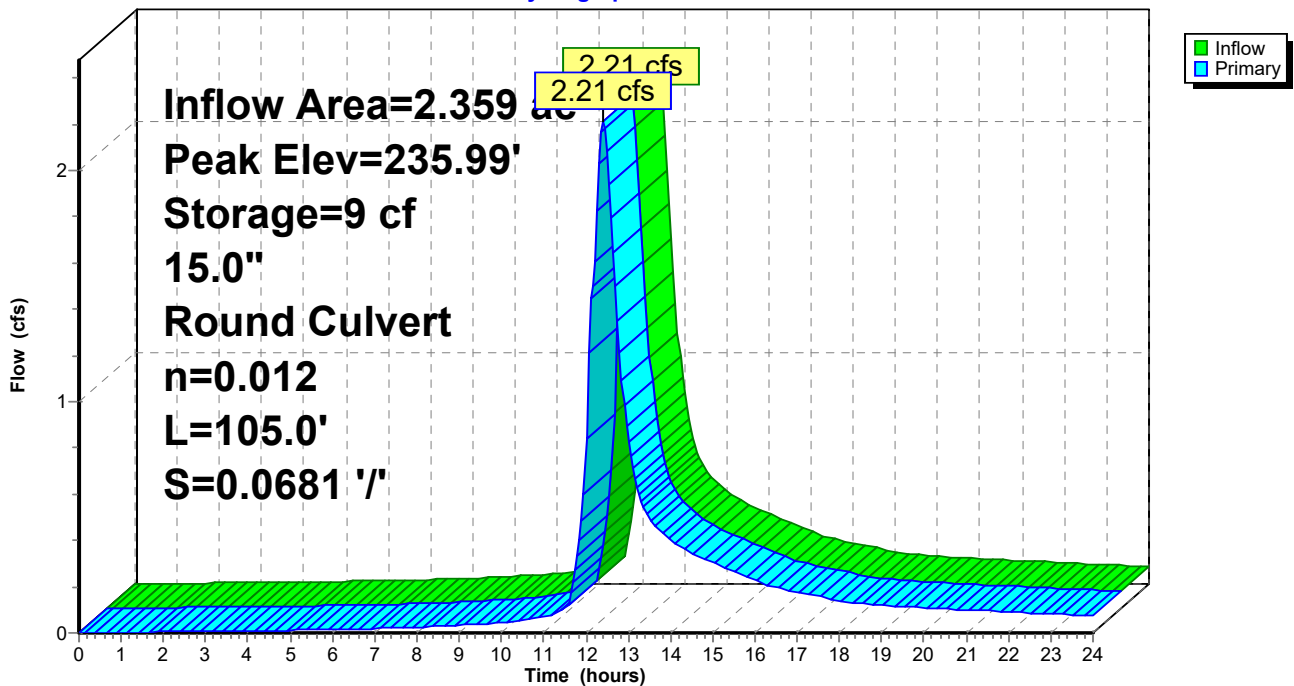
Volume	Invert	Avail.Storage	Storage Description
#1	235.25'	63 cf	4.00'D x 5.00'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	235.25'	15.0" Round 15" HDPE N-12 L= 105.0' Ke= 0.500 Inlet / Outlet Invert= 235.25' / 228.10' S= 0.0681 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=2.21 cfs @ 12.41 hrs HW=235.99' TW=228.82' (Dynamic Tailwater)
 ←1=15" HDPE N-12 (Inlet Controls 2.21 cfs @ 2.93 fps)

Pond C46P: CB #46

Hydrograph



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Summary for Pond D01P: DMH #1

[80] Warning: Exceeded Pond C33P by 0.11' @ 12.15 hrs (1.94 cfs 0.162 af)

Inflow Area = 0.457 ac, 71.01% Impervious, Inflow Depth > 4.45" for 25YR - 24HR event
 Inflow = 2.21 cfs @ 12.09 hrs, Volume= 0.169 af
 Outflow = 2.20 cfs @ 12.09 hrs, Volume= 0.169 af, Atten= 1%, Lag= 0.0 min
 Primary = 2.20 cfs @ 12.09 hrs, Volume= 0.169 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 214.47' @ 13.17 hrs Surf.Area= 13 sf Storage= 28 cf
 Flood Elev= 217.60' Surf.Area= 13 sf Storage= 68 cf

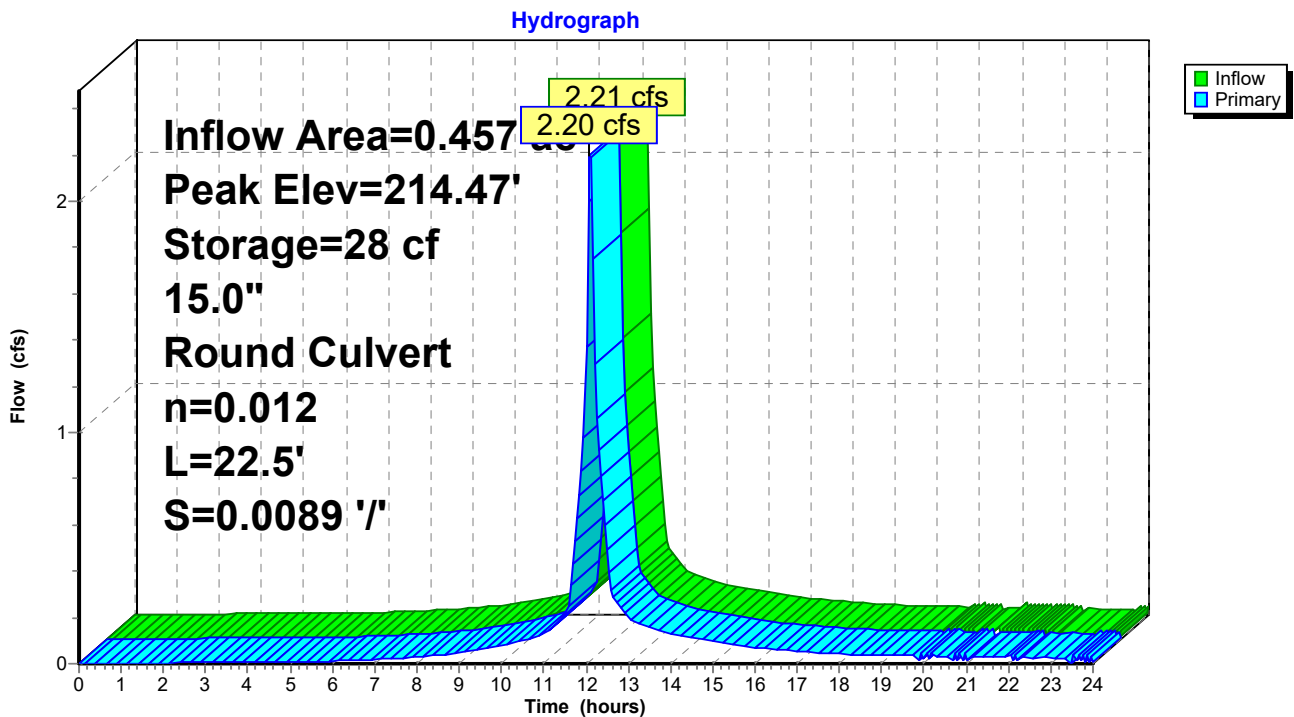
Plug-Flow detention time= 2.4 min calculated for 0.169 af (99% of inflow)
 Center-of-Mass det. time= 0.5 min (786.1 - 785.6)

Volume	Invert	Avail.Storage	Storage Description
#1	212.20'	68 cf	4.00'D x 5.40'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	212.20'	15.0" Round 15" HDPE N-12 L= 22.5' Ke= 0.500 Inlet / Outlet Invert= 212.20' / 212.00' S= 0.0089 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=2.16 cfs @ 12.09 hrs HW=213.88' TW=213.75' (Dynamic Tailwater)
 ←1=15" HDPE N-12 (Inlet Controls 2.16 cfs @ 1.76 fps)

Pond D01P: DMH #1



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Summary for Pond D02P: DMH #2

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

Inflow Area = 0.710 ac, 87.10% Impervious, Inflow Depth > 5.11" for 25YR - 24HR event
 Inflow = 3.84 cfs @ 12.09 hrs, Volume= 0.303 af
 Outflow = 3.84 cfs @ 12.09 hrs, Volume= 0.303 af, Atten= 0%, Lag= 0.0 min
 Primary = 3.84 cfs @ 12.09 hrs, Volume= 0.303 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 223.05' @ 12.09 hrs Surf.Area= 13 sf Storage= 13 cf
 Flood Elev= 226.00' Surf.Area= 13 sf Storage= 50 cf

Plug-Flow detention time= 0.2 min calculated for 0.302 af (100% of inflow)
 Center-of-Mass det. time= 0.1 min (769.9 - 769.8)

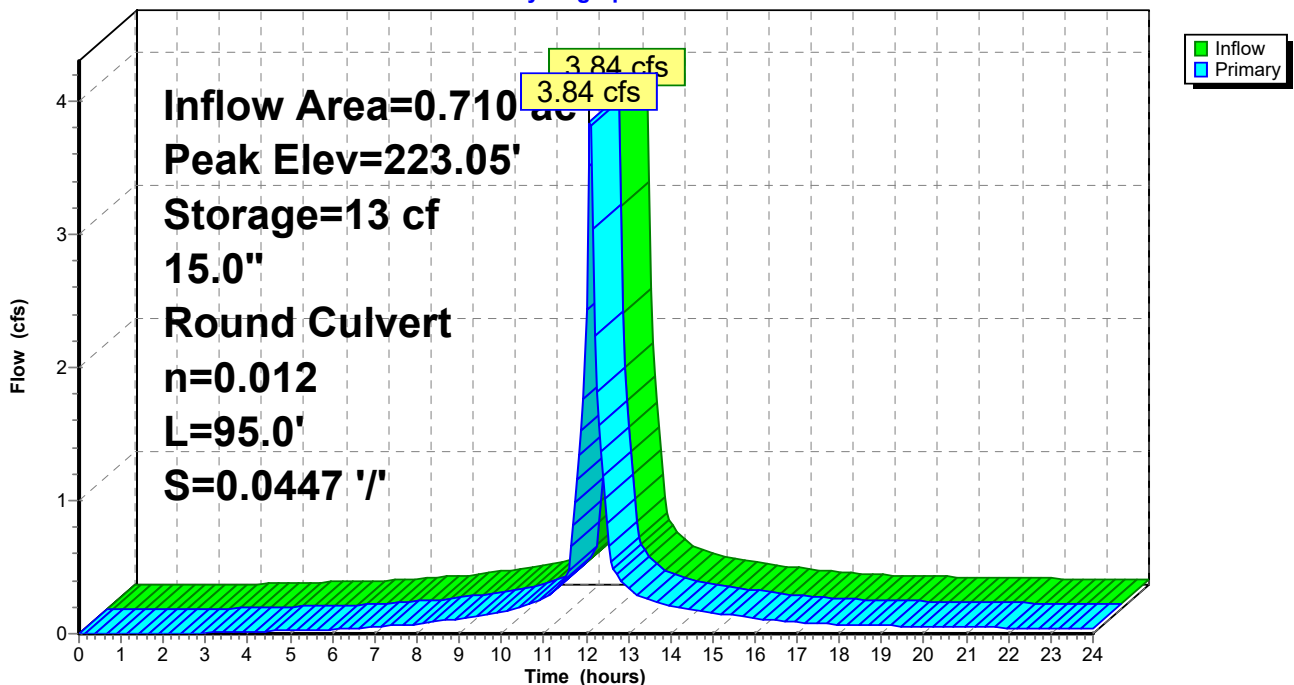
Volume	Invert	Avail.Storage	Storage Description
#1	222.00'	50 cf	4.00'D x 4.00'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	222.00'	15.0" Round 15" HDPE N-12 L= 95.0' Ke= 0.500 Inlet / Outlet Invert= 222.00' / 217.75' S= 0.0447 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=3.75 cfs @ 12.09 hrs HW=223.03' TW=218.72' (Dynamic Tailwater)
 ←1=15" HDPE N-12 (Inlet Controls 3.75 cfs @ 3.46 fps)

Pond D02P: DMH #2

Hydrograph



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Summary for Pond D03P: DMH #3

Inflow Area = 0.711 ac, 18.55% Impervious, Inflow Depth > 2.51" for 25YR - 24HR event
 Inflow = 1.77 cfs @ 12.15 hrs, Volume= 0.149 af
 Outflow = 1.77 cfs @ 12.16 hrs, Volume= 0.149 af, Atten= 0%, Lag= 0.0 min
 Primary = 1.77 cfs @ 12.16 hrs, Volume= 0.149 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 230.36' @ 12.16 hrs Surf.Area= 13 sf Storage= 8 cf
 Flood Elev= 234.70' Surf.Area= 13 sf Storage= 63 cf

Plug-Flow detention time= 0.2 min calculated for 0.148 af (100% of inflow)
 Center-of-Mass det. time= 0.1 min (847.3 - 847.2)

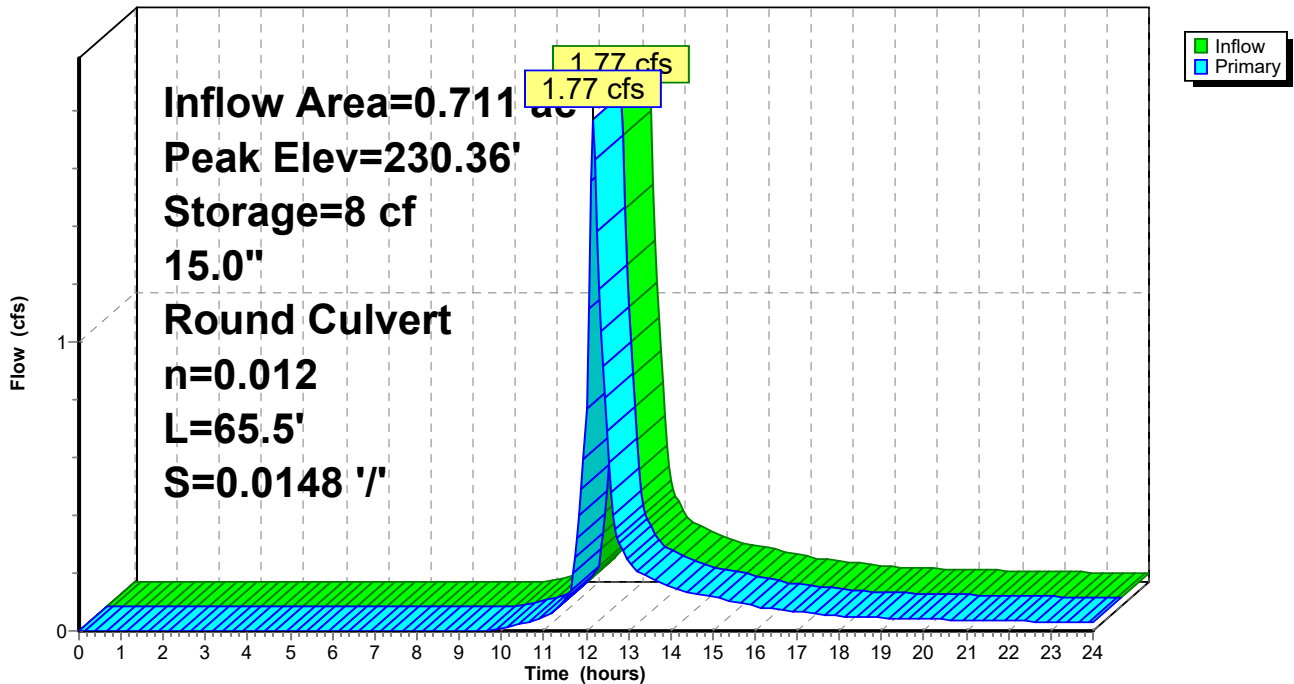
Volume	Invert	Avail.Storage	Storage Description
#1	229.70'	63 cf	4.00'D x 5.00'H 4' Structure

Device	Routing	Invert	Outlet Devices
#1	Primary	229.70'	15.0" Round 15" HDPE N-12 L= 65.5' Ke= 0.500 Inlet / Outlet Invert= 229.70' / 228.73' S= 0.0148 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=1.75 cfs @ 12.16 hrs HW=230.35' TW=229.61' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Outlet Controls 1.75 cfs @ 3.91 fps)

Pond D03P: DMH #3

Hydrograph



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Summary for Pond D04P: DMH #4

Inflow Area = 2.532 ac, 14.46% Impervious, Inflow Depth > 1.93" for 25YR - 24HR event
 Inflow = 2.55 cfs @ 12.38 hrs, Volume= 0.407 af
 Outflow = 2.55 cfs @ 12.38 hrs, Volume= 0.407 af, Atten= 0%, Lag= 0.1 min
 Primary = 2.55 cfs @ 12.38 hrs, Volume= 0.407 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 229.13' @ 15.38 hrs Surf.Area= 13 sf Storage= 14 cf
 Flood Elev= 231.50' Surf.Area= 13 sf Storage= 44 cf

Plug-Flow detention time= 0.4 min calculated for 0.407 af (100% of inflow)
 Center-of-Mass det. time= 0.3 min (848.2 - 847.9)

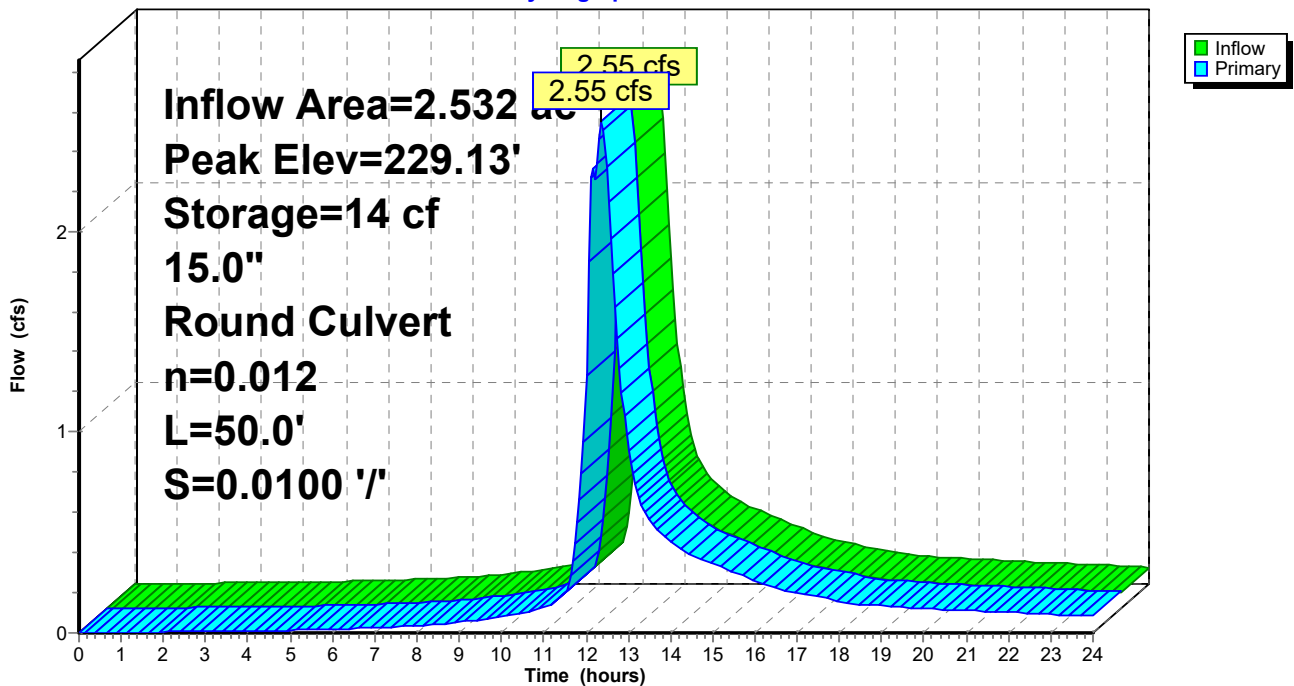
Volume	Invert	Avail.Storage	Storage Description
#1	228.00'	44 cf	4.00'D x 3.50'H 4' Structure

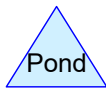
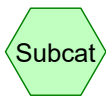
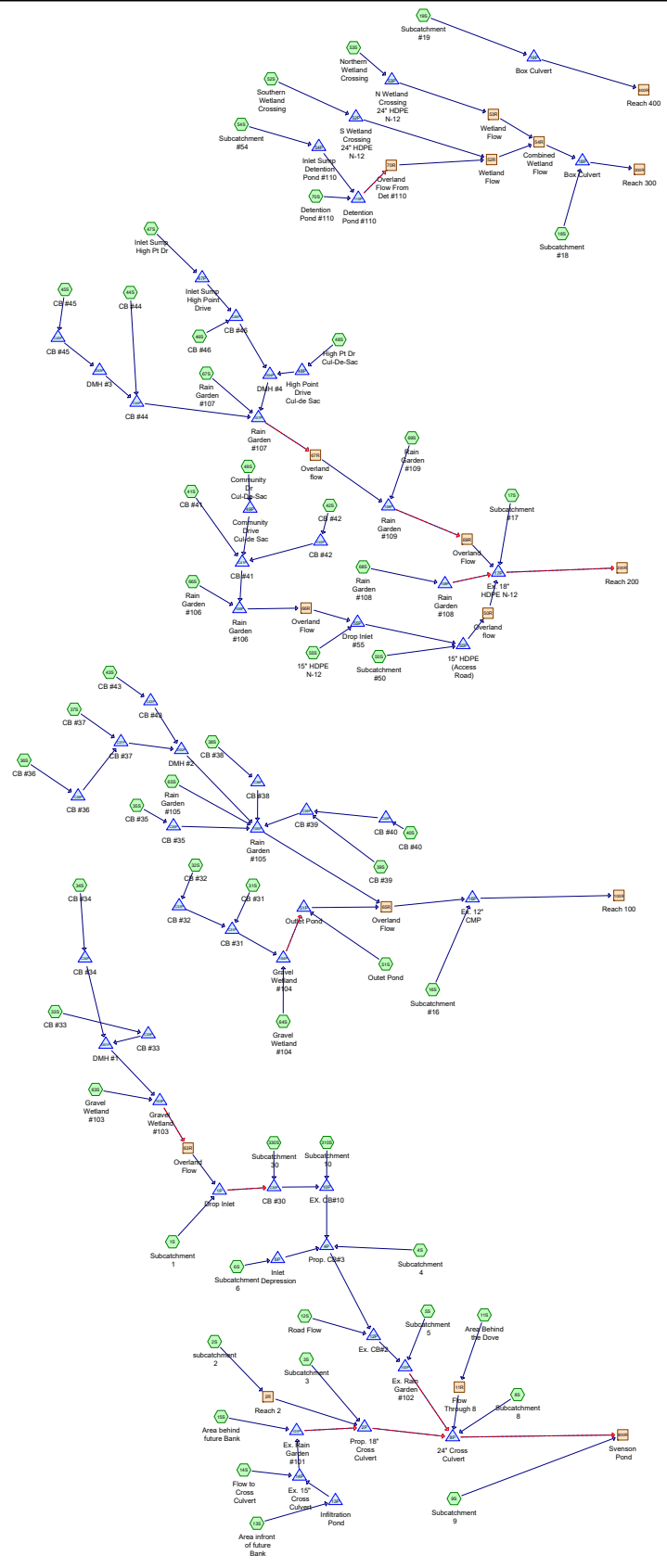
Device	Routing	Invert	Outlet Devices
#1	Primary	228.00'	15.0" Round 15" HDPE N-12 L= 50.0' Ke= 0.500 Inlet / Outlet Invert= 228.00' / 227.50' S= 0.0100 1/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=2.54 cfs @ 12.38 hrs HW=228.82' TW=227.95' (Dynamic Tailwater)
 ↳ 1=15" HDPE N-12 (Barrel Controls 2.54 cfs @ 4.25 fps)

Pond D04P: DMH #4

Hydrograph





Routing Diagram for 20-097 Proposed Analysis
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Type III 24-hr 2YR - 24HR Rainfall=3.08"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1	Runoff Area=257,558 sf 0.40% Impervious Runoff Depth>0.01" Flow Length=1,542' Tc=32.6 min CN=43 Runoff=0.01 cfs 0.006 af
Subcatchment 2S: subcatchment 2	Runoff Area=764,518 sf 0.65% Impervious Runoff Depth>0.14" Flow Length=2,418' Tc=59.1 min CN=52 Runoff=0.38 cfs 0.205 af
Subcatchment 3S: Subcatchment 3	Runoff Area=118,503 sf 0.00% Impervious Runoff Depth=0.00" Flow Length=993' Tc=20.7 min CN=38 Runoff=0.00 cfs 0.000 af
Subcatchment 4S: Subcatchment 4	Runoff Area=9,068 sf 100.00% Impervious Runoff Depth>2.85" Flow Length=207' Tc=6.0 min CN=98 Runoff=0.61 cfs 0.049 af
Subcatchment 5S: Subcatchment 5	Runoff Area=22,497 sf 40.08% Impervious Runoff Depth>0.47" Flow Length=212' Tc=7.0 min CN=63 Runoff=0.18 cfs 0.020 af
Subcatchment 6S: Subcatchment 6	Runoff Area=25,520 sf 84.67% Impervious Runoff Depth>1.97" Tc=6.0 min CN=89 Runoff=1.32 cfs 0.096 af
Subcatchment 8S: Subcatchment 8	Runoff Area=25,776 sf 25.48% Impervious Runoff Depth>0.06" Flow Length=152' Tc=10.4 min UI Adjusted CN=47 Runoff=0.00 cfs 0.003 af
Subcatchment 9S: Subcatchment 9	Runoff Area=45,641 sf 11.38% Impervious Runoff Depth>0.01" Flow Length=259' Tc=13.4 min UI Adjusted CN=42 Runoff=0.00 cfs 0.001 af
Subcatchment 11S: Area Behind the Dove	Runoff Area=84,194 sf 13.93% Impervious Runoff Depth>0.02" Flow Length=636' Tc=29.3 min UI Adjusted CN=44 Runoff=0.00 cfs 0.003 af
Subcatchment 12S: Road Flow	Runoff Area=4,388 sf 100.00% Impervious Runoff Depth>2.85" Tc=6.0 min CN=98 Runoff=0.29 cfs 0.024 af
Subcatchment 13S: Area in front of future	Runoff Area=29,777 sf 30.66% Impervious Runoff Depth>0.27" Flow Length=175' Tc=12.4 min CN=57 Runoff=0.08 cfs 0.015 af
Subcatchment 14S: Flow to Cross Culvert	Runoff Area=7,713 sf 59.39% Impervious Runoff Depth>0.96" Tc=6.0 min CN=74 Runoff=0.18 cfs 0.014 af
Subcatchment 15S: Area behind future	Runoff Area=17,796 sf 67.02% Impervious Runoff Depth>1.25" Tc=6.0 min CN=79 Runoff=0.58 cfs 0.042 af
Subcatchment 16S: Subcatchment #16	Runoff Area=124,823 sf 1.96% Impervious Runoff Depth>0.01" Flow Length=344' Tc=16.5 min UI Adjusted CN=43 Runoff=0.01 cfs 0.003 af
Subcatchment 17S: Subcatchment #17	Runoff Area=152,689 sf 2.08% Impervious Runoff Depth>0.24" Flow Length=591' Tc=30.6 min CN=56 Runoff=0.25 cfs 0.070 af
Subcatchment 18S: Subcatchment #18	Runoff Area=170,513 sf 0.61% Impervious Runoff Depth>0.36" Flow Length=376' Tc=17.1 min CN=60 Runoff=0.69 cfs 0.118 af

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Subcatchment 19S: Subcatchment #19	Runoff Area=690,822 sf 0.00% Impervious Runoff Depth>0.19" Flow Length=1,832' Tc=46.3 min CN=54 Runoff=0.61 cfs 0.247 af
Subcatchment 31S: CB #31	Runoff Area=6,795 sf 55.78% Impervious Runoff Depth>1.58" Tc=6.0 min CN=84 Runoff=0.28 cfs 0.021 af
Subcatchment 32S: CB #32	Runoff Area=5,694 sf 79.08% Impervious Runoff Depth>2.06" Tc=6.0 min CN=90 Runoff=0.31 cfs 0.022 af
Subcatchment 33S: CB #33	Runoff Area=14,734 sf 60.85% Impervious Runoff Depth>1.58" Tc=6.0 min CN=84 Runoff=0.61 cfs 0.045 af
Subcatchment 34S: CB #34	Runoff Area=5,164 sf 100.00% Impervious Runoff Depth>2.85" Tc=6.0 min CN=98 Runoff=0.35 cfs 0.028 af
Subcatchment 35S: CB #35	Runoff Area=6,367 sf 67.93% Impervious Runoff Depth>1.73" Tc=6.0 min CN=86 Runoff=0.29 cfs 0.021 af
Subcatchment 36S: CB #36	Runoff Area=7,548 sf 93.27% Impervious Runoff Depth>2.63" Tc=6.0 min CN=96 Runoff=0.49 cfs 0.038 af
Subcatchment 37S: CB #37	Runoff Area=9,102 sf 80.61% Impervious Runoff Depth>2.14" Tc=6.0 min CN=91 Runoff=0.51 cfs 0.037 af
Subcatchment 38S: CB #38	Runoff Area=8,387 sf 77.58% Impervious Runoff Depth>2.06" Tc=6.0 min CN=90 Runoff=0.45 cfs 0.033 af
Subcatchment 39S: CB #39	Runoff Area=9,406 sf 38.75% Impervious Runoff Depth>1.13" Tc=6.0 min CN=77 Runoff=0.27 cfs 0.020 af
Subcatchment 40S: CB #40	Runoff Area=3,206 sf 100.00% Impervious Runoff Depth>2.85" Tc=6.0 min CN=98 Runoff=0.21 cfs 0.017 af
Subcatchment 41S: CB #41	Runoff Area=3,664 sf 87.72% Impervious Runoff Depth>2.43" Tc=6.0 min CN=94 Runoff=0.22 cfs 0.017 af
Subcatchment 42S: CB #42	Runoff Area=4,646 sf 81.42% Impervious Runoff Depth>2.24" Tc=6.0 min CN=92 Runoff=0.27 cfs 0.020 af
Subcatchment 43S: CB #43	Runoff Area=14,297 sf 87.98% Impervious Runoff Depth>2.43" Tc=6.0 min CN=94 Runoff=0.88 cfs 0.066 af
Subcatchment 44S: CB #44	Runoff Area=30,768 sf 38.03% Impervious Runoff Depth>0.90" Flow Length=493' Tc=14.6 min CN=73 Runoff=0.53 cfs 0.053 af
Subcatchment 45S: CB #45	Runoff Area=30,969 sf 18.55% Impervious Runoff Depth>0.67" Flow Length=265' Tc=10.4 min UI Adjusted CN=68 Runoff=0.40 cfs 0.039 af
Subcatchment 46S: CB #46	Runoff Area=7,198 sf 100.00% Impervious Runoff Depth>2.85" Tc=6.0 min CN=98 Runoff=0.48 cfs 0.039 af
Subcatchment 47S: Inlet Sump High Pt Dr	Runoff Area=95,547 sf 3.02% Impervious Runoff Depth>0.21" Flow Length=862' Tc=26.2 min UI Adjusted CN=55 Runoff=0.14 cfs 0.039 af

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Subcatchment48S: High Pt Dr Cul-De-Sac	Runoff Area=7,531 sf 77.93% Impervious Runoff Depth>2.14" Tc=6.0 min CN=91 Runoff=0.42 cfs 0.031 af
Subcatchment49S: Community Dr	Runoff Area=10,872 sf 69.81% Impervious Runoff Depth>1.89" Tc=6.0 min CN=88 Runoff=0.54 cfs 0.039 af
Subcatchment50S: Subcatchment#50	Runoff Area=20,749 sf 0.00% Impervious Runoff Depth>0.21" Flow Length=209' Tc=15.8 min CN=55 Runoff=0.03 cfs 0.009 af
Subcatchment51S: Outet Pond	Runoff Area=2,846 sf 0.00% Impervious Runoff Depth>0.40" Tc=6.0 min CN=61 Runoff=0.02 cfs 0.002 af
Subcatchment52S: Southern Wetland	Runoff Area=237,763 sf 0.00% Impervious Runoff Depth>0.21" Flow Length=1,157' Tc=26.8 min CN=55 Runoff=0.34 cfs 0.097 af
Subcatchment53S: Northern Wetland	Runoff Area=23,588 sf 0.00% Impervious Runoff Depth>0.24" Flow Length=497' Tc=20.6 min CN=56 Runoff=0.05 cfs 0.011 af
Subcatchment54S: Subcatchment#54	Runoff Area=118,144 sf 0.71% Impervious Runoff Depth>0.30" Flow Length=1,159' Tc=25.9 min CN=58 Runoff=0.31 cfs 0.067 af
Subcatchment55S: 15" HDPE N-12	Runoff Area=4,389 sf 0.00% Impervious Runoff Depth>0.40" Tc=6.0 min CN=61 Runoff=0.03 cfs 0.003 af
Subcatchment63S: Gravel Wetland #103	Runoff Area=4,821 sf 0.00% Impervious Runoff Depth>0.40" Tc=6.0 min CN=61 Runoff=0.03 cfs 0.004 af
Subcatchment64S: Gravel Wetland #104	Runoff Area=1,940 sf 0.00% Impervious Runoff Depth>0.40" Tc=6.0 min CN=61 Runoff=0.01 cfs 0.001 af
Subcatchment65S: Rain Garden #105	Runoff Area=12,647 sf 3.41% Impervious Runoff Depth>0.62" Tc=6.0 min CN=67 Runoff=0.17 cfs 0.015 af
Subcatchment66S: Rain Garden #106	Runoff Area=34,434 sf 4.69% Impervious Runoff Depth>0.54" Flow Length=211' Tc=15.3 min UI Adjusted CN=65 Runoff=0.28 cfs 0.036 af
Subcatchment67S: Rain Garden #107	Runoff Area=22,575 sf 0.00% Impervious Runoff Depth>0.39" Flow Length=92' Tc=10.9 min CN=61 Runoff=0.12 cfs 0.017 af
Subcatchment68S: Rain Garden #108	Runoff Area=7,430 sf 45.91% Impervious Runoff Depth>1.18" Tc=6.0 min CN=78 Runoff=0.23 cfs 0.017 af
Subcatchment69S: Rain Garden #109	Runoff Area=78,911 sf 0.00% Impervious Runoff Depth>0.39" Flow Length=493' Tc=14.4 min CN=61 Runoff=0.38 cfs 0.059 af
Subcatchment70S: Detention Pond #110	Runoff Area=24,497 sf 0.00% Impervious Runoff Depth>0.33" Flow Length=273' Tc=12.3 min CN=59 Runoff=0.09 cfs 0.015 af
Subcatchment310S: Subcatchment 10	Runoff Area=9,312 sf 47.01% Impervious Runoff Depth>0.76" Tc=6.0 min CN=70 Runoff=0.17 cfs 0.014 af

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Subcatchment 330S: Subcatchment 30	Runoff Area=5,360 sf	77.01% Impervious	Runoff Depth>1.97"						
	Tc=6.0 min	CN=89	Runoff=0.28 cfs	0.020 af					
Reach 2R: Reach 2	Avg. Flow Depth=0.09'	Max Vel=1.27 fps	Inflow=0.38 cfs	0.205 af	n=0.022	L=220.0'	S=0.0091 '/'	Capacity=24.64 cfs	Outflow=0.38 cfs 0.204 af
Reach 11R: Flow Through 8	Avg. Flow Depth=0.02'	Max Vel=0.24 fps	Inflow=0.00 cfs	0.003 af	n=0.035	L=76.0'	S=0.0132 '/'	Capacity=7.77 cfs	Outflow=0.00 cfs 0.003 af
Reach 50R: Overland flow	Avg. Flow Depth=0.05'	Max Vel=0.88 fps	Inflow=0.08 cfs	0.045 af	n=0.025	L=42.0'	S=0.0179 '/'	Capacity=186.81 cfs	Outflow=0.08 cfs 0.045 af
Reach 52R: Wetland Flow	Avg. Flow Depth=0.08'	Max Vel=0.79 fps	Inflow=0.34 cfs	0.160 af	n=0.045	L=123.0'	S=0.0285 '/'	Capacity=17.83 cfs	Outflow=0.33 cfs 0.159 af
Reach 53R: Wetland Flow	Avg. Flow Depth=0.03'	Max Vel=0.46 fps	Inflow=0.05 cfs	0.011 af	n=0.045	L=135.0'	S=0.0370 '/'	Capacity=20.35 cfs	Outflow=0.04 cfs 0.011 af
Reach 54R: Combined Wetland Flow	Avg. Flow Depth=0.06'	Max Vel=1.97 fps	Inflow=0.38 cfs	0.170 af	n=0.045	L=87.0'	S=0.1379 '/'	Capacity=610.11 cfs	Outflow=0.38 cfs 0.170 af
Reach 63R: Overland Flow	Avg. Flow Depth=0.01'	Max Vel=0.48 fps	Inflow=0.02 cfs	0.022 af	n=0.030	L=126.0'	S=0.0476 '/'	Capacity=43.27 cfs	Outflow=0.02 cfs 0.021 af
Reach 65R: Overland Flow	Avg. Flow Depth=0.05'	Max Vel=0.68 fps	Inflow=0.13 cfs	0.094 af	n=0.035	L=342.1'	S=0.0270 '/'	Capacity=22.35 cfs	Outflow=0.13 cfs 0.093 af
Reach 66R: Overland Flow	Avg. Flow Depth=0.02'	Max Vel=0.98 fps	Inflow=0.03 cfs	0.034 af	n=0.025	L=48.0'	S=0.0677 '/'	Capacity=24.68 cfs	Outflow=0.03 cfs 0.034 af
Reach 67R: Overland flow	Avg. Flow Depth=0.00'	Max Vel=0.00 fps	Inflow=0.00 cfs	0.000 af	n=0.030	L=180.0'	S=0.0250 '/'	Capacity=39.17 cfs	Outflow=0.00 cfs 0.000 af
Reach 69R: Overland Flow	Avg. Flow Depth=0.03'	Max Vel=0.63 fps	Inflow=0.05 cfs	0.047 af	n=0.035	L=70.0'	S=0.0429 '/'	Capacity=111.48 cfs	Outflow=0.05 cfs 0.047 af
Reach 70R: Overland Flow From Det	Avg. Flow Depth=0.05'	Max Vel=1.28 fps	Inflow=0.10 cfs	0.063 af	n=0.035	L=61.0'	S=0.0820 '/'	Capacity=60.79 cfs	Outflow=0.10 cfs 0.062 af
Reach 100R: Reach 100			Inflow=0.13 cfs	0.096 af					Outflow=0.13 cfs 0.096 af
Reach 200R: Reach 200			Inflow=0.39 cfs	0.174 af					Outflow=0.39 cfs 0.174 af
Reach 300R: Reach 300			Inflow=0.92 cfs	0.287 af					Outflow=0.92 cfs 0.287 af
Reach 400R: Reach 400			Inflow=0.61 cfs	0.246 af					Outflow=0.61 cfs 0.246 af
Reach 800R: Svenson Pond			Inflow=0.91 cfs	0.469 af					Outflow=0.91 cfs 0.469 af

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Pond 1P: Drop Inlet	Peak Elev=200.83' Storage=0 cf Inflow=0.03 cfs 0.028 af Primary=0.03 cfs 0.028 af Secondary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.028 af
Pond 2P: Prop. 18" Cross Culvert	Peak Elev=198.39' Storage=9 cf Inflow=0.49 cfs 0.234 af 18.0" Round Culvert n=0.012 L=60.0' S=0.0100 '/' Outflow=0.44 cfs 0.234 af
Pond 4P: Prop. CB#3	Peak Elev=200.13' Storage=0.000 af Inflow=2.31 cfs 0.207 af 15.0" Round Culvert n=0.012 L=93.7' S=0.0053 '/' Outflow=2.31 cfs 0.207 af
Pond 6P: Inlet Depression	Peak Elev=200.56' Storage=115 cf Inflow=1.32 cfs 0.096 af 15.0" Round Culvert n=0.012 L=30.0' S=0.0233 '/' Outflow=1.27 cfs 0.096 af
Pond 8P: 24" Cross Culvert	Peak Elev=197.01' Storage=37 cf Inflow=0.91 cfs 0.468 af Primary=0.91 cfs 0.468 af Secondary=0.00 cfs 0.000 af Outflow=0.91 cfs 0.468 af
Pond 10P: EX. CB#10	Peak Elev=200.50' Storage=5 cf Inflow=0.45 cfs 0.061 af 15.0" Round Culvert n=0.012 L=153.9' S=0.0050 '/' Outflow=0.45 cfs 0.061 af
Pond 12P: Ex. CB#2	Peak Elev=199.58' Storage=0.000 af Inflow=2.60 cfs 0.231 af 15.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=2.61 cfs 0.231 af
Pond 13P: Infiltration Pond	Peak Elev=203.03' Storage=64 cf Inflow=0.08 cfs 0.015 af Discarded=0.03 cfs 0.015 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.015 af
Pond 14P: Ex. 15" Cross Culvert	Peak Elev=201.64' Storage=93 cf Inflow=0.18 cfs 0.014 af Discarded=0.01 cfs 0.007 af Primary=0.10 cfs 0.007 af Outflow=0.11 cfs 0.014 af
Pond 16P: Ex. 12" CMP	Peak Elev=203.49' Storage=29 cf Inflow=0.13 cfs 0.097 af Outflow=0.13 cfs 0.096 af
Pond 17P: Ex. 18" HDPE N-12	Peak Elev=202.56' Storage=30 cf Inflow=0.39 cfs 0.174 af Primary=0.39 cfs 0.174 af Secondary=0.00 cfs 0.000 af Outflow=0.39 cfs 0.174 af
Pond 18P: Box Culvert	Peak Elev=190.50' Storage=13 cf Inflow=0.92 cfs 0.287 af 36.0" x 36.0" Box Culvert n=0.012 L=28.0' S=0.0018 '/' Outflow=0.92 cfs 0.287 af
Pond 19P: Box Culvert	Peak Elev=183.29' Storage=3 cf Inflow=0.61 cfs 0.247 af 36.0" x 36.0" Box Culvert n=0.012 L=52.0' S=-0.0085 '/' Outflow=0.61 cfs 0.246 af
Pond 47P: Inlet Sump High Point Drive	Peak Elev=236.92' Storage=6 cf Inflow=0.14 cfs 0.039 af 15.0" Round Culvert n=0.012 L=23.0' S=0.0609 '/' Outflow=0.14 cfs 0.039 af
Pond 48P: High Point Drive Cul-de Sac	Peak Elev=236.28' Storage=113 cf Inflow=0.42 cfs 0.031 af 15.0" Round Culvert n=0.012 L=50.0' S=0.0130 '/' Outflow=0.37 cfs 0.031 af
Pond 49P: Community Drive Cul-de Sac	Peak Elev=217.52' Storage=161 cf Inflow=0.54 cfs 0.039 af 15.0" Round Culvert n=0.012 L=53.5' S=0.0121 '/' Outflow=0.54 cfs 0.036 af
Pond 50P: 15" HDPE (Access Road)	Peak Elev=203.39' Storage=14 cf Inflow=0.08 cfs 0.045 af 15.0" Round Culvert n=0.012 L=42.0' S=0.0060 '/' Outflow=0.08 cfs 0.045 af

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Pond 51P: Outlet Pond	Peak Elev=213.60' Storage=582 cf Inflow=0.02 cfs 0.013 af Outflow=0.00 cfs 0.000 af
Pond 52P: S Wetland Crossing 24" HDPE N-12	Peak Elev=213.65' Storage=5 cf Inflow=0.34 cfs 0.097 af 24.0" Round Culvert w/ 6.0" inside fill n=0.024 L=36.0' S=0.0278 '/' Outflow=0.34 cfs 0.097 af
Pond 53P: N Wetland Crossing 24" HDPE N-12	Peak Elev=215.54' Storage=1 cf Inflow=0.05 cfs 0.011 af 24.0" Round Culvert w/ 6.0" inside fill n=0.024 L=25.0' S=0.0600 '/' Outflow=0.05 cfs 0.011 af
Pond 54P: Inlet Sump Detention Pond #110	Peak Elev=222.25' Storage=17 cf Inflow=0.31 cfs 0.067 af 15.0" Round Culvert n=0.012 L=35.0' S=0.0571 '/' Outflow=0.31 cfs 0.067 af
Pond 55P: Drop Inlet #55	Peak Elev=203.87' Storage=0.000 af Inflow=0.05 cfs 0.037 af 15.0" Round Culvert n=0.012 L=93.2' S=0.0054 '/' Outflow=0.05 cfs 0.037 af
Pond 101P: Ex. Rain Garden #101	Peak Elev=201.04' Storage=872 cf Inflow=0.63 cfs 0.049 af Primary=0.23 cfs 0.030 af Secondary=0.00 cfs 0.000 af Outflow=0.23 cfs 0.030 af
Pond 102P: Ex. Rain Garden #102	Peak Elev=199.39' Storage=3,647 cf Inflow=2.78 cfs 0.251 af Primary=0.46 cfs 0.228 af Secondary=0.00 cfs 0.000 af Outflow=0.46 cfs 0.228 af
Pond 103P: Gravel Wetland #103	Peak Elev=213.60' Storage=2,396 cf Inflow=0.98 cfs 0.076 af Primary=0.02 cfs 0.022 af Secondary=0.00 cfs 0.000 af Outflow=0.02 cfs 0.022 af
Pond 104P: Gravel Wetland #104	Peak Elev=216.07' Storage=1,414 cf Inflow=0.58 cfs 0.043 af Primary=0.01 cfs 0.011 af Secondary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.011 af
Pond 105P: Rain Garden #105	Peak Elev=218.30' Storage=7,387 cf Inflow=3.25 cfs 0.247 af Outflow=0.13 cfs 0.094 af
Pond 106P: Rain Garden #106	Peak Elev=217.53' Storage=3,299 cf Inflow=1.15 cfs 0.107 af Outflow=0.03 cfs 0.034 af
Pond 107P: Rain Garden #107	Peak Elev=227.45' Storage=8,864 cf Inflow=1.70 cfs 0.218 af Discarded=0.01 cfs 0.015 af Primary=0.00 cfs 0.000 af Secondary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.015 af
Pond 108P: Rain Garden #108	Peak Elev=204.88' Storage=358 cf Inflow=0.23 cfs 0.017 af Primary=0.02 cfs 0.012 af Secondary=0.00 cfs 0.000 af Outflow=0.02 cfs 0.012 af
Pond 109P: Rain Garden #109	Peak Elev=214.56' Storage=1,077 cf Inflow=0.38 cfs 0.059 af Primary=0.05 cfs 0.047 af Secondary=0.00 cfs 0.000 af Outflow=0.05 cfs 0.047 af
Pond 110P: Detention Pond #110	Peak Elev=218.30' Storage=1,282 cf Inflow=0.37 cfs 0.082 af Primary=0.10 cfs 0.063 af Secondary=0.00 cfs 0.000 af Outflow=0.10 cfs 0.063 af
Pond C30P: CB #30	Peak Elev=200.62' Storage=4 cf Inflow=0.29 cfs 0.048 af 15.0" Round Culvert n=0.012 L=25.0' S=0.0052 '/' Outflow=0.29 cfs 0.048 af
Pond C31P: CB #31	Peak Elev=216.07' Storage=24 cf Inflow=0.58 cfs 0.042 af 15.0" Round Culvert n=0.012 L=18.0' S=0.0083 '/' Outflow=0.57 cfs 0.042 af
Pond C32P: CB #32	Peak Elev=216.06' Storage=21 cf Inflow=0.31 cfs 0.022 af 15.0" Round Culvert n=0.012 L=26.0' S=0.0058 '/' Outflow=0.30 cfs 0.022 af

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Type III 24-hr 2YR - 24HR Rainfall=3.08"

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Pond C33P: CB #33	Peak Elev=213.59' Storage=14 cf Inflow=0.61 cfs 0.045 af 15.0" Round Culvert n=0.012 L=28.7' S=0.0070 '/' Outflow=0.61 cfs 0.044 af
Pond C34P: CB #34	Peak Elev=216.82' Storage=7 cf Inflow=0.35 cfs 0.028 af 15.0" Round Culvert n=0.012 L=63.5' S=0.0669 '/' Outflow=0.35 cfs 0.028 af
Pond C35P: CB #35	Peak Elev=218.30' Storage=19 cf Inflow=0.29 cfs 0.021 af 15.0" Round Culvert n=0.012 L=10.0' S=0.0300 '/' Outflow=0.28 cfs 0.021 af
Pond C36P: CB #36	Peak Elev=225.05' Storage=5 cf Inflow=0.49 cfs 0.038 af 15.0" Round Culvert n=0.012 L=162.0' S=0.0050 '/' Outflow=0.49 cfs 0.038 af
Pond C37P: CB #37	Peak Elev=224.11' Storage=6 cf Inflow=0.99 cfs 0.075 af 15.0" Round Culvert n=0.012 L=84.0' S=0.0183 '/' Outflow=1.00 cfs 0.075 af
Pond C38P: CB #38	Peak Elev=219.50' Storage=4 cf Inflow=0.45 cfs 0.033 af 15.0" Round Culvert n=0.012 L=13.0' S=0.0138 '/' Outflow=0.45 cfs 0.033 af
Pond C39P: CB #39	Peak Elev=218.30' Storage=23 cf Inflow=0.48 cfs 0.037 af 15.0" Round Culvert n=0.012 L=15.0' S=0.0167 '/' Outflow=0.47 cfs 0.037 af
Pond C40P: CB #40	Peak Elev=218.30' Storage=16 cf Inflow=0.21 cfs 0.017 af 15.0" Round Culvert n=0.012 L=31.7' S=0.0126 '/' Outflow=0.21 cfs 0.017 af
Pond C41P: CB #41	Peak Elev=217.53' Storage=22 cf Inflow=1.03 cfs 0.072 af 15.0" Round Culvert n=0.012 L=17.5' S=0.0143 '/' Outflow=1.02 cfs 0.072 af
Pond C42P: CB #42	Peak Elev=217.52' Storage=16 cf Inflow=0.27 cfs 0.020 af 15.0" Round Culvert n=0.012 L=26.0' S=0.0154 '/' Outflow=0.27 cfs 0.019 af
Pond C43P: CB #43	Peak Elev=224.32' Storage=6 cf Inflow=0.88 cfs 0.066 af 15.0" Round Culvert n=0.012 L=48.0' S=0.0371 '/' Outflow=0.88 cfs 0.066 af
Pond C44P: CB #44	Peak Elev=229.08' Storage=6 cf Inflow=0.90 cfs 0.093 af 15.0" Round Culvert n=0.012 L=87.0' S=0.0187 '/' Outflow=0.91 cfs 0.093 af
Pond C45P: CB #45	Peak Elev=230.79' Storage=4 cf Inflow=0.40 cfs 0.039 af 15.0" Round Culvert n=0.012 L=65.0' S=0.0108 '/' Outflow=0.40 cfs 0.039 af
Pond C46P: CB #46	Peak Elev=235.57' Storage=4 cf Inflow=0.48 cfs 0.078 af 15.0" Round Culvert n=0.012 L=105.0' S=0.0681 '/' Outflow=0.48 cfs 0.078 af
Pond D01P: DMH #1	Peak Elev=213.59' Storage=18 cf Inflow=0.96 cfs 0.072 af 15.0" Round Culvert n=0.012 L=22.5' S=0.0089 '/' Outflow=0.95 cfs 0.072 af
Pond D02P: DMH #2	Peak Elev=222.67' Storage=8 cf Inflow=1.87 cfs 0.142 af 15.0" Round Culvert n=0.012 L=95.0' S=0.0447 '/' Outflow=1.87 cfs 0.142 af
Pond D03P: DMH #3	Peak Elev=229.99' Storage=4 cf Inflow=0.40 cfs 0.039 af 15.0" Round Culvert n=0.012 L=65.5' S=0.0148 '/' Outflow=0.40 cfs 0.039 af

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Pond D04P: DMH #4

Peak Elev=228.43' Storage=5 cf Inflow=0.84 cfs 0.109 af
15.0" Round Culvert n=0.012 L=50.0' S=0.0100 '/ Outflow=0.84 cfs 0.109 af

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Type III 24-hr 10YR - 24HR Rainfall=4.64"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1	Runoff Area=257,558 sf 0.40% Impervious Runoff Depth>0.25" Flow Length=1,542' Tc=32.6 min CN=43 Runoff=0.32 cfs 0.125 af
Subcatchment 2S: subcatchment 2	Runoff Area=764,518 sf 0.65% Impervious Runoff Depth>0.63" Flow Length=2,418' Tc=59.1 min CN=52 Runoff=3.64 cfs 0.927 af
Subcatchment 3S: Subcatchment 3	Runoff Area=118,503 sf 0.00% Impervious Runoff Depth>0.11" Flow Length=993' Tc=20.7 min CN=38 Runoff=0.04 cfs 0.024 af
Subcatchment 4S: Subcatchment 4	Runoff Area=9,068 sf 100.00% Impervious Runoff Depth>4.40" Flow Length=207' Tc=6.0 min CN=98 Runoff=0.92 cfs 0.076 af
Subcatchment 5S: Subcatchment 5	Runoff Area=22,497 sf 40.08% Impervious Runoff Depth>1.28" Flow Length=212' Tc=7.0 min CN=63 Runoff=0.68 cfs 0.055 af
Subcatchment 6S: Subcatchment 6	Runoff Area=25,520 sf 84.67% Impervious Runoff Depth>3.43" Tc=6.0 min CN=89 Runoff=2.25 cfs 0.167 af
Subcatchment 8S: Subcatchment 8	Runoff Area=25,776 sf 25.48% Impervious Runoff Depth>0.41" Flow Length=152' Tc=10.4 min UI Adjusted CN=47 Runoff=0.11 cfs 0.020 af
Subcatchment 9S: Subcatchment 9	Runoff Area=45,641 sf 11.38% Impervious Runoff Depth>0.22" Flow Length=259' Tc=13.4 min UI Adjusted CN=42 Runoff=0.05 cfs 0.019 af
Subcatchment 11S: Area Behind the Dove	Runoff Area=84,194 sf 13.93% Impervious Runoff Depth>0.29" Flow Length=636' Tc=29.3 min UI Adjusted CN=44 Runoff=0.14 cfs 0.047 af
Subcatchment 12S: Road Flow	Runoff Area=4,388 sf 100.00% Impervious Runoff Depth>4.40" Tc=6.0 min CN=98 Runoff=0.45 cfs 0.037 af
Subcatchment 13S: Area in front of future	Runoff Area=29,777 sf 30.66% Impervious Runoff Depth>0.92" Flow Length=175' Tc=12.4 min CN=57 Runoff=0.47 cfs 0.052 af
Subcatchment 14S: Flow to Cross Culvert	Runoff Area=7,713 sf 59.39% Impervious Runoff Depth>2.08" Tc=6.0 min CN=74 Runoff=0.42 cfs 0.031 af
Subcatchment 15S: Area behind future	Runoff Area=17,796 sf 67.02% Impervious Runoff Depth>2.49" Tc=6.0 min CN=79 Runoff=1.17 cfs 0.085 af
Subcatchment 16S: Subcatchment #16	Runoff Area=124,823 sf 1.96% Impervious Runoff Depth>0.26" Flow Length=344' Tc=16.5 min UI Adjusted CN=43 Runoff=0.19 cfs 0.061 af
Subcatchment 17S: Subcatchment #17	Runoff Area=152,689 sf 2.08% Impervious Runoff Depth>0.85" Flow Length=591' Tc=30.6 min CN=56 Runoff=1.57 cfs 0.249 af
Subcatchment 18S: Subcatchment #18	Runoff Area=170,513 sf 0.61% Impervious Runoff Depth>1.09" Flow Length=376' Tc=17.1 min CN=60 Runoff=3.10 cfs 0.356 af

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Subcatchment 19S: Subcatchment #19	Runoff Area=690,822 sf 0.00% Impervious Runoff Depth>0.74" Flow Length=1,832' Tc=46.3 min CN=54 Runoff=4.74 cfs 0.978 af
Subcatchment 31S: CB #31	Runoff Area=6,795 sf 55.78% Impervious Runoff Depth>2.94" Tc=6.0 min CN=84 Runoff=0.52 cfs 0.038 af
Subcatchment 32S: CB #32	Runoff Area=5,694 sf 79.08% Impervious Runoff Depth>3.53" Tc=6.0 min CN=90 Runoff=0.51 cfs 0.038 af
Subcatchment 33S: CB #33	Runoff Area=14,734 sf 60.85% Impervious Runoff Depth>2.94" Tc=6.0 min CN=84 Runoff=1.14 cfs 0.083 af
Subcatchment 34S: CB #34	Runoff Area=5,164 sf 100.00% Impervious Runoff Depth>4.40" Tc=6.0 min CN=98 Runoff=0.52 cfs 0.043 af
Subcatchment 35S: CB #35	Runoff Area=6,367 sf 67.93% Impervious Runoff Depth>3.13" Tc=6.0 min CN=86 Runoff=0.52 cfs 0.038 af
Subcatchment 36S: CB #36	Runoff Area=7,548 sf 93.27% Impervious Runoff Depth>4.17" Tc=6.0 min CN=96 Runoff=0.75 cfs 0.060 af
Subcatchment 37S: CB #37	Runoff Area=9,102 sf 80.61% Impervious Runoff Depth>3.63" Tc=6.0 min CN=91 Runoff=0.84 cfs 0.063 af
Subcatchment 38S: CB #38	Runoff Area=8,387 sf 77.58% Impervious Runoff Depth>3.53" Tc=6.0 min CN=90 Runoff=0.76 cfs 0.057 af
Subcatchment 39S: CB #39	Runoff Area=9,406 sf 38.75% Impervious Runoff Depth>2.32" Tc=6.0 min CN=77 Runoff=0.58 cfs 0.042 af
Subcatchment 40S: CB #40	Runoff Area=3,206 sf 100.00% Impervious Runoff Depth>4.40" Tc=6.0 min CN=98 Runoff=0.33 cfs 0.027 af
Subcatchment 41S: CB #41	Runoff Area=3,664 sf 87.72% Impervious Runoff Depth>3.95" Tc=6.0 min CN=94 Runoff=0.36 cfs 0.028 af
Subcatchment 42S: CB #42	Runoff Area=4,646 sf 81.42% Impervious Runoff Depth>3.74" Tc=6.0 min CN=92 Runoff=0.44 cfs 0.033 af
Subcatchment 43S: CB #43	Runoff Area=14,297 sf 87.98% Impervious Runoff Depth>3.95" Tc=6.0 min CN=94 Runoff=1.39 cfs 0.108 af
Subcatchment 44S: CB #44	Runoff Area=30,768 sf 38.03% Impervious Runoff Depth>2.00" Flow Length=493' Tc=14.6 min CN=73 Runoff=1.24 cfs 0.117 af
Subcatchment 45S: CB #45	Runoff Area=30,969 sf 18.55% Impervious Runoff Depth>1.62" Flow Length=265' Tc=10.4 min UI Adjusted CN=68 Runoff=1.11 cfs 0.096 af
Subcatchment 46S: CB #46	Runoff Area=7,198 sf 100.00% Impervious Runoff Depth>4.40" Tc=6.0 min CN=98 Runoff=0.73 cfs 0.061 af
Subcatchment 47S: Inlet Sump High Pt Dr	Runoff Area=95,547 sf 3.02% Impervious Runoff Depth>0.80" Flow Length=862' Tc=26.2 min UI Adjusted CN=55 Runoff=0.95 cfs 0.146 af

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Subcatchment48S: High Pt Dr Cul-De-Sac	Runoff Area=7,531 sf 77.93% Impervious Tc=6.0 min CN=91	Runoff Depth>3.63" Runoff=0.69 cfs 0.052 af
Subcatchment49S: Community Dr	Runoff Area=10,872 sf 69.81% Impervious Tc=6.0 min CN=88	Runoff Depth>3.33" Runoff=0.93 cfs 0.069 af
Subcatchment50S: Subcatchment#50	Runoff Area=20,749 sf 0.00% Impervious Flow Length=209' Tc=15.8 min CN=55	Runoff Depth>0.80" Runoff=0.25 cfs 0.032 af
Subcatchment51S: Outlet Pond	Runoff Area=2,846 sf 0.00% Impervious Tc=6.0 min CN=61	Runoff Depth>1.16" Runoff=0.08 cfs 0.006 af
Subcatchment52S: Southern Wetland	Runoff Area=237,763 sf 0.00% Impervious Flow Length=1,157' Tc=26.8 min CN=55	Runoff Depth>0.80" Runoff=2.34 cfs 0.364 af
Subcatchment53S: Northern Wetland	Runoff Area=23,588 sf 0.00% Impervious Flow Length=497' Tc=20.6 min CN=56	Runoff Depth>0.86" Runoff=0.28 cfs 0.039 af
Subcatchment54S: Subcatchment#54	Runoff Area=118,144 sf 0.71% Impervious Flow Length=1,159' Tc=25.9 min CN=58	Runoff Depth>0.97" Runoff=1.55 cfs 0.219 af
Subcatchment55S: 15" HDPE N-12	Runoff Area=4,389 sf 0.00% Impervious Tc=6.0 min CN=61	Runoff Depth>1.16" Runoff=0.12 cfs 0.010 af
Subcatchment63S: Gravel Wetland #103	Runoff Area=4,821 sf 0.00% Impervious Tc=6.0 min CN=61	Runoff Depth>1.16" Runoff=0.13 cfs 0.011 af
Subcatchment64S: Gravel Wetland #104	Runoff Area=1,940 sf 0.00% Impervious Tc=6.0 min CN=61	Runoff Depth>1.16" Runoff=0.05 cfs 0.004 af
Subcatchment65S: Rain Garden #105	Runoff Area=12,647 sf 3.41% Impervious Tc=6.0 min CN=67	Runoff Depth>1.56" Runoff=0.50 cfs 0.038 af
Subcatchment66S: Rain Garden #106	Runoff Area=34,434 sf 4.69% Impervious Flow Length=211' Tc=15.3 min UI Adjusted CN=65	Runoff Depth>1.41" Runoff=0.91 cfs 0.093 af
Subcatchment67S: Rain Garden #107	Runoff Area=22,575 sf 0.00% Impervious Flow Length=92' Tc=10.9 min CN=61	Runoff Depth>1.15" Runoff=0.52 cfs 0.050 af
Subcatchment68S: Rain Garden #108	Runoff Area=7,430 sf 45.91% Impervious Tc=6.0 min CN=78	Runoff Depth>2.41" Runoff=0.47 cfs 0.034 af
Subcatchment69S: Rain Garden #109	Runoff Area=78,911 sf 0.00% Impervious Flow Length=493' Tc=14.4 min CN=61	Runoff Depth>1.15" Runoff=1.64 cfs 0.174 af
Subcatchment70S: Detention Pond #110	Runoff Area=24,497 sf 0.00% Impervious Flow Length=273' Tc=12.3 min CN=59	Runoff Depth>1.03" Runoff=0.46 cfs 0.048 af
Subcatchment310S: Subcatchment 10	Runoff Area=9,312 sf 47.01% Impervious Tc=6.0 min CN=70	Runoff Depth>1.77" Runoff=0.43 cfs 0.032 af

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Subcatchment 330S: Subcatchment 30	Runoff Area=5,360 sf	77.01% Impervious	Runoff Depth>3.43"	
	Tc=6.0 min	CN=89	Runoff=0.47 cfs	0.035 af
Reach 2R: Reach 2	Avg. Flow Depth=0.35'	Max Vel=2.79 fps	Inflow=3.64 cfs	0.927 af
	n=0.022 L=220.0'	S=0.0091 '/'	Capacity=24.64 cfs	Outflow=3.64 cfs 0.926 af
Reach 11R: Flow Through 8	Avg. Flow Depth=0.08'	Max Vel=0.68 fps	Inflow=0.14 cfs	0.047 af
	n=0.035 L=76.0'	S=0.0132 '/'	Capacity=7.77 cfs	Outflow=0.14 cfs 0.047 af
Reach 50R: Overland flow	Avg. Flow Depth=0.12'	Max Vel=1.44 fps	Inflow=0.41 cfs	0.181 af
	n=0.025 L=42.0'	S=0.0179 '/'	Capacity=186.81 cfs	Outflow=0.40 cfs 0.181 af
Reach 52R: Wetland Flow	Avg. Flow Depth=0.20'	Max Vel=1.47 fps	Inflow=2.55 cfs	0.600 af
	n=0.045 L=123.0'	S=0.0285 '/'	Capacity=17.83 cfs	Outflow=2.55 cfs 0.600 af
Reach 53R: Wetland Flow	Avg. Flow Depth=0.07'	Max Vel=0.82 fps	Inflow=0.28 cfs	0.039 af
	n=0.045 L=135.0'	S=0.0370 '/'	Capacity=20.35 cfs	Outflow=0.28 cfs 0.039 af
Reach 54R: Combined Wetland Flow	Avg. Flow Depth=0.21'	Max Vel=4.05 fps	Inflow=2.80 cfs	0.638 af
	n=0.045 L=87.0'	S=0.1379 '/'	Capacity=610.11 cfs	Outflow=2.80 cfs 0.638 af
Reach 63R: Overland Flow	Avg. Flow Depth=0.03'	Max Vel=0.85 fps	Inflow=0.12 cfs	0.070 af
	n=0.030 L=126.0'	S=0.0476 '/'	Capacity=43.27 cfs	Outflow=0.12 cfs 0.069 af
Reach 65R: Overland Flow	Avg. Flow Depth=0.09'	Max Vel=1.07 fps	Inflow=0.56 cfs	0.296 af
	n=0.035 L=342.1'	S=0.0270 '/'	Capacity=22.35 cfs	Outflow=0.54 cfs 0.294 af
Reach 66R: Overland Flow	Avg. Flow Depth=0.06'	Max Vel=1.71 fps	Inflow=0.21 cfs	0.140 af
	n=0.025 L=48.0'	S=0.0677 '/'	Capacity=24.68 cfs	Outflow=0.21 cfs 0.139 af
Reach 67R: Overland flow	Avg. Flow Depth=0.11'	Max Vel=1.40 fps	Inflow=0.36 cfs	0.262 af
	n=0.030 L=180.0'	S=0.0250 '/'	Capacity=39.17 cfs	Outflow=0.36 cfs 0.261 af
Reach 69R: Overland Flow	Avg. Flow Depth=0.08'	Max Vel=1.20 fps	Inflow=0.42 cfs	0.369 af
	n=0.035 L=70.0'	S=0.0429 '/'	Capacity=111.48 cfs	Outflow=0.42 cfs 0.369 af
Reach 70R: Overland Flow From Det	Avg. Flow Depth=0.10'	Max Vel=2.02 fps	Inflow=0.44 cfs	0.237 af
	n=0.035 L=61.0'	S=0.0820 '/'	Capacity=60.79 cfs	Outflow=0.44 cfs 0.237 af
Reach 100R: Reach 100			Inflow=0.65 cfs	0.355 af
			Outflow=0.65 cfs	0.355 af
Reach 200R: Reach 200			Inflow=2.24 cfs	0.822 af
			Outflow=2.24 cfs	0.822 af
Reach 300R: Reach 300			Inflow=5.24 cfs	0.994 af
			Outflow=5.24 cfs	0.994 af
Reach 400R: Reach 400			Inflow=4.74 cfs	0.978 af
			Outflow=4.74 cfs	0.978 af
Reach 800R: Svenson Pond			Inflow=5.10 cfs	1.695 af
			Outflow=5.10 cfs	1.695 af

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Pond 1P: Drop Inlet	Peak Elev=201.07' Storage=1 cf Inflow=0.42 cfs 0.195 af Primary=0.42 cfs 0.195 af Secondary=0.00 cfs 0.000 af Outflow=0.42 cfs 0.195 af
Pond 2P: Prop. 18" Cross Culvert	Peak Elev=199.06' Storage=117 cf Inflow=3.95 cfs 1.035 af 18.0" Round Culvert n=0.012 L=60.0' S=0.0100 ' Outflow=3.95 cfs 1.035 af
Pond 4P: Prop. CB#3	Peak Elev=200.59' Storage=0.000 af Inflow=3.89 cfs 0.505 af 15.0" Round Culvert n=0.012 L=93.7' S=0.0053 ' Outflow=3.89 cfs 0.505 af
Pond 6P: Inlet Depression	Peak Elev=200.87' Storage=209 cf Inflow=2.25 cfs 0.167 af 15.0" Round Culvert n=0.012 L=30.0' S=0.0233 ' Outflow=2.10 cfs 0.167 af
Pond 8P: 24" Cross Culvert	Peak Elev=197.72' Storage=341 cf Inflow=5.07 cfs 1.676 af Primary=5.06 cfs 1.676 af Secondary=0.00 cfs 0.000 af Outflow=5.06 cfs 1.676 af
Pond 10P: EX. CB#10	Peak Elev=200.78' Storage=9 cf Inflow=0.91 cfs 0.261 af 15.0" Round Culvert n=0.012 L=153.9' S=0.0050 ' Outflow=0.90 cfs 0.261 af
Pond 12P: Ex. CB#2	Peak Elev=200.20' Storage=0.000 af Inflow=4.33 cfs 0.542 af 15.0" Round Culvert n=0.012 L=20.0' S=0.0050 ' Outflow=4.33 cfs 0.542 af
Pond 13P: Infiltration Pond	Peak Elev=203.32' Storage=858 cf Inflow=0.47 cfs 0.052 af Discarded=0.06 cfs 0.050 af Primary=0.00 cfs 0.000 af Outflow=0.06 cfs 0.050 af
Pond 14P: Ex. 15" Cross Culvert	Peak Elev=201.76' Storage=195 cf Inflow=0.42 cfs 0.031 af Discarded=0.02 cfs 0.011 af Primary=0.25 cfs 0.020 af Outflow=0.26 cfs 0.031 af
Pond 16P: Ex. 12" CMP	Peak Elev=203.80' Storage=150 cf Inflow=0.66 cfs 0.356 af Outflow=0.65 cfs 0.355 af
Pond 17P: Ex. 18" HDPE N-12	Peak Elev=203.06' Storage=158 cf Inflow=2.25 cfs 0.822 af Primary=2.24 cfs 0.822 af Secondary=0.00 cfs 0.000 af Outflow=2.24 cfs 0.822 af
Pond 18P: Box Culvert	Peak Elev=191.05' Storage=49 cf Inflow=5.24 cfs 0.994 af 36.0" x 36.0" Box Culvert n=0.012 L=28.0' S=0.0018 ' Outflow=5.24 cfs 0.994 af
Pond 19P: Box Culvert	Peak Elev=183.75' Storage=10 cf Inflow=4.74 cfs 0.978 af 36.0" x 36.0" Box Culvert n=0.012 L=52.0' S=-0.0085 ' Outflow=4.74 cfs 0.978 af
Pond 47P: Inlet Sump High Point Drive	Peak Elev=237.21' Storage=29 cf Inflow=0.95 cfs 0.146 af 15.0" Round Culvert n=0.012 L=23.0' S=0.0609 ' Outflow=0.95 cfs 0.146 af
Pond 48P: High Point Drive Cul-de Sac	Peak Elev=236.37' Storage=153 cf Inflow=0.69 cfs 0.052 af 15.0" Round Culvert n=0.012 L=50.0' S=0.0130 ' Outflow=0.63 cfs 0.052 af
Pond 49P: Community Drive Cul-de Sac	Peak Elev=218.18' Storage=350 cf Inflow=0.93 cfs 0.069 af 15.0" Round Culvert n=0.012 L=53.5' S=0.0121 ' Outflow=0.88 cfs 0.065 af
Pond 50P: 15" HDPE (Access Road)	Peak Elev=203.59' Storage=37 cf Inflow=0.41 cfs 0.181 af 15.0" Round Culvert n=0.012 L=42.0' S=0.0060 ' Outflow=0.41 cfs 0.181 af

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Type III 24-hr 10YR - 24HR Rainfall=4.64"

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Pond 51P: Outlet Pond	Peak Elev=214.02' Storage=907 cf Inflow=0.32 cfs 0.053 af Outflow=0.12 cfs 0.032 af
Pond 52P: S Wetland Crossing 24" HDPE N-12	Peak Elev=214.03' Storage=31 cf Inflow=2.34 cfs 0.364 af 24.0" Round Culvert w/ 6.0" inside fill n=0.024 L=36.0' S=0.0278 '/' Outflow=2.34 cfs 0.363 af
Pond 53P: N Wetland Crossing 24" HDPE N-12	Peak Elev=215.63' Storage=4 cf Inflow=0.28 cfs 0.039 af 24.0" Round Culvert w/ 6.0" inside fill n=0.024 L=25.0' S=0.0600 '/' Outflow=0.28 cfs 0.039 af
Pond 54P: Inlet Sump Detention Pond #110	Peak Elev=222.60' Storage=48 cf Inflow=1.55 cfs 0.219 af 15.0" Round Culvert n=0.012 L=35.0' S=0.0571 '/' Outflow=1.55 cfs 0.219 af
Pond 55P: Drop Inlet #55	Peak Elev=204.00' Storage=0.000 af Inflow=0.22 cfs 0.149 af 15.0" Round Culvert n=0.012 L=93.2' S=0.0054 '/' Outflow=0.22 cfs 0.149 af
Pond 101P: Ex. Rain Garden #101	Peak Elev=201.68' Storage=1,878 cf Inflow=1.39 cfs 0.104 af Primary=0.30 cfs 0.085 af Secondary=0.00 cfs 0.000 af Outflow=0.30 cfs 0.085 af
Pond 102P: Ex. Rain Garden #102	Peak Elev=200.11' Storage=5,927 cf Inflow=5.00 cfs 0.597 af Primary=0.46 cfs 0.475 af Secondary=1.63 cfs 0.099 af Outflow=2.09 cfs 0.574 af
Pond 103P: Gravel Wetland #103	Peak Elev=214.05' Storage=3,493 cf Inflow=1.78 cfs 0.136 af Primary=0.12 cfs 0.070 af Secondary=0.00 cfs 0.000 af Outflow=0.12 cfs 0.070 af
Pond 104P: Gravel Wetland #104	Peak Elev=216.30' Storage=1,675 cf Inflow=1.06 cfs 0.080 af Primary=0.29 cfs 0.046 af Secondary=0.00 cfs 0.000 af Outflow=0.29 cfs 0.046 af
Pond 105P: Rain Garden #105	Peak Elev=219.16' Storage=11,010 cf Inflow=5.60 cfs 0.431 af Outflow=0.44 cfs 0.264 af
Pond 106P: Rain Garden #106	Peak Elev=218.18' Storage=4,908 cf Inflow=2.23 cfs 0.218 af Outflow=0.21 cfs 0.140 af
Pond 107P: Rain Garden #107	Peak Elev=228.19' Storage=13,588 cf Inflow=4.21 cfs 0.522 af Discarded=0.01 cfs 0.016 af Primary=0.36 cfs 0.262 af Secondary=0.00 cfs 0.000 af Outflow=0.37 cfs 0.278 af
Pond 108P: Rain Garden #108	Peak Elev=206.19' Storage=885 cf Inflow=0.47 cfs 0.034 af Primary=0.02 cfs 0.024 af Secondary=0.00 cfs 0.000 af Outflow=0.02 cfs 0.024 af
Pond 109P: Rain Garden #109	Peak Elev=216.99' Storage=4,695 cf Inflow=1.64 cfs 0.435 af Primary=0.42 cfs 0.369 af Secondary=0.00 cfs 0.000 af Outflow=0.42 cfs 0.369 af
Pond 110P: Detention Pond #110	Peak Elev=219.24' Storage=4,018 cf Inflow=1.87 cfs 0.267 af Primary=0.44 cfs 0.237 af Secondary=0.00 cfs 0.000 af Outflow=0.44 cfs 0.237 af
Pond C30P: CB #30	Peak Elev=200.83' Storage=7 cf Inflow=0.49 cfs 0.230 af 15.0" Round Culvert n=0.012 L=25.0' S=0.0052 '/' Outflow=0.48 cfs 0.230 af
Pond C31P: CB #31	Peak Elev=216.30' Storage=27 cf Inflow=1.02 cfs 0.076 af 15.0" Round Culvert n=0.012 L=18.0' S=0.0083 '/' Outflow=1.01 cfs 0.075 af
Pond C32P: CB #32	Peak Elev=216.30' Storage=24 cf Inflow=0.51 cfs 0.038 af 15.0" Round Culvert n=0.012 L=26.0' S=0.0058 '/' Outflow=0.50 cfs 0.038 af

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Pond C33P: CB #33	Peak Elev=214.05' Storage=19 cf Inflow=1.14 cfs 0.083 af 15.0" Round Culvert n=0.012 L=28.7' S=0.0070 ' Outflow=1.13 cfs 0.082 af
Pond C34P: CB #34	Peak Elev=216.89' Storage=8 cf Inflow=0.52 cfs 0.043 af 15.0" Round Culvert n=0.012 L=63.5' S=0.0669 ' Outflow=0.53 cfs 0.043 af
Pond C35P: CB #35	Peak Elev=219.16' Storage=30 cf Inflow=0.52 cfs 0.038 af 15.0" Round Culvert n=0.012 L=10.0' S=0.0300 ' Outflow=0.50 cfs 0.038 af
Pond C36P: CB #36	Peak Elev=225.14' Storage=6 cf Inflow=0.75 cfs 0.060 af 15.0" Round Culvert n=0.012 L=162.0' S=0.0050 ' Outflow=0.75 cfs 0.060 af
Pond C37P: CB #37	Peak Elev=224.25' Storage=8 cf Inflow=1.59 cfs 0.123 af 15.0" Round Culvert n=0.012 L=84.0' S=0.0183 ' Outflow=1.59 cfs 0.123 af
Pond C38P: CB #38	Peak Elev=219.61' Storage=5 cf Inflow=0.76 cfs 0.057 af 15.0" Round Culvert n=0.012 L=13.0' S=0.0138 ' Outflow=0.76 cfs 0.057 af
Pond C39P: CB #39	Peak Elev=219.16' Storage=33 cf Inflow=0.88 cfs 0.068 af 15.0" Round Culvert n=0.012 L=15.0' S=0.0167 ' Outflow=0.87 cfs 0.068 af
Pond C40P: CB #40	Peak Elev=219.16' Storage=27 cf Inflow=0.33 cfs 0.027 af 15.0" Round Culvert n=0.012 L=31.7' S=0.0126 ' Outflow=0.31 cfs 0.027 af
Pond C41P: CB #41	Peak Elev=218.18' Storage=31 cf Inflow=1.66 cfs 0.126 af 15.0" Round Culvert n=0.012 L=17.5' S=0.0143 ' Outflow=1.64 cfs 0.125 af
Pond C42P: CB #42	Peak Elev=218.18' Storage=24 cf Inflow=0.44 cfs 0.033 af 15.0" Round Culvert n=0.012 L=26.0' S=0.0154 ' Outflow=0.43 cfs 0.033 af
Pond C43P: CB #43	Peak Elev=224.45' Storage=7 cf Inflow=1.39 cfs 0.108 af 15.0" Round Culvert n=0.012 L=48.0' S=0.0371 ' Outflow=1.39 cfs 0.108 af
Pond C44P: CB #44	Peak Elev=229.39' Storage=9 cf Inflow=2.29 cfs 0.214 af 15.0" Round Culvert n=0.012 L=87.0' S=0.0187 ' Outflow=2.29 cfs 0.214 af
Pond C45P: CB #45	Peak Elev=231.00' Storage=6 cf Inflow=1.11 cfs 0.096 af 15.0" Round Culvert n=0.012 L=65.0' S=0.0108 ' Outflow=1.11 cfs 0.096 af
Pond C46P: CB #46	Peak Elev=235.76' Storage=6 cf Inflow=1.14 cfs 0.207 af 15.0" Round Culvert n=0.012 L=105.0' S=0.0681 ' Outflow=1.14 cfs 0.207 af
Pond D01P: DMH #1	Peak Elev=214.05' Storage=23 cf Inflow=1.66 cfs 0.126 af 15.0" Round Culvert n=0.012 L=22.5' S=0.0089 ' Outflow=1.65 cfs 0.125 af
Pond D02P: DMH #2	Peak Elev=222.89' Storage=11 cf Inflow=2.98 cfs 0.231 af 15.0" Round Culvert n=0.012 L=95.0' S=0.0447 ' Outflow=2.98 cfs 0.231 af
Pond D03P: DMH #3	Peak Elev=230.20' Storage=6 cf Inflow=1.11 cfs 0.096 af 15.0" Round Culvert n=0.012 L=65.5' S=0.0148 ' Outflow=1.11 cfs 0.096 af

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Pond D04P: DMH #4

Peak Elev=228.59' Storage=7 cf Inflow=1.49 cfs 0.259 af
15.0" Round Culvert n=0.012 L=50.0' S=0.0100 '/ Outflow=1.49 cfs 0.259 af

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Type III 24-hr 25YR - 24HR Rainfall=5.86"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1	Runoff Area=257,558 sf 0.40% Impervious Runoff Depth>0.62" Flow Length=1,542' Tc=32.6 min CN=43 Runoff=1.36 cfs 0.304 af
Subcatchment 2S: subcatchment 2	Runoff Area=764,518 sf 0.65% Impervious Runoff Depth>1.19" Flow Length=2,418' Tc=59.1 min CN=52 Runoff=8.18 cfs 1.744 af
Subcatchment 3S: Subcatchment 3	Runoff Area=118,503 sf 0.00% Impervious Runoff Depth>0.35" Flow Length=993' Tc=20.7 min CN=38 Runoff=0.26 cfs 0.080 af
Subcatchment 4S: Subcatchment 4	Runoff Area=9,068 sf 100.00% Impervious Runoff Depth>5.62" Flow Length=207' Tc=6.0 min CN=98 Runoff=1.17 cfs 0.097 af
Subcatchment 5S: Subcatchment 5	Runoff Area=22,497 sf 40.08% Impervious Runoff Depth>2.08" Flow Length=212' Tc=7.0 min CN=63 Runoff=1.16 cfs 0.089 af
Subcatchment 6S: Subcatchment 6	Runoff Area=25,520 sf 84.67% Impervious Runoff Depth>4.60" Tc=6.0 min CN=89 Runoff=2.97 cfs 0.224 af
Subcatchment 8S: Subcatchment 8	Runoff Area=25,776 sf 25.48% Impervious Runoff Depth>0.87" Flow Length=152' Tc=10.4 min UI Adjusted CN=47 Runoff=0.34 cfs 0.043 af
Subcatchment 9S: Subcatchment 9	Runoff Area=45,641 sf 11.38% Impervious Runoff Depth>0.56" Flow Length=259' Tc=13.4 min UI Adjusted CN=42 Runoff=0.26 cfs 0.049 af
Subcatchment 11S: Area Behind the Dove	Runoff Area=84,194 sf 13.93% Impervious Runoff Depth>0.68" Flow Length=636' Tc=29.3 min UI Adjusted CN=44 Runoff=0.54 cfs 0.109 af
Subcatchment 12S: Road Flow	Runoff Area=4,388 sf 100.00% Impervious Runoff Depth>5.62" Tc=6.0 min CN=98 Runoff=0.56 cfs 0.047 af
Subcatchment 13S: Area in front of future	Runoff Area=29,777 sf 30.66% Impervious Runoff Depth>1.59" Flow Length=175' Tc=12.4 min CN=57 Runoff=0.92 cfs 0.090 af
Subcatchment 14S: Flow to Cross Culvert	Runoff Area=7,713 sf 59.39% Impervious Runoff Depth>3.06" Tc=6.0 min CN=74 Runoff=0.62 cfs 0.045 af
Subcatchment 15S: Area behind future	Runoff Area=17,796 sf 67.02% Impervious Runoff Depth>3.55" Tc=6.0 min CN=79 Runoff=1.66 cfs 0.121 af
Subcatchment 16S: Subcatchment #16	Runoff Area=124,823 sf 1.96% Impervious Runoff Depth>0.62" Flow Length=344' Tc=16.5 min UI Adjusted CN=43 Runoff=0.82 cfs 0.148 af
Subcatchment 17S: Subcatchment #17	Runoff Area=152,689 sf 2.08% Impervious Runoff Depth>1.50" Flow Length=591' Tc=30.6 min CN=56 Runoff=3.12 cfs 0.438 af
Subcatchment 18S: Subcatchment #18	Runoff Area=170,513 sf 0.61% Impervious Runoff Depth>1.82" Flow Length=376' Tc=17.1 min CN=60 Runoff=5.61 cfs 0.595 af

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Subcatchment 19S: Subcatchment#19	Runoff Area=690,822 sf 0.00% Impervious Runoff Depth>1.34" Flow Length=1,832' Tc=46.3 min CN=54 Runoff=9.97 cfs 1.775 af
Subcatchment 31S: CB #31	Runoff Area=6,795 sf 55.78% Impervious Runoff Depth>4.06" Tc=6.0 min CN=84 Runoff=0.72 cfs 0.053 af
Subcatchment 32S: CB #32	Runoff Area=5,694 sf 79.08% Impervious Runoff Depth>4.71" Tc=6.0 min CN=90 Runoff=0.67 cfs 0.051 af
Subcatchment 33S: CB #33	Runoff Area=14,734 sf 60.85% Impervious Runoff Depth>4.06" Tc=6.0 min CN=84 Runoff=1.56 cfs 0.115 af
Subcatchment 34S: CB #34	Runoff Area=5,164 sf 100.00% Impervious Runoff Depth>5.62" Tc=6.0 min CN=98 Runoff=0.66 cfs 0.056 af
Subcatchment 35S: CB #35	Runoff Area=6,367 sf 67.93% Impervious Runoff Depth>4.27" Tc=6.0 min CN=86 Runoff=0.70 cfs 0.052 af
Subcatchment 36S: CB #36	Runoff Area=7,548 sf 93.27% Impervious Runoff Depth>5.38" Tc=6.0 min CN=96 Runoff=0.96 cfs 0.078 af
Subcatchment 37S: CB #37	Runoff Area=9,102 sf 80.61% Impervious Runoff Depth>4.82" Tc=6.0 min CN=91 Runoff=1.09 cfs 0.084 af
Subcatchment 38S: CB #38	Runoff Area=8,387 sf 77.58% Impervious Runoff Depth>4.71" Tc=6.0 min CN=90 Runoff=0.99 cfs 0.076 af
Subcatchment 39S: CB #39	Runoff Area=9,406 sf 38.75% Impervious Runoff Depth>3.35" Tc=6.0 min CN=77 Runoff=0.83 cfs 0.060 af
Subcatchment 40S: CB #40	Runoff Area=3,206 sf 100.00% Impervious Runoff Depth>5.62" Tc=6.0 min CN=98 Runoff=0.41 cfs 0.034 af
Subcatchment 41S: CB #41	Runoff Area=3,664 sf 87.72% Impervious Runoff Depth>5.15" Tc=6.0 min CN=94 Runoff=0.46 cfs 0.036 af
Subcatchment 42S: CB #42	Runoff Area=4,646 sf 81.42% Impervious Runoff Depth>4.93" Tc=6.0 min CN=92 Runoff=0.57 cfs 0.044 af
Subcatchment 43S: CB #43	Runoff Area=14,297 sf 87.98% Impervious Runoff Depth>5.15" Tc=6.0 min CN=94 Runoff=1.78 cfs 0.141 af
Subcatchment 44S: CB #44	Runoff Area=30,768 sf 38.03% Impervious Runoff Depth>2.96" Flow Length=493' Tc=14.6 min CN=73 Runoff=1.87 cfs 0.174 af
Subcatchment 45S: CB #45	Runoff Area=30,969 sf 18.55% Impervious Runoff Depth>2.51" Flow Length=265' Tc=10.4 min UI Adjusted CN=68 Runoff=1.77 cfs 0.149 af
Subcatchment 46S: CB #46	Runoff Area=7,198 sf 100.00% Impervious Runoff Depth>5.62" Tc=6.0 min CN=98 Runoff=0.93 cfs 0.077 af
Subcatchment 47S: Inlet Sump High Pt Dr	Runoff Area=95,547 sf 3.02% Impervious Runoff Depth>1.43" Flow Length=862' Tc=26.2 min UI Adjusted CN=55 Runoff=1.95 cfs 0.261 af

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Subcatchment48S: High Pt Dr Cul-De-Sac	Runoff Area=7,531 sf 77.93% Impervious Runoff Depth>4.82" Tc=6.0 min CN=91 Runoff=0.90 cfs 0.069 af
Subcatchment49S: Community Dr	Runoff Area=10,872 sf 69.81% Impervious Runoff Depth>4.49" Tc=6.0 min CN=88 Runoff=1.24 cfs 0.093 af
Subcatchment50S: Subcatchment#50	Runoff Area=20,749 sf 0.00% Impervious Runoff Depth>1.43" Flow Length=209' Tc=15.8 min CN=55 Runoff=0.52 cfs 0.057 af
Subcatchment51S: Outet Pond	Runoff Area=2,846 sf 0.00% Impervious Runoff Depth>1.91" Tc=6.0 min CN=61 Runoff=0.14 cfs 0.010 af
Subcatchment52S: Southern Wetland	Runoff Area=237,763 sf 0.00% Impervious Runoff Depth>1.43" Flow Length=1,157' Tc=26.8 min CN=55 Runoff=4.80 cfs 0.649 af
Subcatchment53S: Northern Wetland	Runoff Area=23,588 sf 0.00% Impervious Runoff Depth>1.51" Flow Length=497' Tc=20.6 min CN=56 Runoff=0.57 cfs 0.068 af
Subcatchment54S: Subcatchment#54	Runoff Area=118,144 sf 0.71% Impervious Runoff Depth>1.66" Flow Length=1,159' Tc=25.9 min CN=58 Runoff=2.93 cfs 0.375 af
Subcatchment55S: 15" HDPE N-12	Runoff Area=4,389 sf 0.00% Impervious Runoff Depth>1.91" Tc=6.0 min CN=61 Runoff=0.21 cfs 0.016 af
Subcatchment63S: Gravel Wetland #103	Runoff Area=4,821 sf 0.00% Impervious Runoff Depth>1.91" Tc=6.0 min CN=61 Runoff=0.23 cfs 0.018 af
Subcatchment64S: Gravel Wetland #104	Runoff Area=1,940 sf 0.00% Impervious Runoff Depth>1.91" Tc=6.0 min CN=61 Runoff=0.09 cfs 0.007 af
Subcatchment65S: Rain Garden #105	Runoff Area=12,647 sf 3.41% Impervious Runoff Depth>2.42" Tc=6.0 min CN=67 Runoff=0.80 cfs 0.059 af
Subcatchment66S: Rain Garden #106	Runoff Area=34,434 sf 4.69% Impervious Runoff Depth>2.24" Flow Length=211' Tc=15.3 min UI Adjusted CN=65 Runoff=1.51 cfs 0.148 af
Subcatchment67S: Rain Garden #107	Runoff Area=22,575 sf 0.00% Impervious Runoff Depth>1.91" Flow Length=92' Tc=10.9 min CN=61 Runoff=0.93 cfs 0.082 af
Subcatchment68S: Rain Garden #108	Runoff Area=7,430 sf 45.91% Impervious Runoff Depth>3.45" Tc=6.0 min CN=78 Runoff=0.68 cfs 0.049 af
Subcatchment69S: Rain Garden #109	Runoff Area=78,911 sf 0.00% Impervious Runoff Depth>1.91" Flow Length=493' Tc=14.4 min CN=61 Runoff=2.93 cfs 0.288 af
Subcatchment70S: Detention Pond #110	Runoff Area=24,497 sf 0.00% Impervious Runoff Depth>1.74" Flow Length=273' Tc=12.3 min CN=59 Runoff=0.86 cfs 0.082 af
Subcatchment310S: Subcatchment 10	Runoff Area=9,312 sf 47.01% Impervious Runoff Depth>2.69" Tc=6.0 min CN=70 Runoff=0.66 cfs 0.048 af

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Subcatchment 330S: Subcatchment 30	Runoff Area=5,360 sf	77.01% Impervious	Runoff Depth>4.60"	
	Tc=6.0 min	CN=89	Runoff=0.62 cfs	0.047 af
Reach 2R: Reach 2	Avg. Flow Depth=0.55'	Max Vel=3.59 fps	Inflow=8.18 cfs	1.744 af
	n=0.022 L=220.0'	S=0.0091 '/'	Capacity=24.64 cfs	Outflow=8.18 cfs 1.742 af
Reach 11R: Flow Through 8	Avg. Flow Depth=0.15'	Max Vel=1.03 fps	Inflow=0.54 cfs	0.109 af
	n=0.035 L=76.0'	S=0.0132 '/'	Capacity=7.77 cfs	Outflow=0.54 cfs 0.109 af
Reach 50R: Overland flow	Avg. Flow Depth=0.16'	Max Vel=1.80 fps	Inflow=0.83 cfs	0.303 af
	n=0.025 L=42.0'	S=0.0179 '/'	Capacity=186.81 cfs	Outflow=0.83 cfs 0.303 af
Reach 52R: Wetland Flow	Avg. Flow Depth=0.28'	Max Vel=1.84 fps	Inflow=5.25 cfs	1.063 af
	n=0.045 L=123.0'	S=0.0285 '/'	Capacity=17.83 cfs	Outflow=5.25 cfs 1.062 af
Reach 53R: Wetland Flow	Avg. Flow Depth=0.10'	Max Vel=1.01 fps	Inflow=0.57 cfs	0.068 af
	n=0.045 L=135.0'	S=0.0370 '/'	Capacity=20.35 cfs	Outflow=0.56 cfs 0.068 af
Reach 54R: Combined Wetland Flow	Avg. Flow Depth=0.33'	Max Vel=5.20 fps	Inflow=5.76 cfs	1.130 af
	n=0.045 L=87.0'	S=0.1379 '/'	Capacity=610.11 cfs	Outflow=5.76 cfs 1.130 af
Reach 63R: Overland Flow	Avg. Flow Depth=0.04'	Max Vel=1.00 fps	Inflow=0.20 cfs	0.119 af
	n=0.030 L=126.0'	S=0.0476 '/'	Capacity=43.27 cfs	Outflow=0.20 cfs 0.119 af
Reach 65R: Overland Flow	Avg. Flow Depth=0.16'	Max Vel=1.60 fps	Inflow=2.24 cfs	0.471 af
	n=0.035 L=342.1'	S=0.0270 '/'	Capacity=22.35 cfs	Outflow=2.02 cfs 0.469 af
Reach 66R: Overland Flow	Avg. Flow Depth=0.06'	Max Vel=1.90 fps	Inflow=0.30 cfs	0.231 af
	n=0.025 L=48.0'	S=0.0677 '/'	Capacity=24.68 cfs	Outflow=0.30 cfs 0.231 af
Reach 67R: Overland flow	Avg. Flow Depth=0.14'	Max Vel=1.62 fps	Inflow=0.58 cfs	0.483 af
	n=0.030 L=180.0'	S=0.0250 '/'	Capacity=39.17 cfs	Outflow=0.58 cfs 0.482 af
Reach 69R: Overland Flow	Avg. Flow Depth=0.11'	Max Vel=1.54 fps	Inflow=0.94 cfs	0.624 af
	n=0.035 L=70.0'	S=0.0429 '/'	Capacity=111.48 cfs	Outflow=0.94 cfs 0.624 af
Reach 70R: Overland Flow From Det	Avg. Flow Depth=0.12'	Max Vel=2.29 fps	Inflow=0.66 cfs	0.415 af
	n=0.035 L=61.0'	S=0.0820 '/'	Capacity=60.79 cfs	Outflow=0.66 cfs 0.415 af
Reach 100R: Reach 100			Inflow=2.05 cfs	0.617 af
			Outflow=2.05 cfs	0.617 af
Reach 200R: Reach 200			Inflow=4.20 cfs	1.391 af
			Outflow=4.20 cfs	1.391 af
Reach 300R: Reach 300			Inflow=10.32 cfs	1.724 af
			Outflow=10.32 cfs	1.724 af
Reach 400R: Reach 400			Inflow=9.97 cfs	1.775 af
			Outflow=9.97 cfs	1.775 af
Reach 800R: Svenson Pond			Inflow=10.76 cfs	3.096 af
			Outflow=10.76 cfs	3.096 af

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Pond 1P: Drop Inlet	Peak Elev=201.47' Storage=2 cf Inflow=1.56 cfs 0.422 af Primary=1.55 cfs 0.422 af Secondary=0.00 cfs 0.000 af Outflow=1.55 cfs 0.422 af
Pond 2P: Prop. 18" Cross Culvert	Peak Elev=199.81' Storage=1,414 cf Inflow=8.76 cfs 1.976 af 18.0" Round Culvert n=0.012 L=60.0' S=0.0100 '/' Outflow=8.33 cfs 1.976 af
Pond 4P: Prop. CB#3	Peak Elev=201.27' Storage=0.001 af Inflow=4.46 cfs 0.839 af 15.0" Round Culvert n=0.012 L=93.7' S=0.0053 '/' Outflow=4.46 cfs 0.839 af
Pond 6P: Inlet Depression	Peak Elev=201.51' Storage=516 cf Inflow=2.97 cfs 0.224 af 15.0" Round Culvert n=0.012 L=30.0' S=0.0233 '/' Outflow=2.43 cfs 0.224 af
Pond 8P: 24" Cross Culvert	Peak Elev=198.37' Storage=1,119 cf Inflow=10.68 cfs 3.048 af Primary=10.66 cfs 3.047 af Secondary=0.00 cfs 0.000 af Outflow=10.66 cfs 3.047 af
Pond 10P: EX. CB#10	Peak Elev=201.46' Storage=17 cf Inflow=1.74 cfs 0.517 af 15.0" Round Culvert n=0.012 L=153.9' S=0.0050 '/' Outflow=1.75 cfs 0.517 af
Pond 12P: Ex. CB#2	Peak Elev=200.74' Storage=0.001 af Inflow=5.03 cfs 0.886 af 15.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=5.01 cfs 0.886 af
Pond 13P: Infiltration Pond	Peak Elev=203.42' Storage=1,247 cf Inflow=0.92 cfs 0.090 af Discarded=0.07 cfs 0.058 af Primary=0.24 cfs 0.023 af Outflow=0.31 cfs 0.081 af
Pond 14P: Ex. 15" Cross Culvert	Peak Elev=202.12' Storage=651 cf Inflow=0.62 cfs 0.068 af Discarded=0.02 cfs 0.015 af Primary=0.28 cfs 0.053 af Outflow=0.30 cfs 0.068 af
Pond 16P: Ex. 12" CMP	Peak Elev=204.38' Storage=1,402 cf Inflow=2.80 cfs 0.618 af Outflow=2.05 cfs 0.617 af
Pond 17P: Ex. 18" HDPE N-12	Peak Elev=203.44' Storage=402 cf Inflow=4.24 cfs 1.392 af Primary=4.20 cfs 1.391 af Secondary=0.00 cfs 0.000 af Outflow=4.20 cfs 1.391 af
Pond 18P: Box Culvert	Peak Elev=191.50' Storage=148 cf Inflow=10.32 cfs 1.724 af 36.0" x 36.0" Box Culvert n=0.012 L=28.0' S=0.0018 '/' Outflow=10.32 cfs 1.724 af
Pond 19P: Box Culvert	Peak Elev=184.15' Storage=24 cf Inflow=9.97 cfs 1.775 af 36.0" x 36.0" Box Culvert n=0.012 L=52.0' S=-0.0085 '/' Outflow=9.97 cfs 1.775 af
Pond 47P: Inlet Sump High Point Drive	Peak Elev=237.44' Storage=64 cf Inflow=1.95 cfs 0.261 af 15.0" Round Culvert n=0.012 L=23.0' S=0.0609 '/' Outflow=1.95 cfs 0.261 af
Pond 48P: High Point Drive Cul-de Sac	Peak Elev=236.43' Storage=180 cf Inflow=0.90 cfs 0.069 af 15.0" Round Culvert n=0.012 L=50.0' S=0.0130 '/' Outflow=0.84 cfs 0.069 af
Pond 49P: Community Drive Cul-de Sac	Peak Elev=218.85' Storage=636 cf Inflow=1.24 cfs 0.093 af 15.0" Round Culvert n=0.012 L=53.5' S=0.0121 '/' Outflow=0.99 cfs 0.089 af
Pond 50P: 15" HDPE (Access Road)	Peak Elev=203.75' Storage=60 cf Inflow=0.83 cfs 0.304 af 15.0" Round Culvert n=0.012 L=42.0' S=0.0060 '/' Outflow=0.83 cfs 0.303 af

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Pond 51P: Outlet Pond	Peak Elev=214.07' Storage=949 cf Inflow=0.87 cfs 0.087 af Outflow=0.83 cfs 0.066 af
Pond 52P: S Wetland Crossing 24" HDPE N-12	Peak Elev=214.35' Storage=86 cf Inflow=4.80 cfs 0.649 af 24.0" Round Culvert w/ 6.0" inside fill n=0.024 L=36.0' S=0.0278 '/' Outflow=4.80 cfs 0.649 af
Pond 53P: N Wetland Crossing 24" HDPE N-12	Peak Elev=215.71' Storage=6 cf Inflow=0.57 cfs 0.068 af 24.0" Round Culvert w/ 6.0" inside fill n=0.024 L=25.0' S=0.0600 '/' Outflow=0.57 cfs 0.068 af
Pond 54P: Inlet Sump Detention Pond #110	Peak Elev=222.88' Storage=79 cf Inflow=2.93 cfs 0.375 af 15.0" Round Culvert n=0.012 L=35.0' S=0.0571 '/' Outflow=2.93 cfs 0.375 af
Pond 55P: Drop Inlet #55	Peak Elev=204.09' Storage=0.000 af Inflow=0.33 cfs 0.247 af 15.0" Round Culvert n=0.012 L=93.2' S=0.0054 '/' Outflow=0.33 cfs 0.247 af
Pond 101P: Ex. Rain Garden #101	Peak Elev=202.10' Storage=2,682 cf Inflow=1.94 cfs 0.174 af Primary=0.39 cfs 0.155 af Secondary=0.00 cfs 0.000 af Outflow=0.39 cfs 0.155 af
Pond 102P: Ex. Rain Garden #102	Peak Elev=200.21' Storage=6,276 cf Inflow=6.14 cfs 0.975 af Primary=0.46 cfs 0.545 af Secondary=4.50 cfs 0.375 af Outflow=4.96 cfs 0.920 af
Pond 103P: Gravel Wetland #103	Peak Elev=214.46' Storage=4,554 cf Inflow=2.43 cfs 0.187 af Primary=0.20 cfs 0.119 af Secondary=0.00 cfs 0.000 af Outflow=0.20 cfs 0.119 af
Pond 104P: Gravel Wetland #104	Peak Elev=216.47' Storage=1,882 cf Inflow=1.46 cfs 0.110 af Primary=0.79 cfs 0.076 af Secondary=0.00 cfs 0.000 af Outflow=0.79 cfs 0.076 af
Pond 105P: Rain Garden #105	Peak Elev=219.61' Storage=13,225 cf Inflow=7.52 cfs 0.582 af Outflow=1.51 cfs 0.405 af
Pond 106P: Rain Garden #106	Peak Elev=218.85' Storage=7,015 cf Inflow=3.02 cfs 0.315 af Outflow=0.30 cfs 0.231 af
Pond 107P: Rain Garden #107	Peak Elev=229.12' Storage=20,541 cf Inflow=6.78 cfs 0.812 af Discarded=0.01 cfs 0.017 af Primary=0.58 cfs 0.483 af Secondary=0.00 cfs 0.000 af Outflow=0.59 cfs 0.500 af
Pond 108P: Rain Garden #108	Peak Elev=206.51' Storage=1,314 cf Inflow=0.68 cfs 0.049 af Primary=0.02 cfs 0.025 af Secondary=0.02 cfs 0.002 af Outflow=0.05 cfs 0.027 af
Pond 109P: Rain Garden #109	Peak Elev=217.80' Storage=6,590 cf Inflow=2.93 cfs 0.770 af Primary=0.94 cfs 0.624 af Secondary=0.00 cfs 0.000 af Outflow=0.94 cfs 0.624 af
Pond 110P: Detention Pond #110	Peak Elev=220.33' Storage=7,901 cf Inflow=3.50 cfs 0.456 af Primary=0.66 cfs 0.415 af Secondary=0.00 cfs 0.000 af Outflow=0.66 cfs 0.415 af
Pond C30P: CB #30	Peak Elev=201.36' Storage=13 cf Inflow=1.63 cfs 0.470 af 15.0" Round Culvert n=0.012 L=25.0' S=0.0052 '/' Outflow=1.64 cfs 0.469 af
Pond C31P: CB #31	Peak Elev=216.49' Storage=29 cf Inflow=1.38 cfs 0.104 af 15.0" Round Culvert n=0.012 L=18.0' S=0.0083 '/' Outflow=1.36 cfs 0.103 af
Pond C32P: CB #32	Peak Elev=216.49' Storage=26 cf Inflow=0.67 cfs 0.051 af 15.0" Round Culvert n=0.012 L=26.0' S=0.0058 '/' Outflow=0.66 cfs 0.051 af

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Pond C33P: CB #33	Peak Elev=214.47' Storage=25 cf Inflow=1.56 cfs 0.115 af 15.0" Round Culvert n=0.012 L=28.7' S=0.0070 ' Outflow=1.55 cfs 0.114 af
Pond C34P: CB #34	Peak Elev=216.93' Storage=9 cf Inflow=0.66 cfs 0.056 af 15.0" Round Culvert n=0.012 L=63.5' S=0.0669 ' Outflow=0.67 cfs 0.055 af
Pond C35P: CB #35	Peak Elev=219.62' Storage=35 cf Inflow=0.70 cfs 0.052 af 15.0" Round Culvert n=0.012 L=10.0' S=0.0300 ' Outflow=0.68 cfs 0.051 af
Pond C36P: CB #36	Peak Elev=225.21' Storage=7 cf Inflow=0.96 cfs 0.078 af 15.0" Round Culvert n=0.012 L=162.0' S=0.0050 ' Outflow=0.96 cfs 0.078 af
Pond C37P: CB #37	Peak Elev=224.35' Storage=9 cf Inflow=2.05 cfs 0.162 af 15.0" Round Culvert n=0.012 L=84.0' S=0.0183 ' Outflow=2.06 cfs 0.162 af
Pond C38P: CB #38	Peak Elev=219.68' Storage=6 cf Inflow=0.99 cfs 0.076 af 15.0" Round Culvert n=0.012 L=13.0' S=0.0138 ' Outflow=0.99 cfs 0.075 af
Pond C39P: CB #39	Peak Elev=219.62' Storage=39 cf Inflow=1.23 cfs 0.094 af 15.0" Round Culvert n=0.012 L=15.0' S=0.0167 ' Outflow=1.20 cfs 0.094 af
Pond C40P: CB #40	Peak Elev=219.62' Storage=33 cf Inflow=0.41 cfs 0.034 af 15.0" Round Culvert n=0.012 L=31.7' S=0.0126 ' Outflow=0.39 cfs 0.034 af
Pond C41P: CB #41	Peak Elev=218.85' Storage=39 cf Inflow=1.99 cfs 0.168 af 15.0" Round Culvert n=0.012 L=17.5' S=0.0143 ' Outflow=1.98 cfs 0.168 af
Pond C42P: CB #42	Peak Elev=218.85' Storage=33 cf Inflow=0.57 cfs 0.044 af 15.0" Round Culvert n=0.012 L=26.0' S=0.0154 ' Outflow=0.55 cfs 0.043 af
Pond C43P: CB #43	Peak Elev=224.53' Storage=8 cf Inflow=1.78 cfs 0.141 af 15.0" Round Culvert n=0.012 L=48.0' S=0.0371 ' Outflow=1.79 cfs 0.141 af
Pond C44P: CB #44	Peak Elev=229.62' Storage=12 cf Inflow=3.54 cfs 0.323 af 15.0" Round Culvert n=0.012 L=87.0' S=0.0187 ' Outflow=3.54 cfs 0.323 af
Pond C45P: CB #45	Peak Elev=231.15' Storage=8 cf Inflow=1.77 cfs 0.149 af 15.0" Round Culvert n=0.012 L=65.0' S=0.0108 ' Outflow=1.77 cfs 0.149 af
Pond C46P: CB #46	Peak Elev=235.99' Storage=9 cf Inflow=2.21 cfs 0.338 af 15.0" Round Culvert n=0.012 L=105.0' S=0.0681 ' Outflow=2.21 cfs 0.338 af
Pond D01P: DMH #1	Peak Elev=214.47' Storage=28 cf Inflow=2.21 cfs 0.169 af 15.0" Round Culvert n=0.012 L=22.5' S=0.0089 ' Outflow=2.20 cfs 0.169 af
Pond D02P: DMH #2	Peak Elev=223.05' Storage=13 cf Inflow=3.84 cfs 0.303 af 15.0" Round Culvert n=0.012 L=95.0' S=0.0447 ' Outflow=3.84 cfs 0.303 af
Pond D03P: DMH #3	Peak Elev=230.36' Storage=8 cf Inflow=1.77 cfs 0.149 af 15.0" Round Culvert n=0.012 L=65.5' S=0.0148 ' Outflow=1.77 cfs 0.149 af

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Pond D04P: DMH #4

Peak Elev=229.13' Storage=14 cf Inflow=2.55 cfs 0.407 af
15.0" Round Culvert n=0.012 L=50.0' S=0.0100 '/ Outflow=2.55 cfs 0.407 af

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1	Runoff Area=257,558 sf 0.40% Impervious Runoff Depth>1.06" Flow Length=1,542' Tc=32.6 min CN=43 Runoff=2.92 cfs 0.523 af
Subcatchment 2S: subcatchment 2	Runoff Area=764,518 sf 0.65% Impervious Runoff Depth>1.81" Flow Length=2,418' Tc=59.1 min CN=52 Runoff=13.44 cfs 2.652 af
Subcatchment 3S: Subcatchment 3	Runoff Area=118,503 sf 0.00% Impervious Runoff Depth>0.69" Flow Length=993' Tc=20.7 min CN=38 Runoff=0.78 cfs 0.156 af
Subcatchment 4S: Subcatchment 4	Runoff Area=9,068 sf 100.00% Impervious Runoff Depth>6.76" Flow Length=207' Tc=6.0 min CN=98 Runoff=1.40 cfs 0.117 af
Subcatchment 5S: Subcatchment 5	Runoff Area=22,497 sf 40.08% Impervious Runoff Depth>2.90" Flow Length=212' Tc=7.0 min CN=63 Runoff=1.65 cfs 0.125 af
Subcatchment 6S: Subcatchment 6	Runoff Area=25,520 sf 84.67% Impervious Runoff Depth>5.70" Tc=6.0 min CN=89 Runoff=3.64 cfs 0.278 af
Subcatchment 8S: Subcatchment 8	Runoff Area=25,776 sf 25.48% Impervious Runoff Depth>1.40" Flow Length=152' Tc=10.4 min UI Adjusted CN=47 Runoff=0.67 cfs 0.069 af
Subcatchment 9S: Subcatchment 9	Runoff Area=45,641 sf 11.38% Impervious Runoff Depth>0.99" Flow Length=259' Tc=13.4 min UI Adjusted CN=42 Runoff=0.62 cfs 0.086 af
Subcatchment 11S: Area Behind the Dove	Runoff Area=84,194 sf 13.93% Impervious Runoff Depth>1.14" Flow Length=636' Tc=29.3 min UI Adjusted CN=44 Runoff=1.12 cfs 0.184 af
Subcatchment 12S: Road Flow	Runoff Area=4,388 sf 100.00% Impervious Runoff Depth>6.76" Tc=6.0 min CN=98 Runoff=0.68 cfs 0.057 af
Subcatchment 13S: Area in front of future	Runoff Area=29,777 sf 30.66% Impervious Runoff Depth>2.31" Flow Length=175' Tc=12.4 min CN=57 Runoff=1.41 cfs 0.131 af
Subcatchment 14S: Flow to Cross Culvert	Runoff Area=7,713 sf 59.39% Impervious Runoff Depth>4.04" Tc=6.0 min CN=74 Runoff=0.82 cfs 0.060 af
Subcatchment 15S: Area behind future	Runoff Area=17,796 sf 67.02% Impervious Runoff Depth>4.58" Tc=6.0 min CN=79 Runoff=2.13 cfs 0.156 af
Subcatchment 16S: Subcatchment #16	Runoff Area=124,823 sf 1.96% Impervious Runoff Depth>1.07" Flow Length=344' Tc=16.5 min UI Adjusted CN=43 Runoff=1.80 cfs 0.255 af
Subcatchment 17S: Subcatchment #17	Runoff Area=152,689 sf 2.08% Impervious Runoff Depth>2.20" Flow Length=591' Tc=30.6 min CN=56 Runoff=4.80 cfs 0.643 af
Subcatchment 18S: Subcatchment #18	Runoff Area=170,513 sf 0.61% Impervious Runoff Depth>2.59" Flow Length=376' Tc=17.1 min CN=60 Runoff=8.25 cfs 0.846 af

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Subcatchment 19S: Subcatchment#19	Runoff Area=690,822 sf 0.00% Impervious Runoff Depth>2.00" Flow Length=1,832' Tc=46.3 min CN=54 Runoff=15.83 cfs 2.648 af
Subcatchment 31S: CB #31	Runoff Area=6,795 sf 55.78% Impervious Runoff Depth>5.14" Tc=6.0 min CN=84 Runoff=0.90 cfs 0.067 af
Subcatchment 32S: CB #32	Runoff Area=5,694 sf 79.08% Impervious Runoff Depth>5.82" Tc=6.0 min CN=90 Runoff=0.82 cfs 0.063 af
Subcatchment 33S: CB #33	Runoff Area=14,734 sf 60.85% Impervious Runoff Depth>5.14" Tc=6.0 min CN=84 Runoff=1.95 cfs 0.145 af
Subcatchment 34S: CB #34	Runoff Area=5,164 sf 100.00% Impervious Runoff Depth>6.76" Tc=6.0 min CN=98 Runoff=0.79 cfs 0.067 af
Subcatchment 35S: CB #35	Runoff Area=6,367 sf 67.93% Impervious Runoff Depth>5.36" Tc=6.0 min CN=86 Runoff=0.87 cfs 0.065 af
Subcatchment 36S: CB #36	Runoff Area=7,548 sf 93.27% Impervious Runoff Depth>6.52" Tc=6.0 min CN=96 Runoff=1.15 cfs 0.094 af
Subcatchment 37S: CB #37	Runoff Area=9,102 sf 80.61% Impervious Runoff Depth>5.93" Tc=6.0 min CN=91 Runoff=1.33 cfs 0.103 af
Subcatchment 38S: CB #38	Runoff Area=8,387 sf 77.58% Impervious Runoff Depth>5.82" Tc=6.0 min CN=90 Runoff=1.21 cfs 0.093 af
Subcatchment 39S: CB #39	Runoff Area=9,406 sf 38.75% Impervious Runoff Depth>4.36" Tc=6.0 min CN=77 Runoff=1.08 cfs 0.078 af
Subcatchment 40S: CB #40	Runoff Area=3,206 sf 100.00% Impervious Runoff Depth>6.76" Tc=6.0 min CN=98 Runoff=0.49 cfs 0.041 af
Subcatchment 41S: CB #41	Runoff Area=3,664 sf 87.72% Impervious Runoff Depth>6.28" Tc=6.0 min CN=94 Runoff=0.55 cfs 0.044 af
Subcatchment 42S: CB #42	Runoff Area=4,646 sf 81.42% Impervious Runoff Depth>6.05" Tc=6.0 min CN=92 Runoff=0.69 cfs 0.054 af
Subcatchment 43S: CB #43	Runoff Area=14,297 sf 87.98% Impervious Runoff Depth>6.28" Tc=6.0 min CN=94 Runoff=2.15 cfs 0.172 af
Subcatchment 44S: CB #44	Runoff Area=30,768 sf 38.03% Impervious Runoff Depth>3.92" Flow Length=493' Tc=14.6 min CN=73 Runoff=2.48 cfs 0.231 af
Subcatchment 45S: CB #45	Runoff Area=30,969 sf 18.55% Impervious Runoff Depth>3.40" Flow Length=265' Tc=10.4 min UI Adjusted CN=68 Runoff=2.42 cfs 0.202 af
Subcatchment 46S: CB #46	Runoff Area=7,198 sf 100.00% Impervious Runoff Depth>6.76" Tc=6.0 min CN=98 Runoff=1.11 cfs 0.093 af
Subcatchment 47S: Inlet Sump High Pt Dr	Runoff Area=95,547 sf 3.02% Impervious Runoff Depth>2.11" Flow Length=862' Tc=26.2 min UI Adjusted CN=55 Runoff=3.05 cfs 0.386 af

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Subcatchment48S: High Pt Dr Cul-De-Sac	Runoff Area=7,531 sf 77.93% Impervious Runoff Depth>5.93" Tc=6.0 min CN=91 Runoff=1.10 cfs 0.086 af
Subcatchment49S: Community Dr	Runoff Area=10,872 sf 69.81% Impervious Runoff Depth>5.59" Tc=6.0 min CN=88 Runoff=1.53 cfs 0.116 af
Subcatchment50S: Subcatchment#50	Runoff Area=20,749 sf 0.00% Impervious Runoff Depth>2.12" Flow Length=209' Tc=15.8 min CN=55 Runoff=0.81 cfs 0.084 af
Subcatchment51S: Outlet Pond	Runoff Area=2,846 sf 0.00% Impervious Runoff Depth>2.70" Tc=6.0 min CN=61 Runoff=0.20 cfs 0.015 af
Subcatchment52S: Southern Wetland	Runoff Area=237,763 sf 0.00% Impervious Runoff Depth>2.11" Flow Length=1,157' Tc=26.8 min CN=55 Runoff=7.51 cfs 0.959 af
Subcatchment53S: Northern Wetland	Runoff Area=23,588 sf 0.00% Impervious Runoff Depth>2.21" Flow Length=497' Tc=20.6 min CN=56 Runoff=0.88 cfs 0.100 af
Subcatchment54S: Subcatchment#54	Runoff Area=118,144 sf 0.71% Impervious Runoff Depth>2.39" Flow Length=1,159' Tc=25.9 min CN=58 Runoff=4.41 cfs 0.541 af
Subcatchment55S: 15" HDPE N-12	Runoff Area=4,389 sf 0.00% Impervious Runoff Depth>2.70" Tc=6.0 min CN=61 Runoff=0.31 cfs 0.023 af
Subcatchment63S: Gravel Wetland #103	Runoff Area=4,821 sf 0.00% Impervious Runoff Depth>2.70" Tc=6.0 min CN=61 Runoff=0.34 cfs 0.025 af
Subcatchment64S: Gravel Wetland #104	Runoff Area=1,940 sf 0.00% Impervious Runoff Depth>2.70" Tc=6.0 min CN=61 Runoff=0.14 cfs 0.010 af
Subcatchment65S: Rain Garden #105	Runoff Area=12,647 sf 3.41% Impervious Runoff Depth>3.30" Tc=6.0 min CN=67 Runoff=1.10 cfs 0.080 af
Subcatchment66S: Rain Garden #106	Runoff Area=34,434 sf 4.69% Impervious Runoff Depth>3.09" Flow Length=211' Tc=15.3 min UI Adjusted CN=65 Runoff=2.12 cfs 0.204 af
Subcatchment67S: Rain Garden #107	Runoff Area=22,575 sf 0.00% Impervious Runoff Depth>2.70" Flow Length=92' Tc=10.9 min CN=61 Runoff=1.35 cfs 0.116 af
Subcatchment68S: Rain Garden #108	Runoff Area=7,430 sf 45.91% Impervious Runoff Depth>4.47" Tc=6.0 min CN=78 Runoff=0.87 cfs 0.064 af
Subcatchment69S: Rain Garden #109	Runoff Area=78,911 sf 0.00% Impervious Runoff Depth>2.69" Flow Length=493' Tc=14.4 min CN=61 Runoff=4.26 cfs 0.407 af
Subcatchment70S: Detention Pond #110	Runoff Area=24,497 sf 0.00% Impervious Runoff Depth>2.50" Flow Length=273' Tc=12.3 min CN=59 Runoff=1.28 cfs 0.117 af
Subcatchment310S: Subcatchment 10	Runoff Area=9,312 sf 47.01% Impervious Runoff Depth>3.62" Tc=6.0 min CN=70 Runoff=0.89 cfs 0.064 af

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Subcatchment 330S: Subcatchment 30	Runoff Area=5,360 sf	77.01% Impervious	Runoff Depth>5.70"	
	Tc=6.0 min	CN=89	Runoff=0.76 cfs	0.058 af
Reach 2R: Reach 2	Avg. Flow Depth=0.73'	Max Vel=4.15 fps	Inflow=13.44 cfs	2.652 af
	n=0.022	L=220.0'	S=0.0091 '/	Capacity=24.64 cfs
			Outflow=13.44 cfs	2.650 af
Reach 11R: Flow Through 8	Avg. Flow Depth=0.20'	Max Vel=1.29 fps	Inflow=1.12 cfs	0.184 af
	n=0.035	L=76.0'	S=0.0132 '/	Capacity=7.77 cfs
			Outflow=1.12 cfs	0.184 af
Reach 50R: Overland flow	Avg. Flow Depth=0.25'	Max Vel=2.37 fps	Inflow=2.02 cfs	0.424 af
	n=0.025	L=42.0'	S=0.0179 '/	Capacity=186.81 cfs
			Outflow=2.03 cfs	0.424 af
Reach 52R: Wetland Flow	Avg. Flow Depth=0.35'	Max Vel=2.10 fps	Inflow=8.10 cfs	1.564 af
	n=0.045	L=123.0'	S=0.0285 '/	Capacity=17.83 cfs
			Outflow=8.10 cfs	1.562 af
Reach 53R: Wetland Flow	Avg. Flow Depth=0.12'	Max Vel=1.16 fps	Inflow=0.88 cfs	0.100 af
	n=0.045	L=135.0'	S=0.0370 '/	Capacity=20.35 cfs
			Outflow=0.87 cfs	0.099 af
Reach 54R: Combined Wetland Flow	Avg. Flow Depth=0.42'	Max Vel=6.01 fps	Inflow=8.89 cfs	1.662 af
	n=0.045	L=87.0'	S=0.1379 '/	Capacity=610.11 cfs
			Outflow=8.89 cfs	1.661 af
Reach 63R: Overland Flow	Avg. Flow Depth=0.05'	Max Vel=1.08 fps	Inflow=0.26 cfs	0.166 af
	n=0.030	L=126.0'	S=0.0476 '/	Capacity=43.27 cfs
			Outflow=0.26 cfs	0.166 af
Reach 65R: Overland Flow	Avg. Flow Depth=0.22'	Max Vel=1.91 fps	Inflow=3.62 cfs	0.640 af
	n=0.035	L=342.1'	S=0.0270 '/	Capacity=22.35 cfs
			Outflow=3.60 cfs	0.638 af
Reach 66R: Overland Flow	Avg. Flow Depth=0.14'	Max Vel=3.11 fps	Inflow=1.49 cfs	0.318 af
	n=0.025	L=48.0'	S=0.0677 '/	Capacity=24.68 cfs
			Outflow=1.47 cfs	0.318 af
Reach 67R: Overland flow	Avg. Flow Depth=0.26'	Max Vel=2.40 fps	Inflow=2.06 cfs	0.723 af
	n=0.030	L=180.0'	S=0.0250 '/	Capacity=39.17 cfs
			Outflow=2.06 cfs	0.722 af
Reach 69R: Overland Flow	Avg. Flow Depth=0.18'	Max Vel=2.16 fps	Inflow=2.76 cfs	0.980 af
	n=0.035	L=70.0'	S=0.0429 '/	Capacity=111.48 cfs
			Outflow=2.85 cfs	0.979 af
Reach 70R: Overland Flow From Det	Avg. Flow Depth=0.17'	Max Vel=2.82 fps	Inflow=1.30 cfs	0.605 af
	n=0.035	L=61.0'	S=0.0820 '/	Capacity=60.79 cfs
			Outflow=1.30 cfs	0.605 af
Reach 100R: Reach 100			Inflow=3.05 cfs	0.891 af
			Outflow=3.05 cfs	0.891 af
Reach 200R: Reach 200			Inflow=7.73 cfs	2.084 af
			Outflow=7.73 cfs	2.084 af
Reach 300R: Reach 300			Inflow=15.67 cfs	2.507 af
			Outflow=15.67 cfs	2.507 af
Reach 400R: Reach 400			Inflow=15.83 cfs	2.648 af
			Outflow=15.83 cfs	2.648 af
Reach 800R: Svenson Pond			Inflow=16.08 cfs	4.690 af
			Outflow=16.08 cfs	4.690 af

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Pond 1P: Drop Inlet	Peak Elev=204.62' Storage=12 cf Inflow=3.18 cfs 0.689 af Primary=3.24 cfs 0.689 af Secondary=1.60 cfs 0.007 af Outflow=3.24 cfs 0.689 af
Pond 2P: Prop. 18" Cross Culvert	Peak Elev=201.34' Storage=7,383 cf Inflow=14.62 cfs 3.043 af 18.0" Round Culvert n=0.012 L=60.0' S=0.0100 '/' Outflow=13.03 cfs 3.042 af
Pond 4P: Prop. CB#3	Peak Elev=205.06' Storage=0.001 af Inflow=8.60 cfs 1.232 af 15.0" Round Culvert n=0.012 L=93.7' S=0.0053 '/' Outflow=8.55 cfs 1.232 af
Pond 6P: Inlet Depression	Peak Elev=204.39' Storage=915 cf Inflow=3.64 cfs 0.278 af 15.0" Round Culvert n=0.012 L=30.0' S=0.0233 '/' Outflow=5.84 cfs 0.278 af
Pond 8P: 24" Cross Culvert	Peak Elev=199.01' Storage=2,758 cf Inflow=16.35 cfs 4.605 af Primary=15.91 cfs 4.604 af Secondary=0.00 cfs 0.000 af Outflow=15.91 cfs 4.604 af
Pond 10P: EX. CB#10	Peak Elev=203.92' Storage=58 cf Inflow=4.75 cfs 0.818 af 15.0" Round Culvert n=0.012 L=153.9' S=0.0050 '/' Outflow=5.13 cfs 0.818 af
Pond 12P: Ex. CB#2	Peak Elev=202.53' Storage=0.001 af Inflow=9.08 cfs 1.288 af 15.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=8.84 cfs 1.288 af
Pond 13P: Infiltration Pond	Peak Elev=203.48' Storage=1,532 cf Inflow=1.41 cfs 0.131 af Discarded=0.08 cfs 0.063 af Primary=0.66 cfs 0.055 af Outflow=0.74 cfs 0.118 af
Pond 14P: Ex. 15" Cross Culvert	Peak Elev=202.54' Storage=1,327 cf Inflow=0.90 cfs 0.115 af Discarded=0.03 cfs 0.018 af Primary=0.55 cfs 0.099 af Outflow=0.58 cfs 0.115 af
Pond 16P: Ex. 12" CMP	Peak Elev=204.77' Storage=5,198 cf Inflow=5.37 cfs 0.893 af Outflow=3.05 cfs 0.891 af
Pond 17P: Ex. 18" HDPE N-12	Peak Elev=204.33' Storage=2,057 cf Inflow=9.65 cfs 2.085 af Primary=7.73 cfs 2.084 af Secondary=0.00 cfs 0.000 af Outflow=7.73 cfs 2.084 af
Pond 18P: Box Culvert	Peak Elev=191.91' Storage=381 cf Inflow=15.68 cfs 2.507 af 36.0" x 36.0" Box Culvert n=0.012 L=28.0' S=0.0018 '/' Outflow=15.67 cfs 2.507 af
Pond 19P: Box Culvert	Peak Elev=184.52' Storage=51 cf Inflow=15.83 cfs 2.648 af 36.0" x 36.0" Box Culvert n=0.012 L=52.0' S=-0.0085 '/' Outflow=15.83 cfs 2.648 af
Pond 47P: Inlet Sump High Point Drive	Peak Elev=237.65' Storage=114 cf Inflow=3.05 cfs 0.386 af 15.0" Round Culvert n=0.012 L=23.0' S=0.0609 '/' Outflow=3.04 cfs 0.385 af
Pond 48P: High Point Drive Cul-de Sac	Peak Elev=236.48' Storage=204 cf Inflow=1.10 cfs 0.086 af 15.0" Round Culvert n=0.012 L=50.0' S=0.0130 '/' Outflow=1.03 cfs 0.085 af
Pond 49P: Community Drive Cul-de Sac	Peak Elev=219.10' Storage=765 cf Inflow=1.53 cfs 0.116 af 15.0" Round Culvert n=0.012 L=53.5' S=0.0121 '/' Outflow=1.16 cfs 0.111 af
Pond 50P: 15" HDPE (Access Road)	Peak Elev=204.09' Storage=123 cf Inflow=2.05 cfs 0.425 af 15.0" Round Culvert n=0.012 L=42.0' S=0.0060 '/' Outflow=2.02 cfs 0.424 af

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Pond 51P: Outlet Pond	Peak Elev=214.10' Storage=978 cf Inflow=1.78 cfs 0.120 af Outflow=1.65 cfs 0.099 af
Pond 52P: S Wetland Crossing 24" HDPE N-12	Peak Elev=214.65' Storage=192 cf Inflow=7.51 cfs 0.959 af 24.0" Round Culvert w/ 6.0" inside fill n=0.024 L=36.0' S=0.0278 '/' Outflow=7.50 cfs 0.959 af
Pond 53P: N Wetland Crossing 24" HDPE N-12	Peak Elev=215.78' Storage=10 cf Inflow=0.88 cfs 0.100 af 24.0" Round Culvert w/ 6.0" inside fill n=0.024 L=25.0' S=0.0600 '/' Outflow=0.88 cfs 0.100 af
Pond 54P: Inlet Sump Detention Pond #110	Peak Elev=223.19' Storage=94 cf Inflow=4.41 cfs 0.541 af 15.0" Round Culvert n=0.012 L=35.0' S=0.0571 '/' Outflow=4.48 cfs 0.541 af
Pond 55P: Drop Inlet #55	Peak Elev=204.51' Storage=0.000 af Inflow=1.53 cfs 0.341 af 15.0" Round Culvert n=0.012 L=93.2' S=0.0054 '/' Outflow=1.53 cfs 0.341 af
Pond 101P: Ex. Rain Garden #101	Peak Elev=202.53' Storage=3,561 cf Inflow=2.35 cfs 0.255 af Primary=0.58 cfs 0.232 af Secondary=0.20 cfs 0.005 af Outflow=0.78 cfs 0.236 af
Pond 102P: Ex. Rain Garden #102	Peak Elev=200.30' Storage=6,600 cf Inflow=10.34 cfs 1.413 af Primary=0.46 cfs 0.568 af Secondary=7.97 cfs 0.742 af Outflow=8.43 cfs 1.310 af
Pond 103P: Gravel Wetland #103	Peak Elev=214.90' Storage=5,767 cf Inflow=3.05 cfs 0.235 af Primary=0.26 cfs 0.166 af Secondary=0.00 cfs 0.000 af Outflow=0.26 cfs 0.166 af
Pond 104P: Gravel Wetland #104	Peak Elev=216.57' Storage=2,001 cf Inflow=1.84 cfs 0.139 af Primary=1.41 cfs 0.103 af Secondary=0.20 cfs 0.002 af Outflow=1.61 cfs 0.105 af
Pond 105P: Rain Garden #105	Peak Elev=219.99' Storage=15,181 cf Inflow=9.33 cfs 0.726 af Outflow=2.76 cfs 0.540 af
Pond 106P: Rain Garden #106	Peak Elev=219.09' Storage=7,848 cf Inflow=3.96 cfs 0.411 af Outflow=1.49 cfs 0.318 af
Pond 107P: Rain Garden #107	Peak Elev=229.57' Storage=24,359 cf Inflow=9.41 cfs 1.112 af Discarded=0.01 cfs 0.018 af Primary=1.59 cfs 0.698 af Secondary=0.48 cfs 0.026 af Outflow=2.08 cfs 0.741 af
Pond 108P: Rain Garden #108	Peak Elev=206.55' Storage=1,362 cf Inflow=0.87 cfs 0.064 af Primary=0.02 cfs 0.025 af Secondary=0.24 cfs 0.015 af Outflow=0.26 cfs 0.040 af
Pond 109P: Rain Garden #109	Peak Elev=217.90' Storage=6,836 cf Inflow=4.46 cfs 1.129 af Primary=2.76 cfs 0.980 af Secondary=0.00 cfs 0.000 af Outflow=2.76 cfs 0.980 af
Pond 110P: Detention Pond #110	Peak Elev=221.30' Storage=11,992 cf Inflow=5.29 cfs 0.658 af Primary=1.30 cfs 0.605 af Secondary=0.00 cfs 0.000 af Outflow=1.30 cfs 0.605 af
Pond C30P: CB #30	Peak Elev=204.87' Storage=46 cf Inflow=4.71 cfs 0.754 af 15.0" Round Culvert n=0.012 L=25.0' S=0.0052 '/' Outflow=4.53 cfs 0.754 af
Pond C31P: CB #31	Peak Elev=216.63' Storage=31 cf Inflow=1.71 cfs 0.130 af 15.0" Round Culvert n=0.012 L=18.0' S=0.0083 '/' Outflow=1.70 cfs 0.129 af
Pond C32P: CB #32	Peak Elev=216.61' Storage=28 cf Inflow=0.82 cfs 0.063 af 15.0" Round Culvert n=0.012 L=26.0' S=0.0058 '/' Outflow=0.81 cfs 0.063 af

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Pond C33P: CB #33	Peak Elev=214.90' Storage=30 cf Inflow=1.95 cfs 0.145 af 15.0" Round Culvert n=0.012 L=28.7' S=0.0070 '/' Outflow=1.94 cfs 0.144 af
Pond C34P: CB #34	Peak Elev=216.97' Storage=9 cf Inflow=0.79 cfs 0.067 af 15.0" Round Culvert n=0.012 L=63.5' S=0.0669 '/' Outflow=0.80 cfs 0.067 af
Pond C35P: CB #35	Peak Elev=219.99' Storage=40 cf Inflow=0.87 cfs 0.065 af 15.0" Round Culvert n=0.012 L=10.0' S=0.0300 '/' Outflow=0.85 cfs 0.065 af
Pond C36P: CB #36	Peak Elev=225.27' Storage=7 cf Inflow=1.15 cfs 0.094 af 15.0" Round Culvert n=0.012 L=162.0' S=0.0050 '/' Outflow=1.15 cfs 0.094 af
Pond C37P: CB #37	Peak Elev=224.43' Storage=10 cf Inflow=2.48 cfs 0.197 af 15.0" Round Culvert n=0.012 L=84.0' S=0.0183 '/' Outflow=2.48 cfs 0.197 af
Pond C38P: CB #38	Peak Elev=220.00' Storage=10 cf Inflow=1.21 cfs 0.093 af 15.0" Round Culvert n=0.012 L=13.0' S=0.0138 '/' Outflow=1.21 cfs 0.093 af
Pond C39P: CB #39	Peak Elev=220.00' Storage=44 cf Inflow=1.55 cfs 0.119 af 15.0" Round Culvert n=0.012 L=15.0' S=0.0167 '/' Outflow=1.53 cfs 0.119 af
Pond C40P: CB #40	Peak Elev=220.00' Storage=38 cf Inflow=0.49 cfs 0.041 af 15.0" Round Culvert n=0.012 L=31.7' S=0.0126 '/' Outflow=0.47 cfs 0.041 af
Pond C41P: CB #41	Peak Elev=219.10' Storage=42 cf Inflow=2.36 cfs 0.208 af 15.0" Round Culvert n=0.012 L=17.5' S=0.0143 '/' Outflow=2.35 cfs 0.207 af
Pond C42P: CB #42	Peak Elev=219.10' Storage=36 cf Inflow=0.69 cfs 0.054 af 15.0" Round Culvert n=0.012 L=26.0' S=0.0154 '/' Outflow=0.67 cfs 0.053 af
Pond C43P: CB #43	Peak Elev=224.61' Storage=9 cf Inflow=2.15 cfs 0.172 af 15.0" Round Culvert n=0.012 L=48.0' S=0.0371 '/' Outflow=2.15 cfs 0.172 af
Pond C44P: CB #44	Peak Elev=229.91' Storage=16 cf Inflow=4.80 cfs 0.433 af 15.0" Round Culvert n=0.012 L=87.0' S=0.0187 '/' Outflow=4.80 cfs 0.433 af
Pond C45P: CB #45	Peak Elev=231.29' Storage=10 cf Inflow=2.42 cfs 0.202 af 15.0" Round Culvert n=0.012 L=65.0' S=0.0108 '/' Outflow=2.42 cfs 0.202 af
Pond C46P: CB #46	Peak Elev=236.21' Storage=12 cf Inflow=3.37 cfs 0.478 af 15.0" Round Culvert n=0.012 L=105.0' S=0.0681 '/' Outflow=3.37 cfs 0.478 af
Pond D01P: DMH #1	Peak Elev=214.90' Storage=34 cf Inflow=2.73 cfs 0.211 af 15.0" Round Culvert n=0.012 L=22.5' S=0.0089 '/' Outflow=2.72 cfs 0.211 af
Pond D02P: DMH #2	Peak Elev=223.23' Storage=15 cf Inflow=4.64 cfs 0.369 af 15.0" Round Culvert n=0.012 L=95.0' S=0.0447 '/' Outflow=4.64 cfs 0.369 af
Pond D03P: DMH #3	Peak Elev=230.55' Storage=11 cf Inflow=2.42 cfs 0.202 af 15.0" Round Culvert n=0.012 L=65.5' S=0.0148 '/' Outflow=2.42 cfs 0.202 af

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Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Pond D04P: DMH #4

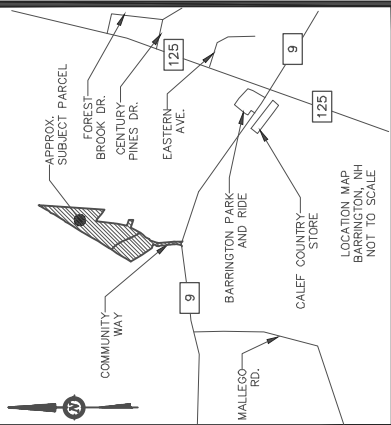
Peak Elev=229.62' Storage=20 cf Inflow=3.78 cfs 0.564 af
15.0" Round Culvert n=0.012 L=50.0' S=0.0100 '/ Outflow=3.77 cfs 0.563 af



BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603) 332-2863
 SCALE: 1 IN. EQUALS 80 FT.
 DATE: JUNE 14, 2021
 FILE NO.: DB 2020 - 097

SITE SPECIFIC SOILS MAP - OVERVIEW 1
 LAND OF DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 BARRINGTON, NH
 COMMUNITY WAY
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

REVISION	DATE	DESCRIPTION



- NOTES:**
- OWNER & APPLICANT: A) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 B) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 - LOT OF RECORD:
 A) TAX MAP 235, LOT 1-1
 B) TAX MAP 235, LOT 3
 - LOT AREA:
 A) 323,215 Sq. Ft., 7.42 Ac.
 B) 743,421 Sq. Ft., 17.07 Ac.
 - S.C.R.D.:
 A) BOOK 4816, PAGE 500
 B) BOOK 4816, PAGE 504
 - ZONING: TOWN CENTER
 FRONTAGE ~ 40.0'
 AREA ~ 20,000 SQUARE FEET
 FRONT SETBACK ~ 20.0'
 NH ROUTE 125/9 SET BACK: ~ 50'
 REAR SETBACK ~ 15.0'
 SIDE SETBACK ~ 15.0'
 COMMERCIAL / RESIDENTIAL BUFFER ~ 50.0'
 WETLANDS/WATERBODY SETBACK ~ 50.0'
 MAX. STRUCTURE HEIGHT: 40.0'
 - I HEREBY CERTIFY THAT, TO THE BEST OF MY KNOWLEDGE & BELIEF, THIS PARCEL DOES NOT FALL WITHIN THE FLOOD PLAIN FLOOD HAZARD ZONE (FLOOD HAZARD ZONE COMMUNITY # -330176, MAP# - 3301760306E, DATED: SEPTEMBER 30, 2015).
 - VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS. HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
 - THE INTENT OF THIS PLAN IS TO SHOW THE SITE SPECIFIC SOILS MAP FOR THE SUBJECT PARCELS.

SITE SPECIFIC SOILS LEGEND

SYMBOL	SOIL TAXONOMIC NAME	HYDROLOGIC SOIL GROUP
■	CHARLTON (VERY STONY)	B
●	CHARLTON (VERY STONY)	B
○	CHARLTON (VERY STONY)	B
□	CHARLTON (VERY STONY)	B
△	HOLLIS (VERY STONY)	C/D
▽	HOLLIS (VERY STONY)	C/D
◇	HOLLIS (VERY STONY)	C/D
◇	HOLLIS CHARLTON COMPLEX (VERY STONY)	C/D
◇	HOLLIS CHARLTON COMPLEX (VERY STONY)	C/D
◇	LEICESTER (VERY STONY)	C
◇	LEICESTER (VERY STONY)	C
◇	LEICESTER (VERY STONY)	C
◇	SUTTON	B
◇	SUTTON	B

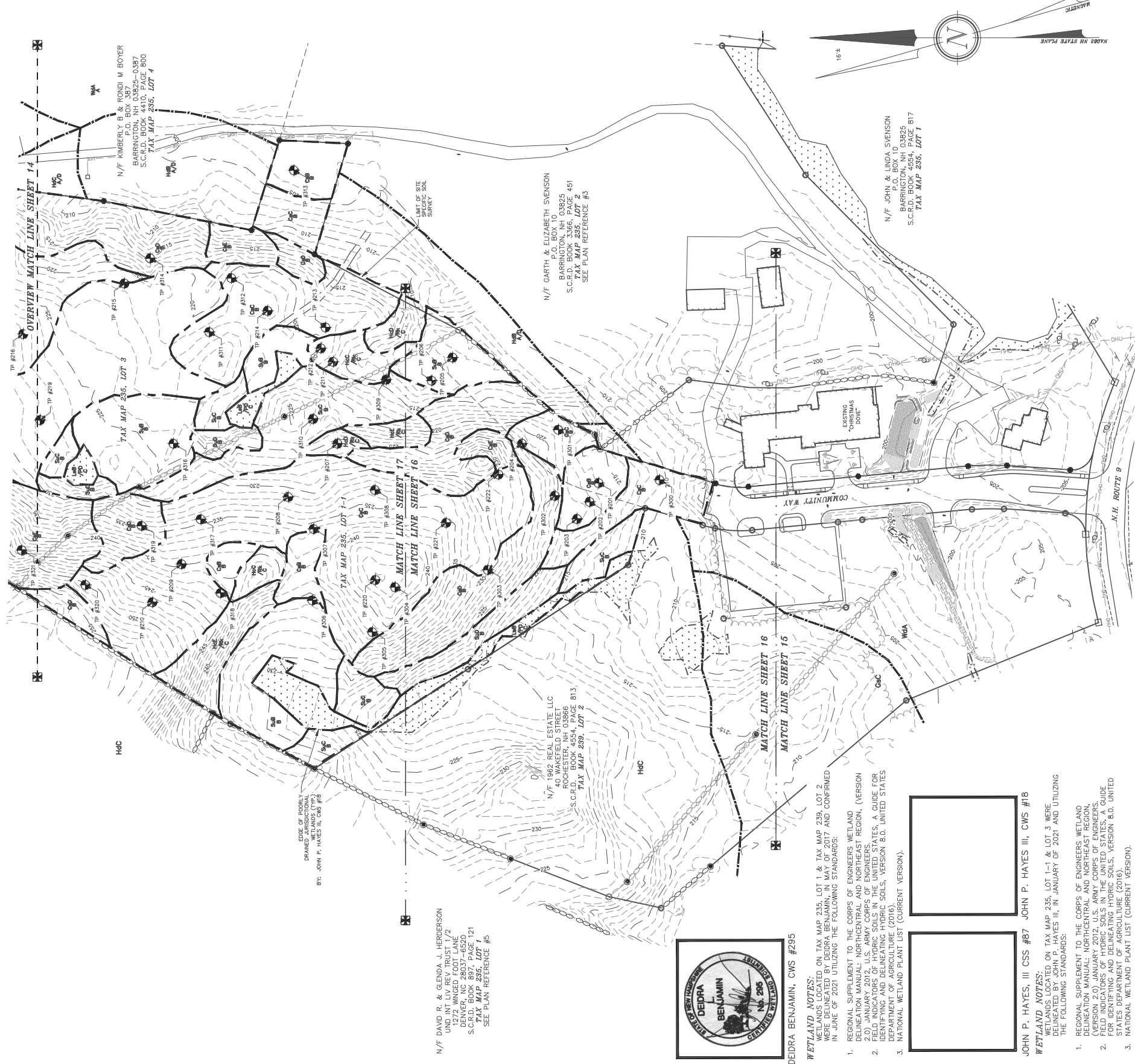
SLOPE: A = 0-3% B = 3-8% C = 8-15% D = 15-25% E = 25-50% F = 50%+

DENOMINATOR: /VPD = VERY POORLY DRAINED /PD = POORLY DRAINED /RW = ROCKY /SWPD = SOMEWHAT POORLY DRAINED /MWD = MODERATELY WELL DRAINED /Rk = ROCKY

- LEGEND:**
- 4"x4" GRANITE BOUND ~TBS~
 - 3/4" REBAR W/ ID CAP ~TBS~
 - GRANITE BOUND ~FND~
 - IRON BOUND/REBAR ~FND/SET~
 - IRON PIPE ~FND~
 - WELL
 - TEST PIT
 - MATCH POINT
 - NSCS SOIL DELINEATION LINE
 - WETLAND LINE
 - 50' WETLAND BUFFER
 - BUILDING SETBACK LINE
 - OVERHEAD UTILITIES LINE
 - DETAILED MATCH LINE
 - SOIL LINE
 - LIMIT OF SOIL SURVEY
 - SCRP SERIES
 - STRIPAS COUNTY REGISTRY OF DEEDS
 - TYP. FOUND
- GRAPHIC SCALE**
 0 40 80 160 320
 (IN FEET)
 1 inch = 80 ft.

FOR TOWN APPROVAL PURPOSES :

THE SUBDIVISION REGULATIONS OF THE TOWN OF BARRINGTON ARE A PART OF THIS PLAN, AND APPROVAL OF THIS PLAN IS CONTINGENT UPON COMPLETION OF ALL REQUIREMENTS OF SAID REGULATIONS. ANY CHANGES, ADDITIONS AND MODIFICATIONS MADE IN WRITING BY THE BOARD AND ATTACHED HERETO.



N/F DAVID R. & GLENDA J. HERDERSON
 1071 WINGED FOOT LANE
 DENVER, NC 28037-6520
 S.C.R.D. BOOK 897, PAGE 121
 TAX MAP 235, LOT 1
 SEE PLAN REFERENCE #5

N/F 1962 REAL ESTATE LLC
 2000 W. 12TH ST.
 ROCHESTER, NH 03866
 S.C.R.D. BOOK 4554, PAGE 813
 TAX MAP 239, LOT 2

N/F JOHN P. HAYES III, CSS #18
 EDGE OF POORLY DRAINED WETLANDS (TYPE 1)
 BY: JOHN P. HAYES III, CSS #18



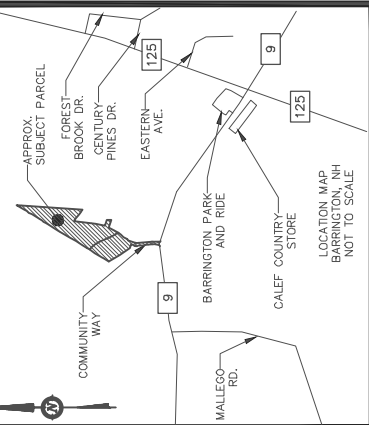
- DEIDRA BENJAMIN, CWS #295
- WETLAND NOTES:**
- WETLANDS LOCATED ON TAX MAP 235, LOT 1 & TAX MAP 239, LOT 2 WERE DELINEATED BY DEIDRA BENJAMIN, IN MAY OF 2017 AND CONFIRMED IN JUNE OF 2021 UTILIZING THE FOLLOWING STANDARDS:
 REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
 FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
 NATIONAL WETLAND PLANT LIST (CURRENT VERSION).
 - JOHN P. HAYES, III CSS #87 JOHN P. HAYES III, CWS #18
 - WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:
 REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
 FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
 NATIONAL WETLAND PLANT LIST (CURRENT VERSION).



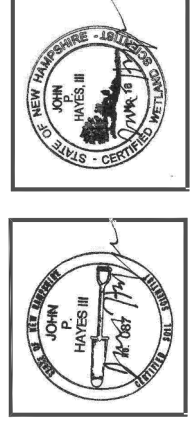
BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603) 332-2863
 SCALE : 1 IN. EQUALS 80 FT.
 DATE : JUNE 14, 2021
 FILE NO. : DB 2020 - 097

SITE SPECIFIC SOILS MAP - OVERVIEW 2
 LAND OF
 DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 COMMUNITY WAY
 BARRINGTON, NH
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

REVISION	DATE	DESCRIPTION



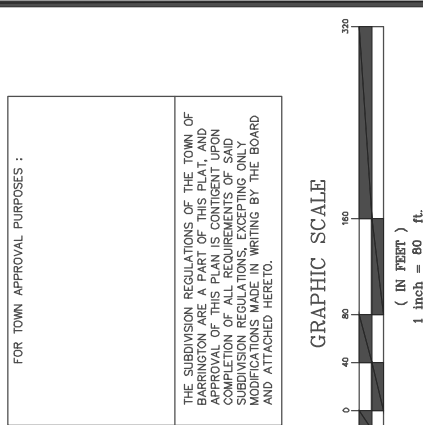
WETLAND NOTES:
 WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:
 1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL, NORTHCENTRAL AND NORTHEAST REGION, (VERSION 4.0) FOR IDENTIFYING AND DELINEATING WETLANDS.
 2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES: A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
 3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).



JOHN P. HAYES, III CSS #87 JOHN P. HAYES III, CWS #18
 N/F MARLA L. LEMOS REV. TRUST
 1164 OCEAN BLVD.
 DOVER, NH 03820
 S.C.R.D. BOOK 4218, PAGE 912
 SEE PLAN REF. #7
 TAX MAP 234, LOT 57



N/F DAVID R. & GLENDA J. HERDERSON
 UND INT LIV REV TRUST 1/2
 1272 WINGED FOOT LANE
 DENVER, NC 28037-6520
 S.C.R.D. BOOK 3857, PAGE 121
 TAX MAP 235, LOT 1
 SEE PLAN REFERENCE #5



FOR TOWN APPROVAL PURPOSES :

THE SUBDIVISION REGULATIONS OF THE TOWN OF BARRINGTON ARE PART OF THIS PLAN AND APPROVAL OF THIS PLAN IS CONTINGENT UPON COMPLETION OF ALL REQUIREMENTS OF SAID SUBDIVISION REGULATIONS, EXCEPTING ONLY THOSE SPECIFICALLY WRITING BY THE BOARD AND ATTACHED HERETO.

- LEGEND:**
- 4"x4" GRANITE BOUND ~TBS~
 - 3/4" REBAR W/ ID CAP ~TBS~
 - 5" IRON BOUND/REBAR ~FND/SET~
 - DRILL HOLE ~FND~
 - IRON PIPE ~FND~
 - WELL
 - TEST PIT
 - MATCH POINT
 - NIRCS SOIL DELINEATION LINE
 - STONE WALL
 - WETLAND LINE
 - 50' WETLAND BUFFER
 - 50' WETLAND BUFFER
 - OVERHEAD UTILITIES LINE
 - OVERVIEW MATCH LINE
 - DETAIL MATCH LINE
 - SOIL LINE SOIL SURVEY
 - SOIL SERIES
 - SOIL SURVEY
 - TYPICAL STRAFFORD COUNTY REGISTRY OF DEEDS
 - S.C.R.D.
 - TP.
 - FND

- NOTES:**
- 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 B.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 - 2.) LOT OF RECORD:
 A.) TAX MAP 235, LOT 1-1
 B.) TAX MAP 235, LOT 3
 - 3.) LOT AREA:
 A.) 323,215 Sq. Ft., 7.42 Ac.
 B.) 743,421 Sq. Ft., 17.07 Ac.
 - 4.) S.C.R.D.:
 A.) BOOK 4816, PAGE 500
 B.) BOOK 4816, PAGE 504
 - 5.) ZONING: TOWN CENTER
 FRONTAGE ~ 40.0'
 MINIMUM LOT SIZE ~ 20,000 SQUARE FEET
 FRONT SETBACK ~ 20.0'
 NH ROUTE 125/9 SET BACK: ~ 50'
 REAR SETBACK ~ 15.0'
 SIDE SETBACK ~ 15.0'
 WETLANDS/WATERBODY BUFFER ~ 50.0'
 WETLANDS/WATERBODY SETBACK ~ 50.0'
 MAX. STRUCTURE HEIGHT: 40.0'
 - 6.) I HEREBY CERTIFY THAT, TO THE BEST OF MY KNOWLEDGE & BELIEF, THIS PLAN IS ACCURATE AND COMPLETELY CORRECT AND THAT I AM A LICENSED PROFESSIONAL ENGINEER IN THE STATE OF NEW HAMPSHIRE.
 HAZARD REF.: FEMA COMMUNITY # 33078, MAP # 33070305E,
 DATED: SEPTEMBER 30, 2015.
 - 7.) VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS.
 ELEVATIONS GATHERED USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
 - 8.) THE INTENT OF THIS PLAN IS TO SHOW THE SITE SPECIFIC SOILS MAP FOR THE SUBJECT PARCELS.

N/F GARTH & ELIZABETH SVENSON
 BARRINGTON, NH 03825
 S.C.R.D. BOOK 3366, PAGE 451
 TAX MAP 235, LOT 2
 SEE PLAN REFERENCE #4

N/F KIMBERLY B. & RONNIE M. BOYER
 E.L.O. BOX 587
 BARRINGTON, NH 03825-0387
 S.C.R.D. BOOK 4410, PAGE 800
 TAX MAP 235, LOT 4

N/F RINDI STORSON
 500 W. RINDI STORSON
 BARRINGTON, NH 03825
 S.C.R.D. BOOK 386, LOT 5
 SEE PLAN REFERENCE #3



DEEDRA BENJAMIN, CWS #295

WETLAND NOTES:
WETLANDS LOCATED ON TAX MAP 235, LOT 1 & TAX MAP 239, LOT 2, AND TAX MAP 235, LOT 3, WERE FIELD SURVEYED AND CONFIRMED IN JUNE OF 2021 UTILIZING THE FOLLOWING STANDARDS:

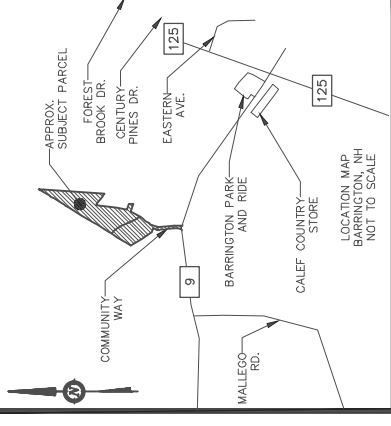
1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL, NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

JOHN P. HAYES, III CSS #87 JOHN P. HAYES III, CWS #18

WETLAND NOTES:
WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:

1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL, NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

FOR TOWN APPROVAL PURPOSES :
THE SUBDIVISION REGULATIONS OF THE TOWN OF BARRINGTON ARE A PART OF THIS PLAN, AND THIS PLAN IS SUBJECT TO ANY CHANGES UPON COMPLETION OF THE REQUIREMENTS FOR SUBDIVISION REGULATIONS, EXCEPTING ONLY MODIFICATIONS MADE IN WRITING BY THE BOARD AND ATTACHED HERETO.



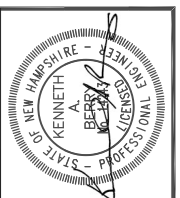
NOTES:

- 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
B.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
- 2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
B.) TAX MAP 235, LOT 3
- 3.) LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
B.) 743,421 Sq. Ft., 17.07 Ac.
- 4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
B.) BOOK 4816, PAGE 504
- 5.) ZONING: TOWN CENTER
FOOTPRINT ~ 40,0'
MINIMUM LOT SIZE ~ 20,000 SQUARE FEET
FRONT SETBACK ~ 20.0'
NH ROUTE 125/9 SETBACK ~ 50'
REAR SETBACK ~ 15.0'
SIDE SETBACK ~ 15.0'
MINIMUM OVERLAP BUFFER ~ 50.0'
WETLANDS/WATERBODY SETBACK ~ 50.0'
MAX. STRUCTURE HEIGHT: 40.0'
- 6.) I HEREBY CERTIFY THAT, TO THE BEST OF MY KNOWLEDGE & BELIEF, THIS PARCEL DOES NOT LIE WITHIN THE FLOOD PLAIN FLOOD HAZARD ZONING DISTRICT COMMUNITY # 330178, WAF# 3501703095E, DATED: SEPTEMBER 30, 2015.
- 7.) VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS. ELEVATIONS GATHERED USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
- 8.) THE INTENT OF THIS PLAN IS TO SHOW THE SITE SPECIFIC SOILS MAP FOR THE SUBJECT PARCELS.
- 9.) NO SSSM WAS PROVIDED FOR THE ORIGINAL 2019 BARRINGTON PLANNING BOARD APPROVAL

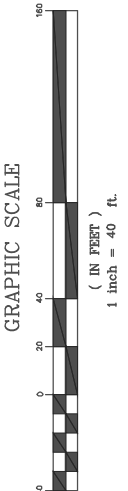
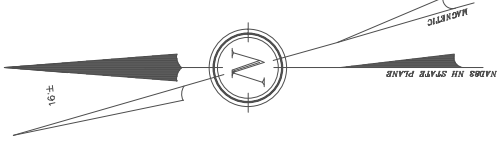
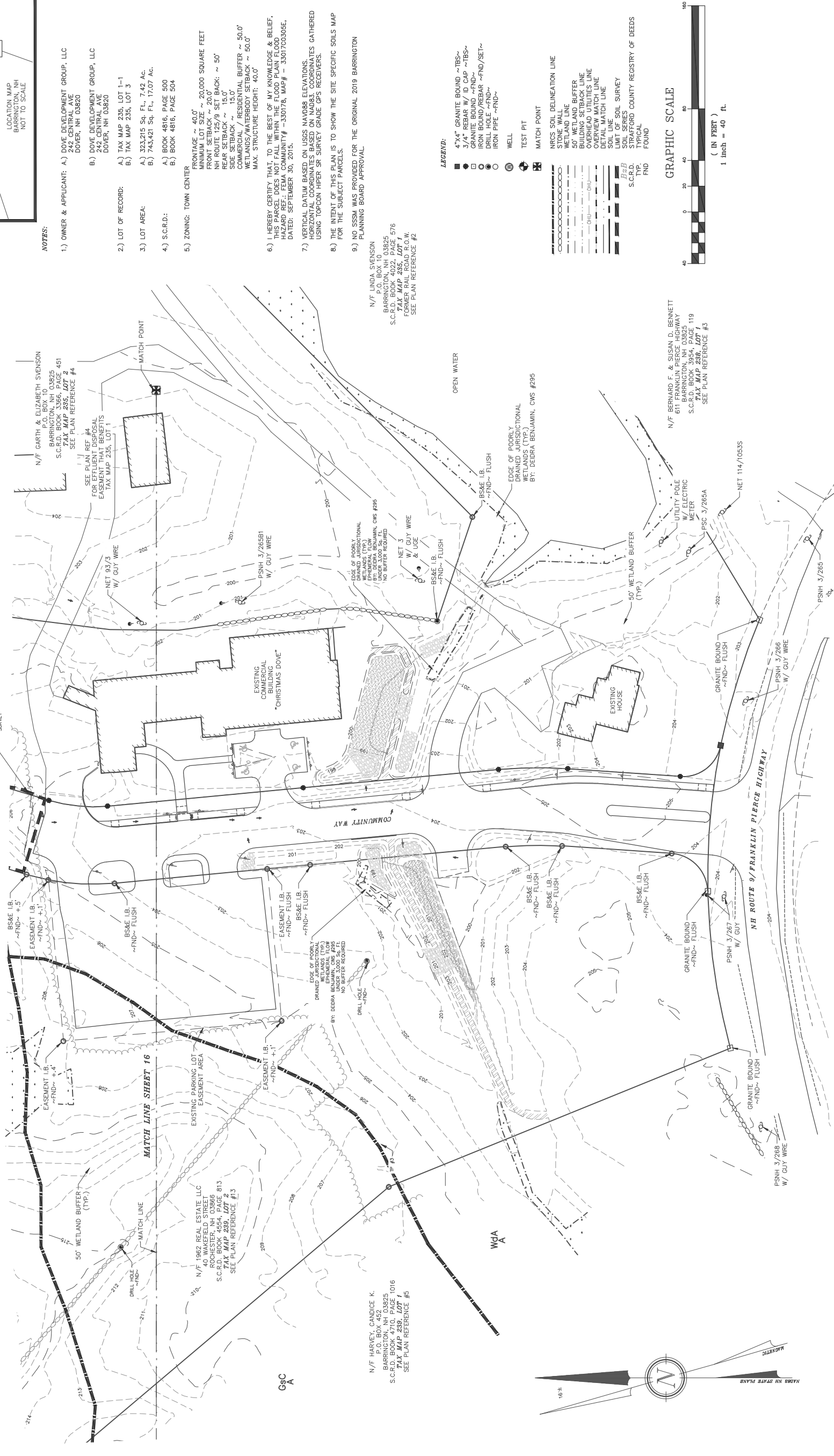
N/F LINDA SVENSON
P.O. BOX 10
BARRINGTON, NH 03825
S.C.R.D. BOOK 4816, PAGE 516
TAX MAP 235, LOT 3
FORMER RAIL ROAD R.O.W.
SEE PLAN REFERENCE #2

N/F HARVEY, CANDICE K.
P.O. BOX 452
BARRINGTON, NH 03825
S.C.R.D. BOOK 4554, PAGE 813
TAX MAP 239, LOT 1
SEE PLAN REFERENCE #5

BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603) 332-2863
SCALE : 1 IN. EQUALS 40 FT.
DATE : JUNE 14, 2021
FILE NO. : DB 2020 - 097



SHEET 15 OF 105




- LEGEND:**
- 4"x4" GRANITE BOUND ~TBS~
 - 3/4" REBAR W/ ID CAP ~TBS~
 - IRON BOUND REBAR ~FND/SET~
 - DRILL HOLE ~FND~
 - IRON PIPE ~FND~
 - WELL
 - TEST PIT
 - MATCH POINT
 - NRCS SOIL DELINEATION LINE
 - STONE WALL
 - WETLAND LINE
 - 50' WETLAND BUFFER
 - OVERHEAD UTILITIES LINE
 - OVERVIEW MATCH LINE
 - DETAIL MATCH LINE
 - SOIL LINE
 - SOIL SURVEY
 - SOIL SERIES
 - S.C.R.D. STRAFFORD COUNTY REGISTRY OF DEEDS
 - TYP. FOUND
 - FND

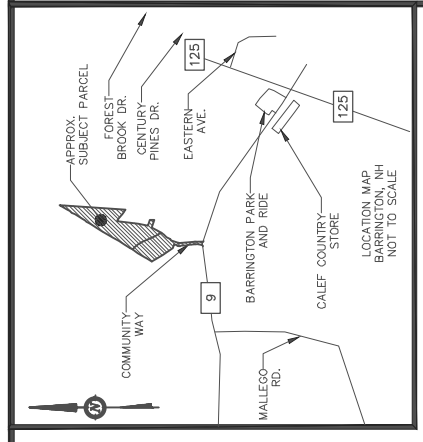
REVISION	DATE	DESCRIPTION

DATE : JUNE 14, 2021
 SCALE : 1 IN. EQUALS 40 FT.
 FILE NO. : DB 2020 - 097

SITE SPECIFIC SOILS MAP - DETAIL 2
 LAND OF
 DOVE DEVELOPMENT GROUP, LLC
 COMMUNITY WAY
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 BARRINGTON, NH
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3



BERRY & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603) 332-2863



- NOTES:
- OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 B.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 - LOT OF RECORD:
 A.) TAX MAP 235, LOT 1-1
 B.) TAX MAP 235, LOT 3
 - LOT AREA:
 A.) 323,215 Sq. Ft., 7.42 Ac.
 B.) 743,421 Sq. Ft., 17.07 Ac.
 - S.C.R.D.:
 A.) BOOK 4816, PAGE 500
 B.) BOOK 4816, PAGE 504
 - ZONING: TOWN CENTER
 FRONTAGE ~ 40.0'
 MINIMAL LOT SIZE ~ 20,000 SQUARE FEET
 FRONT SETBACK ~ 20.0'
 NH ROUTE 125/9 SET BACK ~ 50'
 REAR SETBACK ~ 15.0'
 SIDE SETBACK ~ 15.0'
 COMMERCIAL RESIDENTIAL BUFFER ~ 50.0'
 MAX. STRUCTURE HEIGHT: 40.0'
 - I HEREBY CERTIFY THAT, TO THE BEST OF MY KNOWLEDGE & BELIEF, THIS PARCEL DOES NOT FALL WITHIN THE FLOOD PLAIN FLOOD ZONE. I AM A LICENSED PROFESSIONAL ENGINEER WITH LICENSE # 1255, EXPIRES 09/30/2025, DATED: SEPTEMBER 30, 2015.
 - VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS. ELEVATIONS OBTAINED FROM A TOTAL STATION SURVEY. GRADE GPS RECEIVERS USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
 - THE INTENT OF THIS PLAN IS TO SHOW THE SITE SPECIFIC SOILS MAP FOR THE SUBJECT PARCELS.

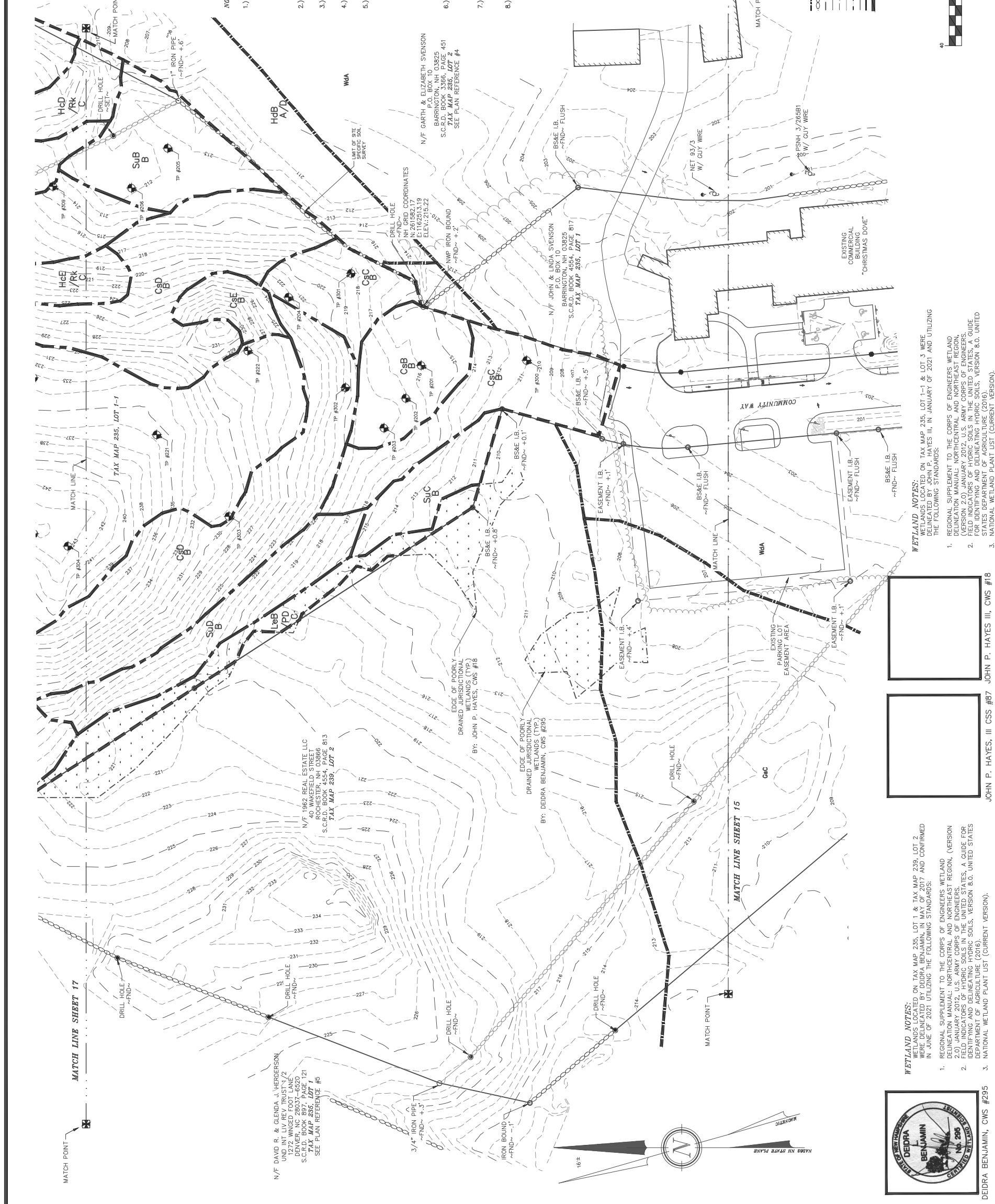
FOR TOWN APPROVAL PURPOSES :

THE SUBDIVISION REGULATIONS OF THE TOWN OF BARRINGTON ARES PART OF THIS PLAN. THE SUBDIVISION REGULATIONS OF ALL REQUIREMENTS OF SAID SUBDIVISION REGULATIONS, EXCEPTING ONLY MODIFICATIONS MADE IN WRITING BY THE BOARD AND ATTACHED HERETO.

LEGEND:


- 4"x4" GRANITE BOUND ~TBS~
- 3/4" REBAR W/ ID CAP ~TBS~
- GRANITE BOUND ~FND~
- IRON PIPE/REBAR ~FND/SET~
- DRILL HOLE ~FND~
- IRON PIPE ~FND~
- WELL
- TEST PIT
- MATCH POINT
- NRCS SOIL DELINEATION LINE
- STONE WALL
- WETLAND LINE
- 50' WETLAND BUFFER
- BUILDING SETBACK LINE
- OVERLAP MATCH LINE
- DETAIL MATCH LINE
- SOIL LINE
- LIMIT OF SOIL SURVEY
- SC.R.D. TYP. STRAFFORD COUNTY REGISTRY OF DEEDS FOUND

GRAPHIC SCALE
 1 inch = 40 ft.
 (IN FEET)



WETLAND NOTES:
 WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:
 1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
 2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 6.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
 3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

WETLAND NOTES:
 WETLANDS LOCATED ON TAX MAP 235, LOT 1 & TAX MAP 239, LOT 2 WERE DELINEATED BY DEIDRA BENJAMIN, IN MAY OF 2017 AND CONFIRMED IN JUNE OF 2021 UTILIZING THE FOLLOWING STANDARDS:
 1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, (VERSION 2.0) JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
 2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 6.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
 3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

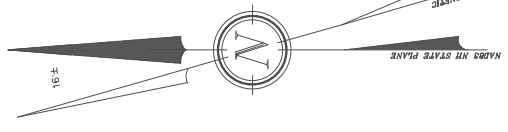
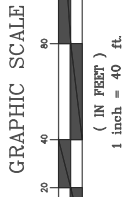


DEIDRA BENJAMIN
 ENGINEER
 LICENSE NO. 295

WETLAND NOTES:
 WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE
 IDENTIFIED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING
 THE FOLLOWING STANDARDS:
 1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND
 Delineation Manual (VERSION 2.0) JANUARY 2012 U.S. ARMY CORPS OF ENGINEERS.
 2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE
 FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED
 STATES DEPARTMENT OF AGRICULTURE (2016).
 3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).
 LEGEND:
 4"x4" GRANITE BOUND ~TBS~
 3/4" REBAR W/ ID CAP ~TBS~
 GRANITE BOUND ~FND~
 IRON BOUND/REBAR ~FND~/SET~
 DRILL HOLE ~FND~
 IRON PIPE ~FND~
 WELL
 TEST PIT
 MATCH POINT
 NRCS SOIL DELINEATION LINE
 WETLAND LINE
 50' WETLAND BUFFER
 BUILDING SETBACK LINE
 OVERHEAD UTILITIES LINE
 OVERVIEW WATCH LINE
 SOIL LINE
 LIMIT OF SOIL SURVEY
 SOIL SERIES
 S.C.R.D. COUNTY REGISTRY OF DEEDS
 TYPICAL FOUND

JOHN P. HAYES III, CWS #18

JOHN P. HAYES, III CSS #87

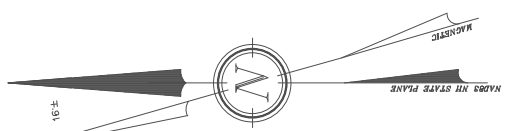
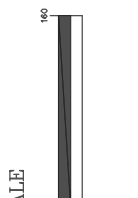


N/F DAVID R. & GLENDA J. HERDERSON
 UND INT LIV REV TRUST 1/2
 1272 WINDY FOOT LANE
 BARRINGTON, NH 03866
 S.C.R.D. BOOK 897, PAGE 121
 TAX MAP 235, LOT 1
 SEE PLAN REFERENCE #5

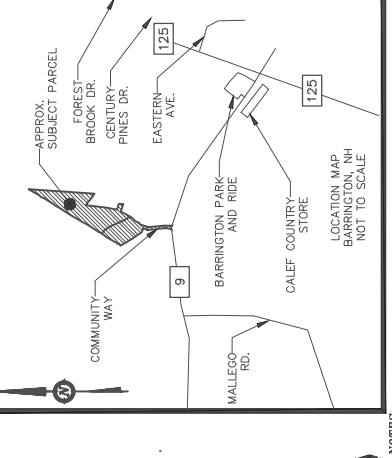
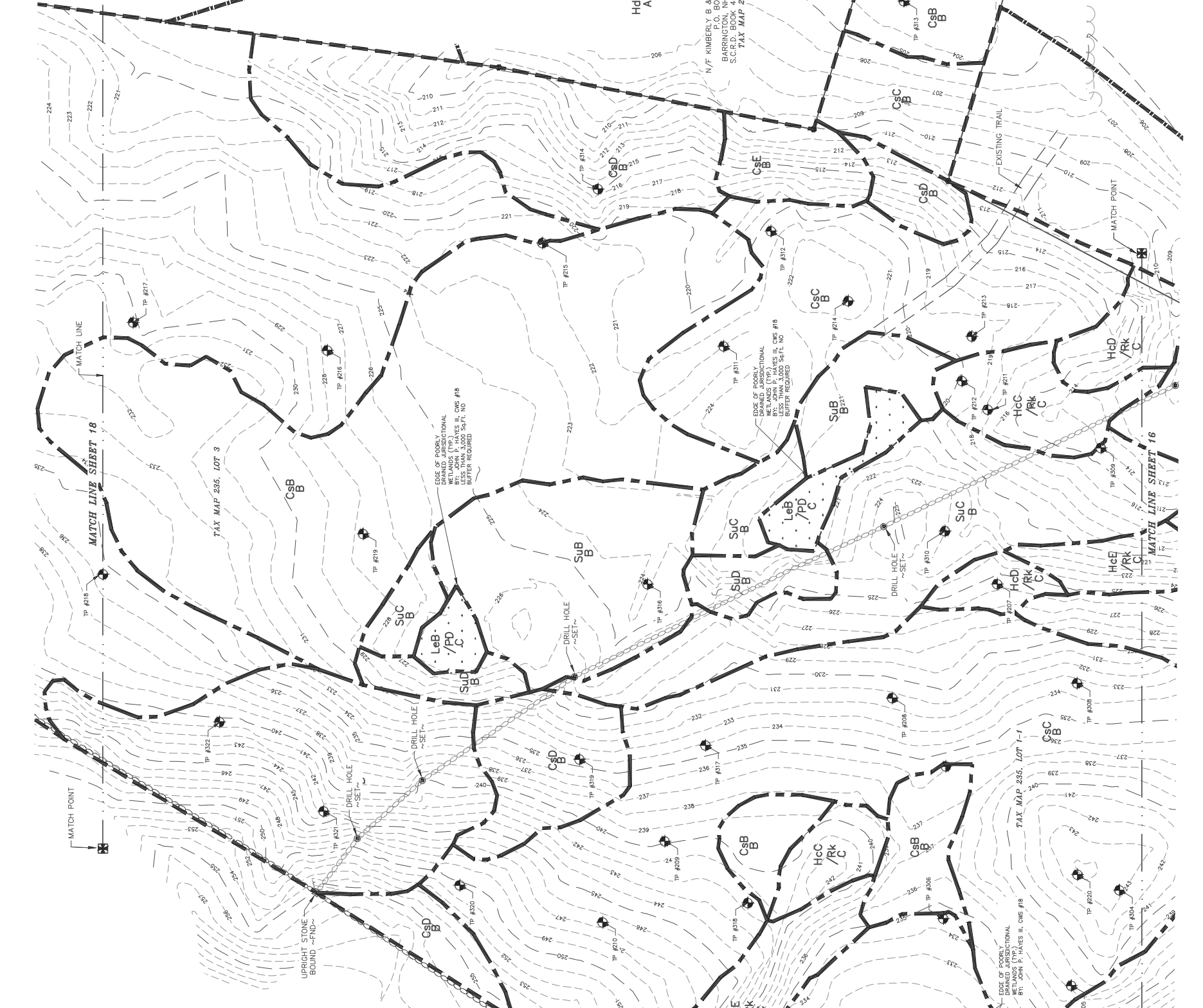
WETLAND NOTES:
 WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE
 IDENTIFIED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING
 THE FOLLOWING STANDARDS:
 1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND
 Delineation Manual (VERSION 2.0) JANUARY 2012 U.S. ARMY CORPS OF ENGINEERS.
 2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE
 FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED
 STATES DEPARTMENT OF AGRICULTURE (2016).
 3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).
 LEGEND:
 4"x4" GRANITE BOUND ~TBS~
 3/4" REBAR W/ ID CAP ~TBS~
 GRANITE BOUND ~FND~
 IRON BOUND/REBAR ~FND~/SET~
 DRILL HOLE ~FND~
 IRON PIPE ~FND~
 WELL
 TEST PIT
 MATCH POINT
 NRCS SOIL DELINEATION LINE
 WETLAND LINE
 50' WETLAND BUFFER
 BUILDING SETBACK LINE
 OVERHEAD UTILITIES LINE
 OVERVIEW WATCH LINE
 SOIL LINE
 LIMIT OF SOIL SURVEY
 SOIL SERIES
 S.C.R.D. COUNTY REGISTRY OF DEEDS
 TYPICAL FOUND

JOHN P. HAYES III, CWS #18

JOHN P. HAYES, III CSS #87



N/F DAVID R. & GLENDA J. HERDERSON
 UND INT LIV REV TRUST 1/2
 1272 WINDY FOOT LANE
 BARRINGTON, NH 03866
 S.C.R.D. BOOK 897, PAGE 121
 TAX MAP 235, LOT 1
 SEE PLAN REFERENCE #5



NOTES:
 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 B.) DOVE DEVELOPMENT GROUP, LLC
 100 CROWN POINT RD
 DOVER, NH 03820
 2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
 B.) TAX MAP 235, LOT 3
 3.) LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
 B.) 743,421 Sq. Ft., 17.07 Ac.
 4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
 B.) BOOK 4816, PAGE 504
 5.) ZONING: TOWN CENTER
 FRONTAGE ~ 40.0'
 MINIMUM LOT SIZE ~ 20,000 SQUARE FEET
 FRONT SETBACK ~ 20.0'
 MINIMUM SIDE/REAR SETBACK ~ 15.0'
 REAR SETBACK/9 SIDE/BACK ~ 50'
 SIDE SETBACK ~ 15.0'
 COMMERCIAL / RESIDENTIAL BUFFER ~ 50.0'
 WETLANDS/WATERBODY SETBACK ~ 50.0'
 MAX. STRUCTURE HEIGHT: 40.0'
 6.) I HEREBY CERTIFY THAT, TO THE BEST OF MY KNOWLEDGE & BELIEF,
 THIS PARCEL DOES NOT FALL WITHIN THE FLOOD PLAIN FLOOD
 HAZARD REF.: FEMA COMMUNITY# -330178, MAP# - 3301700305E,
 DATED: SEPTEMBER 30, 2015.
 7.) VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS.
 HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED
 USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
 8.) THE INTENT OF THIS PLAN IS TO SHOW THE SITE SPECIFIC SOILS MAP
 FOR THE SUBJECT PARCELS.

REVISION	DATE	DESCRIPTION

SITE SPECIFIC SOILS MAP - DETAIL 3
 LAND OF
 DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 BARRINGTON, NH
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603) 332-2863
 SCALE : 1 IN. EQUALS 40 FT.
 DATE : JUNE 14, 2021
 FILE NO. : DB 2020 - 097



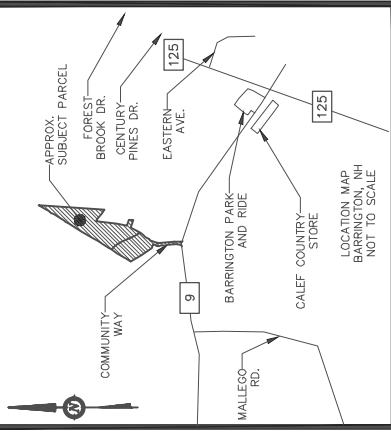
FOR TOWN APPROVAL PURPOSES :
 THE SUBDIVISION REGULATIONS OF THE TOWN OF BARRINGTON ARE A PART OF THIS PLAN AND THE COMPLETION OF ALL REQUIREMENTS OF SAID SUBDIVISION REGULATIONS, EXCEPTING ONLY MODIFICATIONS MADE IN WRITING BY THE BOARD AND ATTACHED HERETO.



BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603) 332-2863
 SCALE : 1 IN. EQUALS 40 FT.
 DATE : JUNE 14, 2021
 FILE NO. : DB 2020 - 097

SITE SPECIFIC SOILS MAP - DETAIL 4
 LAND OF DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 BARRINGTON, NH
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

REVISION	DATE	DESCRIPTION

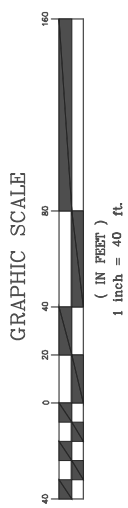


- NOTES:**
- OWNER & APPLICANT: A) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 B) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 - LOT OF RECORD:
 A) TAX MAP 235, LOT 1-1
 B) TAX MAP 235, LOT 3
 - LOT AREA:
 A) 323,215 Sq. Ft., 7.42 Ac.
 B) 743,421 Sq. Ft., 17.07 Ac.
 - S.C.R.D.:
 A) BOOK 4816, PAGE 600
 B) BOOK 4816, PAGE 504
 - ZONING: TOWN CENTER
 FRONTAGE ~ 40.0'
 MINIMUM LOT SIZE ~ 20,000 SQUARE FEET
 REAR SETBACK ~ 50'
 NH ROUTE 125/9 SET BACK: ~ 50'
 REAR SETBACK ~ 15.0'
 SIDE SETBACK ~ 15.0'
 COMMERCIAL / RESIDENTIAL BUFFER ~ 50.0'
 WETLANDS/WATERBODY SETBACK ~ 50.0'
 MAX. STRUCTURE HEIGHT: 40.0'
 - I HEREBY CERTIFY THAT, TO THE BEST OF MY KNOWLEDGE & BELIEF, THIS PARCEL DOES NOT FALL WITHIN THE FLOOD PLAIN FLOOD HAZARD REF.: FEMA COMMUNITY# -330178, MAP# - 33017C0305E, DATED: SEPTEMBER 30, 2015.
 - VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS. HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
 - THE INTENT OF THIS PLAN IS TO SHOW THE SITE SPECIFIC SOILS MAP FOR THE SUBJECT PARCELS.



FOR TOWN APPROVAL PURPOSES :

THE SUBDIVISION REGULATIONS OF THE TOWN OF BARRINGTON ARE A PART OF THIS PLAN, AND APPROVAL OF THIS PLAN IS CONTINGENT UPON COMPLIANCE WITH THE SUBDIVISION AND SUBDIVISION REGULATIONS, EXCEPT ONLY MODIFICATIONS MADE IN WRITING BY THE BOARD AND ATTACHED HERETO.

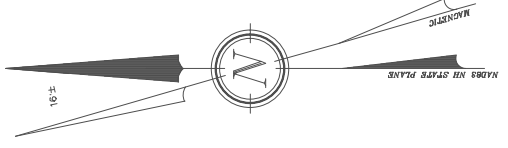


- WETLAND NOTES:**
 WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE DELINEATED BY JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:
- REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND DELINEATION MANUAL: NORTHCENTRAL AND NORTHEAST REGION, 1988, 1990, 1992, 1994, 1996, 1998, 2000, 2002, 2004, 2006, 2008, 2010, 2012, 2014, 2016, 2018, 2020.
 - FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES: A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
 - NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

JOHN P. HAYES, III CSS #87 JOHN P. HAYES III, CWS #18

LEGEND:

- 4"x4" GRANITE BOUND ~TBS~
- 3/4" REBAR W/ ID CAP ~TBS~
- 1/2" IRON PIPE ~REBAR~
- DRILL HOLE ~FND~
- IRON PIPE ~FND~
- WELL
- TEST PIT
- MATCH POINT
- NRCS SOIL DELINEATION LINE
- STONE WALL
- WETLAND LINE
- 50' WETLAND BUFFER
- BUILDING SETBACK LINE
- OVERVIEW MATCH LINE
- DETAIL MATCH LINE
- SOIL LINE SOIL SURVEY
- SOIL SERIES
- STRAFFORD COUNTY REGISTRY OF DEEDS
- TYPICAL
- FND



N/F DAVID R. & GLENDA J. HERDERSON
 UND INT LIV REV TRUST 1/2
 DENVER, CO 80202-6620
 S.C.R.D. BOOK 897, PAGE 121
 TAX MAP 235, LOT 1
 SEE PLAN REFERENCE #5

N/F LINDA SVENSON
 P.O. BOX 10
 BARRINGTON, NH 03825
 S.C.R.D. BOOK 4022, PAGE 576
 TAX MAP 235, LOT 3
 SEE PLAN REFERENCE #3

N/F KIMBERLY B. & RONDI M. BOYER
 BARRINGTON, NH 03825-0387
 S.C.R.D. BOOK 4410, PAGE 800
 TAX MAP 235, LOT 4

N/F LINDA SVENSON
 P.O. BOX 10
 BARRINGTON, NH 03825
 S.C.R.D. BOOK 4022, PAGE 576
 TAX MAP 235, LOT 3
 SEE PLAN REFERENCE #3

- LEGEND:**
- 4"X4" GRANITE BOUND ~TBS~
 - 3/4" REBAR W/ 6" CAP ~TBS~
 - GRANITE BOUND ~FND~
 - IRON BOUND/REBAR ~FND/SET~
 - DRILL HOLE ~FND~
 - IRON PIPE ~FND~
 - WELL
 - TEST PIT
 - MATCH POINT
 - NRCS SOIL DELINEATION LINE
 - STONE WALL
 - WETLAND LINE
 - 50' WETLAND BUFFER
 - BUILDING SETBACK LINE
 - OVERHEAD UTILITIES LINE
 - OVERVIEW MATCH LINE
 - DETAIL MATCH LINE
 - SOIL SURVEY
 - S.O. SERIES
 - STRAFFORD COUNTY REGISTRY OF DEEDS
 - MRP
 - FND

JOHN P. HAYES, III CSS #87 JOHN P. HAYES III, CWS #18

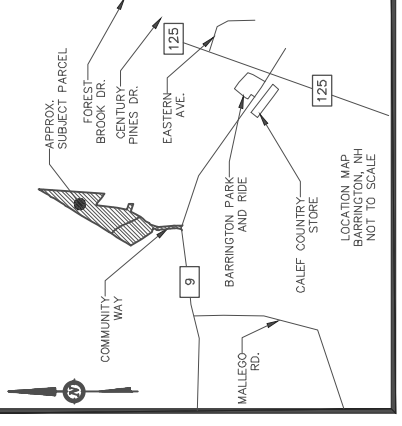
WETLAND NOTES:
 WETLANDS LOCATED ON TAX MAP 235, LOT 1-1 & LOT 3 WERE Delineated by JOHN P. HAYES III, IN JANUARY OF 2021 AND UTILIZING THE FOLLOWING STANDARDS:

1. REGIONAL SUPPLEMENT TO THE CORPS OF ENGINEERS WETLAND Delineation Manual (VERSION 2.0), JANUARY 2012, U.S. ARMY CORPS OF ENGINEERS.
2. FIELD INDICATORS OF HYDRIC SOILS IN THE UNITED STATES, A GUIDE FOR IDENTIFYING AND DELINEATING HYDRIC SOILS, VERSION 8.0, UNITED STATES DEPARTMENT OF AGRICULTURE (2016).
3. NATIONAL WETLAND PLANT LIST (CURRENT VERSION).

N/F MARLA L. LEMOS REV. TRUST
 1164 OCEAN BLVD.
 RYE, NH 03870
 S.C.R.D. BOOK 4218, PAGE 912
 TAX MAP 234, LOT 57

N/F LINDA SVENSON
 1000 WINDY HILL RD.
 BARRINGTON, NH 03825
 S.C.R.D. BOOK 4022, PAGE 576
 TAX MAP 288, LOT 3
 SEE PLAN REFERENCE #5

N/F DAVID R. & GLENDA J. HERDERSON
 UNIT 10, WINDY HILL TRUST #2
 1272 WINGED FOOT LANE
 DENVER, NC 28037-6520
 S.C.R.D. BOOK 897, PAGE 121
 SEE PLAN REFERENCE #5



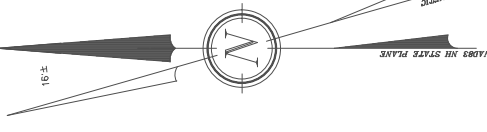
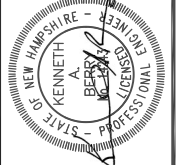
NOTES:

- 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 B.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
- 2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
 B.) TAX MAP 235, LOT 3
- 3.) LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
 B.) 743,421 Sq. Ft., 17.07 Ac.
- 4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
 B.) BOOK 4816, PAGE 504
- 5.) ZONING: TOWN CENTER
 FRONTAGE ~ 40.0'
 MINIMUM LOT SIZE ~ 20,000 SQUARE FEET
 FRONT SETBACK ~ 20.0'
 REAR SETBACK ~ 14.0'
 SIDE SETBACK ~ 15.0'
 COMMERCIAL / RESIDENTIAL BUFFER ~ 50.0'
 WETLANDS/WATERBODY SETBACK ~ 50.0'
 MAX. STRUCTURE HEIGHT: 40.0'
- 6.) I HEREBY CERTIFY THAT, TO THE BEST OF MY KNOWLEDGE & BELIEF, THIS PARCEL DOES NOT FALL WITHIN THE FLOOD PLAIN FLOOD HAZARD REF.: FEMA COMMUNITY# -330176, MAP# - 33017C0305E, DATED: SEPTEMBER 30, 2015.
- 7.) VERTICAL DATUM BASED ON USGS NAVD88 ELEVATIONS. HORIZONTAL COORDINATES BASED ON NAD83. COORDINATES GATHERED USING TOPCON HIPER SR SURVEY GRADE GPS RECEIVERS.
- 8.) THE INTENT OF THIS PLAN IS TO SHOW THE SITE SPECIFIC SOILS MAP FOR THE SUBJECT PARCELS.

REVISION	DATE	DESCRIPTION

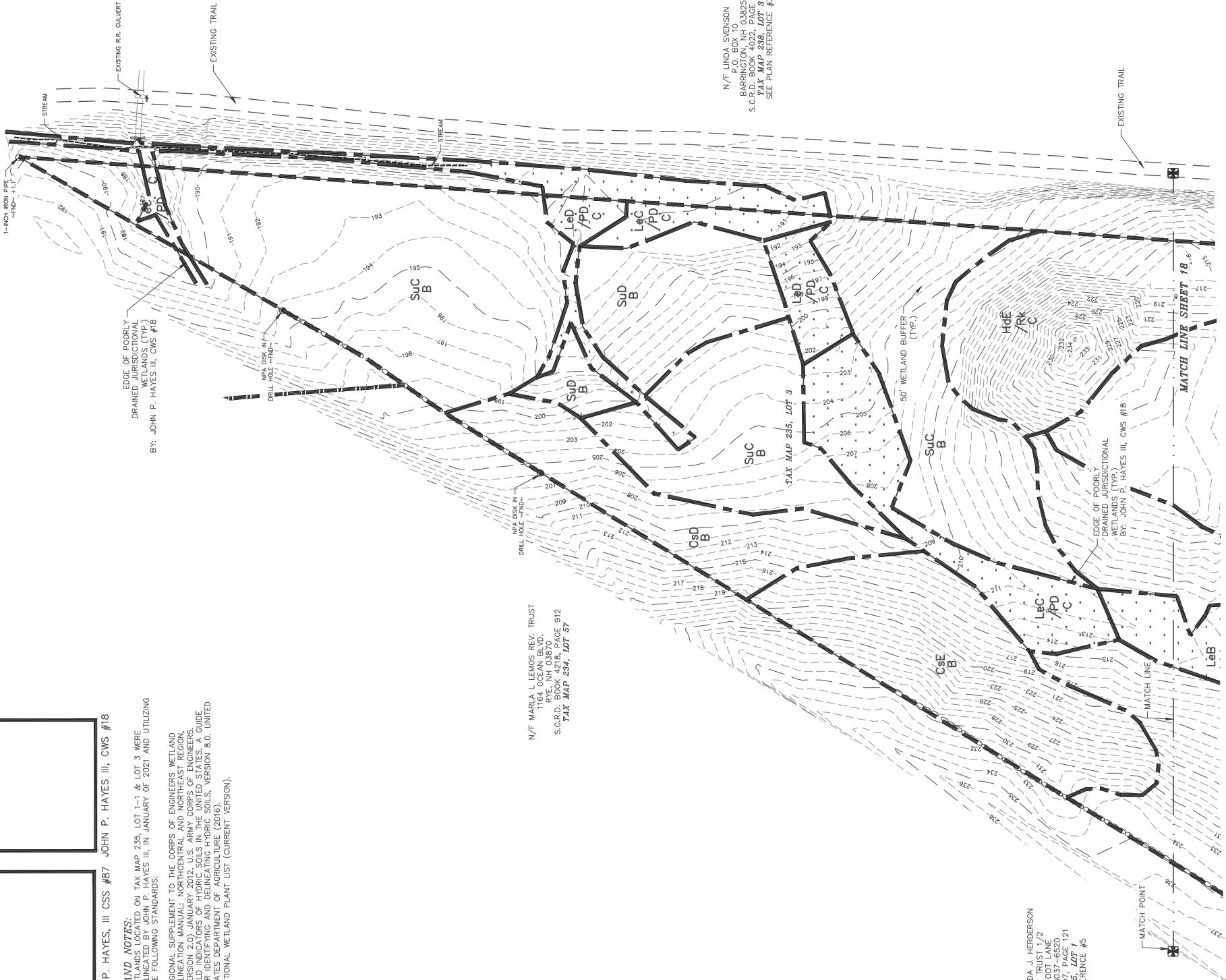
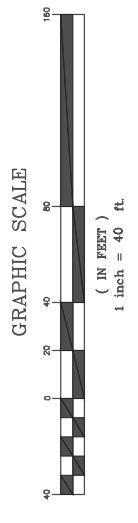
SITE SPECIFIC SOILS MAP - DETAIL 5
 LAND OF
 DOVE DEVELOPMENT GROUP, LLC
 COMMUNITY WAY
 BARRINGTON, NH
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 SCALE: 1 IN. EQUALS 40 FT.
 DATE: JUNE 14, 2021
 FILE NO.: DB 2020 - 097
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603) 332-2863
 SCALE: 1 IN. EQUALS 40 FT.
 DATE: JUNE 14, 2021
 FILE NO.: DB 2020 - 097



FOR TOWN APPROVAL PURPOSES:

THE SUBDIVISION REGULATIONS OF THE TOWN OF BARRINGTON ARE A PART OF THIS PLAN, AND APPROVAL OF THIS PLAN IS CONTINGENT UPON COMPLETION OF ALL REQUIREMENTS OF SAID REGULATIONS. ANY CHANGES, EXCEPTING ONE, MODIFICATIONS, OR ADDITIONS MUST BE WRITTEN BY THE BOARD AND ATTACHED HERETO.



Appendix III - Calculations, Charts, & Graphs

Extreme Precipitation Tables
Rip Rap Calculations
NHDES AoT Spreadsheets
USDA / NRCS Websoil
NRCS Soil Survey Report
Stormwater System Operation & Maintenance Plan
& Inspection and Maintenance Manual
Infiltration Feasibility Report
Watershed Report Card, 303 (d) List, ORW List
Filtrexx

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing	Yes
State	New Hampshire
Location	
Longitude	70.998 degrees West
Latitude	43.215 degrees North
Elevation	0 feet
Date/Time	Mon, 16 Apr 2018 09:46:54 -0400

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.49	0.65	0.81	1.02	1yr	0.70	0.98	1.19	1.53	1.97	2.56	2.81	1yr	2.27	2.71	3.12	3.84	4.41	1yr
2yr	0.32	0.49	0.61	0.80	1.01	1.28	2yr	0.87	1.16	1.49	1.89	2.41	3.08	3.43	2yr	2.73	3.30	3.80	4.52	5.15	2yr
5yr	0.37	0.57	0.72	0.96	1.23	1.57	5yr	1.06	1.44	1.84	2.36	3.03	3.89	4.38	5yr	3.44	4.22	4.84	5.70	6.45	5yr
10yr	0.40	0.63	0.80	1.09	1.42	1.84	10yr	1.22	1.69	2.17	2.80	3.60	4.64	5.28	10yr	4.11	5.08	5.81	6.79	7.64	10yr
25yr	0.46	0.74	0.94	1.30	1.72	2.27	25yr	1.49	2.08	2.69	3.49	4.53	5.86	6.77	25yr	5.19	6.51	7.41	8.57	9.58	25yr
50yr	0.52	0.83	1.06	1.49	2.01	2.67	50yr	1.73	2.45	3.17	4.15	5.40	7.00	8.16	50yr	6.20	7.85	8.91	10.23	11.37	50yr
100yr	0.58	0.94	1.21	1.71	2.33	3.13	100yr	2.01	2.88	3.74	4.92	6.43	8.37	9.85	100yr	7.41	9.47	10.72	12.21	13.50	100yr
200yr	0.65	1.05	1.37	1.96	2.71	3.68	200yr	2.34	3.39	4.42	5.85	7.67	10.01	11.89	200yr	8.85	11.43	12.90	14.58	16.03	200yr
500yr	0.76	1.25	1.63	2.37	3.33	4.55	500yr	2.87	4.21	5.50	7.32	9.66	12.68	15.25	500yr	11.22	14.66	16.48	18.45	20.15	500yr

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.24	0.36	0.44	0.60	0.73	0.90	1yr	0.63	0.88	0.91	1.24	1.52	1.94	2.49	1yr	1.72	2.39	2.93	3.28	3.96	1yr
2yr	0.31	0.48	0.60	0.81	0.99	1.18	2yr	0.86	1.15	1.36	1.82	2.34	2.99	3.34	2yr	2.65	3.21	3.69	4.41	5.03	2yr
5yr	0.35	0.54	0.67	0.92	1.16	1.40	5yr	1.01	1.37	1.61	2.14	2.77	3.61	4.05	5yr	3.19	3.89	4.50	5.35	6.03	5yr
10yr	0.38	0.59	0.73	1.02	1.32	1.60	10yr	1.14	1.56	1.82	2.43	3.12	4.14	4.69	10yr	3.66	4.51	5.23	6.18	6.90	10yr
25yr	0.44	0.67	0.83	1.19	1.57	1.91	25yr	1.35	1.87	2.12	2.84	3.63	4.94	5.68	25yr	4.37	5.46	6.38	7.47	8.25	25yr
50yr	0.49	0.74	0.92	1.33	1.79	2.20	50yr	1.54	2.15	2.37	3.20	4.07	5.65	6.56	50yr	5.00	6.31	7.42	8.63	9.52	50yr
100yr	0.55	0.83	1.03	1.49	2.05	2.52	100yr	1.77	2.47	2.67	3.60	4.54	6.44	7.56	100yr	5.70	7.27	8.65	9.96	10.88	100yr
200yr	0.61	0.92	1.16	1.68	2.35	2.90	200yr	2.03	2.83	2.99	4.05	5.06	7.34	8.83	200yr	6.50	8.49	10.08	11.50	12.46	200yr
500yr	0.72	1.06	1.37	1.99	2.83	3.50	500yr	2.44	3.43	3.50	4.72	5.87	8.68	10.69	500yr	7.68	10.28	12.35	13.93	14.83	500yr

Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.28	0.43	0.53	0.71	0.87	1.07	1yr	0.75	1.05	1.23	1.72	2.18	2.76	3.01	1yr	2.44	2.90	3.34	4.13	4.73	1yr
2yr	0.33	0.50	0.62	0.84	1.03	1.24	2yr	0.89	1.21	1.46	1.94	2.50	3.19	3.54	2yr	2.82	3.40	3.91	4.66	5.31	2yr
5yr	0.39	0.60	0.75	1.02	1.30	1.57	5yr	1.12	1.53	1.83	2.47	3.16	4.18	4.71	5yr	3.70	4.53	5.18	6.06	6.83	5yr
10yr	0.45	0.70	0.86	1.21	1.56	1.90	10yr	1.35	1.86	2.21	3.01	3.80	5.15	5.85	10yr	4.56	5.63	6.41	7.40	8.30	10yr
25yr	0.55	0.84	1.04	1.49	1.96	2.44	25yr	1.69	2.38	2.84	3.91	4.87	6.82	7.82	25yr	6.03	7.52	8.49	9.76	10.74	25yr
50yr	0.64	0.97	1.21	1.74	2.34	2.93	50yr	2.02	2.87	3.44	4.75	5.90	8.43	9.75	50yr	7.46	9.37	10.51	11.97	13.15	50yr
100yr	0.74	1.12	1.41	2.03	2.79	3.53	100yr	2.41	3.46	4.17	5.80	7.16	10.43	12.16	100yr	9.23	11.69	13.01	14.70	16.05	100yr
200yr	0.86	1.30	1.64	2.38	3.32	4.27	200yr	2.86	4.18	5.06	7.08	8.67	12.95	15.07	200yr	11.46	14.49	16.10	18.05	19.62	200yr
500yr	1.05	1.57	2.01	2.93	4.16	5.46	500yr	3.59	5.34	6.52	9.24	11.19	17.28	20.18	500yr	15.30	19.40	21.35	23.72	25.61	500yr



RIP RAP CALCULATIONS
20-097 Dove Development Group

Barrington, NH
Berry Surveying & Engineering
335 Second Crown Point Road
Barrington, NH
14-Jun-21

Rip Rap equations were obtained from the *Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire*. Rip Rap was sized for the 25 year storm event. (Some d50 sizes and T values have been modified)

TAILWATER < HALF THE Do

$La = (1.8 \times Q) / Do^{3/2} + (7 \times Do)$ Q = Peak Flow & Do is Pipe Diameter

W = La + 3*Do or defined channel width

$d50 = (0.02 \times Q^{4/3}) / (Tw \times Do)$ Tw = Tailwater Depth

T = Largest Stone Size x 1.5

Culvert or Catch Basin	Tailwater (Feet) Tw	Discharge (C.F.S.) Q	Diameter of Pipe Do	Length of Rip Rap La (feet)	Width of Rip Rap W (feet)	d50-Stone Rip Rap d50(ft.)	Actual Size	Thickness
---------------------------	---------------------------	----------------------------	---------------------------	-----------------------------------	---------------------------------	----------------------------------	----------------	-----------

15" HDPE (Pond #C30P)	0.25	1.64	1.25	10.9	14.6	0.12	0.50	1.20
15" HDPE (Pond #C31P)	0.25	1.36	1.25	10.5	14.3	0.10	0.50	1.20
15" HDPE (Pond #C35P)	0.25	0.68	1.25	9.6	13.4	0.04	0.50	1.20
15" HDPE (Pond #C38P)	0.25	0.99	1.25	10.0	13.8	0.06	0.50	1.20
15" HDPE (Pond #C39P)	0.25	1.21	1.25	10.3	14.1	0.08	0.50	1.20
15" HDPE (Pond #C41P)	0.25	1.57	1.25	10.8	14.5	0.12	0.50	1.20
15" HDPE (Pond #C44P)	0.25	3.54	1.25	13.3	17.1	0.35	0.50	1.20
15" HDPE (Pond #D01P)	0.25	2.20	1.25	11.6	15.3	0.18	0.50	1.20
15" HDPE (Pond #D02P)	0.25	3.84	1.25	13.7	17.4	0.38	0.50	1.20
15" HDPE (Pond #D04P)	0.25	2.55	1.25	12.0	15.8	0.22	0.50	1.20
15" HDPE (Pond #1P)	0.25	1.56	1.25	10.8	14.5	0.12	0.50	1.20
15" HDPE (Pond #17P)	0.30	3.07	1.50	13.5	18.0	0.20	0.50	1.20
15" HDPE (Pond #47P)	0.25	1.95	1.25	11.3	15.0	0.16	0.50	1.20
15" HDPE (Pond #48P)	0.25	0.84	1.25	9.8	13.6	0.05	0.50	1.20
15" HDPE (Pond #49P)	0.25	0.57	1.25	9.5	13.2	0.03	0.50	1.20
15" HDPE (Pond #50P)	0.25	0.90	1.25	9.9	13.7	0.06	0.50	1.20
15" HDPE (Pond #54P)	0.25	2.93	1.25	12.5	16.3	0.27	0.50	1.20
15" HDPE (Pond #55P)	0.25	0.32	1.25	9.2	12.9	0.01	0.50	1.20
15" HDPE (Pond #103P)	0.25	0.20	1.25	9.0	12.8	0.01	0.50	1.20
15" HDPE (Pond #104P)	0.25	0.79	1.25	9.8	13.5	0.05	0.50	1.20
15" HDPE (Pond #105P)	0.30	1.51	1.50	12.0	16.5	0.08	0.50	1.20
15" HDPE (Pond #106P)	0.25	0.27	1.25	9.1	12.8	0.01	0.50	1.20
15" HDPE (Pond #107P)	0.25	0.58	1.25	9.5	13.2	0.03	0.50	1.20
15" HDPE (Pond #108P)	0.10	0.02	0.50	3.6	5.1	0.00	0.50	1.20
15" HDPE (Pond #109P)	0.25	0.97	1.25	10.0	13.7	0.06	0.50	1.20
15" HDPE (Pond #110P)	0.25	0.39	1.25	9.3	13.0	0.02	0.50	1.20

Please note that the designer chose to use the 25 Year Event for the dimensional calculations.

Table 7-24 -- Recommended Rip Rap Gradation Ranges			
d50 Size =	0.5	Feet	6 Inches
% of Weight Smaller Than the Given d50 Size	Size of Stone (Inches)		
	From	To	
100%	9	12	
85%	8	11	
50%	6	9	
50%	6	9	
15%	2	3	



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name: _____ **Rain Garden #101 (Existing)**

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

Yes		Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.07(a).	
1.27	ac	A = Area draining to the practice	
0.59	ac	A_i = Impervious area draining to the practice	
0.46	decimal	l = Percent impervious area draining to the practice, in decimal form	
0.47	unitless	R_v = Runoff coefficient = $0.05 + (0.9 \times l)$	
0.59	ac-in	WQV = 1" x R_v x A	
2,153	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
538	cf	25% x WQV (check calc for sediment forebay volume)	
1,615	cf	75% x WQV (check calc for surface sand filter volume)	
Sediment Forebay		Method of Pretreatment? (not required for clean or roof runoff)	
629	cf	V_{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
Calculate time to drain if system IS NOT underdrained:			
	sf	A_{SA} = Surface area of the practice	
	iph	$K_{SAT_{DESIGN}}$ = Design infiltration rate ¹	
	Yes/No	If K_{SAT} (prior to factor of safety) is < 0.50 iph, has an underdrain been provided? (Use the calculations below)	
-	hours	T_{DRAIN} = Drain time = $V / (A_{SA} * I_{DESIGN})$	≤ 72-hrs
Calculate time to drain if system IS underdrained:			
202.01	ft	E_{WQV} = Elevation of WQV (attach stage-storage table)	
0.35	cfs	Q_{WQV} = Discharge at the E_{WQV} (attach stage-discharge table)	
3.42	hours	T_{DRAIN} = Drain time = $2WQV/Q_{WQV}$	≤ 72-hrs
199.50	feet	E_{FC} = Elevation of the bottom of the filter course material ²	
198.50	feet	E_{UD} = Invert elevation of the underdrain (UD), if applicable	
199.00	feet	E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test pit)	
190.00	feet	E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test pit)	
1.00	feet	$D_{FC\ to\ UD}$ = Depth to UD from the bottom of the filter course	≥ 1'
9.50	feet	$D_{FC\ to\ ROCK}$ = Depth to bedrock from the bottom of the filter course	≥ 1'
0.50	feet	$D_{FC\ to\ SHWT}$ = Depth to SHWT from the bottom of the filter course	≥ 1'
202.53	ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
203.00	ft	Elevation of the top of the practice	
YES		50 peak elevation ≤ Elevation of the top of the practice	← yes
If a surface sand filter or underground sand filter is proposed:			
YES	ac	Drainage Area check.	< 10 ac
	cf	V = Volume of storage ³ (attach a stage-storage table)	≥ 75%WQV
	inches	D_{FC} = Filter course thickness	18", or 24" if within GPA
Sheet		Note what sheet in the plan set contains the filter course specification.	
Yes/No		Access grate provided?	← yes

If a bioretention area is proposed:			
YES	ac	Drainage Area no larger than 5 ac?	← yes
3,113	cf	V = Volume of storage ³ (attach a stage-storage table)	≥ WQV
18.0	inches	D _{FC} = Filter course thickness	18", or 24" if within GPA
Sheet	R101	Note what sheet in the plan set contains the filter course specification	
2.0	:1	Pond side slopes	> 3:1
Sheet	R101	Note what sheet in the plan set contains the planting plans and surface cover	
If porous pavement is proposed:			
		Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	acres	A _{SA} = Surface area of the pervious pavement	
	:1	Ratio of the contributing area to the pervious surface area	≤ 5:1
	inches	D _{FC} = Filter course thickness	12", or 18" if within GPA
Sheet		Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)

1. Rate of the limiting layer (either the filter course or the underlying soil). K_{sat_{design}} includes factor of safety. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
2. See lines 34, 40 and 48 for required depths of filter media.
3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet structure, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes: Rain Garden #101 was constructed in 2019 as part of the initial Christmas Lane construction on land of 1962 Real Estate, LLC.

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/28/2021

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Summary for Pond 101P: Ex. Rain Garden #101

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=32)

[80] Warning: Exceeded Pond 14P by 0.13' @ 12.25 hrs (0.95 cfs 0.038 af)

Inflow Area = 1.269 ac, 46.37% Impervious, Inflow Depth > 2.41" for 50YR - 24HR event
 Inflow = 2.35 cfs @ 12.10 hrs, Volume= 0.255 af
 Outflow = 0.78 cfs @ 12.77 hrs, Volume= 0.236 af, Atten= 67%, Lag= 40.5 min
 Primary = 0.58 cfs @ 12.77 hrs, Volume= 0.232 af
 Secondary = 0.20 cfs @ 12.77 hrs, Volume= 0.005 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 202.53' @ 12.77 hrs Surf.Area= 2,521 sf Storage= 3,561 cf
 Flood Elev= 203.00' Surf.Area= 3,677 sf Storage= 5,022 cf

Plug-Flow detention time= 108.5 min calculated for 0.236 af (92% of inflow)
 Center-of-Mass det. time= 76.6 min (897.7 - 821.2)

Volume	Invert	Avail.Storage	Storage Description
#1	198.50'	384 cf	Stone Bed (Irregular) Listed below (Recalc) -Impervious 959 cf Overall x 40.0% Voids
#2	199.50'	288 cf	Bio Media (Irregular) Listed below -Impervious 1,439 cf Overall x 20.0% Voids
#3	201.00'	3,722 cf	Open Storage (Irregular) Listed below (Recalc)
#4	200.00'	629 cf	Forebay (Irregular) Listed below (Recalc) -Impervious
		5,022 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
198.50	959	250.0	0	0	959
199.50	959	250.0	959	959	1,209

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
199.50	959	250.0	0	0	959
201.00	959	250.0	1,439	1,439	1,334

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
201.00	959	250.0	0	0	959
202.00	1,494	284.0	1,217	1,217	2,428
203.00	3,677	596.0	2,505	3,722	24,281

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
200.00	55	35.0	0	0	55
201.00	281	320.0	153	153	8,108
202.00	702	445.0	476	629	15,727

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Device	Routing	Invert	Outlet Devices
#1	Secondary	202.50'	20.0' long x 4.0' breadth E-Spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.67 2.65 2.66 2.66 2.68 2.72 2.73 2.76 2.79 2.88 3.07 3.32
#2	Primary	198.50'	6.0" Round 6" U.D. L= 20.0' Ke= 0.500 Inlet / Outlet Invert= 198.50' / 198.30' S= 0.0100 '/' Cc= 0.900 n= 0.012, Flow Area= 0.20 sf
#3	Device 2	201.00'	10.000 in/hr Exfiltration over Surface area

Primary OutFlow Max=0.58 cfs @ 12.77 hrs HW=202.53' TW=200.34' (Dynamic Tailwater)

↳ **2=6" U.D.** (Passes 0.58 cfs of 1.38 cfs potential flow)

↳ **3=Exfiltration** (Exfiltration Controls 0.58 cfs)

Secondary OutFlow Max=0.19 cfs @ 12.77 hrs HW=202.53' TW=200.34' (Dynamic Tailwater)

↳ **1=E-Spillway** (Weir Controls 0.19 cfs @ 0.38 fps)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Area-Storage for Pond 101P: Ex. Rain Garden #101

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
198.50	0	0	201.10	1,007	953
198.55	0	19	201.15	1,032	1,020
198.60	0	38	201.20	1,057	1,089
198.65	0	58	201.25	1,082	1,161
198.70	0	77	201.30	1,107	1,234
198.75	0	96	201.35	1,133	1,310
198.80	0	115	201.40	1,159	1,388
198.85	0	134	201.45	1,185	1,469
198.90	0	153	201.50	1,212	1,551
198.95	0	173	201.55	1,239	1,637
199.00	0	192	201.60	1,266	1,724
199.05	0	211	201.65	1,293	1,814
199.10	0	230	201.70	1,321	1,907
199.15	0	249	201.75	1,349	2,002
199.20	0	269	201.80	1,378	2,100
199.25	0	288	201.85	1,406	2,200
199.30	0	307	201.90	1,435	2,303
199.35	0	326	201.95	1,464	2,409
199.40	0	345	202.00	1,494	2,517
199.45	0	364	202.05	1,580	2,594
199.50	0	384	202.10	1,669	2,675
199.55	0	393	202.15	1,760	2,761
199.60	0	403	202.20	1,853	2,851
199.65	0	412	202.25	1,949	2,946
199.70	0	422	202.30	2,047	3,046
199.75	0	432	202.35	2,148	3,151
199.80	0	441	202.40	2,251	3,261
199.85	0	451	202.45	2,357	3,376
199.90	0	460	202.50	2,465	3,497
199.95	0	470	202.55	2,575	3,623
200.00	0	480	202.60	2,688	3,754
200.05	0	492	202.65	2,803	3,892
200.10	0	505	202.70	2,921	4,035
200.15	0	518	202.75	3,041	4,184
200.20	0	532	202.80	3,163	4,339
200.25	0	546	202.85	3,288	4,500
200.30	0	561	202.90	3,415	4,668
200.35	0	576	202.95	3,545	4,842
200.40	0	591	203.00	3,677	5,022
200.45	0	607			
200.50	0	624			
200.55	0	641			
200.60	0	659			
200.65	0	677			
200.70	0	696			
200.75	0	716			
200.80	0	736			
200.85	0	757			
200.90	0	779			
200.95	0	801			
201.00	959	825			
201.05	983	888			

WQV Draw-down
 Linear Interpolation
 2,153 CF Storage above
 stone = 202.01'

See next Stage-Area-Storage Table
 for storage volume

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Discharge for Pond 101P: Ex. Rain Garden #101

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
198.50	0.00	0.00	0.00	201.10	0.23	0.23	0.00
198.55	0.00	0.00	0.00	201.15	0.24	0.24	0.00
198.60	0.00	0.00	0.00	201.20	0.24	0.24	0.00
198.65	0.00	0.00	0.00	201.25	0.25	0.25	0.00
198.70	0.00	0.00	0.00	201.30	0.26	0.26	0.00
198.75	0.00	0.00	0.00	201.35	0.26	0.26	0.00
198.80	0.00	0.00	0.00	201.40	0.27	0.27	0.00
198.85	0.00	0.00	0.00	201.45	0.27	0.27	0.00
198.90	0.00	0.00	0.00	201.50	0.28	0.28	0.00
198.95	0.00	0.00	0.00	201.55	0.29	0.29	0.00
199.00	0.00	0.00	0.00	201.60	0.29	0.29	0.00
199.05	0.00	0.00	0.00	201.65	0.30	0.30	0.00
199.10	0.00	0.00	0.00	201.70	0.31	0.31	0.00
199.15	0.00	0.00	0.00	201.75	0.31	0.31	0.00
199.20	0.00	0.00	0.00	201.80	0.32	0.32	0.00
199.25	0.00	0.00	0.00	201.85	0.33	0.33	0.00
199.30	0.00	0.00	0.00	201.90	0.33	0.33	0.00
199.35	0.00	0.00	0.00	201.95	0.34	0.34	0.00
199.40	0.00	0.00	0.00	202.00	0.35	0.35	0.00
199.45	0.00	0.00	0.00	202.05	0.37	0.37	0.00
199.50	0.00	0.00	0.00	202.10	0.39	0.39	0.00
199.55	0.00	0.00	0.00	202.15	0.41	0.41	0.00
199.60	0.00	0.00	0.00	202.20	0.43	0.43	0.00
199.65	0.00	0.00	0.00	202.25	0.45	0.45	0.00
199.70	0.00	0.00	0.00	202.30	0.47	0.47	0.00
199.75	0.00	0.00	0.00	202.35	0.50	0.50	0.00
199.80	0.00	0.00	0.00	202.40	0.52	0.52	0.00
199.85	0.00	0.00	0.00	202.45	0.55	0.55	0.00
199.90	0.00	0.00	0.00	202.50	0.57	0.57	0.00
199.95	0.00	0.00	0.00	202.55	1.13	0.60	0.53
200.00	0.00	0.00	0.00	202.60	2.13	0.62	1.51
200.05	0.00	0.00	0.00	202.65	3.41	0.65	2.77
200.10	0.00	0.00	0.00	202.70	4.93	0.68	4.26
200.15	0.00	0.00	0.00	202.75	6.75	0.70	6.05
200.20	0.00	0.00	0.00	202.80	8.82	0.73	8.08
200.25	0.00	0.00	0.00	202.85	11.11	0.76	10.35
200.30	0.00	0.00	0.00	202.90	13.64	0.79	12.85
200.35	0.00	0.00	0.00	202.95	16.38	0.82	15.56
200.40	0.00	0.00	0.00	203.00	19.34	0.85	18.49
200.45	0.00	0.00	0.00				
200.50	0.00	0.00	0.00				
200.55	0.00	0.00	0.00				
200.60	0.00	0.00	0.00				
200.65	0.00	0.00	0.00				
200.70	0.00	0.00	0.00				
200.75	0.00	0.00	0.00				
200.80	0.00	0.00	0.00				
200.85	0.00	0.00	0.00				
200.90	0.00	0.00	0.00				
200.95	0.00	0.00	0.00				
201.00	0.22	0.22	0.00				
201.05	0.23	0.23	0.00				

Elevation 202.01' =
0.35 CFS discharge

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Printed 6/28/2021

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Stage-Area-Storage for Pond 101P: Ex. Rain Garden #101

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
198.50	0	0	201.10	1,007	953
198.55	0	19	201.15	1,032	1,020
198.60	0	38	201.20	1,057	1,089
198.65	0	58	201.25	1,082	1,161
198.70	0	77	201.30	1,107	1,234
198.75	0	96	201.35	1,133	1,310
198.80	0	115	201.40	1,159	1,388
198.85	0	134	201.45	1,185	1,469
198.90	0	153	201.50	1,212	1,551
198.95	0	173	201.55	1,239	1,637
199.00	0	192	201.60	1,266	1,724
199.05	0	211	201.65	1,293	1,814
199.10	0	230	201.70	1,321	1,907
199.15	0	249	201.75	1,349	2,002
199.20	0	269	201.80	1,378	2,100
199.25	0	288	201.85	1,406	2,200
199.30	0	307	201.90	1,435	2,303
199.35	0	326	201.95	1,464	2,409
199.40	0	345	202.00	1,494	2,517
199.45	0	364	202.05	1,580	2,594
199.50	0	384	202.10	1,669	2,675
199.55	0	393	202.15	1,760	2,761
199.60	0	403	202.20	1,853	2,851
199.65	0	412	202.25	1,949	2,946
199.70	0	422	202.30	2,047	3,046
199.75	0	432	202.35	2,148	3,151
199.80	0	441	202.40	2,251	3,261
199.85	0	451	202.45	2,357	3,376
199.90	0	460	202.50	2,465	3,497
199.95	0	470	202.55	2,575	3,623
200.00	0	480	202.60	2,688	3,754
200.05	0	492	202.65	2,803	3,892
200.10	0	505	202.70	2,921	4,035
200.15	0	518	202.75	3,041	4,184
200.20	0	532	202.80	3,163	4,339
200.25	0	546	202.85	3,288	4,500
200.30	0	561	202.90	3,415	4,668
200.35	0	576	202.95	3,545	4,842
200.40	0	591	203.00	3,677	5,022
200.45	0	607			
200.50	0	624			
200.55	0	641			
200.60	0	659			
200.65	0	677			
200.70	0	696			
200.75	0	716			
200.80	0	736			
200.85	0	757			
200.90	0	779			
200.95	0	801			
201.00	959	825			
201.05	983	888			

Linear Interpolation
 Lowest Orifice = 202.50'
 Storage Volume = 3,113 CF

 3,497 CF - 384CF = 3,113 CF



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name: _____

Rain Garden #102 (Existing)

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

Yes	Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.07(a).	
8.23 ac	A = Area draining to the practice	
0.85 ac	A_i = Impervious area draining to the practice	
0.10 decimal	l = Percent impervious area draining to the practice, in decimal form	
0.14 unitless	R_v = Runoff coefficient = $0.05 + (0.9 \times l)$	
1.18 ac-in	WQV = 1" x R_v x A	
4,270 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
1,068 cf	25% x WQV (check calc for sediment forebay volume)	
3,203 cf	75% x WQV (check calc for surface sand filter volume)	
Sediment Forebay	Method of Pretreatment? (not required for clean or roof runoff)	
1,106 cf	V_{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
Calculate time to drain if system IS NOT underdrained:		
sf	A_{SA} = Surface area of the practice	
iph	K_{SAT_DESIGN} = Design infiltration rate ¹	
	If K_{SAT} (prior to factor of safety) is < 0.50 iph, has an underdrain been provided? (Use the calculations below)	
Yes/No		
- hours	T_{DRAIN} = Drain time = $V / (A_{SA} * I_{DESIGN})$	≤ 72-hrs
Calculate time to drain if system IS underdrained:		
199.91 ft	E_{WQV} = Elevation of WQV (attach stage-storage table)	
0.46 cfs	Q_{WQV} = Discharge at the E_{WQV} (attach stage-discharge table)	
5.16 hours	T_{DRAIN} = Drain time = $2WQV/Q_{WQV}$	≤ 72-hrs
197.50 feet	E_{FC} = Elevation of the bottom of the filter course material ²	
196.50 feet	E_{UD} = Invert elevation of the underdrain (UD), if applicable	
198.50 feet	E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test pit)	
190.00 feet	E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test pit)	
1.00 feet	$D_{FC\ to\ UD}$ = Depth to UD from the bottom of the filter course	≥ 1'
7.50 feet	$D_{FC\ to\ ROCK}$ = Depth to bedrock from the bottom of the filter course	≥ 1'
(1.00) feet	$D_{FC\ to\ SHWT}$ = Depth to SHWT from the bottom of the filter course	≥ 1'
200.30 ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
200.50 ft	Elevation of the top of the practice	
YES	50 peak elevation ≤ Elevation of the top of the practice	← yes
If a surface sand filter or underground sand filter is proposed:		
YES ac	Drainage Area check.	< 10 ac
cf	V = Volume of storage ³ (attach a stage-storage table)	≥ 75%WQV
inches	D_{FC} = Filter course thickness	18", or 24" if within GPA
Sheet	Note what sheet in the plan set contains the filter course specification.	
Yes/No	Access grate provided?	← yes

If a bioretention area is proposed:			
NO	ac	Drainage Area no larger than 5 ac?	← yes
4,580	cf	V = Volume of storage ³ (attach a stage-storage table)	≥ WQV
18.0	inches	D _{FC} = Filter course thickness	18", or 24" if within GPA
Sheet	R102	Note what sheet in the plan set contains the filter course specification	
2.0	:1	Pond side slopes	> 3:1
Sheet	R102	Note what sheet in the plan set contains the planting plans and surface cover	
If porous pavement is proposed:			
		Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	acres	A _{SA} = Surface area of the pervious pavement	
	:1	Ratio of the contributing area to the pervious surface area	≤ 5:1
	inches	D _{FC} = Filter course thickness	12", or 18" if within GPA
Sheet		Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)

1. Rate of the limiting layer (either the filter course or the underlying soil). K_{sat_design} includes factor of safety. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
2. See lines 34, 40 and 48 for required depths of filter media.
3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet structure, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes: Rain Garden #101 was constructed in 2019 as part of the initial Christmas Lane construction on land of John & Linda Svenson.

31,150 SF of pavement has been removed from the impervious surface to account for the pre-existing parking lot and paved are of the Christmas Dove & used for WQV Calculations

67,950 SF (1.56 Ac) of impervious - 31,150 SF (0.72 Ac.) pre-existing pavement = 36,800 SF (0.85 Ac)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/28/2021

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Summary for Pond 102P: Ex. Rain Garden #102

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)

Inflow Area = 8.228 ac, 18.90% Impervious, Inflow Depth > 2.06" for 50YR - 24HR event
 Inflow = 10.33 cfs @ 12.15 hrs, Volume= 1.413 af
 Outflow = 8.43 cfs @ 12.17 hrs, Volume= 1.310 af, Atten= 18%, Lag= 1.4 min
 Primary = 0.46 cfs @ 11.85 hrs, Volume= 0.568 af
 Secondary = 7.97 cfs @ 12.17 hrs, Volume= 0.742 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 200.30' @ 12.17 hrs Surf.Area= 1,994 sf Storage= 6,600 cf
 Flood Elev= 200.50' Surf.Area= 1,994 sf Storage= 7,317 cf

Plug-Flow detention time= 69.9 min calculated for 1.310 af (93% of inflow)
 Center-of-Mass det. time= 33.0 min (893.8 - 860.8)

Volume	Invert	Avail.Storage	Storage Description
#1	196.50'	798 cf	Stone Base (Irregular) Listed below (Recalc) -Impervious 1,994 cf Overall x 40.0% Voids
#2	197.50'	598 cf	Bio Media (Irregular) Listed below (Recalc) 2,991 cf Overall x 20.0% Voids
#3	199.00'	4,816 cf	Open Storage (Irregular) Listed below (Recalc) -Impervious
#4	197.00'	1,106 cf	Forebay (Irregular) Listed below (Recalc) -Impervious
		7,317 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
196.50	1,994	198.7	0	0	1,994
197.50	1,994	198.7	1,994	1,994	2,193

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
197.50	1,994	198.7	0	0	1,994
199.00	1,994	198.7	2,991	2,991	2,292

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
199.00	2,793	272.2	0	0	2,793
200.00	3,352	285.2	3,068	3,068	3,433
200.50	3,640	291.5	1,748	4,816	3,757

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
197.00	336	93.0	0	0	336
198.00	547	108.0	437	437	596
199.00	798	127.0	669	1,106	970

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/28/2021

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Device	Routing	Invert	Outlet Devices
#1	Primary	196.50'	6.0" Round 6" U.D. L= 20.0' Ke= 0.500 Inlet / Outlet Invert= 196.50' / 196.40' S= 0.0050 '/' Cc= 0.900 n= 0.012, Flow Area= 0.20 sf
#2	Device 1	197.50'	10.000 in/hr Exfil. To UD over Surface area
#3	Secondary	200.00'	20.0' long x 4.0' breadth E-Spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.67 2.65 2.66 2.66 2.68 2.72 2.73 2.76 2.79 2.88 3.07 3.32

Primary OutFlow Max=0.46 cfs @ 11.85 hrs HW=199.11' TW=196.98' (Dynamic Tailwater)

↑1=6" U.D. (Passes 0.46 cfs of 1.36 cfs potential flow)

↑2=Exfil. To UD (Exfiltration Controls 0.46 cfs)

Secondary OutFlow Max=7.39 cfs @ 12.17 hrs HW=200.28' TW=198.14' (Dynamic Tailwater)

↑3=E-Spillway (Weir Controls 7.39 cfs @ 1.30 fps)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Area-Storage for Pond 102P: Ex. Rain Garden #102

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
196.50	0	0	199.10	1,994	2,784
196.55	0	40	199.15	1,994	2,927
196.60	0	80	199.20	1,994	3,071
196.65	0	120	199.25	1,994	3,217
196.70	0	160	199.30	1,994	3,364
196.75	0	199	199.35	1,994	3,512
196.80	0	239	199.40	1,994	3,662
196.85	0	279	199.45	1,994	3,813
196.90	0	319	199.50	1,994	3,966
196.95	0	359	199.55	1,994	4,120
197.00	0	399	199.60	1,994	4,275
197.05	0	456	199.65	1,994	4,432
197.10	0	513	199.70	1,994	4,590
197.15	0	571	199.75	1,994	4,750
197.20	0	629	199.80	1,994	4,911
197.25	0	688	199.85	1,994	5,074
197.30	0	747	199.90	1,994	5,238
197.35	0	807	199.95	1,994	5,403
197.40	0	868	200.00	1,994	5,570
197.45	0	928	200.05	1,994	5,738
197.50	1,994	990	200.10	1,994	5,908
197.55	1,994	1,032	200.15	1,994	6,079
197.60	1,994	1,074	200.20	1,994	6,252
197.65	1,994	1,117	200.25	1,994	6,426
197.70	1,994	1,161	200.30	1,994	6,601
197.75	1,994	1,205	200.35	1,994	6,778
197.80	1,994	1,250	200.40	1,994	6,956
197.85	1,994	1,295	200.45	1,994	7,136
197.90	1,994	1,341	200.50	1,994	7,317
197.95	1,994	1,387			
198.00	1,994	1,434			
198.05	1,994	1,482			
198.10	1,994	1,530			
198.15	1,994	1,579			
198.20	1,994	1,628			
198.25	1,994	1,678			
198.30	1,994	1,728			
198.35	1,994	1,780			
198.40	1,994	1,831			
198.45	1,994	1,884			
198.50	1,994	1,937			
198.55	1,994	1,990			
198.60	1,994	2,044			
198.65	1,994	2,099			
198.70	1,994	2,155			
198.75	1,994	2,211			
198.80	1,994	2,268			
198.85	1,994	2,325			
198.90	1,994	2,383			
198.95	1,994	2,442			
199.00	1,994	2,502			
199.05	1,994	2,642			

WQV Draw-down
 Linear Interpolation
 4,270 CF Storage above
 stone = 199.91'

See next Stage-Area-Storage Table
 for storage volume

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Discharge for Pond 102P: Ex. Rain Garden #102

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
196.50	0.00	0.00	0.00	199.10	0.46	0.46	0.00
196.55	0.00	0.00	0.00	199.15	0.46	0.46	0.00
196.60	0.00	0.00	0.00	199.20	0.46	0.46	0.00
196.65	0.00	0.00	0.00	199.25	0.46	0.46	0.00
196.70	0.00	0.00	0.00	199.30	0.46	0.46	0.00
196.75	0.00	0.00	0.00	199.35	0.46	0.46	0.00
196.80	0.00	0.00	0.00	199.40	0.46	0.46	0.00
196.85	0.00	0.00	0.00	199.45	0.46	0.46	0.00
196.90	0.00	0.00	0.00	199.50	0.46	0.46	0.00
196.95	0.00	0.00	0.00	199.55	0.46	0.46	0.00
197.00	0.00	0.00	0.00	199.60	0.46	0.46	0.00
197.05	0.00	0.00	0.00	199.65	0.46	0.46	0.00
197.10	0.00	0.00	0.00	199.70	0.46	0.46	0.00
197.15	0.00	0.00	0.00	199.75	0.46	0.46	0.00
197.20	0.00	0.00	0.00	199.80	0.46	0.46	0.00
197.25	0.00	0.00	0.00	199.85	0.46	0.46	0.00
197.30	0.00	0.00	0.00	199.90	0.46	0.46	0.00
197.35	0.00	0.00	0.00	199.95	0.46	0.46	0.00
197.40	0.00	0.00	0.00	200.00	0.46	0.46	0.00
197.45	0.00	0.00	0.00	200.05	0.99	0.46	0.53
197.50	0.46	0.46	0.00	200.10	1.97	0.46	1.51
197.55	0.46	0.46	0.00	200.15	3.23	0.46	2.77
197.60	0.46	0.46	0.00	200.20	4.72	0.46	4.26
197.65	0.46	0.46	0.00	200.25	6.51	0.46	6.05
197.70	0.46	0.46	0.00	200.30	8.55	0.46	8.08
197.75	0.46	0.46	0.00	200.35	10.81	0.46	10.35
197.80	0.46	0.46	0.00	200.40	13.31	0.46	12.85
197.85	0.46	0.46	0.00	200.45	16.02	0.46	15.56
197.90	0.46	0.46	0.00	200.50	18.95	0.46	18.49
197.95	0.46	0.46	0.00				
198.00	0.46	0.46	0.00				
198.05	0.46	0.46	0.00				
198.10	0.46	0.46	0.00				
198.15	0.46	0.46	0.00				
198.20	0.46	0.46	0.00				
198.25	0.46	0.46	0.00				
198.30	0.46	0.46	0.00				
198.35	0.46	0.46	0.00				
198.40	0.46	0.46	0.00				
198.45	0.46	0.46	0.00				
198.50	0.46	0.46	0.00				
198.55	0.46	0.46	0.00				
198.60	0.46	0.46	0.00				
198.65	0.46	0.46	0.00				
198.70	0.46	0.46	0.00				
198.75	0.46	0.46	0.00				
198.80	0.46	0.46	0.00				
198.85	0.46	0.46	0.00				
198.90	0.46	0.46	0.00				
198.95	0.46	0.46	0.00				
199.00	0.46	0.46	0.00				
199.05	0.46	0.46	0.00				

Elevation 199.91' =
0.46 CFS discharge

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/28/2021

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Stage-Area-Storage for Pond 102P: Ex. Rain Garden #102

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
196.50	0	0	199.10	1,994	2,784
196.55	0	40	199.15	1,994	2,927
196.60	0	80	199.20	1,994	3,071
196.65	0	120	199.25	1,994	3,217
196.70	0	160	199.30	1,994	3,364
196.75	0	199	199.35	1,994	3,512
196.80	0	239	199.40	1,994	3,662
196.85	0	279	199.45	1,994	3,813
196.90	0	319	199.50	1,994	3,966
196.95	0	359	199.55	1,994	4,120
197.00	0	399	199.60	1,994	4,275
197.05	0	456	199.65	1,994	4,432
197.10	0	513	199.70	1,994	4,590
197.15	0	571	199.75	1,994	4,750
197.20	0	629	199.80	1,994	4,911
197.25	0	688	199.85	1,994	5,074
197.30	0	747	199.90	1,994	5,238
197.35	0	807	199.95	1,994	5,403
197.40	0	868	200.00	1,994	5,570
197.45	0	928	200.05	1,994	5,738
197.50	1,994	990	200.10	1,994	5,908
197.55	1,994	1,032	200.15	1,994	6,079
197.60	1,994	1,074	200.20	1,994	6,252
197.65	1,994	1,117	200.25	1,994	6,426
197.70	1,994	1,161	200.30	1,994	6,601
197.75	1,994	1,205	200.35	1,994	6,778
197.80	1,994	1,250	200.40	1,994	6,956
197.85	1,994	1,295	200.45	1,994	7,136
197.90	1,994	1,341	200.50	1,994	7,317
197.95	1,994	1,387			
198.00	1,994	1,434			
198.05	1,994	1,482			
198.10	1,994	1,530			
198.15	1,994	1,579			
198.20	1,994	1,628			
198.25	1,994	1,678			
198.30	1,994	1,728			
198.35	1,994	1,780			
198.40	1,994	1,831			
198.45	1,994	1,884			
198.50	1,994	1,937			
198.55	1,994	1,990			
198.60	1,994	2,044			
198.65	1,994	2,099			
198.70	1,994	2,155			
198.75	1,994	2,211			
198.80	1,994	2,268			
198.85	1,994	2,325			
198.90	1,994	2,383			
198.95	1,994	2,442			
199.00	1,994	2,502			
199.05	1,994	2,642			

Linear Interpolation
 Lowest Outlet = 200.00'
 Storage Volume = 4,580 CF

5,570 CF - 990CF = 4,580 CF



INFILTRATION PRACTICE CRITERIA (Env-Wq 1508.06)

Type/Node Name: **Infiltration Pond (13P)**

Enter the type of infiltration practice (e.g., basin, trench) and the node name in the drainage analysis, if applicable.

YES		Have you reviewed Env-Wq 1508.06(a) to ensure that infiltration is allowed?	← yes
0.68	ac	A = Area draining to the practice	
0.21	ac	A _i = Impervious area draining to the practice	
0.31	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.33	unitless	R _v = Runoff coefficient = 0.05 + (0.9 x I)	
0.22	ac-in	WQV = 1" x R _v x A	
809	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
202	cf	25% x WQV (check calc for sediment forebay volume)	
N/A		Method of pretreatment? (not required for clean or roof runoff)	
N/A	cf	V _{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
975	cf	V = Volume ¹ (attach a stage-storage table)	≥ WQV
1,934	sf	A _{SA} = Surface area of the bottom of the pond	
0.71	iph	K _{sat} _{DESIGN} = Design infiltration rate ²	
7.1	hours	I _{DRAIN} = Drain time = V / (A _{SA} * I _{DESIGN})	≤ 72-hrs
203.00	feet	E _{BTM} = Elevation of the bottom of the basin	
198.00	feet	E _{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test pit)	
190.00	feet	E _{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test pit)	
5.00	feet	D _{SHWT} = Separation from SHWT	≥ *³
13.0	feet	D _{ROCK} = Separation from bedrock	≥ *³
	ft	D _{amend} = Depth of amended soil, if applicable due high infiltration rate	≥ 24"
	ft	D _T = Depth of trench, if trench proposed	4 - 10 ft
	Yes/No	If a trench or underground system is proposed, has observation well been provided?	← yes
		If a trench is proposed, does material meet Env-Wq 1508.06(k)(2) requirements. ⁴	← yes
YES	Yes/No	If a basin is proposed, Is the perimeter curvilinear, and basin floor flat?	← yes
3.0	:1	If a basin is proposed, pond side slopes.	≥ 3:1
203.32	ft	Peak elevation of the 10-year storm event (infiltration can be used in analysis)	
203.48	ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
203.75	ft	Elevation of the top of the practice (if a basin, this is the elevation of the berm)	
YES		10 peak elevation ≤ Elevation of the top of the trench? ⁵	← yes
YES		If a basin is proposed, 50-year peak elevation ≤ Elevation of berm?	← yes

1. Volume below the lowest invert of the outlet structure and excludes forebay volume
2. K_{sat}_{DESIGN} includes a factor of safety. See Env-Wq 1504.14 for requirements for determining the infiltr. rate
3. 1' separation if treatment not required; 4' for treatment in GPAs & WSIPAs; & 3' in all other areas.
4. Clean, washed well graded diameter of 1.5 to 3 inches above the in-situ soil.
5. If 50-year peak elevation exceeds top of trench, the overflow must be routed in HydroCAD as secondary discharge.

Designer's Notes:

Infiltration Pond #13P was constructed in 2019 as part of the initial Christmas Lane construction on land of 1962 Real Estate LLC.

20-097 Proposed Analysis

Type III 24-hr 10YR - 24HR Rainfall=4.64"

Prepared by {enter your company name here}

Printed 6/28/2021

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Summary for Pond 13P: Infiltration Pond

Inflow Area = 0.684 ac, 30.66% Impervious, Inflow Depth > 0.92" for 10YR - 24HR event
 Inflow = 0.47 cfs @ 12.21 hrs, Volume= 0.052 af
 Outflow = 0.06 cfs @ 14.67 hrs, Volume= 0.050 af, Atten= 88%, Lag= 147.8 min
 Discarded = 0.06 cfs @ 14.67 hrs, Volume= 0.050 af
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 203.32' @ 14.67 hrs Surf.Area= 3,547 sf Storage= 858 cf
 Flood Elev= 203.50' Surf.Area= 4,691 sf Storage= 1,606 cf

Plug-Flow detention time= 182.6 min calculated for 0.050 af (95% of inflow)
 Center-of-Mass det. time= 158.3 min (1,054.3 - 896.0)

Volume	Invert	Avail.Storage	Storage Description			
#1	203.00'	3,001 cf	Open Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
203.00	1,934	235.0	0	0	1,934	
203.75	6,520	429.0	3,001	3,001	12,188	

Device	Routing	Invert	Outlet Devices												
#1	Discarded	203.00'	0.710 in/hr Exfiltration over Surface area												
#2	Primary	203.35'	5.0' long x 1.0' breadth Broad-Crested Rectangular Weir												
			Head (feet)	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60	1.80	2.00	2.50	3.00
			Coef. (English)	2.69	2.72	2.75	2.85	2.98	3.08	3.20	3.28	3.31	3.30	3.31	3.32

Discarded OutFlow Max=0.06 cfs @ 14.67 hrs HW=203.32' (Free Discharge)
 ↑1=Exfiltration (Exfiltration Controls 0.06 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=203.00' TW=201.50' (Dynamic Tailwater)
 ↑2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/28/2021

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Summary for Pond 13P: Infiltration Pond

Inflow Area = 0.684 ac, 30.66% Impervious, Inflow Depth > 2.31" for 50YR - 24HR event
 Inflow = 1.41 cfs @ 12.19 hrs, Volume= 0.131 af
 Outflow = 0.74 cfs @ 12.48 hrs, Volume= 0.118 af, Atten= 48%, Lag= 17.7 min
 Discarded = 0.08 cfs @ 12.48 hrs, Volume= 0.063 af
 Primary = 0.66 cfs @ 12.48 hrs, Volume= 0.055 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 203.48' @ 12.48 hrs Surf.Area= 4,584 sf Storage= 1,532 cf
 Flood Elev= 203.50' Surf.Area= 4,691 sf Storage= 1,606 cf

Plug-Flow detention time= 116.7 min calculated for 0.118 af (90% of inflow)
 Center-of-Mass det. time= 68.3 min (933.4 - 865.2)

Volume	Invert	Avail.Storage	Storage Description			
#1	203.00'	3,001 cf	Open Storage (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
203.00	1,934	235.0	0	0	1,934	
203.75	6,520	429.0	3,001	3,001	12,188	

Device	Routing	Invert	Outlet Devices												
#1	Discarded	203.00'	0.710 in/hr Exfiltration over Surface area												
#2	Primary	203.35'	5.0' long x 1.0' breadth Broad-Crested Rectangular Weir												
			Head (feet)	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60	1.80	2.00	2.50	3.00
			Coef. (English)	2.69	2.72	2.75	2.85	2.98	3.08	3.20	3.28	3.31	3.30	3.31	3.32

Discarded OutFlow Max=0.08 cfs @ 12.48 hrs HW=203.48' (Free Discharge)
 ↑1=Exfiltration (Exfiltration Controls 0.08 cfs)

Primary OutFlow Max=0.66 cfs @ 12.48 hrs HW=203.48' TW=202.46' (Dynamic Tailwater)
 ↑2=Broad-Crested Rectangular Weir (Weir Controls 0.66 cfs @ 0.98 fps)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/28/2021

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Stage-Area-Storage for Pond 13P: Infiltration Pond

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
203.00	1,934	0	203.52	4,826	1,701
203.01	1,977	20	203.53	4,895	1,750
203.02	2,021	40	203.54	4,963	1,799
203.03	2,066	60	203.55	5,033	1,849
203.04	2,110	81	203.56	5,102	1,900
203.05	2,156	102	203.57	5,173	1,951
203.06	2,201	124	203.58	5,244	2,003
203.07	2,248	146	203.59	5,315	2,056
203.08	2,294	169	203.60	5,386	2,110
203.09	2,342	192	203.61	5,459	2,164
203.10	2,389	216	203.62	5,531	2,219
203.11	2,437	240	203.63	5,605	2,274
203.12	2,486	265	203.64	5,678	2,331
203.13	2,535	290	203.65	5,752	2,388
203.14	2,585	315	203.66	5,827	2,446
203.15	2,635	341	203.67	5,902	2,505
203.16	2,685	368	203.68	5,978	2,564
203.17	2,737	395	203.69	6,054	2,624
203.18	2,788	423	203.70	6,130	2,685
203.19	2,840	451	203.71	6,207	2,747
203.20	2,893	479	203.72	6,285	2,809
203.21	2,946	509	203.73	6,363	2,872
203.22	2,999	538	203.74	6,441	2,936
203.23	3,053	569	203.75	6,520	3,001
203.24	3,107	599			
203.25	3,162	631			
203.26	3,218	663			
203.27	3,273	695			
203.28	3,330	728			
203.29	3,387	762			
203.30	3,444	796			
203.31	3,502	831			
203.32	3,560	866			
203.33	3,619	902			
203.34	3,678	938			
203.35	3,738	975			
203.36	3,798	1,013			
203.37	3,858	1,051			
203.38	3,920	1,090			
203.39	3,981	1,130			
203.40	4,043	1,170			
203.41	4,106	1,211			
203.42	4,169	1,252			
203.43	4,233	1,294			
203.44	4,297	1,337			
203.45	4,361	1,380			
203.46	4,426	1,424			
203.47	4,492	1,468			
203.48	4,558	1,514			
203.49	4,624	1,560			
203.50	4,691	1,606			
203.51	4,758	1,653			

Linear Interpolation
 Lowest Outlet = 203.35'
 Storage Volume = 975 CF



INFILTRATION PRACTICE CRITERIA (Env-Wq 1508.06)

Type/Node Name: Ex. 15" Cross Culvert (14P)

Enter the type of infiltration practice (e.g., basin, trench) and the node name in the drainage analysis, if applicable.

YES		Have you reviewed Env-Wq 1508.06(a) to ensure that infiltration is allowed?	← yes
0.86	ac	A = Area draining to the practice	
0.31	ac	A _i = Impervious area draining to the practice	
0.37	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.38	unitless	R _v = Runoff coefficient = 0.05 + (0.9 x I)	
0.33	ac-in	WQV = 1" x R _v x A	
1,185	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
296	cf	25% x WQV (check calc for sediment forebay volume)	
N/A		Method of pretreatment? (not required for clean or roof runoff)	
N/A	cf	V _{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
-	cf	V = Volume ¹ (attach a stage-storage table)	≥ WQV
560	sf	A _{SA} = Surface area of the bottom of the pond	
0.71	iph	K _{sat} _{DESIGN} = Design infiltration rate ²	
35.8	hours	I _{DRAIN} = Drain time = V / (A _{SA} * I _{DESIGN})	≤ 72-hrs
201.50	feet	E _{BTM} = Elevation of the bottom of the basin	
196.50	feet	E _{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test pit)	
188.50	feet	E _{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test pit)	
5.00	feet	D _{SHWT} = Separation from SHWT	≥ *³
13.0	feet	D _{ROCK} = Separation from bedrock	≥ *³
	ft	D _{amend} = Depth of amended soil, if applicable due high infiltration rate	≥ 24"
	ft	D _T = Depth of trench, if trench proposed	4 - 10 ft
	Yes/No	If a trench or underground system is proposed, has observation well been provided?	← yes
		If a trench is proposed, does material meet Env-Wq 1508.06(k)(2) requirements. ⁴	← yes
YES	Yes/No	If a basin is proposed, Is the perimeter curvilinear, and basin floor flat?	← yes
3.0	:1	If a basin is proposed, pond side slopes.	≥ 3:1
201.76	ft	Peak elevation of the 10-year storm event (infiltration can be used in analysis)	
202.54	ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
203.00	ft	Elevation of the top of the practice (if a basin, this is the elevation of the berm)	
YES		10 peak elevation ≤ Elevation of the top of the trench? ⁵	← yes
YES		If a basin is proposed, 50-year peak elevation ≤ Elevation of berm?	← yes

1. Volume below the lowest invert of the outlet structure and excludes forebay volume
2. K_{sat}_{DESIGN} includes a factor of safety. See Env-Wq 1504.14 for requirements for determining the infiltr. rate
3. 1' separation if treatment not required; 4' for treatment in GPAs & WSIPAs; & 3' in all other areas.
4. Clean, washed well graded diameter of 1.5 to 3 inches above the in-situ soil.
5. If 50-year peak elevation exceeds top of trench, the overflow must be routed in HydroCAD as secondary discharge.

Designer's Notes:

Ex. Cross Culvert #14P was constructed in 2019 as part of the initial Christmas Lane construction on land of 1962 Real Estate LLC.

20-097 Proposed Analysis

Type III 24-hr 10YR - 24HR Rainfall=4.64"

Prepared by {enter your company name here}

Printed 6/28/2021

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Summary for Pond 14P: Ex. 15" Cross Culvert

Inflow Area = 0.861 ac, 36.57% Impervious, Inflow Depth > 0.43" for 10YR - 24HR event
 Inflow = 0.42 cfs @ 12.10 hrs, Volume= 0.031 af
 Outflow = 0.26 cfs @ 12.16 hrs, Volume= 0.031 af, Atten= 38%, Lag= 3.8 min
 Discarded = 0.02 cfs @ 12.26 hrs, Volume= 0.011 af
 Primary = 0.25 cfs @ 12.16 hrs, Volume= 0.020 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 201.76' @ 12.26 hrs Surf.Area= 961 sf Storage= 195 cf
 Flood Elev= 203.00' Surf.Area= 1,948 sf Storage= 2,162 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)
 Center-of-Mass det. time= 18.8 min (859.4 - 840.6)

Volume	Invert	Avail.Storage	Storage Description			
#1	201.50'	2,162 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
201.50	560	120.0	0	0	560	
202.00	1,428	163.0	480	480	1,531	
203.00	1,948	182.0	1,681	2,162	2,080	

Device	Routing	Invert	Outlet Devices	
#1	Primary	201.50'	15.0" Round 15" HDPE N-12 L= 50.0' Ke= 0.500 Inlet / Outlet Invert= 201.50' / 201.00' S= 0.0100 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf	
#2	Discarded	201.50'	0.710 in/hr Exfiltration over Surface area	

Discarded OutFlow Max=0.02 cfs @ 12.26 hrs HW=201.76' (Free Discharge)
 ↑**2=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.24 cfs @ 12.16 hrs HW=201.75' TW=201.39' (Dynamic Tailwater)
 ↑**1=15" HDPE N-12** (Outlet Controls 0.24 cfs @ 2.12 fps)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/28/2021

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Summary for Pond 14P: Ex. 15" Cross Culvert

Inflow Area = 0.861 ac, 36.57% Impervious, Inflow Depth > 1.60" for 50YR - 24HR event
 Inflow = 0.90 cfs @ 12.42 hrs, Volume= 0.115 af
 Outflow = 0.58 cfs @ 12.57 hrs, Volume= 0.115 af, Atten= 36%, Lag= 8.7 min
 Discarded = 0.03 cfs @ 12.74 hrs, Volume= 0.018 af
 Primary = 0.55 cfs @ 12.57 hrs, Volume= 0.099 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 202.54' @ 12.74 hrs Surf.Area= 1,700 sf Storage= 1,327 cf
 Flood Elev= 203.00' Surf.Area= 1,948 sf Storage= 2,162 cf

Plug-Flow detention time= 47.1 min calculated for 0.114 af (100% of inflow)
 Center-of-Mass det. time= 45.9 min (857.8 - 811.8)

Volume	Invert	Avail.Storage	Storage Description			
#1	201.50'	2,162 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
201.50	560	120.0	0	0	560	
202.00	1,428	163.0	480	480	1,531	
203.00	1,948	182.0	1,681	2,162	2,080	

Device	Routing	Invert	Outlet Devices	
#1	Primary	201.50'	15.0" Round 15" HDPE N-12 L= 50.0' Ke= 0.500 Inlet / Outlet Invert= 201.50' / 201.00' S= 0.0100 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf	
#2	Discarded	201.50'	0.710 in/hr Exfiltration over Surface area	

Discarded OutFlow Max=0.03 cfs @ 12.74 hrs HW=202.54' (Free Discharge)
 ↑**2=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=0.67 cfs @ 12.57 hrs HW=202.51' TW=202.48' (Dynamic Tailwater)
 ↑**1=15" HDPE N-12** (Outlet Controls 0.67 cfs @ 0.87 fps)



GRAVEL WETLAND DESIGN CRITERIA (Env-Wq 1508.05)

Type/Node Name: Gravel Wetland #103

Enter the node name in the drainage analysis if applicable.

0.57	ac	A = Area draining to the practice	
0.32	ac	A_i = Impervious area draining to the practice	
0.57	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.56	unitless	R_v = Runoff coefficient = $0.05 + (0.9 \times I)$	
0.32	ac-in	$WQV = 1'' \times R_v \times A$	
1,162	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
116	cf	10% x WQV (check calc for sediment forebay)	
523	cf	45% x WQV (check calc for gravel wetland treatment bay volume)	
311	cf	V_{SED} = Sediment forebay volume	≥ 10%WQV
561	cf	V_{TB1} = Volume of treatment bay 1 ¹	≥ 45%WQV
555	cf	V_{TB2} = Volume of treatment bay 2 ¹	≥ 45%WQV
0.03	cfs	$2Q_{avg} = 2 * WQV / 24 \text{ hrs} * (1\text{hr} / 3600 \text{ sec})$ ⁴	
212.96	ft	E_{WQV} = Elevation of WQV (attach stage-storage table)	
0.01	cfs	Q_{WQV} = Discharge at the E_{WQV} (attach stage-discharge table)	< $2Q_{avg}$
64.54	hours	T_{ED} = Drawdown time of extended detention = $2WQV/Q_{WQV}$	≥ 24-hrs
3.00	:1	Pond side slopes	≥ 3:1
215.42	ft	Elevation of SHWT	
213.42	ft	SHWT - 2 feet	
211.67	ft	E_{pp} = Elevation of the permanent pool (elevation of lowest orifice) ³	≤ $E_{SHWT} - 2 \text{ ft}$
16.5, 16	ft	Length of the flow path between the inlet and outlet in each cell	≥ 15 ft
Angle Grate		What mechanism is proposed to prevent the outlet structure from clogging (applicable for orifices/weirs with a dimension of ≤6")?	
214.90	ft	Peak elevation of the 50-year storm event (E_{50})	
216.00	ft	Berm elevation of the pond	
YES		$E_{50} \leq$ the berm elevation?	← yes
Qualified professional that developed the planting plan Name, Profession: KAB/KRP			

1. Volume stored above the wetland soil and below the high flow by-pass.

2. To ensure orifice is sized so that WQV is released at a relatively stable rate.

3. 4" to 8" below the wetland soil. If lowest orifice is higher than (SHWT - 2 feet), and saturated hydraulic conductivity (K_{sat}) is greater than 0.015 in/hr, the system must be lined.

Designer's Notes: K_{sat} Sutton & K_{sat} Charlton > than 0.015 in/hr. System to be lined w/ low perm material

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/28/2021

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Summary for Pond 103P: Gravel Wetland #103

[80] Warning: Exceeded Pond D01P by 0.01' @ 22.35 hrs (0.68 cfs 0.028 af)

Inflow Area = 0.567 ac, 57.16% Impervious, Inflow Depth > 4.98" for 50YR - 24HR event
 Inflow = 3.05 cfs @ 12.09 hrs, Volume= 0.235 af
 Outflow = 0.26 cfs @ 13.09 hrs, Volume= 0.166 af, Atten= 91%, Lag= 60.1 min
 Primary = 0.26 cfs @ 13.09 hrs, Volume= 0.166 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 214.90' @ 13.09 hrs Surf.Area= 4,631 sf Storage= 5,767 cf
 Flood Elev= 216.00' Surf.Area= 5,371 sf Storage= 9,385 cf

Plug-Flow detention time= 268.3 min calculated for 0.166 af (70% of inflow)
 Center-of-Mass det. time= 173.2 min (962.3 - 789.1)

Volume	Invert	Avail.Storage	Storage Description
#1	211.67'	32 cf	4.00'D x 2.57'H 4' Outlet Structure
#2	212.00'	561 cf	Cell 1 (Irregular) Listed below (Recalc)
#3	212.00'	555 cf	Cell 2 (Irregular) Listed below (Recalc)
#4	213.00'	7,925 cf	Open Water Storage (Irregular) Listed below (Recalc)
#5	212.00'	311 cf	Sediment Forebay (Irregular) Listed below (Recalc)
		9,385 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
212.00	434	78.7	0	0	434
213.00	698	97.5	561	561	712

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
212.00	426	79.3	0	0	426
213.00	695	98.2	555	555	707

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
213.00	1,515	153.7	0	0	1,515
214.00	2,373	196.6	1,928	1,928	2,724
215.00	2,990	215.5	2,676	4,604	3,377
216.00	3,665	234.3	3,322	7,925	4,086

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
212.00	47	26.8	0	0	47
213.00	147	45.3	92	92	159
214.00	300	63.8	219	311	329

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/28/2021

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Device	Routing	Invert	Outlet Devices
#1	Primary	211.67'	15.0" Round 15" N-12 HDPE L= 20.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 211.67' / 211.00' S= 0.0335 '/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	211.67'	0.7" Vert. 0.75" Orifice Goose Neck C= 0.600
#3	Device 1	213.75'	3.0" Vert. 3" Orifice C= 0.600
#4	Device 1	215.45'	48.0" Horiz. 48" Structure C= 0.600 Limited to weir flow at low heads
#5	Secondary	215.50'	5.0' long x 7.0' breadth 5' Emergency Spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65 2.65 2.66 2.65 2.66 2.68 2.70 2.73 2.78

Primary OutFlow Max=0.26 cfs @ 13.09 hrs HW=214.90' TW=211.05' (Dynamic Tailwater)

- ↑ 1=15" N-12 HDPE (Passes 0.26 cfs of 9.54 cfs potential flow)
- ↑ 2=0.75" Orifice Goose Neck (Orifice Controls 0.02 cfs @ 8.61 fps)
- ↑ 3=3" Orifice (Orifice Controls 0.24 cfs @ 4.87 fps)
- ↑ 4=48" Structure (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=211.67' TW=211.00' (Dynamic Tailwater)

- ↑ 5=5' Emergency Spillway (Controls 0.00 cfs)

20-097 Proposed Analysis

Type III 24-hr 2YR - 24HR Rainfall=3.08"

Prepared by {enter your company name here}

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Stage-Area-Storage for Pond 103P: Gravel Wetland #103

Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
211.67	0	214.27	4,050
211.72	1	214.32	4,177
211.77	1	214.37	4,306
211.82	2	214.42	4,436
211.87	3	214.47	4,568
211.92	3	214.52	4,702
211.97	4	214.57	4,837
212.02	23	214.62	4,973
212.07	70	214.67	5,112
212.12	118	214.72	5,251
212.17	168	214.77	5,393
212.22	220	214.82	5,535
212.27	273	214.87	5,680
212.32	327	214.92	5,826
212.37	383	214.97	5,974
212.42	440	215.02	6,123
212.47	499	215.07	6,274
212.52	560	215.12	6,427
212.57	622	215.17	6,581
212.62	686	215.22	6,737
212.67	751	215.27	6,894
212.72	818	215.32	7,053
212.77	887	215.37	7,214
212.82	957	215.42	7,376
212.87	1,029	215.47	7,540
212.92	1,103	215.52	7,706
212.97	1,179	215.57	7,874
213.02	1,259	215.62	8,043
213.07	1,344	215.67	8,214
213.12	1,432	215.72	8,386
213.17	1,523	215.77	8,561
213.22	1,615	215.82	8,737
213.27	1,710	215.87	8,914
213.32	1,808	215.92	9,094
213.37	1,907	215.97	9,275
213.42	2,010		
213.47	2,114		
213.52	2,222		
213.57	2,331		
213.62	2,444		
213.67	2,559		
213.72	2,676		
213.77	2,796		
213.82	2,919		
213.87	3,045		
213.92	3,173		
213.97	3,304		
214.02	3,432		
214.07	3,553		
214.12	3,675		
214.17	3,799		
214.22	3,924		

Linear Interpolation
1162 CF Storage = 212.96'

20-097 Proposed Analysis

Type III 24-hr 2YR - 24HR Rainfall=3.08"

Prepared by {enter your company name here}

Printed 6/17/2021

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Stage-Discharge for Pond 103P: Gravel Wetland #103

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
211.67	0.00	0.00	0.00	214.27	0.17	0.17	0.00
211.72	0.00	0.00	0.00	214.32	0.18	0.18	0.00
211.77	0.00	0.00	0.00	214.37	0.19	0.19	0.00
211.82	0.00	0.00	0.00	214.42	0.20	0.20	0.00
211.87	0.01	0.01	0.00	214.47	0.20	0.20	0.00
211.92	0.01	0.01	0.00	214.52	0.21	0.21	0.00
211.97	0.01	0.01	0.00	214.57	0.22	0.22	0.00
212.02	0.01	0.01	0.00	214.62	0.23	0.23	0.00
212.07	0.01	0.01	0.00	214.67	0.23	0.23	0.00
212.12	0.01	0.01	0.00	214.72	0.24	0.24	0.00
212.17	0.01	0.01	0.00	214.77	0.25	0.25	0.00
212.22	0.01	0.01	0.00	214.82	0.25	0.25	0.00
212.27	0.01	0.01	0.00	214.87	0.26	0.26	0.00
212.32	0.01	0.01	0.00	214.92	0.26	0.26	0.00
212.37	0.01	0.01	0.00	214.97	0.27	0.27	0.00
212.42	0.01	0.01	0.00	215.02	0.28	0.28	0.00
212.47	0.01	0.01	0.00	215.07	0.28	0.28	0.00
212.52	0.01	0.01	0.00	215.12	0.29	0.29	0.00
212.57	0.01	0.01	0.00	215.17	0.29	0.29	0.00
212.62	0.01	0.01	0.00	215.22	0.30	0.30	0.00
212.67	0.01	0.01	0.00	215.27	0.30	0.30	0.00
212.72	0.01	0.01	0.00	215.32	0.31	0.31	0.00
212.77	0.01	0.01	0.00	215.37	0.31	0.31	0.00
212.82	0.01	0.01	0.00	215.42	0.32	0.32	0.00
212.87	0.01	0.01	0.00	215.47	0.44	0.44	0.00
212.92	0.01	0.01	0.00	215.52	1.12	1.09	0.03
212.97	0.01	0.01	0.00	215.57	2.26	2.04	0.22
213.02	0.01	0.01	0.00	215.62	3.72	3.22	0.50
213.07	0.02	0.02	0.00	215.67	5.42	4.58	0.84
213.12	0.02	0.02	0.00	215.72	7.36	6.11	1.24
213.17	0.02	0.02	0.00	215.77	9.50	7.79	1.71
213.22	0.02	0.02	0.00	215.82	11.84	9.60	2.24
213.27	0.02	0.02	0.00	215.87	13.99	11.17	2.82
213.32	0.02	0.02	0.00	215.92	14.70	11.25	3.45
213.37	0.02	0.02	0.00	215.97	15.49	11.33	4.16
213.42	0.02	0.02	0.00				
213.47	0.02	0.02	0.00				
213.52	0.02	0.02	0.00				
213.57	0.02	0.02	0.00				
213.62	0.02	0.02	0.00				
213.67	0.02	0.02	0.00				
213.72	0.02	0.02	0.00				
213.77	0.02	0.02	0.00				
213.82	0.03	0.03	0.00				
213.87	0.05	0.05	0.00				
213.92	0.07	0.07	0.00				
213.97	0.09	0.09	0.00				
214.02	0.11	0.11	0.00				
214.07	0.12	0.12	0.00				
214.12	0.14	0.14	0.00				
214.17	0.15	0.15	0.00				
214.22	0.16	0.16	0.00				

Elevation 212.96' =
0.01 CFS discharge

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/28/2021

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Summary for Pond 104P: Gravel Wetland #104

[80] Warning: Exceeded Pond C31P by 0.01' @ 22.85 hrs (0.57 cfs 0.065 af)

Inflow Area = 0.331 ac, 57.47% Impervious, Inflow Depth > 5.04" for 50YR - 24HR event
 Inflow = 1.84 cfs @ 12.09 hrs, Volume= 0.139 af
 Outflow = 1.61 cfs @ 12.15 hrs, Volume= 0.105 af, Atten= 12%, Lag= 3.7 min
 Primary = 1.41 cfs @ 12.15 hrs, Volume= 0.103 af
 Secondary = 0.20 cfs @ 12.15 hrs, Volume= 0.002 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 216.57' @ 12.15 hrs Surf.Area= 2,276 sf Storage= 2,001 cf
 Flood Elev= 217.00' Surf.Area= 2,431 sf Storage= 2,575 cf

Plug-Flow detention time= 140.3 min calculated for 0.105 af (76% of inflow)
 Center-of-Mass det. time= 56.2 min (850.0 - 793.8)

Volume	Invert	Avail.Storage	Storage Description
#1	213.67'	34 cf	4.00'D x 2.73'H 4' Outlet Structure
#2	214.00'	1,004 cf	Single Cell (Irregular) Listed below (Recalc)
#3	214.00'	311 cf	Sediment Forebay (Irregular) Listed below (Recalc)
#4	216.00'	1,226 cf	Open Water Storage (Irregular) Listed below (Recalc)
		2,575 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
214.00	305	87.3	0	0	305
215.00	496	101.5	397	397	538
216.00	725	117.0	607	1,004	829

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
214.00	40	24.5	0	0	40
215.00	155	57.8	91	91	262
216.00	291	73.5	219	311	439

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
216.00	1,059	165.1	0	0	1,059
217.00	1,402	177.7	1,226	1,226	1,443

Device	Routing	Invert	Outlet Devices
#1	Primary	213.67'	15.0" Round 15" N-12 HDPE L= 20.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 213.67' / 213.00' S= 0.0335 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	213.67'	0.5" Vert. 0.50" Orifice Goose Neck C= 0.600
#3	Device 1	216.10'	12.0" W x 3.0" H Vert. 3" X 12" Box Orifice C= 0.600
#4	Device 1	216.40'	12.0" Horiz. 12" Horizontal Orifice C= 0.600 Limited to weir flow at low heads
#5	Secondary	216.50'	5.0' long x 7.0' breadth E-Spillway

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Head (feet)	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60	1.80	2.00
	2.50	3.00	3.50	4.00	4.50	5.00	5.50			
Coef. (English)	2.40	2.52	2.70	2.68	2.68	2.67	2.66	2.65	2.65	
	2.65	2.66	2.65	2.66	2.68	2.70	2.73	2.78		

Primary OutFlow Max=1.40 cfs @ 12.15 hrs HW=216.57' TW=213.93' (Dynamic Tailwater)

- ↑ 1=15" N-12 HDPE (Passes 1.40 cfs of 8.90 cfs potential flow)
- ↑ 2=0.50" Orifice Goose Neck (Orifice Controls 0.01 cfs @ 7.81 fps)
- ↑ 3=3" X 12" Box Orifice (Orifice Controls 0.70 cfs @ 2.79 fps)
- ↑ 4=12" Horizontal Orifice (Weir Controls 0.69 cfs @ 1.33 fps)

Secondary OutFlow Max=0.20 cfs @ 12.15 hrs HW=216.57' TW=213.93' (Dynamic Tailwater)

- ↑ 5=E-Spillway (Weir Controls 0.20 cfs @ 0.61 fps)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Area-Storage for Pond 104P: Gravel Wetland #104

Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
213.67	0	216.27	1,645
213.72	1	216.32	1,703
213.77	1	216.37	1,762
213.82	2	216.42	1,822
213.87	3	216.47	1,882
213.92	3	216.52	1,943
213.97	4	216.57	2,005
214.02	11	216.62	2,068
214.07	30	216.67	2,132
214.12	49	216.72	2,197
214.17	69	216.77	2,262
214.22	89	216.82	2,329
214.27	110	216.87	2,396
214.32	132	216.92	2,464
214.37	154	216.97	2,533
214.42	177		
214.47	201		
214.52	226		
214.57	252		
214.62	278		
214.67	305		
214.72	333		
214.77	361		
214.82	391		
214.87	421		
214.92	453		
214.97	485		
215.02	518		
215.07	552		
215.12	587		
215.17	622		
215.22	659		
215.27	696		
215.32	734		
215.37	773		
215.42	813		
215.47	854		
215.52	895		
215.57	938		
215.62	981		
215.67	1,026		
215.72	1,071		
215.77	1,118		
215.82	1,165		
215.87	1,213		
215.92	1,263		
215.97	1,313		
216.02	1,365		
216.07	1,419		
216.12	1,474		
216.17	1,530		
216.22	1,587		

Linear Interpolation
682 CF Storage = 215.25'

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Discharge for Pond 104P: Gravel Wetland #104

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
213.67	0.00	0.00	0.00	216.27	0.24	0.24	0.00
213.72	0.00	0.00	0.00	216.32	0.34	0.34	0.00
213.77	0.00	0.00	0.00	216.37	0.45	0.45	0.00
213.82	0.00	0.00	0.00	216.42	0.56	0.56	0.00
213.87	0.00	0.00	0.00	216.47	0.79	0.79	0.00
213.92	0.00	0.00	0.00	216.52	1.12	1.09	0.03
213.97	0.00	0.00	0.00	216.57	1.66	1.43	0.22
214.02	0.00	0.00	0.00	216.62	2.32	1.82	0.50
214.07	0.00	0.00	0.00	216.67	3.09	2.25	0.84
214.12	0.00	0.00	0.00	216.72	3.96	2.72	1.24
214.17	0.00	0.00	0.00	216.77	4.91	3.20	1.71
214.22	0.00	0.00	0.00	216.82	5.63	3.39	2.24
214.27	0.00	0.00	0.00	216.87	6.39	3.57	2.82
214.32	0.01	0.01	0.00	216.92	7.20	3.74	3.45
214.37	0.01	0.01	0.00	216.97	8.07	3.90	4.16
214.42	0.01	0.01	0.00				
214.47	0.01	0.01	0.00				
214.52	0.01	0.01	0.00				
214.57	0.01	0.01	0.00				
214.62	0.01	0.01	0.00				
214.67	0.01	0.01	0.00				
214.72	0.01	0.01	0.00				
214.77	0.01	0.01	0.00				
214.82	0.01	0.01	0.00				
214.87	0.01	0.01	0.00				
214.92	0.01	0.01	0.00				
214.97	0.01	0.01	0.00				
215.02	0.01	0.01	0.00				
215.07	0.01	0.01	0.00				
215.12	0.01	0.01	0.00				
215.17	0.01	0.01	0.00				
215.22	0.01	0.01	0.00				
215.27	0.01	0.01	0.00				
215.32	0.01	0.01	0.00				
215.37	0.01	0.01	0.00				
215.42	0.01	0.01	0.00				
215.47	0.01	0.01	0.00				
215.52	0.01	0.01	0.00				
215.57	0.01	0.01	0.00				
215.62	0.01	0.01	0.00				
215.67	0.01	0.01	0.00				
215.72	0.01	0.01	0.00				
215.77	0.01	0.01	0.00				
215.82	0.01	0.01	0.00				
215.87	0.01	0.01	0.00				
215.92	0.01	0.01	0.00				
215.97	0.01	0.01	0.00				
216.02	0.01	0.01	0.00				
216.07	0.01	0.01	0.00				
216.12	0.02	0.02	0.00				
216.17	0.07	0.07	0.00				
216.22	0.14	0.14	0.00				

Elevation 215.25' =
0.01 CFS discharge



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name: _____

Rain Garden #105

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

Yes	Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.07(a).	
1.63 ac	A = Area draining to the practice	
1.03 ac	A_i = Impervious area draining to the practice	
0.64 decimal	l = Percent impervious area draining to the practice, in decimal form	
0.62 unitless	R_v = Runoff coefficient = $0.05 + (0.9 \times l)$	
1.01 ac-in	WQV = 1" x R_v x A	
3,676 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
919 cf	25% x WQV (check calc for sediment forebay volume)	
2,757 cf	75% x WQV (check calc for surface sand filter volume)	
Sediment Forebay (2) Method of Pretreatment? (not required for clean or roof runoff)		
745,758 cf	V_{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
Calculate time to drain if system IS NOT underdrained:		
N/A sf	A_{SA} = Surface area of the practice	
N/A iph	$K_{SAT_{DESIGN}}$ = Design infiltration rate ¹	
If K_{SAT} (prior to factor of safety) is < 0.50 iph, has an underdrain been provided? (Use the calculations below)		
N/A Yes/No		
- hours	T_{DRAIN} = Drain time = $V / (A_{SA} * I_{DESIGN})$	≤ 72-hrs
Calculate time to drain if system IS underdrained:		
217.36 ft	E_{WQV} = Elevation of WQV (attach stage-storage table)	
0.06 cfs	Q_{WQV} = Discharge at the E_{WQV} (attach stage-discharge table)	
34.03 hours	T_{DRAIN} = Drain time = $2WQV/Q_{WQV}$	≤ 72-hrs
213.75 feet	E_{FC} = Elevation of the bottom of the filter course material ²	
212.75 feet	E_{UD} = Invert elevation of the underdrain (UD), if applicable	
212.00 feet	E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test pit)	
208.67 feet	E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test pit)	
1.00 feet	$D_{FC\ to\ UD}$ = Depth to UD from the bottom of the filter course	≥ 1'
5.08 feet	$D_{FC\ to\ ROCK}$ = Depth to bedrock from the bottom of the filter course	≥ 1'
1.75 feet	$D_{FC\ to\ SHWT}$ = Depth to SHWT from the bottom of the filter course	≥ 1'
219.99 ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
220.50 ft	Elevation of the top of the practice	
YES	50 peak elevation ≤ Elevation of the top of the practice	← yes
If a surface sand filter or underground sand filter is proposed:		
YES ac	Drainage Area check.	< 10 ac
cf	V = Volume of storage ³ (attach a stage-storage table)	≥ 75%WQV
inches	D_{FC} = Filter course thickness	18", or 24" if within GPA
Sheet	Note what sheet in the plan set contains the filter course specification.	
Yes/No	Access grate provided?	← yes

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Summary for Pond 105P: Rain Garden #105

[80] Warning: Exceeded Pond C35P by 0.02' @ 18.30 hrs (0.82 cfs 0.151 af)

[80] Warning: Exceeded Pond C39P by 0.02' @ 23.85 hrs (0.75 cfs 0.052 af)

Inflow Area = 1.629 ac, 63.51% Impervious, Inflow Depth > 5.35" for 50YR - 24HR event
 Inflow = 9.33 cfs @ 12.09 hrs, Volume= 0.726 af
 Outflow = 2.76 cfs @ 12.43 hrs, Volume= 0.540 af, Atten= 70%, Lag= 20.2 min
 Primary = 2.76 cfs @ 12.43 hrs, Volume= 0.540 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 219.99' @ 12.43 hrs Surf.Area= 1,331 sf Storage= 15,181 cf
 Flood Elev= 220.50' Surf.Area= 1,331 sf Storage= 18,035 cf

Plug-Flow detention time= 213.9 min calculated for 0.540 af (74% of inflow)
 Center-of-Mass det. time= 126.7 min (908.7 - 781.9)

Volume	Invert	Avail.Storage	Storage Description
#1	212.75'	532 cf	Stone (Irregular) Listed below (Recalc) -Impervious 1,331 cf Overall x 40.0% Voids
#2	213.75'	532 cf	Bio-media (Irregular) Listed below (Recalc) 2,662 cf Overall x 20.0% Voids
#3	216.00'	3,584 cf	RG Cell (Irregular) Listed below (Recalc) -Impervious
#4	218.00'	11,794 cf	Open Water Storage (Irregular) Listed below (Recalc) -Impervious
#5	215.75'	89 cf	Loam (Irregular) Listed below (Recalc) -Impervious 447 cf Overall x 20.0% Voids
#6	216.00'	745 cf	Sediment Forebay #1 (Irregular) Listed below (Recalc) -Impervious
#7	216.00'	758 cf	Sediment Forebay #2 (Irregular) Listed below (Recalc) -Impervious
		18,035 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
212.75	1,331	159.0	0	0	1,331
213.75	1,331	159.0	1,331	1,331	1,490

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
213.75	1,331	159.0	0	0	1,331
215.75	1,331	159.0	2,662	2,662	1,649

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
216.00	1,331	159.0	0	0	1,331
217.00	1,787	175.8	1,553	1,553	1,809
218.00	2,285	192.8	2,031	3,584	2,340

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
218.00	3,654	268.0	0	0	3,654
219.00	4,485	286.8	4,062	4,062	4,529
220.00	5,380	306.3	4,926	8,988	5,496
220.50	5,846	315.7	2,806	11,794	5,987

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
215.75	1,787	176.7	0	0	1,787
216.00	1,787	176.7	447	447	1,831

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
216.00	185	59.4	0	0	185
217.00	365	77.2	270	270	390
218.00	595	94.9	475	745	647

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
216.00	188	82.9	0	0	188
217.00	367	77.3	273	273	295
218.00	614	97.7	485	758	593

Device	Routing	Invert	Outlet Devices
#1	Primary	212.75'	18.0" Round 18" HDPE N-12 L= 85.0' Ke= 0.500 Inlet / Outlet Invert= 212.75' / 212.00' S= 0.0088 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	212.75'	1.0" Vert. 1" Orifice C= 0.600
#3	Device 2	213.75'	10.000 in/hr Exfiltration over Surface area
#4	Device 1	220.00'	15.0" Horiz. 15" Horizontal Orifice C= 0.600 Limited to weir flow at low heads
#5	Device 1	218.10'	3.0" Vert. 3" Orifice C= 0.600
#6	Device 1	219.00'	9.0" W x 12.0" H Vert. 12" X 12" Box Orifice C= 0.600

Primary OutFlow Max=2.75 cfs @ 12.43 hrs HW=219.99' TW=212.71' (Dynamic Tailwater)

- 1=18" HDPE N-12 (Passes 2.75 cfs of 21.50 cfs potential flow)
- 2=1" Orifice (Orifice Controls 0.07 cfs @ 12.92 fps)
- 3=Exfiltration (Passes 0.07 cfs of 0.31 cfs potential flow)
- 4=15" Horizontal Orifice (Controls 0.00 cfs)
- 5=3" Orifice (Orifice Controls 0.31 cfs @ 6.40 fps)
- 6=12" X 12" Box Orifice (Orifice Controls 2.37 cfs @ 3.19 fps)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Area-Storage for Pond 105P: Rain Garden #105

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
212.75	0	0	217.95	1,331	6,068
212.85	0	53	218.05	1,331	6,425
212.95	0	106	218.15	1,331	6,799
213.05	0	160	218.25	1,331	7,180
213.15	0	213	218.35	1,331	7,569
213.25	0	266	218.45	1,331	7,967
213.35	0	319	218.55	1,331	8,373
213.45	0	373	218.65	1,331	8,787
213.55	0	426	218.75	1,331	9,210
213.65	0	479	218.85	1,331	9,641
213.75	1,331	532	218.95	1,331	10,081
213.85	1,331	559	219.05	1,331	10,529
213.95	1,331	586	219.15	1,331	10,986
214.05	1,331	612	219.25	1,331	11,452
214.15	1,331	639	219.35	1,331	11,927
214.25	1,331	666	219.45	1,331	12,410
214.35	1,331	692	219.55	1,331	12,902
214.45	1,331	719	219.65	1,331	13,403
214.55	1,331	745	219.75	1,331	13,914
214.65	1,331	772	219.85	1,331	14,433
214.75	1,331	799	219.95	1,331	14,962
214.85	1,331	825	220.05	1,331	15,500
214.95	1,331	852	220.15	1,331	16,047
215.05	1,331	878	220.25	1,331	16,603
215.15	1,331	905	220.35	1,331	17,169
215.25	1,331	932	220.45	1,331	17,744
215.35	1,331	958			
215.45	1,331	985			
215.55	1,331	1,012			
215.65	1,331	1,038			
215.75	1,331	1,065			
215.85	1,331	1,101			
215.95	1,331	1,136			
216.05	1,331	1,240			
216.15	1,331	1,418			
216.25	1,331	1,603			
216.35	1,331	1,796			
216.45	1,331	1,997			
216.55	1,331	2,206			
216.65	1,331	2,423			
216.75	1,331	2,648			
216.85	1,331	2,882			
216.95	1,331	3,125			
217.05	1,331	3,377			
217.15	1,331	3,638			
217.25	1,331	3,908			
217.35	1,331	4,187			
217.45	1,331	4,476			
217.55	1,331	4,774			
217.65	1,331	5,083			
217.75	1,331	5,401			
217.85	1,331	5,729			

WQV Draw-down
 Linear Interpolation
 3,676 CF Storage above
 stone = 217.36'

See next Stage-Area-Storage Table
 for storage volume

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Discharge for Pond 105P: Rain Garden #105

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
212.75	0.00	214.83	0.04	216.91	0.05	218.99	0.27
212.79	0.00	214.87	0.04	216.95	0.05	219.03	0.29
212.83	0.00	214.91	0.04	216.99	0.05	219.07	0.33
212.87	0.00	214.95	0.04	217.03	0.05	219.11	0.38
212.91	0.00	214.99	0.04	217.07	0.05	219.15	0.43
212.95	0.00	215.03	0.04	217.11	0.05	219.19	0.50
212.99	0.00	215.07	0.04	217.15	0.05	219.23	0.57
213.03	0.00	215.11	0.04	217.19	0.06	219.27	0.65
213.07	0.00	215.15	0.04	217.23	0.06	219.31	0.73
213.11	0.00	215.19	0.04	217.27	0.06	219.35	0.82
213.15	0.00	215.23	0.04	217.31	0.06	219.39	0.91
213.19	0.00	215.27	0.04	217.35	0.06	219.43	1.01
213.23	0.00	215.31	0.04	217.39	0.06	219.47	1.11
213.27	0.00	215.35	0.04	217.43	0.06	219.51	1.21
213.31	0.00	215.39	0.04	217.47	0.06	219.55	1.32
213.35	0.00	215.43	0.04	217.51	0.06	219.59	1.44
213.39	0.00	215.47	0.04	217.55	0.06	219.63	1.55
213.43	0.00	215.51	0.04	217.59	0.06	219.67	1.67
213.47	0.00	215.55	0.04	217.63	0.06	219.71	1.80
213.51	0.00	215.59	0.04	217.67	0.06	219.75	1.92
213.55	0.00	215.63	0.04	217.71	0.06	219.79	2.06
213.59	0.00	215.67	0.04	217.75	0.06	219.83	2.19
213.63	0.00	215.71	0.04	217.79	0.06	219.87	2.33
213.67	0.00	215.75	0.05	217.83	0.06	219.91	2.47
213.71	0.00	215.79	0.05	217.87	0.06	219.95	2.61
213.75	0.03	215.83	0.05	217.91	0.06	219.99	2.76
213.79	0.03	215.87	0.05	217.95	0.06	220.03	2.96
213.83	0.03	215.91	0.05	217.99	0.06	220.07	3.25
213.87	0.03	215.95	0.05	218.03	0.06	220.11	3.59
213.91	0.03	215.99	0.05	218.07	0.06	220.15	3.97
213.95	0.03	216.03	0.05	218.11	0.06	220.19	4.39
213.99	0.03	216.07	0.05	218.15	0.07	220.23	4.84
214.03	0.03	216.11	0.05	218.19	0.08	220.27	5.32
214.07	0.03	216.15	0.05	218.23	0.09	220.31	5.82
214.11	0.03	216.19	0.05	218.27	0.11	220.35	6.35
214.15	0.03	216.23	0.05	218.31	0.13	220.39	6.91
214.19	0.03	216.27	0.05	218.35	0.15	220.43	7.48
214.23	0.03	216.31	0.05	218.39	0.16	220.47	7.99
214.27	0.03	216.35	0.05	218.43	0.17		
214.31	0.03	216.39	0.05	218.47	0.18		
214.35	0.03	216.43	0.05	218.51	0.19		
214.39	0.03	216.47	0.05	218.55	0.20		
214.43	0.03	216.51	0.05	218.59	0.21		
214.47	0.03	216.55	0.05	218.63	0.21		
214.51	0.03	216.59	0.05	218.67	0.22		
214.55	0.03	216.63	0.05	218.71	0.23		
214.59	0.04	216.67	0.05	218.75	0.24		
214.63	0.04	216.71	0.05	218.79	0.24		
214.67	0.04	216.75	0.05	218.83	0.25		
214.71	0.04	216.79	0.05	218.87	0.25		
214.75	0.04	216.83	0.05	218.91	0.26		
214.79	0.04	216.87	0.05	218.95	0.27		

Elevation 217.36' =
0.06 CFS discharge

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

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Stage-Area-Storage for Pond 105P: Rain Garden #105

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
212.75	0	0	217.95	1,331	6,068
212.85	0	53	<u>218.05</u>	<u>1,331</u>	<u>6,425</u>
212.95	0	106	218.15	1,331	6,799
213.05	0	160	218.25	1,331	7,180
213.15	0	213	218.35	1,331	7,569
213.25	0	266	218.45	1,331	7,967
213.35	0	319	218.55	1,331	8,373
213.45	0	373	218.65	1,331	8,787
213.55	0	426	218.75	1,331	9,210
<u>213.65</u>	<u>0</u>	<u>479</u>	218.85	1,331	9,641
213.75	1,331	532	218.95	1,331	10,081
213.85	1,331	559	219.05	1,331	10,529
213.95	1,331	586	219.15	1,331	10,986
214.05	1,331	612	219.25	1,331	11,452
214.15	1,331	639	219.35	1,331	11,927
214.25	1,331	666	219.45	1,331	12,410
214.35	1,331	692	219.55	1,331	12,902
214.45	1,331	719	219.65	1,331	13,403
214.55	1,331	745	219.75	1,331	13,914
214.65	1,331	772	219.85	1,331	14,433
214.75	1,331	799	219.95	1,331	14,962
214.85	1,331	825	220.05	1,331	15,500
214.95	1,331	852	220.15	1,331	16,047
215.05	1,331	878	220.25	1,331	16,603
215.15	1,331	905	220.35	1,331	17,169
215.25	1,331	932	220.45	1,331	17,744
215.35	1,331	958			
215.45	1,331	985			
215.55	1,331	1,012			
215.65	1,331	1,038			
215.75	1,331	1,065			
215.85	1,331	1,101			
215.95	1,331	1,136			
216.05	1,331	1,240			
216.15	1,331	1,418			
216.25	1,331	1,603			
216.35	1,331	1,796			
216.45	1,331	1,997			
216.55	1,331	2,206			
216.65	1,331	2,423			
216.75	1,331	2,648			
216.85	1,331	2,882			
216.95	1,331	3,125			
217.05	1,331	3,377			
217.15	1,331	3,638			
217.25	1,331	3,908			
217.35	1,331	4,187			
217.45	1,331	4,476			
217.55	1,331	4,774			
217.65	1,331	5,083			
217.75	1,331	5,401			
217.85	1,331	5,729			

Linear Interpolation

Lowest Orifice = 218.10'

Storage Volume = 6,080 CF

$$6,612 \text{ CF} - 532 \text{ CF} = 6,080 \text{ CF}$$



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name:

Rain Garden #106

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

Yes	Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.07(a).	
1.23 ac	A = Area draining to the practice	
0.37 ac	A_i = Impervious area draining to the practice	
0.30 decimal	l = Percent impervious area draining to the practice, in decimal form	
0.32 unitless	R_v = Runoff coefficient = $0.05 + (0.9 \times l)$	
0.40 ac-in	WQV = $1'' \times R_v \times A$	
1,439 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
360 cf	25% x WQV (check calc for sediment forebay volume)	
1,079 cf	75% x WQV (check calc for surface sand filter volume)	
Sediment Forebay	Method of Pretreatment? (not required for clean or roof runoff)	
500 cf	V_{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
Calculate time to drain if system IS NOT underdrained:		
N/A sf	A_{SA} = Surface area of the practice	
N/A iph	$K_{sat_{DESIGN}}$ = Design infiltration rate ¹	
N/A Yes/No	If K_{sat} (prior to factor of safety) is < 0.50 iph, has an underdrain been provided? (Use the calculations below)	
- hours	T_{DRAIN} = Drain time = $V / (A_{SA} * I_{DESIGN})$	≤ 72-hrs
Calculate time to drain if system IS underdrained:		
216.49 ft	E_{WQV} = Elevation of WQV (attach stage-storage table)	
0.03 cfs	Q_{WQV} = Discharge at the E_{WQV} (attach stage-discharge table)	
26.64 hours	T_{DRAIN} = Drain time = $2WQV/Q_{WQV}$	≤ 72-hrs
212.75 feet	E_{FC} = Elevation of the bottom of the filter course material ²	
211.75 feet	E_{UD} = Invert elevation of the underdrain (UD), if applicable	
215.33 feet	E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test pit)	
215.33 feet	E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test pit)	
1.00 feet	$D_{FC\ to\ UD}$ = Depth to UD from the bottom of the filter course	≥ 1'
(2.58) feet	$D_{FC\ to\ ROCK}$ = Depth to bedrock from the bottom of the filter course	≥ 1'
(2.58) feet	$D_{FC\ to\ SHWT}$ = Depth to SHWT from the bottom of the filter course	≥ 1'
219.09 ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
220.00 ft	Elevation of the top of the practice	
YES	50 peak elevation ≤ Elevation of the top of the practice	← yes
If a surface sand filter or underground sand filter is proposed:		
YES ac	Drainage Area check.	< 10 ac
cf	V = Volume of storage ³ (attach a stage-storage table)	≥ 75%WQV
inches	D_{FC} = Filter course thickness	18", or 24" if within GPA
Sheet	Note what sheet in the plan set contains the filter course specification.	
Yes/No	Access grate provided?	← yes

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/28/2021

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Summary for Pond 106P: Rain Garden #106

Inflow Area = 1.231 ac, 30.22% Impervious, Inflow Depth > 4.01" for 50YR - 24HR event
 Inflow = 3.96 cfs @ 12.13 hrs, Volume= 0.411 af
 Outflow = 1.49 cfs @ 12.55 hrs, Volume= 0.318 af, Atten= 62%, Lag= 25.3 min
 Primary = 1.49 cfs @ 12.55 hrs, Volume= 0.318 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 219.09' @ 12.55 hrs Surf.Area= 391 sf Storage= 7,848 cf
 Flood Elev= 220.00' Surf.Area= 391 sf Storage= 11,576 cf

Plug-Flow detention time= 247.5 min calculated for 0.317 af (77% of inflow)
 Center-of-Mass det. time= 158.8 min (984.9 - 826.1)

Volume	Invert	Avail.Storage	Storage Description
#1	211.75'	156 cf	Stone (Irregular) Listed below (Recalc) -Impervious 391 cf Overall x 40.0% Voids
#2	212.75'	156 cf	Bio-media (Irregular) Listed below (Recalc) 782 cf Overall x 20.0% Voids
#3	215.00'	10,744 cf	Open Water Storage (Irregular) Listed below (Recalc) -Impervious
#4	214.75'	20 cf	Loam (Irregular) Listed below (Recalc) -Impervious 98 cf Overall x 20.0% Voids
#5	215.00'	500 cf	Sediment Forebay (Irregular) Listed below (Recalc) -Impervious
		11,576 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
211.75	391	90.7	0	0	391
212.75	391	90.7	391	391	482

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
212.75	391	90.7	0	0	391
214.75	391	90.7	782	782	572

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
215.00	391	90.7	0	0	391
216.00	680	109.0	529	529	698
217.00	1,404	149.4	1,020	1,549	1,539
218.00	2,730	229.3	2,031	3,580	3,955
219.00	3,498	255.5	3,106	6,686	4,994
220.00	4,645	388.2	4,058	10,744	11,799

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
214.75	391	90.7	0	0	391
215.00	391	90.7	98	98	414

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
215.00	104	39.3	0	0	104
216.00	238	57.1	166	166	249
217.00	439	77.5	333	500	477

Device	Routing	Invert	Outlet Devices
#1	Primary	211.75'	15.0" Round 15" HDPE N-12 L= 95.0' Ke= 0.500 Inlet / Outlet Invert= 211.75' / 211.00' S= 0.0079 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	211.75'	0.7" Vert. 0.75" Orifice C= 0.600
#3	Device 2	212.75'	10.000 in/hr Exfiltration over Surface area
#4	Device 1	217.50'	3.0" Vert. 3" Orifice C= 0.600
#5	Device 1	219.00'	48.0" Horiz. 48" Top Structure C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=1.48 cfs @ 12.55 hrs HW=219.09' TW=211.14' (Dynamic Tailwater)

- 1=15" HDPE N-12 (Passes 1.48 cfs of 14.00 cfs potential flow)
- 2=0.75" Orifice (Orifice Controls 0.03 cfs @ 13.02 fps)
- 3=Exfiltration (Passes 0.03 cfs of 0.09 cfs potential flow)
- 4=3" Orifice (Orifice Controls 0.29 cfs @ 5.83 fps)
- 5=48" Top Structure (Weir Controls 1.16 cfs @ 1.00 fps)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Area-Storage for Pond 106P: Rain Garden #106

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
211.75	0	0	216.95	391	2,291
211.85	0	16	217.05	391	2,453
211.95	0	31	217.15	391	2,605
212.05	0	47	217.25	391	2,768
212.15	0	63	217.35	391	2,944
212.25	0	78	217.45	391	3,132
212.35	0	94	217.55	391	3,333
212.45	0	109	217.65	391	3,548
212.55	0	125	217.75	391	3,777
212.65	0	141	217.85	391	4,020
212.75	391	156	217.95	391	4,277
212.85	391	164	218.05	391	4,549
212.95	391	172	218.15	391	4,830
213.05	391	180	218.25	391	5,117
213.15	391	188	218.35	391	5,412
213.25	391	196	218.45	391	5,715
213.35	391	203	218.55	391	6,025
213.45	391	211	218.65	391	6,343
213.55	391	219	218.75	391	6,669
213.65	391	227	218.85	391	7,003
213.75	391	235	218.95	391	7,344
213.85	391	242	219.05	391	7,694
213.95	391	250	219.15	391	8,055
214.05	391	258	219.25	391	8,426
214.15	391	266	219.35	391	8,809
214.25	391	274	219.45	391	9,203
214.35	391	282	219.55	391	9,608
214.45	391	289	219.65	391	10,024
214.55	391	297	219.75	391	10,453
214.65	391	305	219.85	391	10,893
214.75	391	313	219.95	391	11,345
214.85	391	321			
214.95	391	328			
215.05	391	358			
215.15	391	411			
215.25	391	468			
215.35	391	528			
215.45	391	593			
215.55	391	662			
215.65	391	735			
215.75	391	813			
215.85	391	895			
215.95	391	982			
216.05	391	1,075			
216.15	391	1,174			
216.25	391	1,282			
216.35	391	1,398			
216.45	391	1,523			
216.55	391	1,657			
216.65	391	1,801			
216.75	391	1,954			
216.85	391	2,117			

WQV Draw-down
 Linear Interpolation
 1,439 CF Storage above
 stone = 216.47'

See next Stage-Area-Storage Table
 for storage volume

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Discharge for Pond 106P: Rain Garden #106

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
211.75	0.00	213.83	0.02	215.91	0.03	217.99	0.17
211.79	0.00	213.87	0.02	215.95	0.03	218.03	0.18
211.83	0.00	213.91	0.02	215.99	0.03	218.07	0.19
211.87	0.00	213.95	0.02	216.03	0.03	218.11	0.20
211.91	0.00	213.99	0.02	216.07	0.03	218.15	0.20
211.95	0.00	214.03	0.02	216.11	0.03	218.19	0.21
211.99	0.00	214.07	0.02	216.15	0.03	218.23	0.22
212.03	0.00	214.11	0.02	216.19	0.03	218.27	0.22
212.07	0.00	214.15	0.02	216.23	0.03	218.31	0.23
212.11	0.00	214.19	0.02	216.27	0.03	218.35	0.23
212.15	0.00	214.23	0.02	216.31	0.03	218.39	0.24
212.19	0.00	214.27	0.02	216.35	0.03	218.43	0.25
212.23	0.00	214.31	0.02	216.39	0.03	218.47	0.25
212.27	0.00	214.35	0.02	216.43	0.03	218.51	0.26
212.31	0.00	214.39	0.02	216.47	0.03	218.55	0.26
212.35	0.00	214.43	0.02	216.51	0.03	218.59	0.27
212.39	0.00	214.47	0.02	216.55	0.03	218.63	0.27
212.43	0.00	214.51	0.02	216.59	0.03	218.67	0.28
212.47	0.00	214.55	0.02	216.63	0.03	218.71	0.28
212.51	0.00	214.59	0.02	216.67	0.03	218.75	0.28
212.55	0.00	214.63	0.02	216.71	0.03	218.79	0.29
212.59	0.00	214.67	0.02	216.75	0.03	218.83	0.29
212.63	0.00	214.71	0.02	216.79	0.03	218.87	0.30
212.67	0.00	214.75	0.02	216.83	0.03	218.91	0.30
212.71	0.00	214.79	0.02	216.87	0.03	218.95	0.31
212.75	0.01	214.83	0.02	216.91	0.03	218.99	0.31
212.79	0.01	214.87	0.02	216.95	0.03	219.03	0.53
212.83	0.01	214.91	0.02	216.99	0.03	219.07	1.08
212.87	0.01	214.95	0.02	217.03	0.03	219.11	1.82
212.91	0.01	214.99	0.02	217.07	0.03	219.15	2.71
212.95	0.01	215.03	0.02	217.11	0.03	219.19	3.73
212.99	0.01	215.07	0.02	217.15	0.03	219.23	4.87
213.03	0.01	215.11	0.02	217.19	0.03	219.27	6.10
213.07	0.01	215.15	0.02	217.23	0.03	219.31	7.43
213.11	0.01	215.19	0.02	217.27	0.03	219.35	8.85
213.15	0.02	215.23	0.02	217.31	0.03	219.39	10.36
213.19	0.02	215.27	0.02	217.35	0.03	219.43	11.94
213.23	0.02	215.31	0.02	217.39	0.03	219.47	13.60
213.27	0.02	215.35	0.02	217.43	0.03	219.51	14.42
213.31	0.02	215.39	0.02	217.47	0.03	219.55	14.46
213.35	0.02	215.43	0.02	217.51	0.03	219.59	14.50
213.39	0.02	215.47	0.02	217.55	0.04	219.63	14.54
213.43	0.02	215.51	0.02	217.59	0.05	219.67	14.57
213.47	0.02	215.55	0.02	217.63	0.06	219.71	14.61
213.51	0.02	215.59	0.03	217.67	0.08	219.75	14.65
213.55	0.02	215.63	0.03	217.71	0.10	219.79	14.69
213.59	0.02	215.67	0.03	217.75	0.12	219.83	14.73
213.63	0.02	215.71	0.03	217.79	0.13	219.87	14.77
213.67	0.02	215.75	0.03	217.83	0.14	219.91	14.81
213.71	0.02	215.79	0.03	217.87	0.15	219.95	14.85
213.75	0.02	215.83	0.03	217.91	0.16	219.99	14.89
213.79	0.02	215.87	0.03	217.95	0.17		

Elevation 216.47' =
0.03 CFS discharge

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

Printed 6/17/2021

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Stage-Area-Storage for Pond 106P: Rain Garden #106

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
211.75	0	0	216.95	391	2,291
211.85	0	16	217.05	391	2,453
211.95	0	31	217.15	391	2,605
212.05	0	47	217.25	391	2,768
212.15	0	63	217.35	391	2,944
212.25	0	78	217.45	391	3,132
212.35	0	94	217.55	391	3,333
212.45	0	109	217.65	391	3,548
212.55	0	125	217.75	391	3,777
212.65	0	141	217.85	391	4,020
212.75	391	156	217.95	391	4,277
212.85	391	164	218.05	391	4,549
212.95	391	172	218.15	391	4,830
213.05	391	180	218.25	391	5,117
213.15	391	188	218.35	391	5,412
213.25	391	196	218.45	391	5,715
213.35	391	203	218.55	391	6,025
213.45	391	211	218.65	391	6,343
213.55	391	219	218.75	391	6,669
213.65	391	227	218.85	391	7,003
213.75	391	235	218.95	391	7,344
213.85	391	242	219.05	391	7,694
213.95	391	250	219.15	391	8,055
214.05	391	258	219.25	391	8,426
214.15	391	266	219.35	391	8,809
214.25	391	274	219.45	391	9,203
214.35	391	282	219.55	391	9,608
214.45	391	289	219.65	391	10,024
214.55	391	297	219.75	391	10,453
214.65	391	305	219.85	391	10,893
214.75	391	313	219.95	391	11,345
214.85	391	321			
214.95	391	328			
215.05	391	358			
215.15	391	411			
215.25	391	468			
215.35	391	528			
215.45	391	593			
215.55	391	662			
215.65	391	735			
215.75	391	813			
215.85	391	895			
215.95	391	982			
216.05	391	1,075			
216.15	391	1,174			
216.25	391	1,282			
216.35	391	1,398			
216.45	391	1,523			
216.55	391	1,657			
216.65	391	1,801			
216.75	391	1,954			
216.85	391	2,117			

Linear Interpolation
 Lowest Orifice = 217.50'
 Storage Volume = 3,077 CF



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name: _____

Rain Garden #107 W/ Infiltration

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

Yes		Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.07(a).	
4.47	ac	A = Area draining to the practice	
0.77	ac	A _I = Impervious area draining to the practice	
0.17	decimal	l = Percent impervious area draining to the practice, in decimal form	
0.20	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x l)	
0.91	ac-in	WQV = 1" x Rv x A	
3,315	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
829	cf	25% x WQV (check calc for sediment forebay volume)	
2,486	cf	75% x WQV (check calc for surface sand filter volume)	
Sediment Forebay (2) Method of Pretreatment? (not required for clean or roof runoff)			
641, 7143	cf	V _{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
Calculate time to drain if system IS NOT underdrained:			
2,135	sf	A _{SA} = Surface area of the practice	
0.30	iph	K _{sat} _{DESIGN} = Design infiltration rate ¹	
		If K _{sat} (prior to factor of safety) is < 0.50 iph, has an underdrain been provided? (Use the calculations below)	
N/A	Yes/No		
62.1	hours	T _{DRAIN} = Drain time = V / (A _{SA} * I _{DESIGN})	≤ 72-hrs
Calculate time to drain if system IS underdrained:			
N/A	ft	E _{WQV} = Elevation of WQV (attach stage-storage table)	
N/A	cfs	Q _{WQV} = Discharge at the E _{WQV} (attach stage-discharge table)	
-	hours	T _{DRAIN} = Drain time = 2WQV/Q _{WQV}	≤ 72-hrs
223.75	feet	E _{FC} = Elevation of the bottom of the filter course material ²	
N/A	feet	E _{UD} = Invert elevation of the underdrain (UD), if applicable	
221.23	feet	E _{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test pit)	
221.23	feet	E _{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test pit)	
#VALUE!	feet	D _{FC to UD} = Depth to UD from the bottom of the filter course	≥ 1'
2.52	feet	D _{FC to ROCK} = Depth to bedrock from the bottom of the filter course	≥ 1'
2.52	feet	D _{FC to SHWT} = Depth to SHWT from the bottom of the filter course	≥ 1'
229.57	ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
230.00	ft	Elevation of the top of the practice	
YES		50 peak elevation ≤ Elevation of the top of the practice	← yes
If a surface sand filter or underground sand filter is proposed:			
YES	ac	Drainage Area check.	< 10 ac
	cf	V = Volume of storage ³ (attach a stage-storage table)	≥ 75%WQV
	inches	D _{FC} = Filter course thickness	18", or 24" if within GPA
Sheet		Note what sheet in the plan set contains the filter course specification.	
	Yes/No	Access grate provided?	← yes

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

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Summary for Pond 107P: Rain Garden #107

Inflow Area = 4.467 ac, 17.16% Impervious, Inflow Depth > 2.99" for 50YR - 24HR event
 Inflow = 9.41 cfs @ 12.17 hrs, Volume= 1.112 af
 Outflow = 2.08 cfs @ 13.04 hrs, Volume= 0.741 af, Atten= 78%, Lag= 51.9 min
 Discarded = 0.01 cfs @ 9.45 hrs, Volume= 0.018 af
 Primary = 1.59 cfs @ 13.04 hrs, Volume= 0.698 af
 Secondary = 0.48 cfs @ 13.04 hrs, Volume= 0.026 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 229.57' @ 13.04 hrs Surf.Area= 2,135 sf Storage= 24,359 cf
 Flood Elev= 230.00' Surf.Area= 2,135 sf Storage= 28,192 cf

Plug-Flow detention time= 283.0 min calculated for 0.740 af (67% of inflow)
 Center-of-Mass det. time= 177.9 min (1,019.3 - 841.4)

Volume	Invert	Avail.Storage	Storage Description
#1	222.75'	854 cf	Stone (Irregular) Listed below (Recalc) -Impervious 2,135 cf Overall x 40.0% Voids
#2	223.75'	854 cf	Bio-media (Irregular) Listed below (Recalc) 4,270 cf Overall x 20.0% Voids
#3	225.75'	107 cf	Loam (Irregular) Listed below (Recalc) -Impervious 534 cf Overall x 20.0% Voids
#4	226.00'	16,356 cf	Infiltration Cell Storage (Irregular) Listed below (Recalc) -Impervious
#5	229.00'	8,667 cf	Open Water Storage (Irregular) Listed below (Recalc) -Impervious
#6	227.00'	641 cf	Sediment Forebay #1 (Irregular) Listed below (Recalc) -Impervious
#7	227.00'	714 cf	Sediment Forebay #2 (Irregular) Listed below (Recalc) -Impervious
		28,192 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
222.75	2,135	177.0	0	0	2,135
223.75	2,135	177.0	2,135	2,135	2,312

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
223.75	2,135	177.0	0	0	2,135
225.75	2,135	177.0	4,270	4,270	2,489

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
225.75	2,135	177.0	0	0	2,135
226.00	2,135	177.0	534	534	2,179

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
226.00	3,961	245.8	0	0	3,961
227.00	5,137	273.0	4,536	4,536	5,114
228.00	5,903	291.7	5,516	10,052	6,000
229.00	6,715	310.3	6,305	16,356	6,941

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
229.00	8,122	357.5	0	0	8,122
230.00	9,223	376.4	8,667	8,667	9,285

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
227.00	115	41.3	0	0	115
228.00	312	74.3	205	205	424
229.00	571	103.5	435	641	847

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
227.00	144	49.8	0	0	144
228.00	345	81.0	237	237	475
229.00	622	111.6	477	714	954

Device	Routing	Invert	Outlet Devices
#1	Primary	223.50'	15.0" Round 15" HDPE N-12 L= 20.0' Ke= 0.500 Inlet / Outlet Invert= 223.50' / 223.00' S= 0.0250 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Discarded	223.75'	0.300 in/hr Exfiltration over Surface area
#3	Device 1	227.50'	3.0" Vert. 3" Orifice X 2.00 C= 0.600
#4	Device 1	229.40'	15.0" Horiz. 15" Horizontal Orifice C= 0.600 Limited to weir flow at low heads
#5	Secondary	229.50'	10.0' long x 7.0' breadth 10' Emergency Spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65 2.65 2.66 2.65 2.66 2.68 2.70 2.73 2.78

Discarded OutFlow Max=0.01 cfs @ 9.45 hrs HW=223.79' (Free Discharge)
 ↳ **2=Exfiltration** (Exfiltration Controls 0.01 cfs)

Primary OutFlow Max=1.58 cfs @ 13.04 hrs HW=229.57' TW=223.25' (Dynamic Tailwater)
 ↳ **1=15" HDPE N-12** (Passes 1.58 cfs of 13.79 cfs potential flow)
 ↳ **3=3" Orifice** (Orifice Controls 0.66 cfs @ 6.72 fps)
 ↳ **4=15" Horizontal Orifice** (Weir Controls 0.92 cfs @ 1.36 fps)

Secondary OutFlow Max=0.47 cfs @ 13.04 hrs HW=229.57' TW=223.25' (Dynamic Tailwater)
 ↳ **5=10' Emergency Spillway** (Weir Controls 0.47 cfs @ 0.65 fps)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Area-Storage for Pond 107P: Rain Garden #107

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
222.75	0	0	227.95	2,135	11,983
222.85	0	85	228.05	2,135	12,639
222.95	0	171	228.15	2,135	13,307
223.05	0	256	228.25	2,135	13,989
223.15	0	342	228.35	2,135	14,683
223.25	0	427	228.45	2,135	15,390
223.35	0	512	228.55	2,135	16,111
223.45	0	598	228.65	2,135	16,845
223.55	0	683	228.75	2,135	17,594
223.65	0	769	228.85	2,135	18,356
223.75	2,135	854	228.95	2,135	19,132
223.85	2,135	897	229.05	2,135	19,933
223.95	2,135	939	229.15	2,135	20,756
224.05	2,135	982	229.25	2,135	21,590
224.15	2,135	1,025	229.35	2,135	22,434
224.25	2,135	1,068	229.45	2,135	23,290
224.35	2,135	1,110	229.55	2,135	24,156
224.45	2,135	1,153	229.65	2,135	25,033
224.55	2,135	1,196	229.75	2,135	25,922
224.65	2,135	1,238	229.85	2,135	26,822
224.75	2,135	1,281	229.95	2,135	27,733
224.85	2,135	1,324			
224.95	2,135	1,366			
225.05	2,135	1,409			
225.15	2,135	1,452			
225.25	2,135	1,495			
225.35	2,135	1,537			
225.45	2,135	1,580			
225.55	2,135	1,623			
225.65	2,135	1,665			
225.75	2,135	1,708			
225.85	2,135	1,751			
225.95	2,135	1,793			
226.05	2,135	2,014			
226.15	2,135	2,421			
226.25	2,135	2,840			
226.35	2,135	3,270			
226.45	2,135	3,711			
226.55	2,135	4,164			
226.65	2,135	4,629			
226.75	2,135	5,106			
226.85	2,135	5,594			
226.95	2,135	6,096			
227.05	2,135	6,622			
227.15	2,135	7,172			
227.25	2,135	7,733			
227.35	2,135	8,305			
227.45	2,135	8,889			
227.55	2,135	9,484			
227.65	2,135	10,090			
227.75	2,135	10,709			
227.85	2,135	11,340			

Linear Interpolation

Lowest Orifice = 227.50'

Storage Volume =

$$9,187 \text{ CF} - 854 \text{ CF} = 8,332 \text{ CF}$$



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name: _____

Rain Garden #108

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

Yes	Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.07(a).	
0.17 ac	A = Area draining to the practice	
0.08 ac	A_i = Impervious area draining to the practice	
0.46 decimal	l = Percent impervious area draining to the practice, in decimal form	
0.46 unitless	R_v = Runoff coefficient = $0.05 + (0.9 \times l)$	
0.08 ac-in	WQV = 1" x R_v x A	
288 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
72 cf	25% x WQV (check calc for sediment forebay volume)	
216 cf	75% x WQV (check calc for surface sand filter volume)	
Sediment Forebay	Method of Pretreatment? (not required for clean or roof runoff)	
72 cf	V_{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
Calculate time to drain if system IS NOT underdrained:		
N/A sf	A_{SA} = Surface area of the practice	
N/A iph	$K_{SAT_{DESIGN}}$ = Design infiltration rate ¹	
N/A Yes/No	If K_{SAT} (prior to factor of safety) is < 0.50 iph, has an underdrain been provided? (Use the calculations below)	
- hours	T_{DRAIN} = Drain time = $V / (A_{SA} * I_{DESIGN})$	≤ 72-hrs
Calculate time to drain if system IS underdrained:		
205.82 ft	E_{WQV} = Elevation of WQV (attach stage-storage table)	
0.02 cfs	Q_{WQV} = Discharge at the E_{WQV} (attach stage-discharge table)	
7.99 hours	T_{DRAIN} = Drain time = $2WQV/Q_{WQV}$	≤ 72-hrs
203.50 feet	E_{FC} = Elevation of the bottom of the filter course material ²	
202.50 feet	E_{UD} = Invert elevation of the underdrain (UD), if applicable	
199.42 feet	E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test pit)	
199.42 feet	E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test pit)	
1.00 feet	$D_{FC\ to\ UD}$ = Depth to UD from the bottom of the filter course	≥ 1'
4.08 feet	$D_{FC\ to\ ROCK}$ = Depth to bedrock from the bottom of the filter course	≥ 1'
4.08 feet	$D_{FC\ to\ SHWT}$ = Depth to SHWT from the bottom of the filter course	≥ 1'
206.55 ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
207.00 ft	Elevation of the top of the practice	
YES	50 peak elevation ≤ Elevation of the top of the practice	← yes
If a surface sand filter or underground sand filter is proposed:		
YES ac	Drainage Area check.	< 10 ac
cf	V = Volume of storage ³ (attach a stage-storage table)	≥ 75%WQV
inches	D_{FC} = Filter course thickness	18", or 24" if within GPA
Sheet	Note what sheet in the plan set contains the filter course specification.	
Yes/No	Access grate provided?	← yes

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

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Summary for Pond 108P: Rain Garden #108

Inflow Area = 0.171 ac, 45.91% Impervious, Inflow Depth > 4.47" for 50YR - 24HR event
 Inflow = 0.87 cfs @ 12.09 hrs, Volume= 0.064 af
 Outflow = 0.26 cfs @ 12.45 hrs, Volume= 0.040 af, Atten= 70%, Lag= 21.4 min
 Primary = 0.02 cfs @ 18.76 hrs, Volume= 0.025 af
 Secondary = 0.24 cfs @ 12.45 hrs, Volume= 0.015 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 206.55' @ 12.45 hrs Surf.Area= 530 sf Storage= 1,362 cf
 Flood Elev= 207.00' Surf.Area= 530 sf Storage= 2,072 cf

Plug-Flow detention time= 258.2 min calculated for 0.040 af (62% of inflow)
 Center-of-Mass det. time= 156.6 min (968.9 - 812.3)

Volume	Invert	Avail.Storage	Storage Description
#1	202.50'	212 cf	Stone (Irregular) Listed below (Recalc) -Impervious 530 cf Overall x 40.0% Voids
#2	203.50'	212 cf	Bio-media (Irregular) Listed below (Recalc) 1,060 cf Overall x 20.0% Voids
#3	205.50'	27 cf	Loam (Irregular) Listed below (Recalc) -Impervious 133 cf Overall x 20.0% Voids
#4	205.75'	1,550 cf	Open Water Storage (Irregular) Listed below (Recalc) -Impervious
#5	205.75'	72 cf	Forebay (Irregular) Listed below (Recalc) -Impervious
		2,072 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
202.50	530	89.7	0	0	530
203.50	530	89.7	530	530	620

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
203.50	530	89.7	0	0	530
205.50	530	89.7	1,060	1,060	709

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
205.50	530	89.7	0	0	530
205.75	530	89.7	133	133	552

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
205.75	530	89.7	0	0	530
206.00	1,050	140.4	194	194	1,459
206.50	1,297	161.2	586	779	1,964
207.00	1,800	205.6	771	1,550	3,263

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
205.75	62	28.3	0	0	62
206.00	83	32.5	18	18	84
206.50	133	41.4	54	72	139

Device	Routing	Invert	Outlet Devices
#1	Primary	202.50'	6.0" Round 6" HDPE N-12 UD L= 22.5' Ke= 0.500 Inlet / Outlet Invert= 202.50' / 202.25' S= 0.0111 '/' Cc= 0.900 n= 0.012, Flow Area= 0.20 sf
#2	Device 1	202.50'	0.7" Vert. 0.75" Orifice C= 0.600
#3	Device 2	203.50'	10.000 in/hr Exfiltration over Surface area
#4	Device 2	206.40'	24.0" Horiz. 24" Drop Inlet C= 0.600 Limited to weir flow at low heads
#5	Secondary	206.50'	10.0' long x 7.0' breadth 10' Emergency spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65 2.65 2.66 2.65 2.66 2.68 2.70 2.73 2.78

Primary OutFlow Max=0.02 cfs @ 18.76 hrs HW=206.48' TW=202.84' (Dynamic Tailwater)

↑ **1=6" HDPE N-12 UD** (Passes 0.02 cfs of 1.73 cfs potential flow)

↑ **2=0.75" Orifice** (Orifice Controls 0.02 cfs @ 9.18 fps)

↑ **3=Exfiltration** (Passes < 0.12 cfs potential flow)

↑ **4=24" Drop Inlet** (Passes < 0.43 cfs potential flow)

Secondary OutFlow Max=0.24 cfs @ 12.45 hrs HW=206.55' TW=203.82' (Dynamic Tailwater)

↑ **5=10' Emergency spillway** (Weir Controls 0.24 cfs @ 0.51 fps)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Area-Storage for Pond 108P: Rain Garden #108

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
202.50	0	0	205.10	530	382
202.55	0	11	205.15	530	387
202.60	0	21	205.20	530	392
202.65	0	32	205.25	530	398
202.70	0	42	205.30	530	403
202.75	0	53	205.35	530	408
202.80	0	64	205.40	530	413
202.85	0	74	205.45	530	419
202.90	0	85	205.50	530	424
202.95	0	95	205.55	530	429
203.00	0	106	205.60	530	435
203.05	0	117	205.65	530	440
203.10	0	127	205.70	530	445
203.15	0	138	205.75	530	451
203.20	0	148	<u>205.80</u>	<u>530</u>	<u>482</u>
203.25	0	159	205.85	530	519
203.30	0	170	205.90	530	561
203.35	0	180	205.95	530	609
203.40	0	191	206.00	530	662
203.45	0	201	206.05	530	720
<u>203.50</u>	<u>530</u>	<u>212</u>	206.10	530	778
203.55	530	217	206.15	530	839
203.60	530	223	206.20	530	900
203.65	530	228	206.25	530	963
203.70	530	233	206.30	530	1,028
203.75	530	239	206.35	530	1,094
203.80	530	244	206.40	530	1,162
203.85	530	249	206.45	530	1,231
203.90	530	254	206.50	530	1,302
203.95	530	260	206.55	530	1,368
204.00	530	265	206.60	530	1,436
204.05	530	270	206.65	530	1,507
204.10	530	276	206.70	530	1,580
204.15	530	281	206.75	530	1,656
204.20	530	286	206.80	530	1,734
204.25	530	292	206.85	530	1,814
204.30	530	297	206.90	530	1,898
204.35	530	302	206.95	530	1,984
204.40	530	307	207.00	530	2,072
204.45	530	313			
204.50	530	318			
204.55	530	323			
204.60	530	329			
204.65	530	334			
204.70	530	339			
204.75	530	345			
204.80	530	350			
204.85	530	355			
204.90	530	360			
204.95	530	366			
205.00	530	371			
205.05	530	376			

WQV Draw-down
 Linear Interpolation
 288 CF Storage above
 stone = 205.82'

500 CF - 212 CF = 288 CF

See next Stage-Area-Storage Table
 for storage volume

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Discharge for Pond 108P: Rain Garden #108

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
202.50	0.00	0.00	0.00	205.10	0.02	0.02	0.00
202.55	0.00	0.00	0.00	205.15	0.02	0.02	0.00
202.60	0.00	0.00	0.00	205.20	0.02	0.02	0.00
202.65	0.00	0.00	0.00	205.25	0.02	0.02	0.00
202.70	0.00	0.00	0.00	205.30	0.02	0.02	0.00
202.75	0.00	0.00	0.00	205.35	0.02	0.02	0.00
202.80	0.00	0.00	0.00	205.40	0.02	0.02	0.00
202.85	0.00	0.00	0.00	205.45	0.02	0.02	0.00
202.90	0.00	0.00	0.00	205.50	0.02	0.02	0.00
202.95	0.00	0.00	0.00	205.55	0.02	0.02	0.00
203.00	0.00	0.00	0.00	205.60	0.02	0.02	0.00
203.05	0.00	0.00	0.00	205.65	0.02	0.02	0.00
203.10	0.00	0.00	0.00	205.70	0.02	0.02	0.00
203.15	0.00	0.00	0.00	205.75	0.02	0.02	0.00
203.20	0.00	0.00	0.00	<u>205.80</u>	<u>0.02</u>	<u>0.02</u>	<u>0.00</u>
203.25	0.00	0.00	0.00	205.85	0.02	0.02	0.00
203.30	0.00	0.00	0.00	205.90	0.02	0.02	0.00
203.35	0.00	0.00	0.00	205.95	0.02	0.02	0.00
203.40	0.00	0.00	0.00	206.00	0.02	0.02	0.00
203.45	0.00	0.00	0.00	206.05	0.02	0.02	0.00
203.50	0.01	0.01	0.00	206.10	0.02	0.02	0.00
203.55	0.01	0.01	0.00	206.15	0.02	0.02	0.00
203.60	0.01	0.01	0.00	206.20	0.02	0.02	0.00
203.65	0.01	0.01	0.00	206.25	0.02	0.02	0.00
203.70	0.01	0.01	0.00	206.30	0.02	0.02	0.00
203.75	0.01	0.01	0.00	206.35	0.03	0.03	0.00
203.80	0.01	0.01	0.00	206.40	0.03	0.03	0.00
203.85	0.01	0.01	0.00	206.45	0.03	0.03	0.00
203.90	0.02	0.02	0.00	206.50	0.03	0.03	0.00
203.95	0.02	0.02	0.00	206.55	0.29	0.03	0.27
204.00	0.02	0.02	0.00	206.60	0.78	0.03	0.76
204.05	0.02	0.02	0.00	206.65	1.42	0.03	1.39
204.10	0.02	0.02	0.00	206.70	2.17	0.03	2.15
204.15	0.02	0.02	0.00	206.75	3.06	0.03	3.04
204.20	0.02	0.02	0.00	206.80	4.07	0.03	4.04
204.25	0.02	0.02	0.00	206.85	5.18	0.03	5.16
204.30	0.02	0.02	0.00	206.90	6.40	0.03	6.38
204.35	0.02	0.02	0.00	206.95	7.77	0.03	7.74
204.40	0.02	0.02	0.00	207.00	9.25	0.03	9.23
204.45	0.02	0.02	0.00				
204.50	0.02	0.02	0.00				
204.55	0.02	0.02	0.00				
204.60	0.02	0.02	0.00				
204.65	0.02	0.02	0.00				
204.70	0.02	0.02	0.00				
204.75	0.02	0.02	0.00				
204.80	0.02	0.02	0.00				
204.85	0.02	0.02	0.00				
204.90	0.02	0.02	0.00				
204.95	0.02	0.02	0.00				
205.00	0.02	0.02	0.00				
205.05	0.02	0.02	0.00				

Elevation 205.82' =
0.02 CFS discharge

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Area-Storage for Pond 108P: Rain Garden #108

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
202.50	0	0	205.10	530	382
202.55	0	11	205.15	530	387
202.60	0	21	205.20	530	392
202.65	0	32	205.25	530	398
202.70	0	42	205.30	530	403
202.75	0	53	205.35	530	408
202.80	0	64	205.40	530	413
202.85	0	74	205.45	530	419
202.90	0	85	205.50	530	424
202.95	0	95	205.55	530	429
203.00	0	106	205.60	530	435
203.05	0	117	205.65	530	440
203.10	0	127	205.70	530	445
203.15	0	138	205.75	530	451
203.20	0	148	205.80	530	482
203.25	0	159	205.85	530	519
203.30	0	170	205.90	530	561
203.35	0	180	205.95	530	609
203.40	0	191	206.00	530	662
203.45	0	201	206.05	530	720
203.50	530	212	206.10	530	778
203.55	530	217	206.15	530	839
203.60	530	223	206.20	530	900
203.65	530	228	206.25	530	963
203.70	530	233	206.30	530	1,028
203.75	530	239	206.35	530	1,094
203.80	530	244	206.40	530	1,162
203.85	530	249	206.45	530	1,231
203.90	530	254	206.50	530	1,302
203.95	530	260	206.55	530	1,368
204.00	530	265	206.60	530	1,436
204.05	530	270	206.65	530	1,507
204.10	530	276	206.70	530	1,580
204.15	530	281	206.75	530	1,656
204.20	530	286	206.80	530	1,734
204.25	530	292	206.85	530	1,814
204.30	530	297	206.90	530	1,898
204.35	530	302	206.95	530	1,984
204.40	530	307	207.00	530	2,072
204.45	530	313			
204.50	530	318			
204.55	530	323			
204.60	530	329			
204.65	530	334			
204.70	530	339			
204.75	530	345			
204.80	530	350			
204.85	530	355			
204.90	530	360			
204.95	530	366			
205.00	530	371			
205.05	530	376			

Linear Interpolation
 Lowest Orifice = 206.40'
 Storage Volume = 950 CF

 1,162 CF - 212CF = 950 CF



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name: _____

Rain Garden #109

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

Yes		Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.07(a).	
1.89	ac	A = Area draining to the practice	
-	ac	A _i = Impervious area draining to the practice	
-	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.05	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
0.09	ac-in	WQV = 1" x Rv x A	
343	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
86	cf	25% x WQV (check calc for sediment forebay volume)	
257	cf	75% x WQV (check calc for surface sand filter volume)	
No treatment req		Method of Pretreatment? (not required for clean or roof runoff)	
N/A	cf	V _{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
Calculate time to drain if system IS NOT underdrained:			
N/A	sf	A _{SA} = Surface area of the practice	
N/A	iph	K _{sat} _{DESIGN} = Design infiltration rate ¹	
N/A	Yes/No	If K _{sat} (prior to factor of safety) is < 0.50 iph, has an underdrain been provided? (Use the calculations below)	
-	hours	T _{DRAIN} = Drain time = V / (A _{SA} * I _{DESIGN})	≤ 72-hrs
Calculate time to drain if system IS underdrained:			
214.01	ft	E _{WQV} = Elevation of WQV (attach stage-storage table)	
0.05	cfs	Q _{WQV} = Discharge at the E _{WQV} (attach stage-discharge table)	
3.81	hours	T _{DRAIN} = Drain time = 2WQV/Q _{WQV}	≤ 72-hrs
211.75	feet	E _{FC} = Elevation of the bottom of the filter course material ²	
210.75	feet	E _{UD} = Invert elevation of the underdrain (UD), if applicable	
211.67	feet	E _{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test pit)	
210.17	feet	E _{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test pit)	
1.00	feet	D _{FC to UD} = Depth to UD from the bottom of the filter course	≥ 1'
1.58	feet	D _{FC to ROCK} = Depth to bedrock from the bottom of the filter course	≥ 1'
0.08	feet	D _{FC to SHWT} = Depth to SHWT from the bottom of the filter course	≥ 1'
217.91	ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
218.50	ft	Elevation of the top of the practice	
YES		50 peak elevation ≤ Elevation of the top of the practice	← yes
If a surface sand filter or underground sand filter is proposed:			
YES	ac	Drainage Area check.	< 10 ac
	cf	V = Volume of storage ³ (attach a stage-storage table)	≥ 75%WQV
	inches	D _{FC} = Filter course thickness	18", or 24" if within GPA
Sheet		Note what sheet in the plan set contains the filter course specification.	
Yes/No		Access grate provided?	← yes

If a bioretention area is proposed:			
YES	ac	Drainage Area no larger than 5 ac?	← yes
871	cf	V = Volume of storage ³ (attach a stage-storage table)	≥ WQV
24.0	inches	D _{FC} = Filter course thickness	18", or 24" if within GPA
Sheet	P-109	Note what sheet in the plan set contains the filter course specification	
3.0	:1	Pond side slopes	> 3:1
Sheet	P-109	Note what sheet in the plan set contains the planting plans and surface cover	
If porous pavement is proposed:			
	acres	Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
		A _{SA} = Surface area of the pervious pavement	
	:1	Ratio of the contributing area to the pervious surface area	≤ 5:1
	inches	D _{FC} = Filter course thickness	12", or 18" if within GPA
Sheet		Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)

1. Rate of the limiting layer (either the filter course or the underlying soil). $K_{sat_{design}}$ includes factor of safety. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
2. See lines 34, 40 and 48 for required depths of filter media.
3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet structure, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes: Rain Garden #107 is disconnected from Rain Garden #109 for WQV purposes due to RG #107 infiltrating the 2 YR -24 HR event.

KAB/KRP

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

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Summary for Pond 109P: Rain Garden #109

Inflow Area = 6.279 ac, 12.21% Impervious, Inflow Depth > 2.16" for 50YR - 24HR event
 Inflow = 4.46 cfs @ 12.22 hrs, Volume= 1.129 af
 Outflow = 2.76 cfs @ 13.06 hrs, Volume= 0.980 af, Atten= 38%, Lag= 49.9 min
 Primary = 2.76 cfs @ 13.06 hrs, Volume= 0.980 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 217.90' @ 13.06 hrs Surf.Area= 719 sf Storage= 6,836 cf
 Flood Elev= 218.50' Surf.Area= 719 sf Storage= 8,532 cf

Plug-Flow detention time= 96.1 min calculated for 0.980 af (87% of inflow)
 Center-of-Mass det. time= 37.3 min (999.0 - 961.7)

Volume	Invert	Avail.Storage	Storage Description
#1	210.75'	288 cf	Stone (Irregular) Listed below (Recalc) -Impervious 719 cf Overall x 40.0% Voids
#2	211.75'	288 cf	Bio Media (Irregular) Listed below (Recalc) 1,438 cf Overall x 20.0% Voids
#3	213.75'	36 cf	Loam (Irregular) Listed below (Recalc) -Impervious 180 cf Overall x 20.0% Voids
#4	214.00'	7,920 cf	Open Water Storage (Irregular) Listed below (Recalc) -Impervious
		8,532 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
210.75	719	114.5	0	0	719
211.75	719	114.5	719	719	834

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
211.75	719	114.5	0	0	719
213.75	719	114.5	1,438	1,438	948

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
213.75	719	114.5	0	0	719
214.00	719	114.5	180	180	748

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
214.00	719	114.5	0	0	719
215.00	1,126	139.0	915	915	1,229
216.00	1,591	160.5	1,352	2,267	1,763
217.00	2,111	181.1	1,845	4,112	2,349
218.00	2,683	199.5	2,391	6,503	2,937
218.50	2,990	209.1	1,418	7,920	3,266

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Device	Routing	Invert	Outlet Devices
#1	Primary	210.75'	15.0" Round 15" HDPE N-12 L= 33.0' Ke= 0.500 Inlet / Outlet Invert= 210.75' / 209.00' S= 0.0530 '/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf
#2	Device 1	210.75'	1.0" Vert. 1" Orifice C= 0.600
#3	Device 2	211.75'	10.000 in/hr Exfiltration Through Media over Surface area
#4	Device 1	214.65'	3.0" Vert. 3" Orifice C= 0.600
#5	Device 1	217.75'	48.0" Horiz. 48" Structure C= 0.600 Limited to weir flow at low heads
#6	Secondary	218.00'	10.0' long x 7.0' breadth 10' Emergency Spillway Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65 2.65 2.66 2.65 2.66 2.68 2.70 2.73 2.78

Primary OutFlow Max=2.76 cfs @ 13.06 hrs HW=217.90' TW=208.18' (Dynamic Tailwater)

- ↑ 1=15" HDPE N-12 (Passes 2.76 cfs of 15.09 cfs potential flow)
 - ↑ 2=1" Orifice (Orifice Controls 0.07 cfs @ 12.83 fps)
 - ↑ 3=Exfiltration Through Media (Passes 0.07 cfs of 0.17 cfs potential flow)
 - ↑ 4=3" Orifice (Orifice Controls 0.42 cfs @ 8.50 fps)
 - ↑ 5=48" Structure (Weir Controls 2.27 cfs @ 1.25 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=210.75' TW=208.00' (Dynamic Tailwater)

- ↑ 6=10' Emergency Spillway (Controls 0.00 cfs)

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Area-Storage for Pond 109P: Rain Garden #109

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
210.75	0	0	215.95	719	2,799
210.85	0	29	216.05	719	2,958
210.95	0	58	216.15	719	3,122
211.05	0	86	216.25	719	3,291
211.15	0	115	216.35	719	3,465
211.25	0	144	216.45	719	3,644
211.35	0	173	216.55	719	3,828
211.45	0	201	216.65	719	4,018
211.55	0	230	216.75	719	4,212
211.65	0	259	216.85	719	4,412
211.75	719	288	216.95	719	4,618
211.85	719	302	217.05	719	4,829
211.95	719	316	217.15	719	5,046
212.05	719	331	217.25	719	5,268
212.15	719	345	217.35	719	5,495
212.25	719	360	217.45	719	5,728
212.35	719	374	217.55	719	5,967
212.45	719	388	217.65	719	6,212
212.55	719	403	217.75	719	6,462
212.65	719	417	217.85	719	6,718
212.75	719	431	217.95	719	6,981
212.85	719	446	218.05	719	7,249
212.95	719	460	218.15	719	7,523
213.05	719	475	218.25	719	7,804
213.15	719	489	218.35	719	8,090
213.25	719	503	218.45	719	8,383
213.35	719	518			
213.45	719	532			
213.55	719	546			
213.65	719	561			
213.75	719	575			
213.85	719	590			
213.95	719	604			
214.05	719	648			
214.15	719	723			
214.25	719	802			
214.35	719	886			
214.45	719	973			
214.55	719	1,064			
214.65	719	1,159			
214.75	719	1,258			
214.85	719	1,362			
214.95	719	1,470			
215.05	719	1,583			
215.15	719	1,700			
215.25	719	1,821			
215.35	719	1,947			
215.45	719	2,077			
215.55	719	2,212			
215.65	719	2,351			
215.75	719	2,496			
215.85	719	2,645			

WQV Draw-down
 Linear Interpolation
 343 CF Storage above
 stone = 214.01'

631 CF - 288 CF = 343 CF

See next Stage-Area-Storage Table
 for storage volume

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

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Stage-Discharge for Pond 109P: Rain Garden #109

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
210.75	0.00	0.00	0.00	215.95	0.32	0.32	0.00
210.85	0.00	0.00	0.00	216.05	0.33	0.33	0.00
210.95	0.00	0.00	0.00	216.15	0.34	0.34	0.00
211.05	0.00	0.00	0.00	216.25	0.35	0.35	0.00
211.15	0.00	0.00	0.00	216.35	0.36	0.36	0.00
211.25	0.00	0.00	0.00	216.45	0.37	0.37	0.00
211.35	0.00	0.00	0.00	216.55	0.38	0.38	0.00
211.45	0.00	0.00	0.00	216.65	0.39	0.39	0.00
211.55	0.00	0.00	0.00	216.75	0.40	0.40	0.00
211.65	0.00	0.00	0.00	216.85	0.41	0.41	0.00
211.75	0.03	0.03	0.00	216.95	0.41	0.41	0.00
211.85	0.03	0.03	0.00	217.05	0.42	0.42	0.00
211.95	0.03	0.03	0.00	217.15	0.43	0.43	0.00
212.05	0.03	0.03	0.00	217.25	0.44	0.44	0.00
212.15	0.03	0.03	0.00	217.35	0.45	0.45	0.00
212.25	0.03	0.03	0.00	217.45	0.45	0.45	0.00
212.35	0.03	0.03	0.00	217.55	0.46	0.46	0.00
212.45	0.03	0.03	0.00	217.65	0.47	0.47	0.00
212.55	0.03	0.03	0.00	217.75	0.48	0.48	0.00
212.65	0.04	0.04	0.00	217.85	1.78	1.78	0.00
212.75	0.04	0.04	0.00	217.95	4.17	4.17	0.00
212.85	0.04	0.04	0.00	218.05	7.52	7.25	0.27
212.95	0.04	0.04	0.00	218.15	12.30	10.90	1.39
213.05	0.04	0.04	0.00	218.25	18.08	15.04	3.04
213.15	0.04	0.04	0.00	218.35	20.76	15.61	5.16
213.25	0.04	0.04	0.00	218.45	23.46	15.72	7.74
213.35	0.04	0.04	0.00				
213.45	0.04	0.04	0.00				
213.55	0.04	0.04	0.00				
213.65	0.04	0.04	0.00				
213.75	0.05	0.05	0.00				
213.85	0.05	0.05	0.00				
213.95	0.05	0.05	0.00				
214.05	0.05	0.05	0.00				
214.15	0.05	0.05	0.00				
214.25	0.05	0.05	0.00				
214.35	0.05	0.05	0.00				
214.45	0.05	0.05	0.00				
214.55	0.05	0.05	0.00				
214.65	0.05	0.05	0.00				
214.75	0.07	0.07	0.00				
214.85	0.12	0.12	0.00				
214.95	0.15	0.15	0.00				
215.05	0.18	0.18	0.00				
215.15	0.20	0.20	0.00				
215.25	0.22	0.22	0.00				
215.35	0.24	0.24	0.00				
215.45	0.25	0.25	0.00				
215.55	0.27	0.27	0.00				
215.65	0.28	0.28	0.00				
215.75	0.29	0.29	0.00				
215.85	0.30	0.30	0.00				

Elevation 214.01' =
0.05 CFS discharge

20-097 Proposed Analysis

Type III 24-hr 50YR - 24HR Rainfall=7.00"

Prepared by {enter your company name here}

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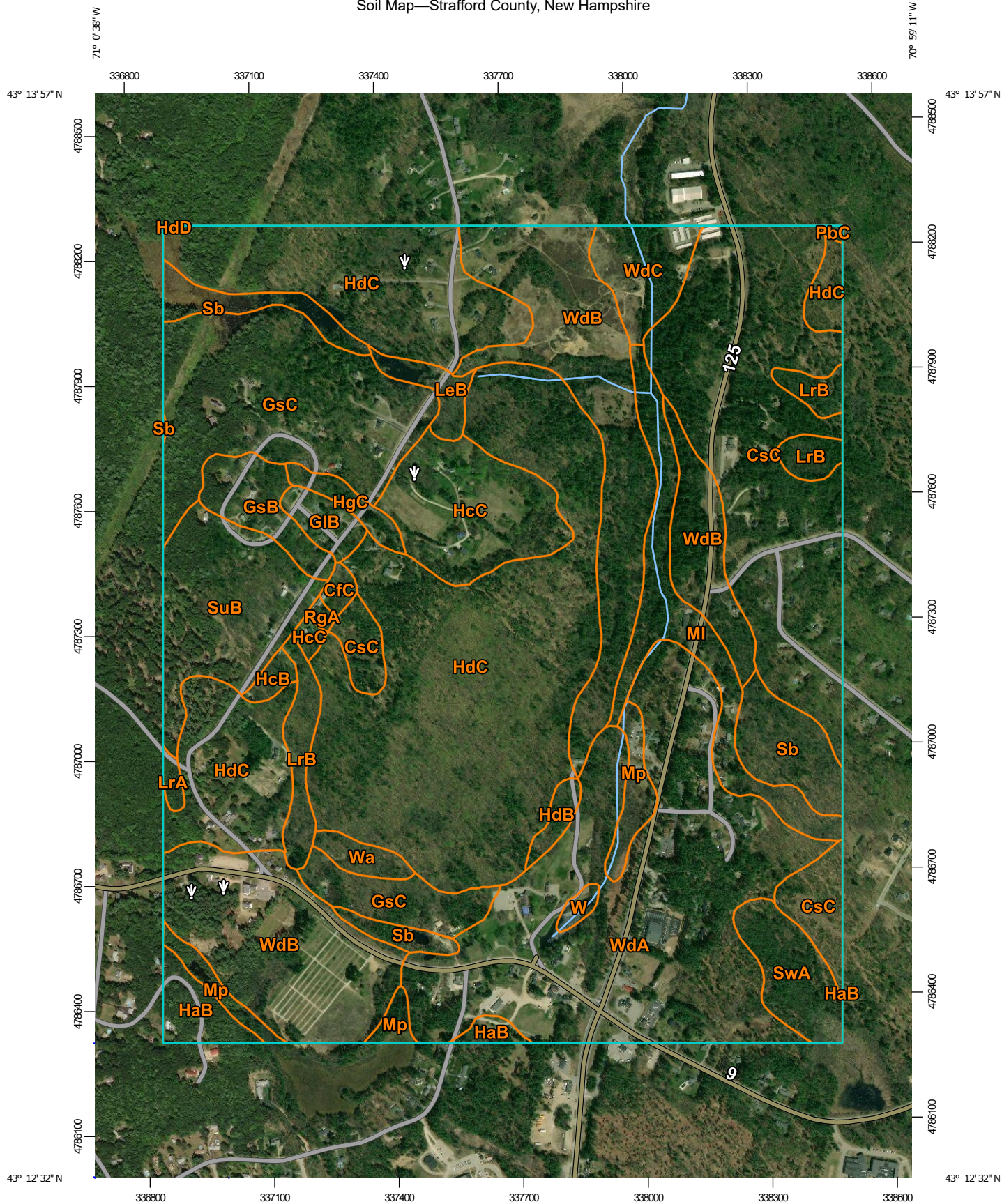
Stage-Area-Storage for Pond 109P: Rain Garden #109

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
210.75	0	0	215.95	719	2,799
210.85	0	29	216.05	719	2,958
210.95	0	58	216.15	719	3,122
211.05	0	86	216.25	719	3,291
211.15	0	115	216.35	719	3,465
211.25	0	144	216.45	719	3,644
211.35	0	173	216.55	719	3,828
211.45	0	201	216.65	719	4,018
211.55	0	230	216.75	719	4,212
211.65	0	259	216.85	719	4,412
211.75	719	288	216.95	719	4,618
211.85	719	302	217.05	719	4,829
211.95	719	316	217.15	719	5,046
212.05	719	331	217.25	719	5,268
212.15	719	345	217.35	719	5,495
212.25	719	360	217.45	719	5,728
212.35	719	374	217.55	719	5,967
212.45	719	388	217.65	719	6,212
212.55	719	403	217.75	719	6,462
212.65	719	417	217.85	719	6,718
212.75	719	431	217.95	719	6,981
212.85	719	446	218.05	719	7,249
212.95	719	460	218.15	719	7,523
213.05	719	475	218.25	719	7,804
213.15	719	489	218.35	719	8,090
213.25	719	503	218.45	719	8,383
213.35	719	518			
213.45	719	532			
213.55	719	546			
213.65	719	561			
213.75	719	575			
213.85	719	590			
213.95	719	604			
214.05	719	648			
214.15	719	723			
214.25	719	802			
214.35	719	886			
214.45	719	973			
214.55	719	1,064			
214.65	719	1,159			
214.75	719	1,258			
214.85	719	1,362			
214.95	719	1,470			
215.05	719	1,583			
215.15	719	1,700			
215.25	719	1,821			
215.35	719	1,947			
215.45	719	2,077			
215.55	719	2,212			
215.65	719	2,351			
215.75	719	2,496			
215.85	719	2,645			

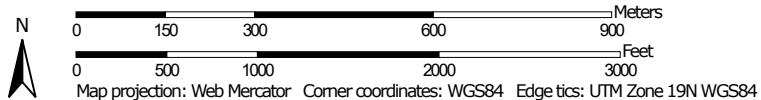
Linear Interpolation
 Lowest Orifice = 214.65'
 Storage Volume = 871 CF

 1,159 CF - 288CF = 871 CF

Soil Map—Strafford County, New Hampshire



Map Scale: 1:12,700 if printed on A portrait (8.5" x 11") sheet.



Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey

12/21/2020
Page 1 of 4

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot



Spoil Area



Stony Spot



Very Stony Spot



Wet Spot



Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Strafford County, New Hampshire

Survey Area Data: Version 20, May 29, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Dec 31, 2009—Sep 9, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
CfC	Charlton fine sandy loam, 8 to 15 percent slopes	1.7	0.2%
CsC	Charlton fine sandy loam, 8 to 15 percent slopes, very stony	97.2	12.2%
GIB	Gloucester fine sandy loam, 3 to 8 percent slopes	5.1	0.6%
GsB	Gloucester very stony fine sandy loam, 3 to 8 percent slopes	10.7	1.3%
GsC	Gloucester very stony fine sandy loam, 8 to 15 percent slopes	65.6	8.2%
HaB	Hinckley loamy sand, 3 to 8 percent slopes	8.9	1.1%
HcB	Hollis-Charlton fine sandy loams, 3 to 8 percent slopes	2.1	0.3%
HcC	Hollis-Charlton fine sandy loams, 8 to 15 percent slopes	28.4	3.6%
HdB	Hollis-Charlton very rocky fine sandy loams, 3 to 8 percent slopes	2.7	0.3%
HdC	Hollis-Charlton very rocky fine sandy loams, 8 to 15 percent slopes	202.3	25.4%
HdD	Hollis-Charlton very rocky fine sandy loams, 15 to 25 percent slopes	0.1	0.0%
HgC	Hollis-Gloucester very rocky fine sandy loams, 8 to 15 percent slopes	4.2	0.5%
LeB	Leicester very stony fine sandy loam, 3 to 8 percent slopes	4.9	0.6%
LrA	Leicester-Ridgebury fine sandy loams, 0 to 3 percent slopes, very stony	1.4	0.2%
LrB	Leicester-Ridgebury fine sandy loams, 3 to 8 percent slopes, very stony	14.0	1.8%
MI	Mixed alluvial land, wet	24.3	3.0%
Mp	Freetown and Swansea mucky peats, 0 to 2 percent slopes	11.1	1.4%
PbC	Paxton fine sandy loam, 8 to 15 percent slopes	0.4	0.1%

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
RgA	Ridgebury fine sandy loam, 0 to 3 percent slopes	0.8	0.1%
Sb	Saugatuck loamy sand	23.0	2.9%
SuB	Sutton fine sandy loam, 0 to 8 percent slopes, very stony	31.3	3.9%
SwA	Swanton fine sandy loam, 0 to 3 percent slopes	12.9	1.6%
W	Water	1.5	0.2%
Wa	Whitman fine sandy loam, 0 to 3 percent slopes, very stony	3.9	0.5%
WdA	Windsor loamy sand, 0 to 3 percent slopes	117.6	14.8%
WdB	Windsor loamy sand, 3 to 8 percent slopes	107.8	13.5%
WdC	Windsor loamy sand, 8 to 15 percent slopes	12.2	1.5%
Totals for Area of Interest		796.1	100.0%

**John P. Hayes III CSS, CWS,
7 Limestone Way
North Hampton, NH 03862
603-205-4396
johnphayes@comcast.net**

3/11/21

**Christopher Berry
Berry Surveying and Engineering
335 Second Crown Point Road
Barrington NH 03825**

Job # 21-007

**3/10/21
Site Specific Soil Survey
Map 235 Lots 1-1 & 3
Christmas Lane Barrington, NH**

Dear Chris,

This letter report presents the findings of a Site Specific Soil Survey conducted on the referenced property by John P. Hayes III on March 11, 2021. The soil survey was conducted in accordance with the New Hampshire Supplement of the Site-Specific Soil Mapping Standard For New Hampshire and Vermont, Version 5.0, December 2017, Special Publication # 3, published by the Society of Soil Scientist of Northern New England.

The property that is subject of the soil survey is located on the north side of Route 9, and northeast of Route 125, in Barrington, NH. The area of the parcel is approximately 23 acres in size. Only the portion of the lot was mapped. The plans used for these soil maps are a 80 scale plan, where 1 inch equals 80 feet, with one foot contours.

The purpose of the soil survey is to provide the client with soils information for urban and suburban or rural land planning. Soil characteristics on the property were evaluated through observation of numerous test holes and hand auger probes conducted throughout the property. Slope phases were determined with the use of the topography provided on the plan. The Site-specific Soil Map Units identified are taken from the New Hampshire State-Wide Numerical Soils Legend, Issue #10 January 2011, and are briefly described below. Official Series Descriptions (OSD) for each of these soil series are enclosed with this report. The soil map units comply with the Range In Characteristics described in the OSD. Dissimilar inclusions are noted above. Limits of the Site Specific mapping units are highlighted on the plan.

Portions of the soil map with the map unit denominator P, contain poorly drained soils. Portions of the map with the denominator Rk, are soils that have the potential to have areas of bedrock substratum within 40 inches of the soil surface.

MAP UNIT #	SOIL TAXANOMIC NAME	DESCRIPTION
CsB (State No. 63)	Charlton (very stony)	The Charlton series consists of very deep, well drained soils formed in loamy melt-out till. They are nearly level to very steep soils on moraines, hills, and ridges. Saturated hydraulic conductivity is moderately high or high. The hydrologic soil group is B. Slope ranges from 3% to 8%.
CsC (State No. 63)	Charlton (very stony)	The Charlton series consists of very deep, well drained soils formed in loamy melt-out till. They are nearly level to very steep soils on moraines, hills, and ridges. Saturated hydraulic conductivity is moderately high or high. The hydrologic soil group is B. Slope ranges from 8% to 15%.
CsD (State No. 63)	Charlton (very stony)	The Charlton series consists of very deep, well drained soils formed in loamy melt-out till. They are nearly level to very steep soils on moraines, hills, and ridges. Saturated hydraulic conductivity is moderately high or high. The hydrologic soil group is B. Slope ranges from 15% to 25%.
CsE (State No. 63)	Charlton (very stony)	The Charlton series consists of very deep, well drained soils formed in loamy melt-out till. They are nearly level to very steep soils on moraines, hills, and ridges. Saturated hydraulic conductivity is moderately high or high. The hydrologic soil group is B. Slope ranges from 25% to 50%.
HcC Rk (State No. 85)	Hollis (very Stony)	The Hollis series consists of well drained and somewhat excessively drained soils formed in a thin mantle of till. They are shallow to bedrock. They are nearly level to very steep upland soils on bedrock-controlled hills and ridges. Saturated hydraulic conductivity is moderately high or high. Depth to hard bedrock ranges from 25 to 50 cm. The hydrologic soil group is D. Slope ranges from 8% to 15%.
HcD Rk (State No. 85)	Hollis (very Stony)	The Hollis series consists of well drained and somewhat excessively drained soils formed in a thin mantle of till. They are shallow to bedrock. They are nearly level to very steep upland soils on bedrock-controlled hills and ridges. Saturated hydraulic conductivity is moderately high or high. Depth to hard bedrock ranges from 25 to 50 cm. The hydrologic soil group is D. Slope ranges from 15% to 25%.

MAP UNIT #	SOIL TAXANOMIC NAME	DESCRIPTION
<u>HcE</u> Rk (State No. 85)	Hollis (very Stony)	The Hollis series consists of well drained and somewhat excessively drained soils formed in a thin mantle of till. They are shallow to bedrock. They are nearly level to very steep upland soils on bedrock-controlled hills and ridges. Saturated hydraulic conductivity is moderately high or high. Depth to hard bedrock ranges from 25 to 50 cm. The hydrologic soil group is D. Slope ranges from 25% to 50%..
<u>HdD</u> Rk (State No. 175)	Hollis Charlton Complex (very stony)	The Hollis series consists of well drained and somewhat excessively drained soils formed in a thin mantle of till. They are shallow to bedrock. They are nearly level to very steep upland soils on bedrock-controlled hills and ridges. Saturated hydraulic conductivity is moderately high or high. Depth to hard bedrock ranges from 25 to 50 cm. The Charlton series consists of very deep, well drained soils formed in loamy melt-out till. They are nearly level to very steep soils on moraines, hills, and ridges. Saturated hydraulic conductivity is moderately high or high. The hydrologic soil group is C/D. Slope ranges from 15% to 25%..
<u>HdE</u> Rk (State No. 175)	Hollis Charlton Complex (very stony)	The Hollis series consists of well drained and somewhat excessively drained soils formed in a thin mantle of till. They are shallow to bedrock. They are nearly level to very steep upland soils on bedrock-controlled hills and ridges. Saturated hydraulic conductivity is moderately high or high. Depth to hard bedrock ranges from 25 to 50 cm. The Charlton series consists of very deep, well drained soils formed in loamy melt-out till. They are nearly level to very steep soils on moraines, hills, and ridges. Saturated hydraulic conductivity is moderately high or high. The hydrologic soil group is C/D. Slope ranges from 25% to 50%..
<u>LeB</u> P (State No. 515)	Leicester (very stony)	The Leicester series consists of very deep, poorly drained soils formed in coarse-loamy till. They are nearly level or gently sloping soils in drainageways and low-lying positions on hills. Permeability is moderate or moderately rapid in the surface layer and subsoil and moderate to rapid in the substratum. The hydrologic soil group is C. Slope ranges from 3% to 8%
<u>LeC</u> P (State No. 515)	Leicester (very stony)	The Leicester series consists of very deep, poorly drained soils formed in coarse-loamy till. They are nearly level or gently sloping soils in drainageways and low-lying positions on hills. Permeability is moderate or moderately rapid in the surface layer and subsoil and moderate to rapid in the substratum. The hydrologic soil group is C. Slope ranges from 8% to 15%

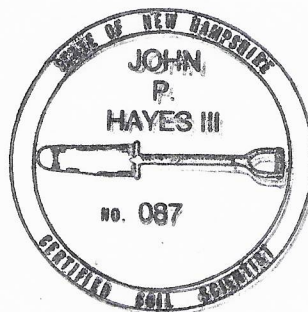
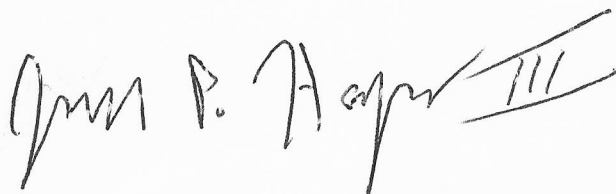
MAP UNIT #	SOIL TAXANOMIC NAME	DESCRIPTION
LeD P (State No. 515)	Leicester (very stony)	The Leicester series consists of very deep, poorly drained soils formed in coarse-loamy till. They are nearly level or gently sloping soils in drainageways and low-lying positions on hills. Permeability is moderate or moderately rapid in the surface layer and subsoil and moderate to rapid in the substratum. The hydrologic soil group is C. Slope ranges from 15% to 25%
SuB (State No. 69)	Sutton	The Sutton series consists of very deep, moderately well drained loamy soils formed in melt-out till. They are nearly level to strongly sloping soils on hills, low ridges, and ground moraines, typically on footslopes, lower backslopes and in slight depressions. Saturated hydraulic conductivity is moderately high or high throughout. The hydrologic soil group is B. Slope ranges from 3% to 8%.
SuC (State No. 69)	Sutton	The Sutton series consists of very deep, moderately well drained loamy soils formed in melt-out till. They are nearly level to strongly sloping soils on hills, low ridges, and ground moraines, typically on footslopes, lower backslopes and in slight depressions. Saturated hydraulic conductivity is moderately high or high throughout. The hydrologic soil group is B. Slope ranges from 8% to 15%.
SuD (State No. 69)	Sutton	The Sutton series consists of very deep, moderately well drained loamy soils formed in melt-out till. They are nearly level to strongly sloping soils on hills, low ridges, and ground moraines, typically on footslopes, lower backslopes and in slight depressions. Saturated hydraulic conductivity is moderately high or high throughout. The hydrologic soil group is B. Slope ranges from 15% to 25%.

Slope Phases

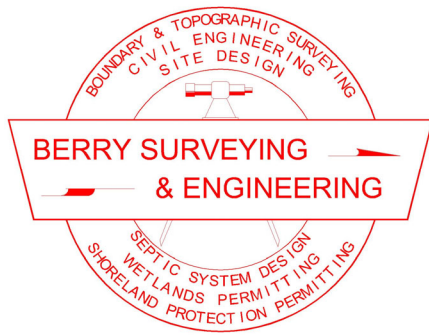
<u>Alpha Slope Symbol</u>	<u>Range</u>
A	0 - 3%
B	3 - 8%
C	8 - 15%
D	15 - 25%
E	25 - 50%
F	> 50%

I trust that this Soil Survey and report meet your current planning needs. Please do not hesitate to contact me if you have any questions.

Sincerely:



John P. Hayes III CSS, CWS



BERRY SURVEYING & ENGINEERING

335 Second Crown Point Road

Barrington, NH 03825

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Fax: (603) 335-4623

www.BerrySurveying.Com

Inspection and Maintenance Manual

Stormwater System Management

The Village at Barrington Square Tax Map 235, Lot 1-1 & Lot 3

Prepared for:

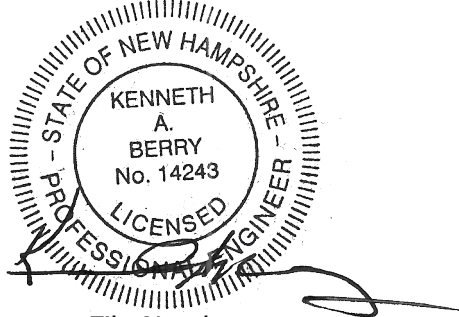
**Dove Development Group, LLC
242 Central Avenue
Dover, NH 03820**

Land of

Dove Development Group LLC

Prepared By

Berry Surveying & Engineering
335 Second Crown Point Road
Barrington, NH 03825
603-332-2863



File Number
DB2020-097

June 14, 2021

Inspection and Maintenance Manual

Stormwater System Management

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Annual Report.....	Page 12
Inspection & Maintenance Manual Checklist.....	Page 13
Inspection & Maintenance Log Sheet.....	Page 16
Deicing Log Sheet	Page 17
Owner Certification.....	Page 18
Operation & Maintenance Plans	Attached – 1 Page
Control of Invasive Plants, NH Department of Agriculture	Attached – 4 Pages
NHDES Green SnoPro Utilization Chart	Attached – 1 Page
UNH Stormwater Center Subsurface Gravel Wetland Design Specifications	10 Pages
Regular Inspection and Maintenance Guidance for GW ... UNHSC / NHDOT	42 Pages

Introduction

The Best Management Practices (BMP) described in this manual are specified in more detail within the plan set giving design details and specifications. The New Hampshire Stormwater Manual, Volume 2, Post-Construction Best Management Practices Selection & Design (December 2008, NHDES & US EPA) is included by reference to this manual. Additional details, construction specifications, and example drawings are provided within this reference. (<http://des.nh.gov/organization/divisions/water/stormwater/>)

The BMP's are covered below in the general order in which the storm water flows. Each BMP has a description and maintenance consideration listed. A Check List table is provided after the narrative to summarize the maintenance responsibilities and schedule. A Log Form is also provided for the owners use.

For details regarding the design of the Storm Water System see also Drainage Analysis & Sediment and Erosion, June 14, 2021, as revised. See also plan set completed for **The Dove Development Group, LLC**, originally dated **June 14, 2021**, as revised.

Robert Baldwin, Managing Member of Dove Development Group, LLC is responsible for the Operation, Inspection, and Maintenance of the Stormwater Management System. A significant step in this responsibility is the Inspection and Maintenance of each component of the system. Ongoing, semi-annual, and annual inspection and maintenance requirements are documented below and must be followed diligently. Failure of any component of the system can result in surface water run-off ponding and/or freezing in the roadway and parking lots, leaving the developed site untreated, and/or causing violations to issued permits. The owner / developer must initiate or expand the Homeowners Association (HOA) and will be responsible as the majority owner of the association. The HOA will then be responsible for the drainage infrastructure. When, and if, the Town of Barrington accepts the roads as public, they may also become responsible for the roads and drainage infrastructure, then becoming the responsible party, for part or the whole. The responsible party must maintain, and have available, plans of the Stormwater System in order properly inspect and maintain the system. (Reduced copies attached.) The responsible party will conduct the inspections, complete the required maintenance, and will maintain the Inspection & Maintenance Check Lists and Logs, and will provide copies with the Annual Report to the Town of Barrington, Land Use Department and provided a copy to NHDES AoT by December 15th of each year.

The owners of Tax Map 235, Lot 1-1 and 3 (to be merged), The Dove Development Group, LLC, are proposing a mixed-use and residential development consisting of 5 commercial first-floor units with 20 apartments on the second & third floor and 25 condominium units, and 5,555 linear feet of roadway, which includes the 560 LF already constructed for Community Way.

Reference is made to 18-005 Inspection & Maintenance Manual for John & Linda Svenson and 1962 Real Estate LLC. (Copy Attached)

The following practices and drainage features will all require periodic inspections and maintenance based on this manual and drainage layout:

Completed Construction:

Infiltration Pond #13 (1962 Real Estate LLC) Formerly Pond #20

Infiltration Pond #14 (1962 Real Estate LLC) Formerly Pond #22

Rain Garden #101 with Underdrain (1962 Real Estate LLC)

Rain Garden #102 with Underdrain (Christmas Dove / J & L Svenson)

Proposed Construction – Dove Development Group, LLC

Culvert Inlet Sumps.

Catch Basins & Drainage Pipes

Drain Manholes

Sediment Forebays for all Treatment Practices

Subsurface Gravel Wetland #103 with Outlet Structure and Spillway

Subsurface Gravel Wetland #104 with Outlet Structure and Spillway

Rip Rap Outlet Protection & Level Spreaders

Rain Garden #105 with Underdrain & Orifice, Outlet Structure, and Spillway

Rain Garden #106 with Underdrain & Orifice, Outlet Structure, and Spillway

Rain Garden with Infiltration #107 with Outlet Structure and Spillway

Rain Garden #108 with Underdrain & Orifice, Outlet Structure, and Spillway

Rain Garden #109 with Underdrain & Orifice, Outlet Structure, and Spillway

Detention Pond #110 with Outlet Structure

Culvert Inlet Sumps

Description: In four locations, to capture the surface water runoff that is trapped within the inside of the residential roadway and residential runoff from back yards, there are Residential Inlet Sumps. This culvert pipes, flared end sections, and constructed sumps will collect the runoff that is directed to that location during and after the residential development. The culvert will allow the runoff to enter the drainage network where the runoff will be pre-treated and treated at a treatment practice. The location of the Residential Inlet Sumps will be marked and identified with painted and distinctive fence post.

Maintenance Considerations: Vegetation and debris will need to be removed from the culvert inlet several times a year, especially late fall after the majority of the leaves have fallen and in the spring. In addition to the sump and culverts themselves, the drainage channel will need to be inspected to ensure that the runoff intended to get to the inlets is making it to the sump. The identification fence post will be inspected for structural condition and painted condition.

Catch Basin, and Drain Manholes

Description: Catch Basins are used throughout the site to capture and, along with culvert pipes and manhole, route surface water runoff to stormwater treatment and detention infrastructure. During construction the catch basins will be protected by inlet protection per the approved construction plans. The practice of street sweeping on a bi-annual basis will help reduce maintenance of these catch basins and culvert pipes.

Note: Deep sump catch basins are not allowed to be used on this proposed development due to wildlife concerns and any manufacturer sump resulting in a catch basin must be filled with washed crushed stone. Sediment should be trapped in the sediment forebays but is also a concern in earlier structures.

Maintenance Considerations: Sediment must be removed from Catch Basins and Manholes on a regular basis, at least twice a year and more often if post-winter maintenance and street sweeping is not conducted. Inspections should be conducted periodically. At a minimum they should be cleaned after snow-melt and after leaf-drop. Disposal of all material, sediment, and debris must be done in accordance with state

and federal regulations. Culvert pipes will be inspected to ensure that surface water runoff is capable of leaving the structures.

Treatment & Conveyance Swales

Description: "Swales are stabilized channels designed to convey runoff at non-erosive velocities." (NHDES SWM) They will be trapezoidal or parabolic in section view. A conveyance swale is intended to move surface water runoff from one point to another where as a treatment swale will slow the velocity to a point where sediment will settle out of the stormwater flow. A treatment swale will be constructed to a width of between four and eight feet and have a minimum length of 100 feet. The flow characteristics will also meet design criteria. See SWM Volume 2, 4.3 Treatment Practices, 5. Treatment Swales, page 123.

Project Intent: The swales are individually designed in the drainage analysis and specified on the design plans. The designed swales must have greater than 85% vegetated growth prior to receiving runoff. The bottom of a treatment swale must be above the seasonal high water table.

Maintenance Considerations: Grassed swales will be inspected twice annually, removing accumulated sediment and gross solids. Grass will be mowed periodically but to a depth of not less than 4 inches. Any damage to the vegetation will be repaired and woody vegetation and invasive vegetation will be removed.

Culvert Pipes, Flared End Sections / Headwalls

Description: Culvert pipes are placed to route surface water runoff from catch basins to drain manholes, and drain manholes to a discharge point conveying the runoff in such a manner that erosion does not take place. Culvert pipes are often terminated with flared end sections or headwalls.

Maintenance Considerations: The entrance and exit of the culvert pipe should be cleaned of any trash and sediment build-up. The culvert should be clear to let runoff pass through the culvert unobstructed. Flared end sections and headwalls should be inspected for erosion and destabilization, with repairs made as required.

Sediment Forebay

Description: A sediment forebay is designed to reduce the velocity of incoming surface water runoff allowing sediment to fall out of suspension initially pre-treating the runoff before it is sent to a treatment structure. This earthen basin will have vegetated side-slopes and a check dam to further reduce and pretreat the runoff. At the point of incoming runoff, the basin will be protected by rip rap outlet protection construction and the outgoing edge will be protected with rip rap. The check dam will be constructed from one side of the basin to the other and cause runoff to either go through or over. The volume of the forebay is generally 10% the volume of the Water Quality Volume (WQV) for gravel wetlands, and 25% for rain gardens. A dewatering drain is designed into the two-foot berm of the forebay. Construction specifications are included in the plan set and New Hampshire Stormwater Manual, Volume 2, 4-4 Pretreatment Practices 1, Sediment Forebays.

If it determined that too much sediment is by-passing the sediment forebay into the stormwater practice, semi-permanent sediment barriers may be warranted in the form of check dams by using a filtering media such as Filtrexx Silt Soxx.

Maintenance Considerations: The basin and slopes will be periodically mowed, at least twice per year ensuring that woody material does not get an opportunity to grow. Sediment accumulated in the basin will be removed and properly disposed of when it reaches half the height of the check dam. Erosion or other damage to the basin will be repaired and revegetated. (See Outlet Protection) Inspect and clean the dewatering drain to ensure runoff is not trapped for more than 72 hours in the forebay.

Infiltration Basins (Infiltration Rain Garden #107) & Detention Ponds

Description: Infiltration Basins and the Infiltration component of some Rain Gardens, are constructed ponds that are intended to detain surface water runoff and during the detention to infiltrate runoff into the ground. Detention Ponds are also constructed ponds with the purpose of detaining runoff but not necessarily for infiltration purposes. During construction it is important that the ground surface not be exposed to traffic or construction equipment to preserve the infiltration capabilities of the existing soil. Construction specifications are included in the plan set and New Hampshire Stormwater Manual, Volume 2, 4-3 Treatment Practices, 3B, In-ground Infiltration Basin and Section 4-6, Conveyance Practices, 2. Detention Basins.

Maintenance Considerations:

Infiltration Basins and Detention Ponds should be inspected at least twice annually and following any rainfall event exceeding 0.25 inches in a twenty-four hour period.

Maintenance rehabilitation will be conducted as warranted by each inspection. Trash and debris will be removed at each inspection.

On an annual basis the infiltration capabilities need to be confirmed by evaluation the drawdown time. If the infiltration system does not drain within 72-hours following a rainfall event, a qualified professional will assess the condition of the basin to determine measures required to restore the infiltration function. This is normally the direct result of sediment accumulation which will be removed to restore the filter media ratio.

Also on an annual basis the vegetation should be inspected to ensure healthy condition. Invasive species need to be removed along with dead or diseased vegetation.

Bio-Filtration System (Rain Gardens) & Bio-Swales

Description: Rain Gardens, or bio-filtration areas are located close to the source of runoff. They are intended to integrate with the site landscaping and become an aesthetically attractive opportunity to provide highly effective stormwater treatment. The rain gardens associated with this proposed development contribute toward recharge of surface water run-off into the ground. It is important that sediment be removed from run-off prior to discharge into the bio-filtration area to preserve the mulch and soil mix ratio. During construction it is important that the ground surface not be exposed to traffic or construction equipment to preserve the infiltration capabilities of the existing soil. Construction specifications are included in the plan set and New Hampshire Stormwater Manual, Volume 2, 4-3 Treatment Practices, 4c Bioretention System. (Bio-media and bio-filtration mean bioretention filter media.)

Maintenance Considerations:

Rain Gardens should be inspected at least twice annually and following any rainfall event exceeding 0.25 inches in a twenty-four hour period. Maintenance rehabilitation will be conducted as warranted by each inspection. Trash and debris will be removed at each inspection.

The design of the rain garden under-drain system includes an orifice in an end-cap. This feature is designed to be disassembled to allow cleaning. This outlet orifice is located within a concrete outlet structure that may contain a control stack or manifold used to control and detain runoff in the system. Although this is designed to be "clean water" after the filtering process, the outlet structure in general is going to require periodic maintenance to ensure that it is discharging runoff properly. If the Rain

Garden retains runoff on the surface for more than 72 hours the performance is not correct and maintenance is required.

On an annual basis the infiltration capabilities need to be confirmed by evaluation the drawdown time. If the bio-filtration system does not drain within 72-hours following a rainfall event, a qualified professional will assess the condition of the rain garden to determine measures required to restore the infiltration function. This is normally the direct result of sediment accumulation which will be removed to restore the filter media ratio or as stated above, an issue with the discharge orifice.

Also on an annual basis the vegetation should be inspected to ensure healthy condition. Invasive species need to be removed along with dead or diseased vegetation.

Subsurface Gravel Wetland

Description: A Gravel Wetland (NHDES SWM 4-3 Treatment Practice 2D) or Subsurface Gravel Wetland consists of a forebay and multiple flow-through treatment cells. During smaller rain events, the surface water runoff is intended to pass from the forebay, into the gravel media through perforated pipes and structures where it passes through an anaerobic environment where the Water Quality Volume will have 24-72 hours of contact time. The forebay is required to contain 10% of the WQV and each of the two cell must contain 45% of the WQV. During larger storm events, the system works as a detention pond. The design of a Subsurface Gravel Wetland will be constructed in accordance with the most current version of the Design Specifications provided by the UNH Stormwater Center and SWM Volume 2, Section 4-3 Treatment Practices, 2d Gravel Wetlands.

Maintenance Considerations: The outlet configuration of the anaerobic subsurface gravel consists of a small discharge orifice that is located in a threaded cap. This goose-neck feature is designed to be disassembled to allow cleaning. This outlet orifice is located within a concrete outlet structure that may contains a control stack or manifold used to control and detain runoff in the system. Although this is designed to be "clean water" after the filtering process, the outlet structure in general is going to require periodic maintenance to ensure that it is discharging runoff properly. If the Subsurface Gravel Wetland retains runoff on the surface for more than 72 hours the performance is not correct and maintenance is required.

Debris will need to be removed from the inlet and outlet structures as well as any buildup of sediment. The surface of the ponded area is intended to have wetland plants which may require periodic replanting, depending on the sediment loading. Sediment buildup in the forebay must be removed to maintain the minimum required volume. See also 9 and 10 of the attached UNHSC Subsurface Gravel Wetland Design

Specifications 2009, and / or UNHSC Subsurface Gravel Wetland Design Specifications 2016 with Maintenance Guidelines and Checklist. See also Design and Maintenance of Subsurface Gravel Wetlands, February 4, 2015, UNHSC / NHDOT with included Checklist for Inspection of Gravel Wetland and Regular Inspection and Maintenance Guidance for Gravel Wetland Stormwater Management Device which is attached.

Rip Rap Outlet Protection, Level Spreaders, & Emergency Spillways

Description: Outlet Protection consists of a riprap apron or preformed scour hole that is designed to provide velocity reduction of the surface water run-off that is leaving a culvert. The design is dependent on the culvert size, soil conditions, velocity, and quantity of the run-off. There are to be no bend or curves at the intersection of the conduit and apron. Level spreaders are intended to provide a level lip where surface water runoff is allowed to continue downhill closer to sheet flow. The level lip is to be constructed as level as possible for the entire length. Emergency Spillways are rip rap reinforced outlets near the top of the berm that allow runoff to leave a practice during periods of very high flow. Ref.: NHDES SWM Volume 2, Section 4-6 Conveyance Practices, 6. Outlet Protection and 1. Detention Ponds, Note 3, Page 158.

Maintenance Considerations: The riprap outlet protection will be inspected annually for damage, which must be corrected immediately. Any sediment buildup will be removed and disposed of correctly. Sediment and subsequent vegetation will build up in the Level Spreader. This material will be cleaned out along with any gross solids and disposed of properly. (See invasive species below) Any rip rap that has been displaced from the original construction will be repaired, especially recreating the level lip.

Stabilization for Long Term Cover

Vegetated Stabilization – Original Planting

All areas that are disturbed during construction will be stabilized with vegetated material within 30 days of breaking ground. Construction will be managed in such a manner that erosion is prevented and that no abutter's property will be subjected to any siltation, unless otherwise permitted. All areas to be planted with grass for long-term cover will follow the specification and on Sheet E-102 using seeding mixture C, as follows:

Mixture	Pounds per Acre	Pounds per 1,000 Sq. Ft.
Tall Fescue	24	0.55
Creeping Red Fescue	24	0.55
Total	48	1.10

Conservation Mix

Mixture	Pounds per Acre	Pounds per 1,000 Sq. Ft.
Tall Fescue	15	0.35
Creeping Red Fescue	15	0.35
Annual Ryegrass	5	0.12
Perennial Ryegrass	5	0.12
Kentucky Bluegrass	15	0.35
White Clover	7	0.16
Total	62	1.45

Conservation Mix will be used to stabilize all 2:1 slopes and all land area disturbed within the wetland buffer. As the site is to be stabilized with erosion control mix as a mulch, the vegetation should be established with a high percentage of white clover for growth to be established.

Rain garden mix

The grass that is planted within a rain garden bio-filtration system within the bio-media must consist of a combination of warm season grass seed and cold season grass seed in order for the grass to start growing for stabilization and continue growing in the sandy well-drained environment. Planting specification will meet the requirements as outlined in 'Vegetation New Hampshire Sand and Gravel Pits' mix 1 (warm season grasses) (15 lbs/ac) and include annual and perennial rye grass seed (15 lbs/ac); the New England native warm season grass mix (23 lbs/ac) by New England Wetland Plants, Inc.; rain garden mix 180 (15 lbs/ac & 15 lbs/ac of rye) / rain garden grass mix 180-1 (20 lbs/ac & 10 lbs/ac of rye) by Ernst Conservation Seeds; or approved equal.

Detention Pond Mix:

The grass that is planted within a Detention Pond will be a mix designed for both inundation and dry conditions such as Ernst Seeds, Retention Basin Floor Mix ERNMX-126.

Subsurface Gravel Wetland Mix:

The grass that is planted within a Subsurface Gravel Wetland will be a diverse mix of species to provide food and cover as well as erosion control in the seasonally flooded conditions such as Ernst Seeds Seasonally Flooded Wildlife Mix ERNMX-128.

Maintenance Considerations: Permanent seeded areas for long-term cover will be inspected on a periodic basis looking for signs of growth loss or erosion. Any areas found to be damaged will be repaired and replanted to reestablish the growth. The grass should be mowed at least twice per year and any dead material removed. Any woody growth that becomes established will need to be cut and removed.

Long-term maintenance of the land cover is critical and must be maintained at least 85% grass / vegetation coverage, must be inspected for concentrated flow, rills, and channels; and must be repaired as necessary to prevent erosion.

CONTROL OF INVASIVE PLANTS

During maintenance activities, check for the presence of invasive plants and remove in a safe manner as described on the following pages. They should be controlled as described on the following pages.

Invasive plants are introduced, alien, or non-native plants, which have been moved by people from their native habitat to a new area. Some exotic plants are imported for human use such as landscaping, erosion control, or food crops. They also can arrive as "hitchhikers" among shipments of other plants, seeds, packing materials, or fresh produce. Some exotic plants become invasive and cause harm by:

- becoming weedy and overgrown;
- killing established shade trees;
- obstructing pipes and drainage systems;
- forming dense beds in water;
- lowering water levels in lakes, streams, and wetlands;
- destroying natural communities;
- promoting erosion on stream banks and hillsides; and
- resisting control except by hazardous chemical.


Annual Report

Description: The owner is responsible to keep an **I & M Activity Log** that documents inspection, maintenance and repairs to the storm water management system, and a **Deicing Log** to track the amount and type of deicing material applied to the site. The original owner is responsible to ensure that any subsequent owner (s) have copies of the Inspection & Maintenance Manual, Stormwater System Management, copies of past logs and check lists. This includes any owner association that might become involved with the property. The Annual Report will be prepared and submitted to the Town of Barrington Land Use Department with copies of both logs and check lists no later than December 15th of each year and made provided to NHDES on that same date. Upon an ownership change, the Annual Report will include the Transfer of Ownership Responsibility Forms duplicated from the form found below.

The plans that accompany this manual includes two sheets, "Drainage Operation, Inspection, & Maintenance Plan". The owners and municipality will also maintain a complete set of the approved original design plans.

Respectfully
BERRY SURVEYING & ENGINEERING

Kevin R. Poulin, EIT
Project Engineer / Manager



Kenneth A. Berry, PE, LLS
CPSWQ, CPESC, CESSWI
Principal, VP – Technical Operations

STORMWATER SYSTEM: INSPECTION AND MAINTENANCE MANUAL

Inspection & Maintenance Manual Checklist

The Village at Barrington Square

Tax Map 235, Lot 1-1 & Lot 3
 Dove Development Group, LLC
 242 Central Avenue, Dover, NH 03820

<input checked="" type="checkbox"/>	Date	BMP / System	Minimum Inspection Frequency	Minimum Inspection Requirements	Maintenance / Cleanout Threshold
		Pavement Sweeping	Three Times Per Year	N/A	N/A
		Litter/Trash Removal	Routinely	Inspect dumpsters, outdoor waste receptacles area, and yard areas.	Parcel will be free of litter/trash.
		Deicing Agents	N/A	N/A	Use salt as the primary agent for roadway safety during winter.
		Invasive Species	Two times per year.	Inspect for Invasive Species	Remove and dispose invasive species.
		Closed Drainage System:			
		Drainage Pipes & Inlet Sumps	2 years per year	Check for sediment accumulation & clogging.	Less than 2" sediment depth
		Catch Basins & Catch Basins	2 times per year	Check for sediment accumulation & clogging.	Sediment accumulated to a depth of 2 feet.

☑	Date	BMP / System	Minimum Inspection Frequency	Minimum Inspection Requirements	Maintenance / Cleanout Threshold
		Subsurface Gravel Wetlands, Rain Gardens, Detention Ponds & Infiltration Ponds	2 times per year	Check for sediment and debris accumulation buildup.	Remove sediment & debris when required. Remove Invasive Species
		Subsurface Gravel Wetland and system clean-outs.	Annually	72-Hour drawdown time evaluation and vegetation evaluation. Underdrain flushing.	Remove dead & diseased vegetation along with all debris, take corrective measures of filtration media if required. Flush underdrain clean-outs with a hose.
		Rain Garden & Infiltration Ponds	Annually	72-Hour drawdown time evaluation and vegetation evaluation. Underdrain flushing.	Remove dead & diseased vegetation along with all debris, take corrective measures of filtration media if required. Flush underdrain clean-outs with a hose.
		Riprap Outlet Protection	Annually	Check for sediment buildup and structure damage.	Remove excess sediment and repair damage.
		Winter Maintenance	Ongoing	Remove snow as directed.	Ongoing

		Post Winter Maintenance	Annually	Remove excess sand, gross solids, and repair vegetation and plantings	Parcel will be free of excess sand, litter/trash. Vegetation per approved plans.
		Annual Report	1 time per year	Submit Annual Report to Barrington Land Use Department and kept on file by the owner.	Report to be submitted on or before December 15th each year. Copies submitted to NHDES by that date.

Inspection Check List:

The following practices and drainage features will all require periodic inspections and maintenance based on this manual and drainage layout:

Culvert Inlet Sumps.

Catch Basins & Drainage Pipes

Drain Manholes

Sediment Forebays for all Treatment Practices

Subsurface Gravel Wetland #103 with Outlet Structure and Spillway

Subsurface Gravel Wetland #104 with Outlet Structure and Spillway

Rip Rap Outlet Protection & Level Spreaders

Rain Garden #105 with Underdrain & Orifice, Outlet Structure, and Spillway

Rain Garden #106 with Underdrain & Orifice, Outlet Structure, and Spillway

Rain Garden with Infiltration #107 with Outlet Structure and Spillway

Rain Garden #108 with Underdrain & Orifice, Outlet Structure, and Spillway

Rain Garden #109 with Underdrain & Orifice, Outlet Structure, and Spillway

Detention Pond #110 with Outlet Structure

STORMWATER SYSTEM OPERATION & MAINTENANCE PLAN CERTIFICATION

Owner	Responsibility
Name: Robert Baldwin, Managing Member Dove Development Group Address: 242 Central Avenue Dover, NH 03820 Telephone: (603) 986-2373 (Mobile)	The owner is responsible for the conduct of all construction activities, and ultimate compliance with all the provisions of the Stormwater System Operation & Maintenance Plan and the implementation of the Inspection and Maintenance Manual.

OWNER CERTIFICATION

I certify under penalty of law that this document and all attachments were prepared under my direction and supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Signed: _____ Date: _____

Printed Name:

Representing:

The Village at Barrington Square

Tax Map 235, Lot 1-1 & Lot 3
Dove Development Group, LLC
242 Central Avenue
Dover, NH 03820

Control of Invasive Plants

New Hampshire
Department of Agriculture,
Markets & Food
Douglas Cygan
603-271-3488
doug.cygan@agr.nh.gov

This guide lists garden plants and weeds which are already causing significant changes to natural areas in the Mid-Atlantic. **Measures for controlling each species are indicated by number, e.g., (3), in the text with a full explanation at the end of this article.** Click on the word [Control](#): to jump to that section. Then click your "back" button to return to the text. Following each section suggested alternative plants are given. These alternatives are native plants, well adapted and needing little care, attractive to birds and butterflies, and an important part of the food web for our indigenous species.

INVASIVE TREES

NORWAY MAPLE (*Acer platanoides*) has large leaves similar to sugar maple. To easily confirm that the plant is Norway maple, break off a leaf and if it's truly Norway maple it will exude milky white sap. Fall foliage is yellow. (Exception: cultivars such as 'Crimson King,' which have red leaves in spring or summer, may have red autumn leaves.) The leaves turn color late, usually in late October after native trees have dropped their foliage. This tree suppresses growth of grass, garden plants, and forest understory beneath it, at least as far as the drip-line. Its wind-borne seeds can germinate and grow in deep shade. The presence of young Norway maples in our woodlands is increasing.

[Control](#): (1); (7), (8), (9), or (10); (11) in mid-October to early November, before the leaves turn color.

TREE OF HEAVEN (*Ailanthus altissima*), is incredibly tough and can grow in the poorest conditions. It produces huge quantities of wind-borne seeds, grows rapidly, and secretes a toxin that kills other plants. Its long compound leaves, with 11-25 lance-shaped leaflets, smell like peanut butter or burnt coffee when crushed. Once established, this tree cannot be removed by mechanical means alone.

[Control](#): (1) - seedlings only. Herbicide - use Garlon 3a (9) with no more than a 1" gap between cuts, or (10); plus (11) on re-growth. Or paint bottom 12" of bark with Garlon 4 Ultra (in February or March to protect surrounding plants). USE MAXIMUM STRENGTH SPECIFIED ON LABEL for all herbicide applications on Ailanthus. Glyphosate is not effective against Ailanthus.

INVASIVE SHRUBS

AUTUMN OLIVE (*Eleagnus umbellata*): Formerly recommended for erosion control and wildlife value, these have proved highly invasive and diminish the overall quality of wildlife habitat.

[Control](#): (1) - up to 4" diameter trunks; (7) or (10) or bury stump. Do not mow.

MULTIFLORA ROSE (*Rosa multiflora*), formerly recommended for erosion control, hedges, and wildlife habitat, becomes a huge shrub that chokes out all other vegetation and is too dense for many species of birds to nest in, though a few favor it. In shade, it grows up trees like a vine. It is covered with white flowers in June. (Our native roses have fewer flowers, mostly pink.) Distinguish multiflora by its size, and by the presence of very hard, curved thorns, and a fringed edge to the leaf stalk.

[Control](#): (1) - pull seedlings, dig out larger plants at least 6" from the crown and 6" down; (4) on extensive infestations; (10) or (11). It may remain green in winter, so herbicide may *applied when other plants are dormant. For foliar application, mix Rodeo with extra sticker-spreader, or use Roundup Sure Shot Foam on small plants.*

BUSH HONEYSUCKLES (*Lonicera spp.*), including Belle, Amur, Morrow's, and Tatarian honeysuckle. (In our region, assume that any honeysuckle is exotic unless it is a scarlet-flowered vine). Bush honeysuckles create denser shade than native shrubs, reducing plant diversity and eliminating nest sites for many forest interior species.

Control: (2) on ornamentals; (1); on shady sites only, brush cut in early spring and again in early fall (3); (4) during the growing season; (7); or (10) late in the growing season.

BLUNT-LEAVED PRIVET (*Ligustrum obtusifolium*). Control: (1); (7) or (10); or trim off all flowers. Do not cut back or mow.

BURNING BUSH, WINGED EUONYMUS (*Euonymus alatus*), identified by wide, corky wings on the branches.

Control: (1); (7) or (10); or trim off all flowers.

JAPANESE BARBERRY (*Berberis thunbergii*), and all cultivars and varieties.

Control: (1); (7) or (10); or trim off all flowers.

INVASIVE WOODY VINES

All of these vines shade out the shrubs and young trees of the forest understory, eventually killing them, and changing the open structure of the forest into a dense tangle. DO NOT PLANT NEXT TO OPEN SPACE.

JAPANESE HONEYSUCKLE (*Lonicera japonica*), including Hall's honeysuckle, has gold-and-white flowers with a heavenly scent and sweet nectar in June. This is probably the familiar honeysuckle of your childhood. It is a rampant grower that spirals around trees, often strangling them.

Control: (1); (3); (10); (11) in fall or early spring when native vegetation is dormant. Plan to re-treat repeatedly.

ORIENTAL BITTERSWEET (*Celastrus orbiculatus*) has almost completely displaced American bittersweet (*C. scandens*). The Asian plant has its flowers and bright orange seed capsules in clusters all along the stem, while the native species bears them only at the branch tips.

Control: (1); keep ornamental plants cut back, remove all fruits as soon as they open, and bag or burn fruits; to eradicate use Garlon 3a (10).

JAPANESE KNOTWEED, MEXICAN BAMBOO (*Polygonum cuspidatum*) can grow in shade. The stems have knotty joints, reminiscent of bamboo. It grows 6-10' tall and has large pointed oval or triangular leaves.

Control: Cut at least 3 times each growing season and/or treat with Rodeo (10) or (11). In gardens, heavy mulch or dense shade may kill it.

INVASIVE HERBACEOUS PLANTS

GARLIC MUSTARD (*Alliaria petiolata*, *A. officinalis*), a white-flowered biennial with rough, scalloped leaves (kidney-, heart- or arrow-shaped), recognizable by the smell of garlic and taste of mustard when its leaves are crushed. (The odor fades by fall.)

Control: Pull before it flowers in spring (1), removing crown and roots. Tamp down soil afterwards. Once it has flowered, cut (2), being careful not to scatter seed, then bag and burn or send to the landfill. (11) may be appropriate in some settings.

JAPANESE STILT GRASS (*Microstegium vimineum*) can be identified by its lime-green color and a line of silvery hairs down the middle of the 2-3" long blade. It tolerates sun or dense shade and quickly invades areas left bare or disturbed by tilling or flooding. An annual grass, it builds up a large seed bank in the soil.

Control: Easily pulled in early to mid-summer (1) - be sure to pull before it goes to seed. If seeds have formed, bag and burn or send to landfill. Mowing weekly or when it has just begun to flower may prevent it from setting seed (3). Use glyphosate (11) or herbicidal soap (less effective) on large infestations. Follow up with (5) in spring.

MILE-A-MINUTE VINE, DEVIL'S TAIL TEARTHUMB (*Polygonum perfoliatum*), a rapidly growing annual vine with triangular leaves, barbed stems, and turquoise berries in August which are spread by birds. It quickly covers and shades out herbaceous plants.

Control: same as for stilt grass.

SPOTTED KNAPWEED (*Centaurea maculosa*), a biennial with thistle-like flowers.

Control: Do NOT pull (1) unless the plant is young and the ground is very soft - the tap root will break off and produce several new plants. Wear sturdy gloves. (2); (6); (10) or (11).

CONTROL MEASURES

- (1) PULL seedlings and small or shallow-rooted plants when soil is moist. Dig out larger plants, including the root systems. Use a forked spade or weed wrench for trees or shrubs.
- (2) DEADHEAD to prevent spread of seeds of invasive plants. Cut off seeds or fruits before they ripen. Bag, and burn or send to a landfill.
- (3) MOW or CUTTING at least 4 times a season to deplete plants' store of nutrients and carbohydrates, reduce seed formation, and kill or minimize spread of plants. If necessary, repeat each year.
- (4) CONTROLLED BURNING during the spring, repeated over several years, allows native vegetation to compete more effectively with the invasive species. This requires a permit. Spot treatment with glyphosate in late fall can be used to make this method more effective.
- (5) Use a CORN-BASED PRE-EMERGENCE HERBICIDE on annual weeds. This product is also an organic fertilizer, i.e., it can stimulate growth of existing plants, including weeds, so it is appropriate for lawns and gardens but may not be appropriate in woodlands.
- (6) In lawns, SPOT TREAT with BROAD-LEAF WEEDKILLER. Good lawn-care practices (test soil; use lime and fertilizer only when soil test shows a need; mow high and frequently; leave clippings on lawn) reduce weed infestations.
- (7) CUT DOWN the tree. Grind out the stump, or clip off re-growth.
- (8) GIRDLE tree: cut through the bark and growing layer (cambium) all around the trunk, about 6" above the ground. Girdling is most effective in spring when the sap is rising, and from middle to late summer when the tree is sending down food to the roots. Clip off sucker sprouts.
- (9) FRILL: Using a machete, hatchet or similar device, hack scars (several holes in larger trees) downward into the cambium layer, and squirt in glyphosate (or triclopyr if recommended in text above). Follow label directions for Injection and Frill Applications. This is most effective from middle to late summer. Clip off any sucker sprouts or treat with glyphosate.
- (10) CUT STEM / CUT STUMP WITH GLYPHOSATE (or triclopyr if specified above). Follow label directions for Cut Stump Application. Clip off sucker sprouts or paint with glyphosate. See Note on Herbicides.
- (11) FOLIAR SPRAY WITH GLYPHOSATE herbicide (see Note on Herbicides). Use a backpack or garden sprayer or mist blower, following label directions. Avoid overspray and/or dripping onto non-target plants, because glyphosate kills most plants except moss. If it rolls off waxy or grass-like foliage, use additional sticker-spreader. Deciduous trees, shrubs, and perennials move nutrients down to the roots in late summer. Glyphosate is particularly effective at this time and when plants have just gone out of flowering. Several invasive species retain their foliage after native plants have lost theirs, and resume growth earlier in spring than most natives. This allows you to treat them without harming the natives. However, the plant must be actively growing for the herbicide to work. Retreatments may be necessary the following year if suckering occurs or the plant hasn't been entirely killed.

NOTE ON HERBICIDES: It is highly recommended that small populations try to be controlled using non-chemical methods wherever feasible. However, for large infestations, and for a few plants specified above, herbicide use is essential. Apply herbicides carefully to avoid non-target plants, glyphosate is the least environmentally damaging herbicide in most cases. Add food coloring for visibility, and a soap-based sticker such as Cide-Kick. Glyphosate is ineffective on some

plants; for these, triclopyr (Garlon) may be indicated. When using herbicides, read the entire label and observe all precautions listed, including proper disposal. If in doubt, call your local Cooperative Extension Service.

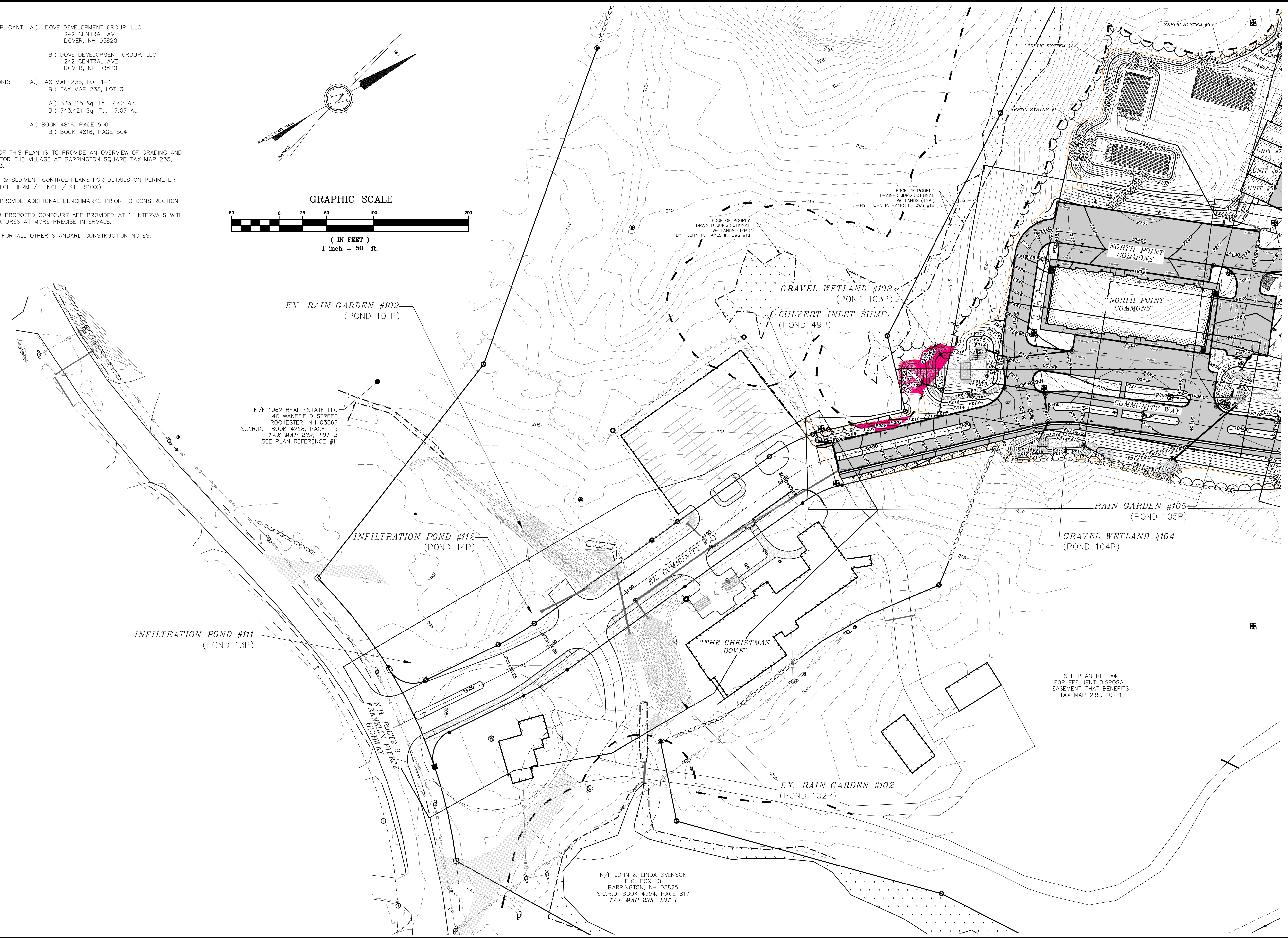
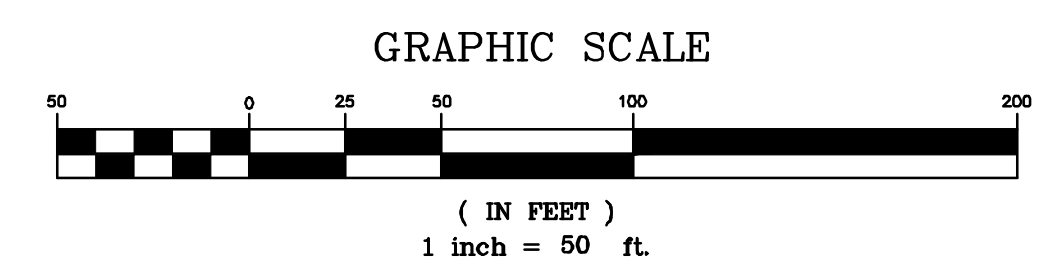
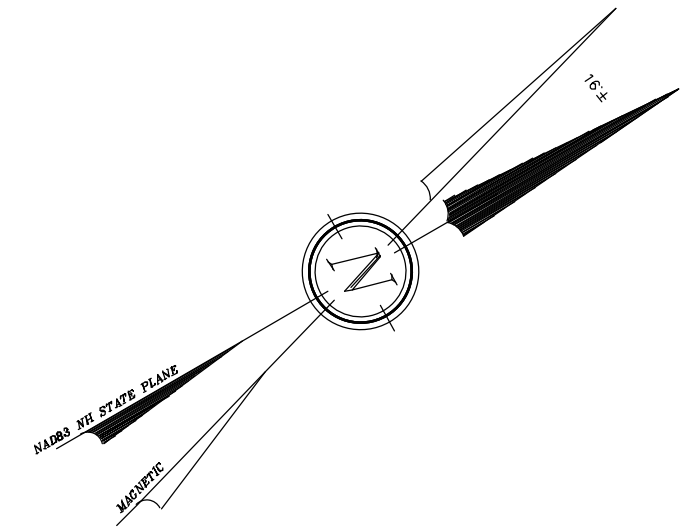
Pavement Temp. (°F) and Trend (↑ ↓)	Weather Condition	Maintenance Actions	Application Rate (lbs/per 1000 sq.ft.)			
			Salt Prewetted/Pre treated with salt brine	Salt Prewetted/Pret reated with other blends	Dry salt	Winter sand
>30 ↑	Snow	Plow, treat intersections only				Not recommended
	Frz. Rain	Apply chemical				Not recommended
30 ↓	Snow	Plow and apply chemical				Not recommended
	Frz. Rain	Apply chemical				Not recommended
25 - 30 ↑	Snow	Plow and apply chemical				Not recommended
	Frz. Rain	Apply chemical				Not recommended
25 - 30 ↓	Snow	Plow and apply chemical				Not recommended
	Frz. Rain	Apply chemical				3.25
20 - 25 ↑	Snow or frz. Rain	Plow and Apply chemical				3.25 for frz. Rain
20 - 25 ↓	Snow	Plow and apply chemical				Not recommended
	Frz. Rain	Apply chemical				3.25
15 - 20 ↑	Snow	Plow and apply chemical				Not recommended
	Frz. Rain	Apply chemical				3.25
15 - 20 ↓	Snow or Frz. Rain	Plow and apply chemical				3.25 for frz. Rain
0 to 15 ↑↓	Snow	Plow, treat with blends, sand hazardous areas	Not recommended		Not recommended	5.0 and spot-treat as needed
< 0	Snow	Plow, treat with blends, sand hazardous areas	Not recommended		Not recommended	5.0 and spot-treat as needed

Table 19. Application Rates for Deicing

These rates & table format are based on road application guidelines (Mn Snow & Ice Control Field Handbook, Manual 2005-1). Develop your own application rates by adjusting your current rates incrementally downward toward these guidelines. Where temperature categories overlap, select the rate most applicable to your situation.

NOTES:

- 1.) OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
B.) DOVE DEVELOPMENT GROUP, LLC
242 CENTRAL AVE
DOVER, NH 03820
- 2.) LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
B.) TAX MAP 235, LOT 3
- 3.) LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
B.) 743,421 Sq. Ft., 17.07 Ac.
- 4.) S.C.R.D.: A.) BOOK 4816, PAGE 500
B.) BOOK 4816, PAGE 504
- 5.) THE INTENT OF THIS PLAN IS TO PROVIDE AN OVERVIEW OF GRADING AND ENGINEERING FOR THE VILLAGE AT BARRINGTON SQUARE TAX MAP 235, LOTS 1-1 & 3.
- 6.) SEE EROSION & SEDIMENT CONTROL PLANS FOR DETAILS ON PERIMETER CONTROL (MULCH BERM / FENCE / SILT SOXX).
- 7.) BS&E IS TO PROVIDE ADDITIONAL BENCHMARKS PRIOR TO CONSTRUCTION.
- 8.) EXISTING AND PROPOSED CONTOURS ARE PROVIDED AT 1' INTERVALS WITH DRAINAGE FEATURES AT MORE PRECISE INTERVALS.
- 9.) SEE SHEET 2 FOR ALL OTHER STANDARD CONSTRUCTION NOTES.



N/F 1962 REAL ESTATE LLC
40 WAKEFIELD STREET
ROCHESTER, NH 03866
S.C.R.D. BOOK 4268, PAGE 115
TAX MAP 239, LOT 2
SEE PLAN REFERENCE #11

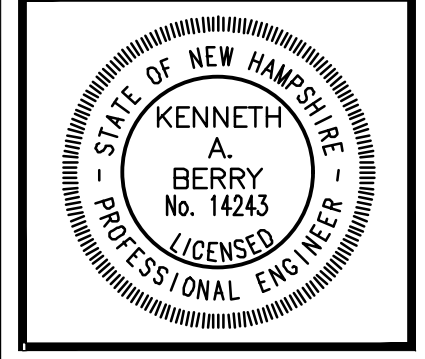
N/F JOHN & LINDA SVENSON
P.O. BOX 10
BARRINGTON, NH 03825
S.C.R.D. BOOK 4554, PAGE 817
TAX MAP 235, LOT 1

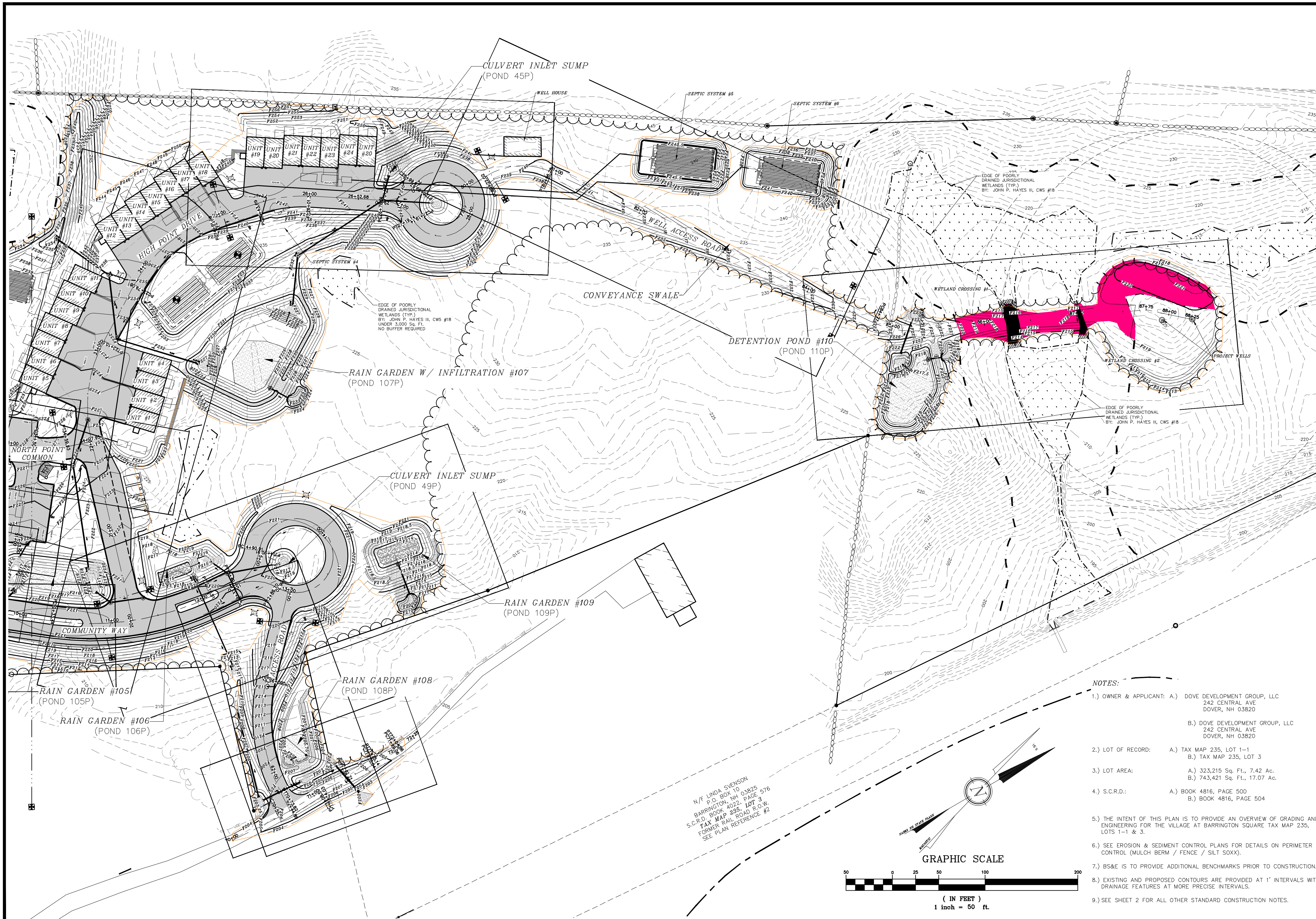
SEE PLAN REF #4
FOR EFFLUENT DISPOSAL
EASEMENT THAT BENEFITS
TAX MAP 235, LOT 1

REVISION	DATE	DESCRIPTION

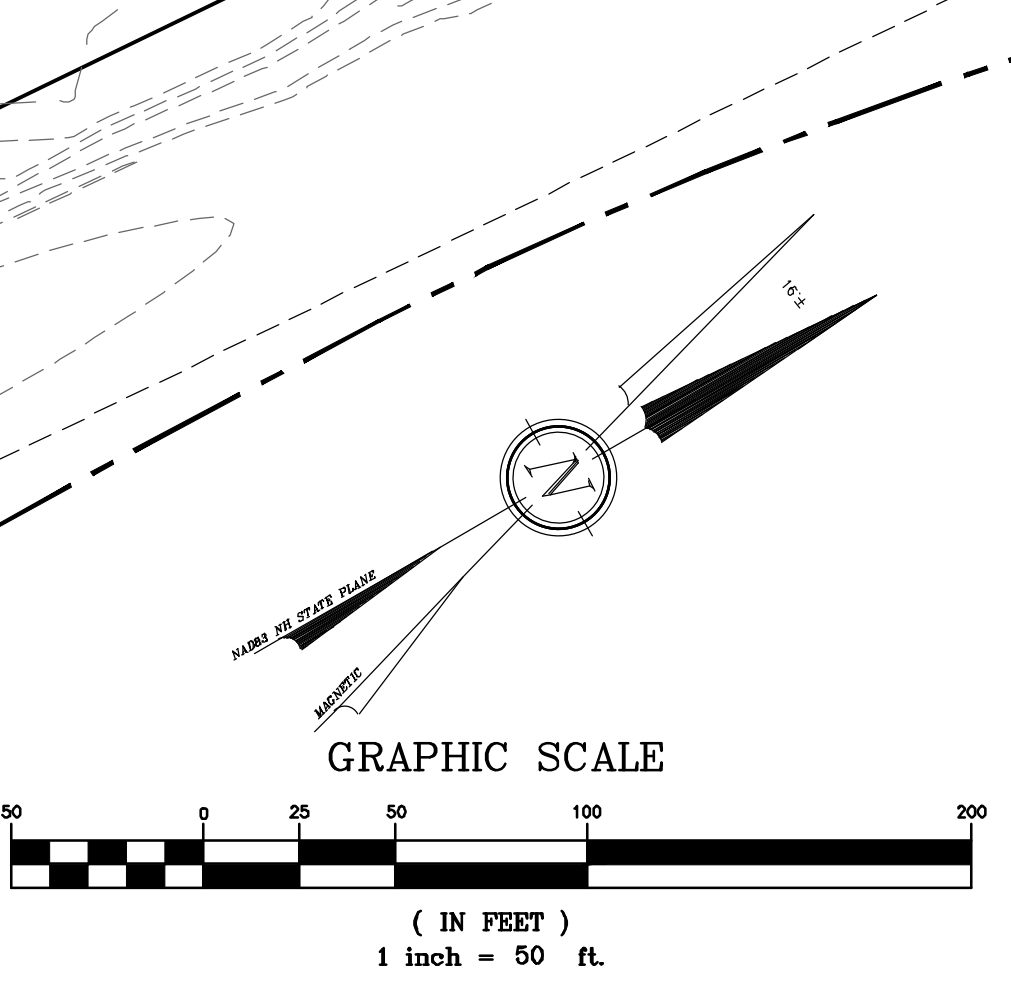
DRAINAGE INSPECTION & MAINTENANCE PLAN SOUTH
LAND OF
DOVE DEVELOPMENT GROUP, LLC
N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
COMMUNITY WAY
BARRINGTON, NH
TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

BERRY SURVEYING & ENGINEERING
335 SECOND CROWN POINT ROAD
BARRINGTON, NH 03825 (603)332-2863
SCALE : 1 IN. EQUALS 50 FT.
DATE : JUNE 14, 2021
FILE NO. : DB 2020 - 097





N/E LINDA SVENSON
 P.O. BOX 10
 BARRINGTON, NH 03825
 S.C.R.D. BOOK 4022 PAGE 576
 TAX MAP 235 LOT 3
 FORMER RAIL ROAD R.O.N.
 SEE PLAN REFERENCE #2



- NOTES:
- OWNER & APPLICANT: A.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 B.) DOVE DEVELOPMENT GROUP, LLC
 242 CENTRAL AVE
 DOVER, NH 03820
 - LOT OF RECORD: A.) TAX MAP 235, LOT 1-1
 B.) TAX MAP 235, LOT 3
 - LOT AREA: A.) 323,215 Sq. Ft., 7.42 Ac.
 B.) 743,421 Sq. Ft., 17.07 Ac.
 - S.C.R.D.: A.) BOOK 4816, PAGE 500
 B.) BOOK 4816, PAGE 504
 - THE INTENT OF THIS PLAN IS TO PROVIDE AN OVERVIEW OF GRADING AND ENGINEERING FOR THE VILLAGE AT BARRINGTON SQUARE TAX MAP 235, LOTS 1-1 & 3.
 - SEE EROSION & SEDIMENT CONTROL PLANS FOR DETAILS ON PERIMETER CONTROL (MULCH BERM / FENCE / SILT SOXX).
 - BS&E IS TO PROVIDE ADDITIONAL BENCHMARKS PRIOR TO CONSTRUCTION.
 - EXISTING AND PROPOSED CONTOURS ARE PROVIDED AT 1' INTERVALS WITH DRAINAGE FEATURES AT MORE PRECISE INTERVALS.
 - SEE SHEET 2 FOR ALL OTHER STANDARD CONSTRUCTION NOTES.

BERRY SURVEYING & ENGINEERING
 335 SECOND CROWN POINT ROAD
 BARRINGTON, NH 03825 (603)332-2863
 SCALE : 1 IN. EQUALS 50 FT.
 DATE : JUNE 14, 2021
 FILE NO. : DB 2020 - 097

DRAINAGE INSPECTION & MAINTENANCE PLAN NORTH
 LAND OF
 DOVE DEVELOPMENT GROUP, LLC
 N.H. ROUTE 9 / FRANKLIN PIERCE HIGHWAY
 COMMUNITY WAY
 BARRINGTON, NH
 TAX MAP 235 LOT 1-1 & MAP 235 LOT 3

REVISION	DATE	DESCRIPTION

Each Watershed Report Card covers a single 12-digit Hydrologic Unit Code (HUC12), on average a 34 square mile area. Each Watershed Report Card has three components;

1. REPORT CARD - A one page card that summarizes the overall use support for Aquatic Life Integrity, Primary Contact (i.e. Swimming), and Secondary Contact (i.e. Boating) Designated Uses on every Assessment Unit ID (AUID) within the HUC12.
2. HUC 12 MAP - A map of the watershed with abbreviated labels for each AUID within the HUC12.
3. ASSESSMENT DETAILS - Anywhere from one to forty pages with the detailed assessment information for each and every AUID in the Report Card and Map.

How are the Surface Water Quality Assessment determinations made?

All readily available data with reliable Quality Assurance/Quality Control is used in the biennial surface water quality assessments. For a full understanding of how the Surface Water Quality Standards (Env-Wq 1700) are translated into surface water quality assessments we urge the reader to review the [2020 Consolidated Assessment and Listing Methodology \(CALM\)](#).

Where can I find more advanced mapping resources?

GIS files are available by assessment cycle at the NHDES [FTP site](#).

I'd like to see the more raw water quality data?

The [web mapping tool](#) allows you to download the data used in the assessment of the primary contact and aquatic life designated uses by clicking on the “[Data Access Waterbody Data \(Aquatic Life and Swimming Uses\)](#)” link for any assessment unit.

How are assessments coded in the report card?

Assessment outcomes are displayed on a color scale as well as an alpha numeric scale that provides additional distinctions for the designated use and parameter level assessments as outlined in the table below.

	Severe	Poor	Likely Bad	No Data	Likely Good	Marginal	Good
	Not Supporting, Severe	Not Supporting, Marginal	Insufficient Information – Potentially Not Supporting	No Data	Insufficient Information – Potentially Full Supporting	Full Support, Marginal	Full Support, Good
CATEGORY	Description						
Category 2	Meets standards					2-M or 2-OBS	2-G
Category 3	Insufficient Information		3-PNS	3-ND	3-PAS		
Category 4	Does not Meet Standards;						
4A	TMDL* Completed	4A-P	4A-M or 4A-T				
4B	Other enforceable measure will correct the issue.	4B-P	4B-M or 4B-T				
4C	Non-pollutant (i.e. exotic weeds)	4C-P	4C-M				
Category 5	TMDL* Needed	5-P	5-M or 5-T				

* [TMDL](#) stands for Total Maximum Daily Load studies

Watershed 305(b) Assessment Summary Report:

Assessment Cycle: Draft 2020

HUC 12: 010600030607

HUC 12 Name: Lower Isinglass River

(Locator map on next page only applies to this HUC12)

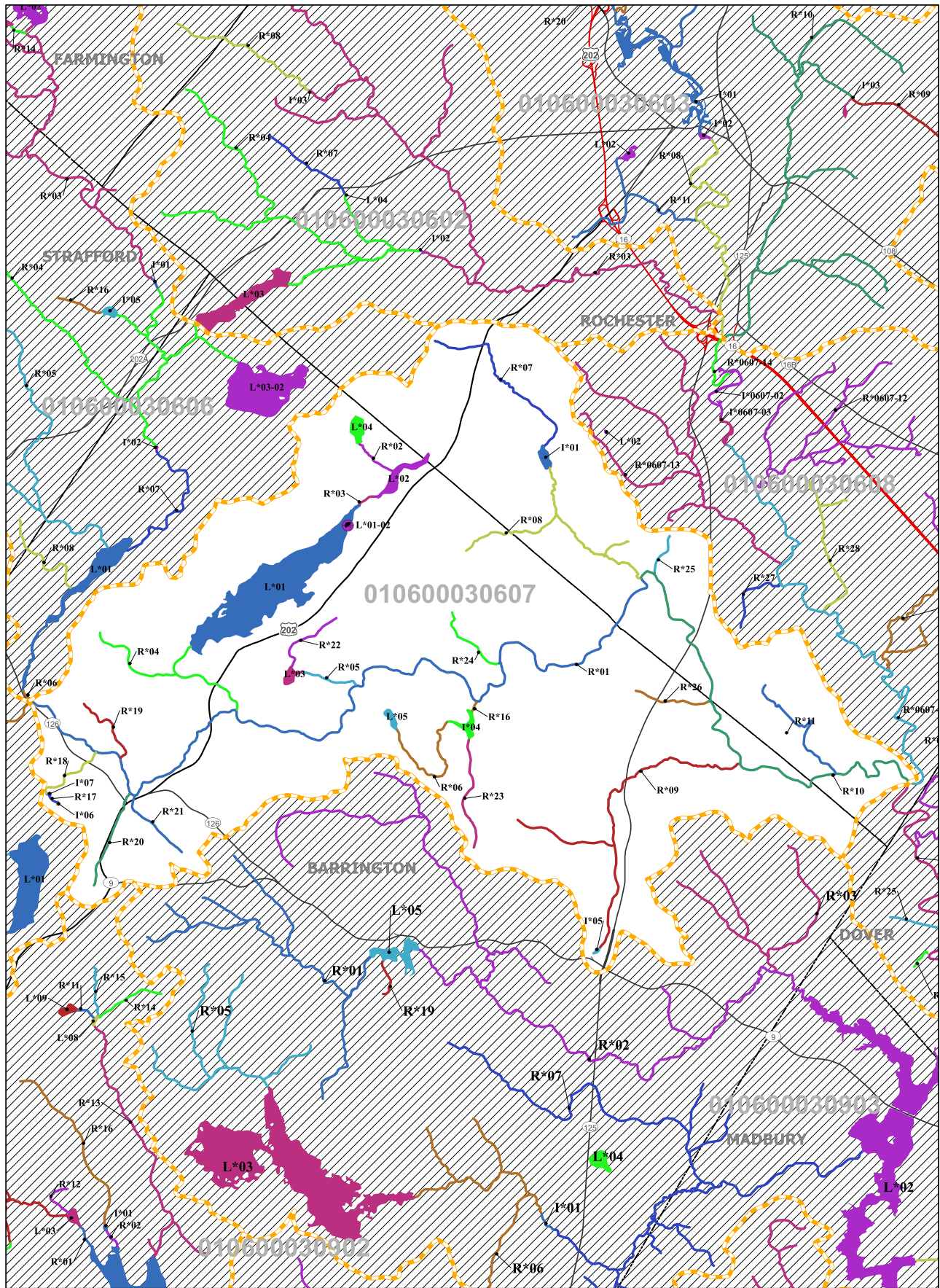
Good	Meets water quality standards/thresholds by a relatively large margin.
Marginal	Meets water quality standards/thresholds but only marginally.
Likely Good	Limited data available, however, the data that is available suggests that the parameter is Potentially Attaining Standards (PAS).
No Current Data	Insufficient information to make an assessment decision.
Likely Bad	Limited data available, however, the data that is available suggests that the parameter is Potentially Not Supporting (PNS) water quality standards.
Poor	Not meeting water quality standards/thresholds. The impairment is marginal.
Severe	Not meeting water quality standards/thresholds. The impairment is more severe and causes poor water quality.



Assessment Unit ID	Map Label	Assessment Unit Name	Aquatic Life	Fish Consump.	Swimming	Boating
NHIMP600030607-01	I*01	Hanson Brook		4A-M	3-ND	3-ND
NHIMP600030607-04	I*04	Unnamed Brook - Scruton Pond Road	3-ND	4A-M	3-ND	3-ND
NHIMP600030607-05	I*05	Unnamed Brook - Fire Protection Pond	3-ND	4A-M	3-ND	3-ND
NHIMP600030607-06	I*06	Unnamed Brook - Golf Course Pond	3-ND	4A-M	3-ND	3-ND
NHIMP600030607-07	I*07	Unnamed Brook - Wildlife And Fire Protection Pond	3-ND	4A-M	3-ND	3-ND
NHLAK600030607-01	L*01	Ayers Pond	4A-M	4A-M	3-PAS	3-PAS
NHLAK600030607-01-02	L*01-02	Ayers Pond - Camp Fireside Beach	3-ND	4A-M	2-M	2-G
NHLAK600030607-02	L*02	Little Long Pond	3-ND	4A-M	3-ND	3-ND
NHLAK600030607-03	L*03	Farm Pond	3-ND	4A-M	3-ND	3-ND
NHLAK600030607-04	L*04	Preston Pond	3-ND	4A-M	3-ND	3-ND
NHLAK600030607-05	L*05	Scruton Pond	3-PNS	4A-M	3-PAS	3-ND
NHRIV600030607-01	R*01	Isinglass River	5-M	4A-M	2-G	2-G

NHRIV600030607-02	R*02	Unnamed Brook - From Preston Pond To Little Long Pong	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-03	R*03	Ayers Pond Brook	5-M	4A-M	3-ND	3-ND
NHRIV600030607-04	R*04	Ayers Pond Brook	5-M	4A-M	3-ND	3-ND
NHRIV600030607-05	R*05	Unnamed Brook - From Farm Pond To Isinglass River	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-06	R*06	Scrutton Pond Brook	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-07	R*07	Unnamed Brook - To Hanson Pond	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-08	R*08	Hanson Brook	5-M	4A-M	3-ND	3-ND
NHRIV600030607-09	R*09	Green Hill Brook	5-M	4A-M	3-ND	3-ND
NHRIV600030607-10	R*10	Isinglass River	5-M	4A-M	4A-M	2-G
NHRIV600030607-11	R*11	Unnamed Brook - To Isinglass River	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-16	R*16	Scrutton Pond Outlet Brook	5-P	4A-M	3-ND	3-ND
NHRIV600030607-17	R*17	Unnamed Brook	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-18	R*18	Unnamed Brook	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-19	R*19	Unnamed Brook	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-20	R*20	Unnamed Brook	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-21	R*21	Unnamed Brook	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-22	R*22	Unnamed Brook	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-23	R*23	Unnamed Brook	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-24	R*24	Unnamed Brook	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-25	R*25	Unnamed Brook	3-ND	4A-M	3-ND	3-ND
NHRIV600030607-26	R*26	Unnamed Brook	3-ND	4A-M	3-ND	3-ND

AUIDs For HUC12: 010600030607 - Lower Isinglass River



	HUC12 Boundaries		4 =
	Town Boundaries		5 =
	Major Roads		6 =
	Interstate Highway		7 =
	US Highway		8 =
	State Highway		9 =

Assessment Unit Coloring

AUs Ending with:

- 0 =
- 1 =
- 2 =
- 3 =



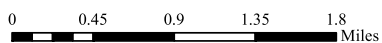
Abbrev. Label HUC 12

L*03 010700060201

↓ ↓

AUID = NH LAK700060201-03

Assessment Unit IDs are derived from the HUC12 they reside within. The labels have been shortened on this map for presentation purposes. Example: the Label "L*03" in HUC12 = 010700060201 represents AUID = "NHLAK700060201-03". In rare cases where an AUID extends beyond the boundary of a single HUC12, additional portions of the end of the HUC 12 number have also been replaced.



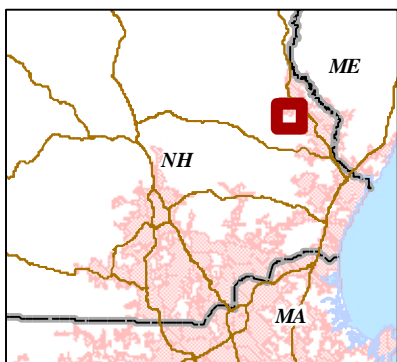
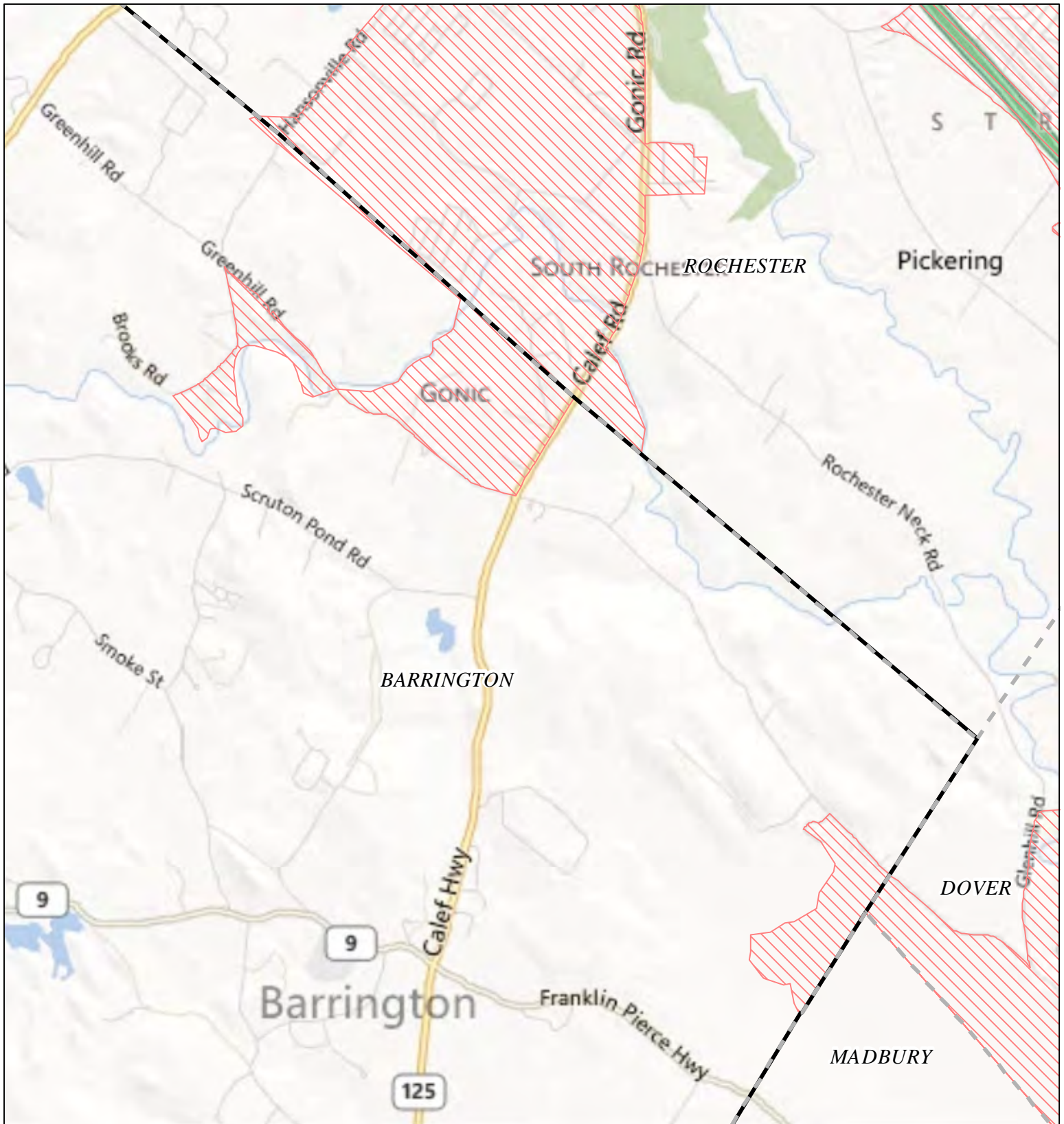
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Designated Use Description	Desig. Use Category	Parameter Name	Parameter Threatened (Y/N)	Last Sample	Last Exceed	Parameter Category	TMDL Priority
Aquatic Life Integrity	5-M	Benthic-Macroinvertebrate Bioassessments (Streams)	N			3-ND	
		Chloride	N	2008	N/A	3-ND	
		Dissolved Oxygen Saturation	N	2008	N/A	3-ND	
		Fishes Bioassessments (Streams)	N			3-ND	
		Oxygen, Dissolved	N	2008	N/A	3-ND	
		Ph	N	2008	2008	5-M	LOW
		Turbidity	N	2008	N/A	3-ND	
Fish Consumption	4A-M	Mercury - Fish Consumption Advisory	N			4A-M	
Potential Drinking Water Supply	2-G						
Primary Contact Recreation	3-ND	Escherichia Coli	N			3-ND	
Secondary Contact Recreation	3-ND	Escherichia Coli	N			3-ND	
Wildlife	3-ND						

Good	Marginal	Likely Good	No Current Data	Likely Bad	Poor	Severe
Meets water quality standards/thresholds by a relatively large margin.	Meets water quality standards/thresholds but only marginally.	Limited data available. The data that is available suggests that the parameter is Potentially Attaining Standards (PAS)	Insufficient information to make an assessment decision.	Limited data available The data that is available suggests that the parameter is Potentially Not Supporting (PNS) water quality standards.	Not meeting water quality standards/thresholds. The impairment is marginal.	Not meeting water quality standards/thresholds The impairment is more severe and causes poor water quality.

Year	Stream Name	Location	Length (Miles)	Assessment	Category	Priority	Assessment Details	Notes
2018	NHRIV600030603-08	COCHeco RIVER	2.428 MILES	4C-P	Non-ORW			
2018	NHRIV600030603-08	COCHeco RIVER	2.428 MILES	5-M	Non-ORW			
2018	NHRIV600030603-08	COCHeco RIVER	2.428 MILES	4A-P	Non-ORW	39772	9/21/2010 NEW HAMPSHIRE STATEWIDE E	
2018	NHRIV600030603-10	WILLOW BROOK	7.347 MILES	5-P	Non-ORW			
2018	NHRIV600030603-10	WILLOW BROOK	7.347 MILES	5-P	Non-ORW			
2018	NHRIV600030603-10	WILLOW BROOK	7.347 MILES	5-M	Non-ORW			
2018	NHRIV600030603-10	WILLOW BROOK	7.347 MILES	4A-P	Non-ORW	39772	9/21/2010 NEW HAMPSHIRE STATEWIDE E	
2018	NHRIV600030603-11	HURD BROOK	1.621 MILES	5-M	Non-ORW			
2018	NHRIV600030604-01	UNNAMED BROOKS - TO BOW LAKE	4.812 MILES	ORW	ORW			
2018	NHRIV600030604-02	UNNAMED BROOK - TO BOW LAKE	1.323 MILES	ORW	ORW			
2018	NHRIV600030604-03	UNNAMED BROOK - TO BOW LAKE	0.873 MILES	ORW	ORW			
2018	NHRIV600030604-04	SHERBOURNE BROOK	2.885 MILES	ORW	ORW			
2018	NHRIV600030604-05	SHERBURNE BROOK - UNNAMED BROOK	0.823 MILES	ORW	ORW			
2018	NHRIV600030604-06	SHERBURNE BROOK	1.357 MILES	ORW	ORW			
2018	NHRIV600030604-07	UNNAMED BROOK - A FROM PINE ROCK FJ STRAFFORD	0.643 MILES	ORW	ORW			
2018	NHRIV600030604-08	UNNAMED BROOK - TO BOW LAKE	0.982 MILES	ORW	ORW			
2018	NHRIV600030604-09	UNNAMED BROOK	0.479 MILES	ORW	ORW			
2018	NHRIV600030604-10	UNNAMED BROOK	0.609 MILES	ORW	ORW			
2018	NHRIV600030604-11	UNNAMED BROOK	0.168 MILES	ORW	ORW			
2018	NHRIV600030604-12	UNNAMED BROOK	0.07 MILES	ORW	ORW			
2018	NHRIV600030604-13	UNNAMED BROOK	0.086 MILES	ORW	ORW			
2018	NHRIV600030604-14	UNNAMED BROOK	1.276 MILES	ORW	ORW			
2018	NHRIV600030604-15	UNNAMED BROOK	0.63 MILES	ORW	ORW			
2018	NHRIV600030604-16	UNNAMED BROOK	2.178 MILES	ORW	ORW			
2018	NHRIV600030605-01	UNNAMED BROOK - TO UNNAMED POND STRAFFORD	3.474 MILES	ORW	ORW			
2018	NHRIV600030605-03	UNNAMED BROOK - TO UNNAMED POND STRAFFORD	1.467 MILES	ORW	ORW			
2018	NHRIV600030605-04	UNNAMED BROOK - TO WILDLIFE POND STRAFFORD	0.31 MILES	ORW	ORW			
2018	NHRIV600030605-05	MOHAWK BROOK	10.233 MILES	ORW	ORW			
2018	NHRIV600030605-06	UNNAMED BROOK - TO UNNAMED POND STRAFFORD	0.75 MILES	ORW	ORW			
2018	NHRIV600030605-07	UNNAMED BROOK - TO HUCKINS MILL POJ STRAFFORD	0.511 MILES	ORW	ORW			
2018	NHRIV600030605-08	UNNAMED BROOK - FROM HUCKINS MILL STRAFFORD	0.469 MILES	ORW	ORW			
2018	NHRIV600030605-09	PENNY BROOK	1.912 MILES	ORW	ORW			
2018	NHRIV600030605-10	ISINGLASS RIVER	0.459 MILES	ORW	ORW			
2018	NHRIV600030605-11	ISINGLASS RIVER	4.467 MILES	ORW	ORW			
2018	NHRIV600030605-12	UNNAMED BROOK - TO ISINGLASS RIVER	2.183 MILES	ORW	ORW			
2018	NHRIV600030605-13	UNNAMED BROOK - TO ISINGLASS RIVER	0.729 MILES	ORW	ORW			
2018	NHRIV600030605-14	STONEHOUSE BROOK - HALL BROOK	7.02 MILES	ORW	ORW			
2018	NHRIV600030605-15	NIPPO BROOK	12.125 MILES	ORW	ORW			
2018	NHRIV600030605-16	ISINGLASS RIVER	0.778 MILES	ORW	ORW			
2018	NHRIV600030605-17	UNNAMED BROOK	1.609 MILES	ORW	ORW			
2018	NHRIV600030605-18	UNNAMED BROOK	0.865 MILES	ORW	ORW			
2018	NHRIV600030605-19	UNNAMED BROOK	0.359 MILES	ORW	ORW			
2018	NHRIV600030605-20	UNNAMED BROOK	0.46 MILES	ORW	ORW			
2018	NHRIV600030606-03	BERRY'S RIVER	5.2 MILES	5-P	Non-ORW			
2018	NHRIV600030606-04	BERRY'S RIVER - UNNAMED BROOK	5.705 MILES	4C-P	Non-ORW			
2018	NHRIV600030606-04	BERRY'S RIVER - UNNAMED BROOK	5.705 MILES	5-M	Non-ORW			
2018	NHRIV600030606-06	BERRY RIVER - FROM LONG POND TO ISIN BARRINGTON	0.107 MILES	5-M	Non-ORW			
2018	NHRIV600030606-06	BERRY RIVER - FROM LONG POND TO ISIN BARRINGTON	0.107 MILES	5-M	Non-ORW			
2018	NHRIV600030606-07	BERRY'S RIVER	1.26 MILES	5-P	Non-ORW			
2018	NHRIV600030607-01	ISINGLASS RIVER	7.336 MILES	5-M	Non-ORW			
2018	NHRIV600030607-01	ISINGLASS RIVER	7.336 MILES	5-P	Non-ORW			
2018	NHRIV600030607-03	AYERS POND BROOK	0.128 MILES	5-M	Non-ORW			
2018	NHRIV600030607-03	AYERS POND BROOK	0.128 MILES	5-M	Non-ORW			
2018	NHRIV600030607-04	AYERS POND BROOK	1.691 MILES	5-M	Non-ORW			
2018	NHRIV600030607-04	AYERS POND BROOK	1.691 MILES	5-M	Non-ORW			
2018	NHRIV600030607-09	GREEN HILL BROOK	3.224 MILES	5-M	Non-ORW			
2018	NHRIV600030607-10	ISINGLASS RIVER	3.796 MILES	5-M	Non-ORW			
2018	NHRIV600030607-10	ISINGLASS RIVER	3.796 MILES	5-M	Non-ORW			
2018	NHRIV600030607-10	ISINGLASS RIVER	3.796 MILES	4A-M	Non-ORW	40663	8/29/2011 58 NH BACTERIA IMPAIRED WA	
2018	NHRIV600030607-15	COCHeco RIVER	4.414 MILES	5-M	Non-ORW			
2018	NHRIV600030607-15	COCHeco RIVER	4.414 MILES	5-M	Non-ORW			
2018	NHRIV600030607-16	SCRUTON POND OUTLET BROOK	0.071 MILES	5-M	Non-ORW			
2018	NHRIV600030607-16	SCRUTON POND OUTLET BROOK	0.071 MILES	5-P	Non-ORW			
2018	NHRIV600030607-16	SCRUTON POND OUTLET BROOK	0.071 MILES	5-P	Non-ORW			
2018	NHRIV600030608-02	BLACKWATER BROOK-CLARK BROOK	15.228 MILES	4A-P	Non-ORW	39772	9/21/2010 NEW HAMPSHIRE STATEWIDE E	
2018	NHRIV600030608-03	COCHeco RIVER - UNNAMED BROOK	3.267 MILES	5-M	Non-ORW			
2018	NHRIV600030608-03	COCHeco RIVER - UNNAMED BROOK	3.267 MILES	5-M	Non-ORW			
2018	NHRIV600030608-03	COCHeco RIVER - UNNAMED BROOK	3.267 MILES	4A-M	Non-ORW	39772	9/21/2010 NEW HAMPSHIRE STATEWIDE E	
2018	NHRIV600030608-04	REYNERS BROOK	1.77 MILES	4A-P	Non-ORW	39772	9/21/2010 NEW HAMPSHIRE STATEWIDE E	
2018	NHRIV600030608-05	COCHeco RIVER	2.06 MILES	5-M	Non-ORW			

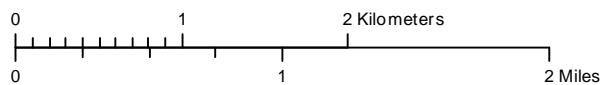
2020	NHRV60030603-10	WILLOW BROOK	ROCHESTER	Yes	7.347	MILES	Aquatic Life integrity	Benthic-Mac invertebrate Bioassessments (Streams)	5-P	LOW	N	2011
2020	NHRV60030603-10	WILLOW BROOK	ROCHESTER	Yes	7.347	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-P	LOW	N	2011
2020	NHRV60030603-10	WILLOW BROOK	ROCHESTER	Yes	7.347	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-P	LOW	N	2011
2020	NHRV60030603-10	WILLOW BROOK	ROCHESTER	Yes	7.347	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2017
2020	NHRV60030603-11	MOHAWK BROOK	ROCHESTER	Yes	1.621	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2007
2020	NHRV60030605-05	MOHAWK BROOK	STRAFFORD, BARRINGTON		10.233	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2009
2020	NHRV60030605-05	MOHAWK BROOK	STRAFFORD, BARRINGTON		10.233	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-P	LOW	N	2009
2020	NHRV60030605-10	MOHAWK BROOK	STRAFFORD, BARRINGTON		4.459	MILES	Aquatic Life integrity	pH	5-P	LOW	N	2009
2020	NHRV60030605-11	SINGLASS RIVER	STRAFFORD, BARRINGTON		4.467	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2019
2020	NHRV60030605-12	UNNAMED BROOK - TO SINGLASS RIVER	STRAFFORD, BARRINGTON		2.883	MILES	Aquatic Life integrity	pH	5-P	LOW	N	2016
2020	NHRV60030605-14	STONEHOUSE BROOK - HALL BROOK	BARRINGTON, NORTHWOOD, STRAFFORD		7.020	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-P	LOW	N	2009
2020	NHRV60030605-14	STONEHOUSE BROOK - HALL BROOK	BARRINGTON, NORTHWOOD, STRAFFORD		7.020	MILES	Aquatic Life integrity	pH	5-P	LOW	N	2009
2020	NHRV60030605-15	NIPPO BROOK	BARRINGTON, STRAFFORD		12.125	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2009
2020	NHRV60030605-15	NIPPO BROOK	BARRINGTON, STRAFFORD		12.125	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2009
2020	NHRV60030605-16	SINGLASS RIVER	STRAFFORD, BARRINGTON		0.778	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2019
2020	NHRV60030605-16	SINGLASS RIVER	STRAFFORD, BARRINGTON		0.778	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2019
2020	NHRV60030606-03	BERRYS RIVER	ROCHESTER, FARMINGTON, ROCHESTER		5.200	MILES	Aquatic Life integrity	pH	5-P	LOW	N	2009
2020	NHRV60030606-04	BERRYS RIVER - UNNAMED BROOK	STRAFFORD, BARRINGTON		5.705	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2007
2020	NHRV60030606-06	BERRYS RIVER - FROM LONG POND TO SINGLASS RIVER	BARRINGTON		0.107	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2007
2020	NHRV60030606-06	BERRYS RIVER - FROM LONG POND TO SINGLASS RIVER	BARRINGTON		0.107	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-M	LOW	N	2009
2020	NHRV60030606-06	BERRYS RIVER - FROM LONG POND TO SINGLASS RIVER	BARRINGTON		0.107	MILES	Aquatic Life integrity	pH	5-P	LOW	N	2009
2020	NHRV60030606-07	BERRYS RIVER	BARRINGTON	Yes	1.260	MILES	Aquatic Life integrity	pH	5-P	LOW	N	2009
2020	NHRV60030607-01	SINGLASS RIVER	BARRINGTON, ROCHESTER	Yes	7.336	MILES	Aquatic Life integrity	Benthic-Mac invertebrate Bioassessments (Streams)	5-M	LOW	N	2015
2020	NHRV60030607-01	SINGLASS RIVER	BARRINGTON, ROCHESTER	Yes	7.336	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2019
2020	NHRV60030607-03	AYERS POND BROOK	BARRINGTON	Yes	0.128	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-M	LOW	N	2009
2020	NHRV60030607-03	AYERS POND BROOK	BARRINGTON	Yes	0.128	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2019
2020	NHRV60030607-04	AYERS POND BROOK	BARRINGTON	Yes	1.691	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-M	LOW	N	2009
2020	NHRV60030607-04	AYERS POND BROOK	BARRINGTON	Yes	1.691	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2019
2020	NHRV60030607-08	HANSON BROOK	ROCHESTER, BARRINGTON	Yes	2.411	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2019
2020	NHRV60030607-09	GREEN HILL BROOK	BARRINGTON	Yes	3.224	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2008
2020	NHRV60030607-10	SINGLASS RIVER	ROCHESTER, BARRINGTON	Yes	3.796	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2019
2020	NHRV60030607-10	SINGLASS RIVER	ROCHESTER, BARRINGTON	Yes	3.796	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2019
2020	NHRV60030607-15	COCHEO RIVER	ROCHESTER, BARRINGTON	Yes	4.414	MILES	Aquatic Life integrity	Iron	5-M	LOW	N	2013
2020	NHRV60030607-15	COCHEO RIVER	ROCHESTER, BARRINGTON	Yes	4.414	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2019
2020	NHRV60030607-16	SCRUTTON POND OUTLET BROOK	BARRINGTON		0.071	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2008
2020	NHRV60030607-16	SCRUTTON POND OUTLET BROOK	BARRINGTON		0.071	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-P	LOW	N	2008
2020	NHRV60030607-16	SCRUTTON POND OUTLET BROOK	BARRINGTON		0.071	MILES	Aquatic Life integrity	pH	5-P	LOW	N	2008
2020	NHRV60030608-03	COCHEO RIVER - UNNAMED BROOK	DOVER, ROCHESTER	Yes	3.267	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2013
2020	NHRV60030608-03	COCHEO RIVER - UNNAMED BROOK	DOVER, ROCHESTER	Yes	3.267	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2013
2020	NHRV60030608-05	COCHEO RIVER	DOVER, ROCHESTER	Yes	2.060	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2013
2020	NHRV60030608-05	COCHEO RIVER	DOVER, ROCHESTER	Yes	2.060	MILES	Aquatic Life integrity	Chloride	5-P	LOW	N	2009
2020	NHRV60030608-06	INDIAN BROOK	DOVER	Yes	1.106	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2009
2020	NHRV60030608-08	FRESH CREEK - TWOMBLY BROOK	ROLLINSFORD, SOMERSWORTH	Yes	4.983	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-M	LOW	N	2009
2020	NHRV60030608-08	FRESH CREEK - TWOMBLY BROOK	ROLLINSFORD, SOMERSWORTH	Yes	4.983	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2009
2020	NHRV60030608-08	FRESH CREEK - TWOMBLY BROOK	ROLLINSFORD, SOMERSWORTH	Yes	4.983	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-P	LOW	N	2009
2020	NHRV60030608-08	FRESH CREEK - TWOMBLY BROOK	ROLLINSFORD, SOMERSWORTH	Yes	4.983	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2009
2020	NHRV60030608-10	ROLLINS BROOK	ROLLINSFORD	Yes	2.856	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2009
2020	NHRV60030608-10	ROLLINS BROOK	ROLLINSFORD	Yes	2.856	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-P	LOW	N	2009
2020	NHRV60030608-10	ROLLINS BROOK	ROLLINSFORD	Yes	2.856	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2009
2020	NHRV60030608-14	UNNAMED TRIB. TO COCHEO RIVER, DOVER (FROM BERRY BROOK)	DOVER	Yes	0.169	MILES	Aquatic Life integrity	Iron	5-M	LOW	N	2013
2020	NHRV60030608-14	UNNAMED TRIB. TO COCHEO RIVER, DOVER (FROM BERRY BROOK)	DOVER	Yes	0.169	MILES	Aquatic Life integrity	Benthic-Mac invertebrate Bioassessments (Streams)	5-M	LOW	N	2001
2020	NHRV60030608-15	BERRY BROOK	DOVER	Yes	1.106	MILES	Aquatic Life integrity	Chloride	5-M	LOW	N	2016
2020	NHRV60030701-01	LAMPREY RIVER - AND HEADWATER TRIBUTARIES	NORTHWOOD, DEERFIELD		13.652	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-P	LOW	N	2016
2020	NHRV60030701-01	LAMPREY RIVER - AND HEADWATER TRIBUTARIES	NORTHWOOD, DEERFIELD		13.652	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-P	LOW	N	2016
2020	NHRV60030701-01	LAMPREY RIVER - AND HEADWATER TRIBUTARIES	NORTHWOOD, DEERFIELD		13.652	MILES	Aquatic Life integrity	pH	5-P	LOW	N	2016
2020	NHRV60030701-01	HARTFORD BROOK	DEERFIELD		10.734	MILES	Aquatic Life integrity	Aluminum	5-M	LOW	N	2006
2020	NHRV60030701-01	HARTFORD BROOK	DEERFIELD		10.734	MILES	Aquatic Life integrity	Benthic-Mac invertebrate Bioassessments (Streams)	5-P	LOW	N	2003
2020	NHRV60030701-08	HARTFORD BROOK	DEERFIELD		10.734	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2006
2020	NHRV60030701-09	LAMPREY RIVER	DEERFIELD		7.767	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2017
2020	NHRV60030701-09	LAMPREY RIVER	DEERFIELD		7.767	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-P	LOW	N	2017
2020	NHRV60030701-09	LAMPREY RIVER	DEERFIELD		7.767	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2017
2020	NHRV60030701-13	LAMPREY RIVER	DEERFIELD		0.041	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2012
2020	NHRV60030701-13	LAMPREY RIVER	DEERFIELD		0.041	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2012
2020	NHRV60030702-06	NORTH BRANCH RIVER - UNNAMED BROOKS	DEERFIELD, CANDIA		5.185	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2017
2020	NHRV60030702-06	NORTH BRANCH RIVER - UNNAMED BROOKS	DEERFIELD, CANDIA		5.185	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-P	LOW	N	2017
2020	NHRV60030702-06	NORTH BRANCH RIVER - UNNAMED BROOKS	DEERFIELD, CANDIA		5.185	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2017
2020	NHRV60030702-07	NORTH BRANCH RIVER - UNNAMED BROOKS	CANDIA, DEERFIELD		10.013	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2017
2020	NHRV60030702-07	NORTH BRANCH RIVER - UNNAMED BROOKS	CANDIA, DEERFIELD		10.013	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-P	LOW	N	2017
2020	NHRV60030702-07	NORTH BRANCH RIVER - UNNAMED BROOKS	CANDIA, DEERFIELD		10.013	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2017
2020	NHRV60030703-01	UNNAMED BROOK - TO ONWAY LAKE	RAYMOND, CANDIA		5.450	MILES	Aquatic Life integrity	Benthic-Mac invertebrate Bioassessments (Streams)	5-P	LOW	N	1998
2020	NHRV60030703-01	UNNAMED BROOK - TO ONWAY LAKE	RAYMOND, CANDIA		5.450	MILES	Aquatic Life integrity	pH	5-M	LOW	N	1998
2020	NHRV60030703-04	DUDLEY BROOK - UNNAMED BROOK	RAYMOND, DEERFIELD, NOTTINGHAM	Yes	4.340	MILES	Aquatic Life integrity	Dissolved oxygen saturation	5-M	LOW	N	2019
2020	NHRV60030703-04	DUDLEY BROOK - UNNAMED BROOK	RAYMOND, DEERFIELD, NOTTINGHAM	Yes	4.340	MILES	Aquatic Life integrity	Lead	5-M	LOW	N	2005
2020	NHRV60030703-04	DUDLEY BROOK - UNNAMED BROOK	RAYMOND, DEERFIELD, NOTTINGHAM	Yes	4.340	MILES	Aquatic Life integrity	Oxygen, Dissolved	5-M	LOW	N	2000
2020	NHRV60030703-04	DUDLEY BROOK - UNNAMED BROOK	RAYMOND, DEERFIELD, NOTTINGHAM	Yes	4.340	MILES	Aquatic Life integrity	pH	5-P	LOW	N	2004
2020	NHRV60030703-04	DUDLEY BROOK - UNNAMED BROOK	RAYMOND, DEERFIELD, NOTTINGHAM	Yes	4.340	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2005
2020	NHRV60030703-05	LAMPREY RIVER	RAYMOND	Yes	2.647	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2019
2020	NHRV60030703-09	LAMPREY RIVER	RAYMOND	Yes	2.295	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2006
2020	NHRV60030703-10	LAMPREY RIVER	RAYMOND	Yes	0.558	MILES	Aquatic Life integrity	pH	5-M	LOW	N	2006



NPDES Phase II Stormwater Program
Automatically Designated MS4 Areas

Barrington NH

 Regulated Area (2000 + 2010 Urbanized Area)



Town Population: 8576
Regulated Population: 159
(Populations estimated from 2010 Census)



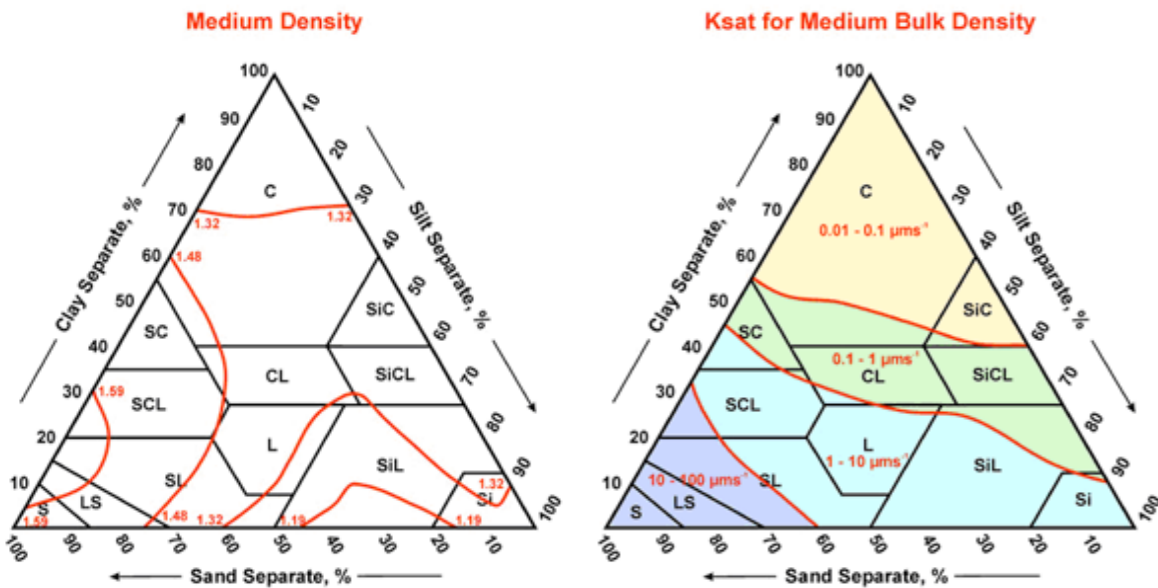
Urbanized Areas, Town Boundaries:
US Census (2000, 2010)
Base map © 2010 Microsoft Corporation
and its data suppliers

K_{sat} VALUES

FOR

NEW HAMPSHIRE SOILS

(Including Hydrologic and DES Soil Lot Sizing Groups)



From: Guide for Estimating Ksat from Soil Properties (Exhibit 618-9). (<http://soils.usda.gov/technical/handbook/contents/part618ex.html>)

Sponsored by the Society of Soil Scientists of Northern New England
 SSSNNE Special Publication No. 5
 September, 2009

K_{sat} VALUES FOR NEW HAMPSHIRE SOILS

ABOUT THE SOCIETY OF SOIL SCIENTISTS OF NORTHERN NEW ENGLAND

The Society of Soil Scientists of Northern New England (SSSNNE) is a non-profit professional organization of soil scientists, both in the private and public sectors, which is dedicated to the advancement of soil science. The Society fosters the profession of soil classification, mapping and interpretation, and encourages the dissemination of information concerning soil science. With the intent of contributing to the general human welfare, the Society seeks to educate the public on the wise use of soils and the associated natural resources.

INTRODUCTION

The publication “K_{sat} Values for New Hampshire Soils” is designed to assist soil scientists, engineers, and other professionals by assembling tables of existing data for all soil series currently on the state soil legend with regard to K_{sat} values and hydrologic groupings (Hyd.Grp.). The need for this information has become more important since the adoption by the New Hampshire Department of Environmental Services of the revised Alteration of Terrain rules for stormwater management. Additional information has been provided for each soil series with regard to landform, temperature regime (Temp.), soil textures, NHDES Soil Lot Size Groupings (Group), whether the soil is a Spodosol (Spodosol?) and other information which will be valuable to a variety of soil information users.

The data for each soil series has been sorted 3 ways for ease of searching:

Table A-Sorted by Numerical Legend

Table B-Sorted by Soil Series Name

Table C-Sorted by NHDES Soil Group for Establishing Lot Size

The report represents cumulative efforts by private soil scientists and NHDES staff with assistance from the USDA Natural Resource Conservation Service.

Comments or inquires on the information in this publication may be directed to the Board of Directors at the following address:

**Society of Soil Scientists
of Northern New England
PO Box 76
Durham, NH 03824**

SATURATED HYDRAULIC CONDUCTIVITY (K_{SAT})

K_{sat} refers to the ease with which pores in a saturated soil transmit water. The estimates presented here are expressed in terms of inches per hour (NRCS official data presents K_{sat} in both micrometers per second and inches per hour). K_{sat} values are based on soil characteristics observed in the field, particularly structure, consistence, porosity, and texture. (USDA NRCS, Web Soil Survey)

Saturated flow occurs when the soil water pressure is positive; that is, when the soil matric potential is zero (saturated wet condition). In most soils this situation takes place when about 95 percent of the total pore space is filled with water. The remaining 5 percent is filled with entrapped air. Saturated hydraulic conductivity cannot be used to describe water movement under unsaturated conditions. (Soil Survey Manual, 1993)

It is commonly known that soil features (and thus data) for a certain soil series name may be slightly different from one county soil survey to the next and the range in characteristics (via the Typical Pedon) may be slightly different. For example – a Marlow soil (series) in Carroll County may have a higher sand content in its B horizon as opposed to a Marlow soil (series) in Coos County; resulting in a slightly different K_{sat} range for the B horizon.

The K_{sat} data for this publication was obtained from the USDA-NRCS Soil Data Mart using the Typical Pedon from the county that best reflected the soil and/or had the most acres of that soil. This data is presented in B and C horizons only as it is assumed that the topsoil (A or A_p horizon) will be removed in typical construction practices.

References:

Web Soil Survey. *Soil Survey Staff, Natural Resources Conservation Service, United States Department of Agriculture. Web Soil Survey. Available online at <http://websoilsurvey.nrcs.usda.gov/>.*

Soil Data Mart. <http://soildatamart.nrcs.usda.gov/>.

Soil Survey Manual. *Soil Survey Division Staff. 1993. Soil survey manual. Soil Conservation Service. U.S. Department of Agriculture Handbook 18.*

HYDROLOGIC SOIL GROUPS

Hydrologic group is a group of soils having the same runoff potential under similar storm and cover conditions.

Hydrologic groups are used in equations that estimate runoff from rainfall. These estimates are needed for solving hydrologic problems that arise in planning stormwater management, watershed protection, and flood-prevention projects and for planning or designing structures for the use, control, and disposal of water.

Classifications assigned to soils were based on the use of rainfall-runoff data from small watersheds and infiltrometer plots. From these data, relationships between soil properties and hydrologic groups were established. Assignment of soils to hydrologic groups is based on the relationship between soil properties and hydrologic groups. Wetness characteristics, permeability after prolonged wetting, and depth to very slowly permeable layers are properties that assist in estimating hydrologic groups. Minimum annual steady ponded infiltration rate for a bare ground surface determines the hydrologic soil groups.

Soil properties that influence runoff potential are those that influence the minimum rate of infiltration for a bare soil after prolonged wetting and when not frozen. These properties are depth to a seasonally high water table, intake rate and permeability after prolonged wetting, and depth to a very slowly permeable layer. (The influence of ground cover is treated independently, not in hydrologic soil groups.).

The soils in the United States are placed into four groups, A, B, C, and D, and three dual classes, *A/D*, *B/D*, and *C/D*. In the definitions of the classes, infiltration rate is the rate at which water enters the soil at the surface and is controlled by the surface conditions. Transmission rate is the rate at which water moves in the soil and is controlled by soil properties. Definitions of the classes are as follows:

Group A- Saturated hydraulic conductivity is very high or in the upper half of high and internal free water occurrence is very deep. Soils in this group have low runoff potential when thoroughly wet. Water is transmitted freely through the soil. Group A soils typically have less than 10 percent clay and more than 90 percent sand or gravel and have gravel or sand textures. Some soils having loamy sand, sandy loam, loam or silt loam textures may be placed in this group if they are well aggregated, of low bulk density, or contain greater than 35 percent rock fragments. The limits on the diagnostic physical characteristics of group A are as follows. The saturated hydraulic conductivity of all soil layers exceeds 40.0 micrometers per second (5.67 inches per hour). The depth to any water impermeable layer is greater than 50 centimeters [20 inches]. The depth to the water table is greater than 60 centimeters [24 inches]. Soils that are deeper than 100 centimeters [40 inches] to a water impermeable layer are in group A if the saturated hydraulic conductivity of all soil layers within 100 centimeters [40 inches] of the surface exceeds 10 micrometers per second (1.42 inches per hour).

Group B- Saturated hydraulic conductivity is in the lower half of high or in the upper half of moderately high and free water occurrence is deep or very deep. Soils in this group have moderately low runoff potential when thoroughly wet. Water transmission through the soil is unimpeded. Group B soils typically have between 10 percent and 20 percent clay and 50 percent to 90 percent sand and have loamy sand or sandy loam textures. Some soils having loam, silt loam, silt, or sandy clay loam textures may be placed in this group if they are well aggregated, of low bulk density, or contain greater than 35 percent rock fragments. The limits on the diagnostic physical characteristics of group B are as follows. The saturated hydraulic conductivity in the least transmissive layer between the surface and 50 centimeters [20 inches] ranges from 10.0 micrometers per second (1.42 inches per hour) to 40.0 micrometers per second (5.67 inches per hour). The depth to any water impermeable layer is greater than 50 centimeters [20 inches]. The depth to the water table is greater than 60 centimeters [24 inches]. Soils that are deeper than 100 centimeters [40 inches] to a water impermeable layer or water table are in group B if the saturated hydraulic conductivity of all soil layers within 100 centimeters [40 inches] of the surface exceeds 4.0 micrometers per second (0.57 inches per hour) but is less than 10.0 micrometers per second (1.42 inches per hour).

Group C- Saturated hydraulic conductivity is in the lower half of moderately high or in the upper half of moderately low and internal free water occurrence is deeper than shallow. Soils in this group have moderately high runoff potential when thoroughly wet. Water transmission through the soil is somewhat restricted. Group C soils typically have between 20 percent and 40 percent clay and less than 50 percent sand and have loam, silt loam, sandy clay loam, clay loam, and silty clay loam textures. Some soils having clay, silty clay, or sandy clay textures may be placed in this group if they are well aggregated, of low bulk density, or contain greater than 35 percent rock fragments. The limits on the diagnostic physical characteristics of group C are as follows. The saturated hydraulic conductivity in the least transmissive layer between the surface and 50 centimeters [20 inches] is between 1.0 micrometers per second (0.14 inches per hour) and 10.0 micrometers per second (1.42 inches per hour). The depth to any water impermeable layer is greater than 50 centimeters [20 inches]. The depth to the water table is greater than 60 centimeters [24 inches]. Soils that are deeper than 100 centimeters [40 inches] to a restriction or water table are in group C if the saturated hydraulic conductivity of all soil layers within 100 centimeters [40 inches] of the surface exceeds 0.40 micrometers per second (0.06 inches per hour) but is less than 4.0 micrometers per second (0.57 inches per hour).

Group D- Saturated hydraulic conductivity is below the upper half of moderately low, and/or internal free water occurrence is shallow or very shallow and transitory through permanent. Soils in this group have high runoff potential when thoroughly wet. Water movement through the soil is restricted or very restricted. Group D soils typically have greater than 40 percent clay, less than 50 percent sand, and have clayey textures. In some areas, they also have high shrink-swell potential. All soils with a depth to a water impermeable layer less than 50 centimeters [20 inches] and all soils with a water table within 60 centimeters [24 inches] of the surface are in this group, although some may have a dual classification, as described in the next section, if they can be adequately drained. The limits on the physical diagnostic characteristics of group D are as follows. For soils with a water impermeable layer at a depth between 50 centimeters and 100 centimeters [20 and 40 inches], the saturated hydraulic conductivity in the least transmissive soil layer is less than or equal to 1.0 micrometers per second (0.14 inches per hour). For soils that are deeper than 100 centimeters [40 inches] to a restriction or water table, the saturated hydraulic

conductivity of all soil layers within 100 centimeters [40 inches] of the surface is less than or equal to 0.40 micrometers per second (0.06 inches per hour).

Dual hydrologic soil groups-Certain wet soils are placed in group D based solely on the presence of a water table within 60 centimeters [24 inches] of the surface even though the saturated hydraulic conductivity may be favorable for water transmission. If these soils can be adequately drained, then they are assigned to dual hydrologic soil groups (*A/D*, *B/D*, and *C/D*) based on their saturated hydraulic conductivity and the water table depth when drained. The first letter applies to the drained condition and the second to the undrained condition. For the purpose of hydrologic soil group, adequately drained means that the seasonal high water table is kept at least 60 centimeters [24 inches] below the surface in a soil where it would be higher in a natural state.

References:

National Engineering Handbook, Natural Resource Conservation Service, U.S. Department of Agriculture.

Soil Data Mart. <http://soildatamart.nrcs.usda.gov/>.

Soil Survey Manual. *Soil Survey Division Staff. 1993. Soil survey manual. Natural Resources Conservation Service. U.S. Department of Agriculture Handbook 18.*

TABLE A

NUMERICAL LEGEND

Soil Series	legend number	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Group	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Occum	1	0.6	2.0	6.00	20.0	B	2	Flood Plain (Bottom Land)	mesic	loamy	no	loamy over loamy sand
Suncook	2	6.0	20.0	6.00	20.0	A	1	Flood Plain (Bottomland)	mesic	sandy	no	occasionally flooded
Lim	3	0.6	2.0	6.00	20.0	C	5	Flood Plain (Bottom Land)	mesic	loamy	no	
Pootatuck	4	0.6	6.0	6.00	20.0	B	3	Flood Plain (Bottom Land)	mesic	loamy	no	single grain in C
Rippowam	5	0.6	6.0	6.00	20.0	C	5	Flood Plain (Bottom Land)	mesic	loamy	no	
Saco	6	0.6	2.0	6.00	20.0	D	6	Flood Plain (Bottom Land)	mesic	silty	no	strata
Hadley	8	0.6	2.0	0.60	6.0	B	2	Flood Plain (Bottom Land)	mesic	silty	no	strata of fine sand
Winooski	9	0.6	6.0	0.60	6.0	B		Flood Plain (Bottom Land)	mesic	silty over loamy	no	
Merrimac	10	2.0	20.0	6.00	20.0	A	1	Outwash and Stream Terraces	mesic	gravely sand	no	loamy cap
Gloucester	11	6.0	20.0	6.00	20.0	A	1	Sandy Till	mesic	sandy-skeletal	no	loamy cap
Hinckley	12	6.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	mesic	sandy-skeletal	no	
Sheepscot	14	6.0	20.0	6.00	20.0	B	3	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	gravely coarse sand
Searsport	15	6.0	20.0	6.00	20.0	D	6	Outwash and Stream Terraces	frigid	sandy	no	organic over sand
Saugatuck	16	0.06	0.2	6.00	20.0	C	5	Outwash and Stream Terraces	mesic	sandy	yes	ortstein
Colton, gravelly	21	6.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	gravely surface
Colton	22	6.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	
Masardis	23	6.0	20.0	6.00	20.0	A	1	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	slate, loamy cap
Agawam	24	6.0	20.0	20.00	100.0	B	2	Outwash and Stream Terraces	mesic	loamy over sandy	no	loamy over sand/gravel
Windsor	26	6.0	20.0	6.00	20.0	A	1	Outwash and Stream Terraces	mesic	sandy	no	
Groveton	27	0.6	2.0	0.60	6.0	B	2	Outwash and Stream Terraces	frigid	loamy	yes	loamy over sandy
Madawaska	28	0.6	2.0	6.00	20.0	B	3	Outwash and Stream Terraces	frigid	loamy over sandy	yes	sandy or sandy-skeletal
Woodbridge	29	0.6	2.0	0.00	0.6	C	3	Firm, platy, loamy till	mesic	loamy	no	sandy loam in Cd
Unadilla	30	0.6	2.0	2.00	20.0	B	2	Terraces and glacial lake plains	mesic	silty	no	silty over gravelly
Hartland	31	0.6	2.0	0.20	2.0	B	2	Terraces and glacial lake plains	mesic	silty	no	very fine sandy loam
Boxford	32	0.1	0.2	0.00	0.2	C	3	Silt and Clay Deposits	mesic	fine	no	silty clay loam
Scitico	33	0.0	0.2	0.00	0.2	C	5	Silt and Clay Deposits	mesic	fine	no	
Wareham	34	6.0	20.0	6.00	20.0	C	5	Outwash and Stream Terraces	mesic	sandy	no	
Champlain	35	6.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	frigid	gravely sand	no	
Adams	36	6.0	20.0	20.00	99.0	A	1	Outwash and Stream Terraces	frigid	sandy	yes	
Melrose	37	2.0	6.0	0.00	0.2	C	3	Sandy/loamy over silt/clay	frigid	loamy over clayey	no	silty clay loam in C
Eldridge	38	6.0	20.0	0.06	0.6	C	3	Sandy/loamy over silt/clay	mesic	sandy over loamy	no	
Millis	39					C	3	Firm, platy, sandy till	frigid	loamy	yes	loamy sand in Cd
Canton	42	2.0	6.0	6.00	20.0	B	2	Loose till, sandy textures	mesic	loamy over sandy	no	loamy over loamy sand
Montauk	44	0.6	6.0	0.06	0.6	C	3	Firm, platy, sandy till	mesic	loamy	no	loamy sand in Cd
Henniker	46	0.6	2.0	0.06	0.6	C	3	Firm, platy, sandy till	frigid	loamy	no	loamy sand in Cd
Madawaska, aquatic	48	0.6	2.0	6.00	20.0	B	3	Outwash and Stream Terraces	frigid	loamy over sandy	yes	sandy or sandy-skeletal
Whitman	49	0.0	0.2	0.00	0.2	D	6	Firm, platy, loamy till	mesic	loamy	no	mucky loam
Hermon	55	2.0	20.0	6.00	20.0	A	1	Sandy Till	frigid	sandy-skeletal	yes	loamy cap
Becket	56	0.6	2.0	0.06	0.6	C	3	Firm, platy, sandy till	frigid	loamy	yes	gravely sandy loam in Cd
Waumbeck	58	2.0	20.0	6.00	20.0	B	3	Loose till, sandy textures	frigid	sandy-skeletal	yes	very cobbly loamy sand
Charlton	62	0.6	6.0	0.60	6.0	B	2	Loose till, loamy textures	mesic	loamy	no	fine sandy loam
Paxton	66	0.6	2.0	0.00	0.2	C	3	Firm, platy, loamy till	mesic	loamy	no	
Sutton	68	0.6	6.0	0.60	6.0	B	3	Loose till, loamy textures	mesic	loamy	no	
Berkshire	72	0.6	6.0	0.60	6.0	B	2	Loose till, loamy textures	frigid	loamy	yes	fine sandy loam
Marlow	76	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	yes	fine sandy loam in Cd
Peru	78	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	yes	
Thorndike	84	0.6	2.0	0.60	2.0	C/D	4	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	less than 20 in. deep
Hollis	86	0.6	6.0	0.60	6.0	C/D	4	Loose till, bedrock	mesic	loamy	no	less than 20 in. deep
Winnecook	88	0.6	2.0	0.60	2.0	C	4	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	20 to 40 in. deep
Chatfield	89	0.6	6.0	0.60	6.0	B	4	Loose till, bedrock	mesic	loamy	no	20 to 40 in. deep
Hogback	91	2.0	6.0	2.00	6.0	C	4	Loose till, bedrock	frigid	loamy	yes	less than 20 in. deep
Lyman	92	2.0	6.0	2.00	6.0	A/D	4	Loose till, bedrock	frigid	loamy	yes	less than 20 in. deep
Woodstock	93	2.0	6.0	2.00	6.0	C/D	4	Loose till, bedrock	frigid	loamy	no	less than 20 in. deep
Rawsonville	98	0.6	6.0	0.60	6.0	C	4	Loose till, bedrock	frigid	loamy	yes	20 to 40 in. deep
Tunbridge	99	0.6	6.0	0.60	6.0	C	4	Loose till, bedrock	frigid	loamy	yes	20 to 40 in. deep

Soil Series	legend number	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Group	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Ondawa	101	0.6	6.0	6.00	20.0	B	2	Flood Plain (Bottom Land)	frigid	loamy	no	loamy over loamy sand
Sunday	102	6.0	20.0	6.00	20.0	A	1	Flood Plain (Bottomland)	frigid	sandy	no	occasionally flooded
Winooski	103	0.6	6.0	0.60	6.0	B	3	Flood Plain (Bottom Land)	mesic	silty	no	very fine sandy loam
Podunk	104	0.6	6.0	6.00	20.0	B	3	Flood Plain (Bottom Land)	frigid	loamy	no	loamy to coarse sand in C
Rumney	105	0.6	6.0	6.00	20.0	C	5	Flood Plain (Bottom Land)	frigid	loamy	no	
Hadley	108	0.6	2.0	0.60	6.0	B	2	Flood Plain (Bottom Land)	mesic	silty	no	strata of fine sand, occ flooded
Limerick	109	0.6	2.0	0.60	2.0	C	5	Flood Plain (Bottom Land)	mesic	silty	no	
Scarboro	115	6.0	20.0	6.00	20.0	D	6	Outwash and Stream Terraces	mesic	sandy	no	organic over sand, non stony
Finch	116					C	3	Outwash and Stream Terraces	frigid	sandy	yes	cemented (ortstein)
Sudbury	118	2.0	6.0	2.00	20.0	B	3	Outwash and Stream Terraces	mesic	sandy	no	loam over gravelly sand
Telos	123	0.6	2.0	0.02	0.2	C	3	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	channery silt loam in Cd
Chesuncook	126	0.6	2.0	0.02	0.2	C	3	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	channery silt loam in Cd
Allagash	127	0.6	2.0	6.00	20.0	B	2	Outwash and Stream Terraces	frigid	loamy over sandy	yes	loamy over sandy
Elliottsville	128	0.6	2.0	0.60	2.0	B	4	Friable till, silty, schist & phyllite	frigid	loamy	yes	20 to 40 in. deep
Hitchcock	130	0.6	2.0	0.06	0.6	B	3	Terraces and glacial lake plains	mesic	silty	no	silt loam to silt in C
Burnham	131	0.2	6.0	0.02	0.2	D	6	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	organic over silt
Dartmouth	132	0.6	2.0	0.06	0.6	B	3	Terraces and glacial lake plains	mesic	silty	no	thin strata silty clay loam
Monson	133	0.6	2.0	0.60	2.0	D	4	Friable till, silty, schist & phyllite	frigid	loamy	yes	less than 20 in. deep
Maybid	134	0.0	0.2	0.00	0.2	D	6	Silt and Clay Deposits	mesic	fine	no	silt over clay
Shapleigh	136					C/D	4	Sandy Till	mesic	sandy	yes	less than 20 in. deep
Monadnock	142	0.6	2.0	2.00	6.0	B	2	Loose till, sandy textures	frigid	loamy over sandy, sandy-skeletal	yes	gravelly loamy sand in C
Acton	146	2.0	20.0	2.00	20.0	B	3	Loose till, sandy textures	mesic	sandy-skeletal	no	cobbly loamy sand
Vassalboro	150					D	6	Organic Materials - Freshwater	frigid	peat	no	deep organic
Success	154	2.0	6.0	6.00	20.0	A	1	Sandy Till	frigid	sandy-skeletal	yes	cemented
Canterbury	166	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	no	loam in Cd
Sunapee	168	0.6	2.0	0.60	6.0	B	3	Loose till, loamy textures	frigid	loamy	yes	
Waskish	195					D	6	Organic Materials - Freshwater	frigid	peat	no	deep organic
Ondawa	201	0.6	6.0	6.00	20.0	B	2	Flood Plain (Bottom Land)	frigid	loamy	no	occ flood, loamy over l. sand
Sunday	202	6.0	20.0	6.00	20.0	A	1	Flood Plain (Bottomland)	frigid	sandy	no	frequently flooded
Fryeburg	208	0.6	2.0	2.00	6.0	B	2	Flood Plain (Bottom Land)	frigid	silty	no	very fine sandy loam
Charles	209	0.6	100.0	0.60	100.0	C	5	Flood Plain (Bottom Land)	frigid	silty	no	
Warwick	210	2.0	6.0	20.00	100.0	A	1	Outwash and Stream Terraces	mesic	loamy-skeletal	no	loamy over slate gravel
Naumburg	214	6.0	20.0	6.00	20.0	C	5	Outwash and Stream Terraces	frigid	sandy	yes	
Boscawen	220	6.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	frigid	sandy-skeletal	no	loamy cap
Bemis	224	0.6	0.2	0.00	0.2	C	5	Firm, platy, loamy till	cryic	loamy	no	
Bice	226	0.6	6.0	0.60	6.0	B	2	Loose till, loamy textures	frigid	loamy	no	sandy loam
Lanesboro	228	0.6	2.0	0.06	0.2	C	3	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	channery silt loam in Cd
Poocham	230	0.6	2.0	0.20	2.0	B	3	Terraces and glacial lake plains	mesic	silty	no	silt loam in C
Buxton	232	0.1	0.6	0.00	0.2	C	3	Silt and Clay Deposits	frigid	fine	no	silty clay
Scantic	233	0.0	0.2	0.00	0.2	D	5	Silt and Clay Deposits	frigid	fine	no	
Biddeford	234	0.0	0.2	0.00	0.2	D	6	Silt and Clay Deposits	frigid	fine	no	organic over clay
Buckland	237	0.6	2.0	0.06	0.2	C	3	Firm, platy, loamy till	frigid	loamy	no	loam in Cd
Elmridge	238	2.0	6.0	0.00	0.2	C	3	Sandy/loamy over silt/clay	mesic	loamy over clayey	no	
Brayton	240	0.6	2.0	0.06	0.6	C	5	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Lyme	246	0.6	6.0	0.60	6.0	C	5	Loose till, sandy textures	frigid	loamy	no	
Millsite	251	0.6	6.0	0.60	6.0	C	4	Loose till, bedrock	frigid	loamy	no	20 to 40 in. deep
Macomber	252	0.6	2.0	0.60	2.0	C	4	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	20 to 40 in. deep
Lombard	259	0.6	6.0	2.00	20.0	C/D	2	Weathered bedrock, phyllite	frigid	loamy	no	very channery
Sunapee var	269	0.6	2.0	0.60	6.0	B	3	Loose till, loamy textures	frigid	loamy	yes	frigid dystrodept
Chatfield Var.	289	0.6	6.0	0.60	6.0	B	3	Loose till, bedrock	mesic	loamy	no	mwd to swpd
Greenwood	295					A/D	6	Organic Materials - Freshwater	frigid	hemic	no	deep organic
Catden	296					A/D	6	Organic Materials - Freshwater	mesic	sapric	no	deep organic
Lovewell	307	0.6	2.0	0.60	2.0	B	3	Flood Plain (Bottom Land)	frigid	silty	no	very fine sandy loam
Quonset	310	2.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	mesic	sandy-skeletal	no	shale
Deerfield	313	6.0	20.0	20.00	100.0	B	3	Outwash and Stream Terraces	mesic	sandy	no	single grain in C

Soil Series	legend number	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Group	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Pipestone	314					B	5	Outwash and Stream Terraces	mesic	sandy	yes	
Mashpee	315	6.0	20.0	6.00	20.0	B	5	Outwash and Stream Terraces	mesic	sandy	yes	
Bernardston	330	0.6	2.0	0.06	0.2	C	3	Firm, platy, silty till, schist & phyllite	mesic	loamy	no	channery silt loam in Cd
Roundabout	333	0.2	2.0	0.06	0.6	C	5	Terraces and glacial lake plains	frigid	silty	no	silt loam in the C
Pittstown	334	0.6	2.0	0.06	0.2	C	3	Firm, platy, silty till, schist & phyllite	mesic	loamy	no	channery silt loam in Cd
Elmwood	338	2.0	6.0	0.00	0.2	C	3	Sandy/loamy over silt/clay	frigid	loamy over clayey	no	
Stissing	340	0.6	2.0	0.06	0.2	C	5	Firm, platy, silty till, schist & phyllite	mesic	loamy	no	
Cardigan	357	0.6	2.0	0.60	2.0	B	4	Friable till, silty, schist & phyllite	mesic	loamy	no	20 to 40 in. deep
Kearsarge	359	0.6	2.0	0.60	2.0	B	4	Friable till, silty, schist & phyllite	mesic	loamy	no	less than 20 in. deep
Dutchess	366	0.6	2.0	0.60	2.0	B	2	Friable till, silty, schist & phyllite	mesic	loamy	no	very channery
Dixfield	378	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	yes	fine sandy loam in Cd
Timakwa	393			6.00	100.0	D	6	Organic Materials - Freshwater	mesic	sandy or sandy-skeletal	no	organic over sand
Chocorua	395			6.00	20.0	D	6	Organic Materials - Freshwater	frigid	sandy or sandy-skeletal	no	organic over sand
Ipswich	397					D	6	Tidal Flat	mesic	hemic/sapric	no	deep organic
Suncook	402	6.0	20.0	6.00	20.0	A	1	Flood Plain (Bottomland)	mesic	sandy	no	frequent flooding
Metallak	404	6.0	100.0	6.00	100.0	B	3	Flood Plain (Bottom Land)	frigid	loamy over sandy	no	sandy or sandy-skeletal
Medomak	406	0.6	2.0	0.60	2.0	D	6	Flood Plain (Bottom Land)	frigid	silty	no	organic over silt
Haven	410	0.6	2.0	20.00	100.0	B	2	Outwash and Stream Terraces	mesic	loamy over sandy	no	loamy over sand/gravel
Duane	413	6.0	20.0	6.00	20.0	B	3	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	cemented (ortstein)
Moosilauke	414	6.0	20.0	6.00	20.0	C	5	Loose till, sandy textures	frigid	sandy	no	
Grange	433	0.6	2.0	0.60	2.0	C	5	Outwash and Stream Terraces	frigid	co. loamy over sandy (skeletal)	no	
Swanton	438	2.0	6.0	0.00	0.2	C	5	Sandy/loamy over silt/clay	frigid	co. loamy over clayey	no	
Shaker	439	2.0	6.0	0.00	0.2	C	5	Sandy/loamy over silt/clay	mesic	co. loamy over clayey	no	
Chichester	442	0.6	2.0	2.00	6.0	B	3	Loose till, sandy textures	frigid	loamy over sandy	no	loamy over loamy sand
Newfields	444	0.6	2.0	0.60	2.0	B	3	Loose till, sandy textures	mesic	loamy over sandy	no	sandy or sandy-skeletal
Scituate	448	0.6	2.0	0.06	0.2	C	3	Firm, platy, sandy till	mesic	loamy	no	loamy sand in Cd
Metacomet	458	0.6	2.0	0.06	0.6	C	3	Firm, platy, sandy till	frigid	loamy	no	loamy sand in Cd
Pennichuck	460	0.6	2.0	0.60	2.0	B	4	Friable till, silty, schist & phyllite	mesic	loamy-skeletal	no	20 to 40 in. deep
Gilmanton	478	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	no	fine sandy loam in Cd
Ossipee	495			0.20	2.0	D	6	Organic Materials - Freshwater	frigid	loamy	no	organic over loam
Natchaug	496			0.20	2.0	D	6	Organic Materials - Freshwater	mesic	loamy	no	organic over loam
Pawcatuck	497			20.00	100.0	D	6	Tidal Flat	mesic	sandy or sandy-skeletal	no	organic over sand
Abenaki	501	0.6	2.0	6.00	99.0	B	2	Outwash and Stream Terraces	frigid	loamy over sandy-skeletal	no	loamy over gravelly
Cohas	505	0.6	2.0	0.60	100.0	C	5	Flood Plain (Bottom Land)	frigid	co. loamy over sandy (skeletal)	no	
Hoosic	510	2.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	mesic	sandy-skeletal	no	slate, loamy cap
Ninigret	513	0.6	6.0	6.00	20.0	B	3	Outwash and Stream Terraces	mesic	loamy over sandy	no	sandy or sandy-skeletal
Leicester	514	0.6	6.0	0.60	20.0	C	5	Loose till, loamy textures	mesic	loamy	no	
Au Gres	516					B	5	Outwash and Stream Terraces	frigid	sandy	yes	single grain, loose
Machias	520	2.0	6.0	6.00	20.0	B	3	Outwash and Stream Terraces	frigid	sandy or sandy-skeletal	yes	strata sand/gravel in C
Stetson	523	0.6	6.0	6.00	20.0	B	2	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	loamy over gravelly
Caesar	526	20.0	100.0	20.00	100.0	A	1	Outwash and Stream Terraces	mesic	coarse sand	no	
Scio	531	0.6	2.0	0.60	2.0	B	3	Terraces and glacial lake plains	mesic	silty	no	gravelly sand in 2C
Belgrade	532	0.6	2.0	0.06	2.0	B	3	Terraces and glacial lake plains	mesic	silty	no	strata of fine sand
Raynham	533	0.2	2.0	0.06	0.2	C	5	Terraces and glacial lake plains	mesic	silty	no	
Binghamville	534	0.2	2.0	0.06	0.2	D	5	Terraces and glacial lake plains	mesic	silty	no	
Suffield	536	0.6	2.0	0.00	0.2	C	3	Sandy/loamy over silt/clay	mesic	silty over clayey	no	deep to clay C
Squamscott	538	6.0	20.0	0.06	0.6	C	5	Sandy/loamy over silt/clay	mesic	sandy over loamy	yes	
Raypol	540	0.6	2.0	6.00	100.0	D	5	Outwash and Stream Terraces	mesic	co. loamy over sandy (skeletal)	no	
Walpole	546	2.0	6.0	6.00	20.0	C	5	Outwash and Stream Terraces	mesic	sandy	no	
Peacham	549	0.6	2.0	0.00	0.2	D	6	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	organic over loam
Skerry	558	0.6	2.0	0.06	0.6	C	3	Firm, platy, sandy till	frigid	loamy	yes	loamy sand in Cd
Plaisted	563	0.6	2.0	0.06	0.6	C	3	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	channery silt loam in Cd
Howland	566	0.6	2.0	0.06	0.2	C	3	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	silt loam, platy in Cd
Monarda	569	0.2	2.0	0.02	0.2	D	5	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Bangor	572	0.6	2.0	0.60	2.0	B	2	Friable till, silty, schist & phyllite	frigid	loamy	yes	silt loam

Soil Series	legend number	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Group	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Dixmont	578	0.6	2.0	0.60	2.0	C	3	Friable till, silty, schist & phyllite	frigid	loamy	yes	silt loam, platy in C
Cabot	589	0.6	2.0	0.06	0.2	D	5	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Westbrook	597			0.00	2.0	D	6	Tidal Flat	mesic	loamy	no	organic over loam
Mundal	610	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	yes	gravely sandy loam in Cd
Croghan	613	20.0	100.0	20.00	100.0	B	3	Outwash and Stream Terraces	frigid	sandy	yes	single grain in C
Kinsman	614	6.0	20.0	6.00	20.0	C	5	Outwash and Stream Terraces	frigid	sandy	yes	
Salmon	630	0.6	2.0	0.60	2.0	B	2	Terraces and glacial lake plains	frigid	silty	yes	very fine sandy loam
Nicholville	632	0.6	2.0	0.60	2.0	C	3	Terraces and glacial lake plains	frigid	silty	yes	very fine sandy loam
Pemi	633	0.6	2.0	0.06	0.6	C	5	Terraces and glacial lake plains	frigid	silty	no	
Pillsbury	646	0.6	2.0	0.06	0.2	C	5	Firm, platy, loamy till	frigid	silty	no	
Ridgebury	656	0.6	6.0	0.00	0.2	C	5	Firm, platy, loamy till	mesic	loamy	no	
Canaan	663	2.0	20.0	2.00	20.0	C	4	Weathered Bedrock Till	frigid	loamy-skeletal	yes	less than 20 in. deep
Redstone	665	2.0	6.0	6.00	20.0	A	1	Weathered Bedrock Till	frigid	fragmental	yes	loamy cap
Sisk	667	0.6	2.0	0.00	0.6	C	3	Firm, platy, loamy till	cryic	loamy	yes	sandy loam in Cd
Surplus	669	0.6	2.0	0.00	0.6	C	3	Firm, platy, loamy till	cryic	loamy	yes	mwd, sandy loam in Cd
Glebe	671	2.0	6.0	2.00	6.0	C	4	Loose till, bedrock	cryic	loamy	yes	20 to 40 in. deep
Saddleback	673	0.6	2.0	0.60	2.0	C/D	4	Loose till, bedrock	cryic	loamy	yes	less than 20 in. deep
Ricker	674	2.0	6.0	2.00	6.0	A	4	Organic over bedrock (up to 4" of mineral)	cryic	fibric to hemic	no	well drained, less than 20 in. deep
Houghtonville	795	0.6	6.0	0.60	6.0	B	2	Loose till, loamy textures	frigid	loamy	yes	cobbly fine sandy loam
Matunuck	797			20.00	100.0	D	6	Tidal Flat	mesic	sandy	no	organic over sand
Meadowsedge	894					D	6	Organic Materials - Freshwater	frigid	peat	no	deep organic
Bucksport	895					D	6	Organic Materials - Freshwater	frigid	sapric	no	deep organic
Colonel	927	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	yes	loam in Cd
Pondicherry	992			6.00	20.0	D	6	Organic Materials - Freshwater	frigid	sandy or sandy-skeletal	no	organic over sand
Wonsqueak	995			0.20	2.0	D	6	Organic Materials - Freshwater	frigid	loamy	no	organic over loam
Glover	NA	0.6	2.0	0.60	2	D	4	Friable till, silty, schist & phyllite	frigid	loamy	no	less than 20 in. deep



no longer recognized
 organic materials

TABLE B
SOIL SERIES

Soil Series	legend number	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Group	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Abenaki	501	0.6	2.0	6.00	99.0	B	2	Outwash and Stream Terraces	frigid	loamy over sandy-skeletal	no	loamy over gravelly
Acton	146	2.0	20.0	2.00	20.0	B	3	Loose till, sandy textures	mesic	sandy-skeletal	no	cobbly loamy sand
Adams	36	6.0	20.0	20.00	99.0	A	1	Outwash and Stream Terraces	frigid	sandy	yes	
Agawam	24	6.0	20.0	20.00	100.0	B	2	Outwash and Stream Terraces	mesic	loamy over sandy	no	loamy over sand/gravel
Allagash	127	0.6	2.0	6.00	20.0	B	2	Outwash and Stream Terraces	frigid	loamy over sandy	yes	loamy over sandy
Au Gres	516					B	5	Outwash and Stream Terraces	frigid	sandy	yes	single grain, loose
Bangor	572	0.6	2.0	0.60	2.0	B	2	Friable till, silty, schist & phyllite	frigid	loamy	yes	silt loam
Becket	56	0.6	2.0	0.06	0.6	C	3	Firm, platy, sandy till	frigid	loamy	yes	gravelly sandy loam in Cd
Belgrade	532	0.6	2.0	0.06	2.0	B	3	Terraces and glacial lake plains	mesic	silty	no	strata of fine sand
Bemis	224	0.6	0.2	0.00	0.2	C	5	Firm, platy, loamy till	cryc	loamy	no	
Berkshire	72	0.6	6.0	0.60	6.0	B	2	Loose till, loamy textures	frigid	loamy	yes	fine sandy loam
Bernardston	330	0.6	2.0	0.06	0.2	C	3	Firm, platy, silty till, schist & phyllite	mesic	loamy	no	channery silt loam in Cd
Bice	226	0.6	6.0	0.60	6.0	B	2	Loose till, loamy textures	frigid	loamy	no	sandy loam
Biddeford	234	0.0	0.2	0.00	0.2	D	6	Silt and Clay Deposits	frigid	fine	no	organic over clay
Binghamville	534	0.2	2.0	0.06	0.2	D	5	Terraces and glacial lake plains	mesic	silty	no	
Boscawen	220	6.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	frigid	sandy-skeletal	no	loamy cap
Boxford	32	0.1	0.2	0.00	0.2	C	3	Silt and Clay Deposits	mesic	fine	no	silty clay loam
Brayton	240	0.6	2.0	0.06	0.6	C	5	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Buckland	237	0.6	2.0	0.06	0.2	C	3	Firm, platy, loamy till	frigid	loamy	no	loam in Cd
Bucksport	895					D	6	Organic Materials - Freshwater	frigid	sapric	no	deep organic
Burnham	131	0.2	6.0	0.02	0.2	D	6	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	organic over silt
Buxton	232	0.1	0.6	0.00	0.2	C	3	Silt and Clay Deposits	frigid	fine	no	silty clay
Cabot	589	0.6	2.0	0.06	0.2	D	5	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Caesar	526	20.0	100.0	20.00	100.0	A	1	Outwash and Stream Terraces	mesic	coarse sand	no	
Canaan	663	2.0	20.0	2.00	20.0	C	4	Weathered Bedrock Till	frigid	loamy-skeletal	yes	less than 20 in. deep
Canterbury	166	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	no	loam in Cd
Canton	42	2.0	6.0	6.00	20.0	B	2	Loose till, sandy textures	mesic	loamy over sandy	no	loamy over loamy sand
Cardigan	357	0.6	2.0	0.60	2.0	B	4	Friable till, silty, schist & phyllite	mesic	loamy	no	20 to 40 in. deep
Catden	296					A/D	6	Organic Materials - Freshwater	mesic	sapric	no	deep organic
Champlain	35	6.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	frigid	gravelly sand	no	
Charles	209	0.6	100.0	0.60	100.0	C	5	Flood Plain (Bottom Land)	frigid	silty	no	
Charlton	62	0.6	6.0	0.60	6.0	B	2	Loose till, loamy textures	mesic	loamy	no	fine sandy loam
Chatfield	89	0.6	6.0	0.60	6.0	B	4	Loose till, bedrock	mesic	loamy	no	20 to 40 in. deep
Chatfield Var.	289	0.6	6.0	0.60	6.0	B	3	Loose till, bedrock	mesic	loamy	no	mwd to swpd
Chesuncook	126	0.6	2.0	0.02	0.2	C	3	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	channery silt loam in Cd
Chichester	442	0.6	2.0	2.00	6.0	B		Loose till, sandy textures	frigid	loamy over sandy	no	loamy over loamy sand
Chocorua	395			6.00	20.0	D	6	Organic Materials - Freshwater	frigid	sandy or sandy-skeletal	no	organic over sand
Cohas	505	0.6	2.0	0.60	100.0	C	5	Flood Plain (Bottom Land)	frigid	co. loamy over sandy (skeletal)	no	
Colonel	927	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	yes	loam in Cd
Colton	22	6.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	
Colton, gravelly	21	6.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	gravelly surface
Croghan	613	20.0	100.0	20.00	100.0	B	3	Outwash and Stream Terraces	frigid	sandy	yes	single grain in C
Dartmouth	132	0.6	2.0	0.06	0.6	B	3	Terraces and glacial lake plains	mesic	silty	no	thin strata silty clay loam
Deerfield	313	6.0	20.0	20.00	100.0	B	3	Outwash and Stream Terraces	mesic	sandy	no	single grain in C
Dixfield	378	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	yes	fine sandy loam in Cd
Dixmont	578	0.6	2.0	0.60	2.0	C	3	Friable till, silty, schist & phyllite	frigid	loamy	yes	silt loam, platy in C
Duane	413	6.0	20.0	6.00	20.0	B	3	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	cemented (ortstein)
Dutchess	366	0.6	2.0	0.60	2.0	B	2	Friable till, silty, schist & phyllite	mesic	loamy	no	very channery
Eldridge	38	6.0	20.0	0.06	0.6	C	3	Sandy/loamy over silt/clay	mesic	sandy over loamy	no	
Elliottsville	128	0.6	2.0	0.60	2.0	B	4	Friable till, silty, schist & phyllite	frigid	loamy	yes	20 to 40 in. deep
Elmridge	238	2.0	6.0	0.00	0.2	C	3	Sandy/loamy over silt/clay	mesic	loamy over clayey	no	
Elmwood	338	2.0	6.0	0.00	0.2	C	3	Sandy/loamy over silt/clay	frigid	loamy over clayey	no	
Finch	116					C	3	Outwash and Stream Terraces	frigid	sandy	yes	cemented (ortstein)

Soil Series	legend number	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Group	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Fryeburg	208	0.6	2.0	2.00	6.0	B	2	Flood Plain (Bottom Land)	frigid	silty	no	very fine sandy loam
Gilmanton	478	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	no	fine sandy loam in Cd
Glebe	671	2.0	6.0	2.00	6.0	C	4	Loose till, bedrock	cryic	loamy	yes	20 to 40 in. deep
Gloucester	11	6.0	20.0	6.00	20.0	A	1	Sandy Till	mesic	sandy-skeletal	no	loamy cap
Glover	NA	0.6	2.0	0.60	2	D	4	Friable till, silty, schist & phyllite	frigid	loamy	no	less than 20 in. deep
Grange	433	0.6	2.0	0.60	2.0	C	5	Outwash and Stream Terraces	frigid	co. loamy over sandy (skeletal)	no	
Greenwood	295					A/D	6	Organic Materials - Freshwater	frigid	hemic	no	deep organic
Groveton	27	0.6	2.0	0.60	6.0	B	2	Outwash and Stream Terraces	frigid	loamy	yes	loamy over sandy
Hadley	8	0.6	2.0	0.60	6.0	B	2	Flood Plain (Bottom Land)	mesic	silty	no	strata of fine sand
Hadley	108	0.6	2.0	0.60	6.0	B	2	Flood Plain (Bottom Land)	mesic	silty	no	strata of fine sand, occ flooded
Hartland	31	0.6	2.0	0.20	2.0	B	2	Terraces and glacial lake plains	mesic	silty	no	very fine sandy loam
Haven	410	0.6	2.0	20.00	100.0	B	2	Outwash and Stream Terraces	mesic	loamy over sandy	no	loamy over sand/gravel
Henniker	46	0.6	2.0	0.06	0.6	C	3	Firm, platy, sandy till	frigid	loamy	no	loamy sand in Cd
Hermon	55	2.0	20.0	6.00	20.0	A	1	Sandy Till	frigid	sandy-skeletal	yes	loamy cap
Hinckley	12	6.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	mesic	sandy-skeletal	no	
Hitchcock	130	0.6	2.0	0.06	0.6	B	3	Terraces and glacial lake plains	mesic	silty	no	silt loam to silt in C
Hogback	91	2.0	6.0	2.00	6.0	C	4	Loose till, bedrock	frigid	loamy	yes	less than 20 in. deep
Hollis	86	0.6	6.0	0.60	6.0	C/D	4	Loose till, bedrock	mesic	loamy	no	less than 20 in. deep
Hoosic	510	2.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	mesic	sandy-skeletal	no	slate, loamy cap
Houghtonville	795	0.6	6.0	0.60	6.0	B	2	Loose till, loamy textures	frigid	loamy	yes	cobbly fine sandy loam
Howland	566	0.6	2.0	0.06	0.2	C	3	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	silt loam, platy in Cd
Ipswich	397					D	6	Tidal Flat	mesic	hemic/sapric	no	deep organic
Kearsarge	359	0.6	2.0	0.60	2.0	B	4	Friable till, silty, schist & phyllite	mesic	loamy	no	less than 20 in. deep
Kinsman	614	6.0	20.0	6.00	20.0	C	5	Outwash and Stream Terraces	frigid	sandy	yes	
Lanesboro	228	0.6	2.0	0.06	0.2	C	3	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	channery silt loam in Cd
Leicester	514	0.6	6.0	0.60	20.0	C	5	Loose till, loamy textures	mesic	loamy	no	
Lim	3	0.6	2.0	6.00	20.0	C	5	Flood Plain (Bottom Land)	mesic	loamy	no	
Limerick	109	0.6	2.0	0.60	2.0	C	5	Flood Plain (Bottom Land)	mesic	silty	no	
Lombard	259	0.6	6.0	2.00	20.0	C/D	2	Weathered bedrock, phyllite	frigid	loamy	no	very channery
Lovewell	307	0.6	2.0	0.60	2.0	B	3	Flood Plain (Bottom Land)	frigid	silty	no	very fine sandy loam
Lyman	92	2.0	6.0	2.00	6.0	A/D	4	Loose till, bedrock	frigid	loamy	yes	less than 20 in. deep
Lyme	246	0.6	6.0	0.60	6.0	C	5	Loose till, sandy textures	frigid	loamy	no	
Machias	520	2.0	6.0	6.00	20.0	B	3	Outwash and Stream Terraces	frigid	sandy or sandy-skeletal	yes	strata sand/gravel in C
Macomber	252	0.6	2.0	0.60	2.0	C	4	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	20 to 40 in. deep
Madawaska	28	0.6	2.0	6.00	20.0	B	3	Outwash and Stream Terraces	frigid	loamy over sandy	yes	sandy or sandy-skeletal
Madawaska, aquel	48	0.6	2.0	6.00	20.0	B	3	Outwash and Stream Terraces	frigid	loamy over sandy	yes	sandy or sandy-skeletal
Marlow	76	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	yes	fine sandy loam in Cd
Masardis	23	6.0	20.0	6.00	20.0	A	1	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	slate, loamy cap
Mashpee	315	6.0	20.0	6.00	20.0	B	5	Outwash and Stream Terraces	mesic	sandy	yes	
Matunuck	797			20.00	100.0	D	6	Tidal Flat	mesic	sandy	no	organic over sand
Maybid	134	0.0	0.2	0.00	0.2	D	6	Silt and Clay Deposits	mesic	fine	no	silt over clay
Meadowsedge	894					D	6	Organic Materials - Freshwater	frigid	peat	no	deep organic
Medomak	406	0.6	2.0	0.60	2.0	D	6	Flood Plain (Bottom Land)	frigid	silty	no	organic over silt
Melrose	37	2.0	6.0	0.00	0.2	C	3	Sandy/loamy over silt/clay	frigid	loamy over clayey	no	silty clay loam in C
Merrimac	10	2.0	20.0	6.00	20.0	A	1	Outwash and Stream Terraces	mesic	gravelly sand	no	loamy cap
Metacomet	458	0.6	2.0	0.06	0.6	C	3	Firm, platy, sandy till	frigid	loamy	no	loamy sand in Cd
Metallak	404	6.0	100.0	6.00	100.0	B	3	Flood Plain (Bottom Land)	frigid	loamy over sandy	no	sandy or sandy-skeletal
Millis	39					C	3	Firm, platy, sandy till	frigid	loamy	yes	loamy sand in Cd
Millsite	251	0.6	6.0	0.60	6.0	C	4	Loose till, bedrock	frigid	loamy	no	20 to 40 in. deep
Monadnock	142	0.6	2.0	2.00	6.0	B	2	Loose till, sandy textures	frigid	loamy over sandy, sandy-skeletal	yes	gravelly loamy sand in C
Monarda	569	0.2	2.0	0.02	0.2	D	5	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Monson	133	0.6	2.0	0.60	2.0	D	4	Friable till, silty, schist & phyllite	frigid	loamy	yes	less than 20 in. deep
Montauk	44	0.6	6.0	0.06	0.6	C	3	Firm, platy, sandy till	mesic	loamy	no	loamy sand in Cd
Moosilauke	414	6.0	20.0	6.00	20.0	C	5	Loose till, sandy textures	frigid	sandy	no	

Soil Series	legend number	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Group	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Mundal	610	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	yes	gravelly sandy loam in Cd
Natchaug	496			0.20	2.0	D	6	Organic Materials - Freshwater	mesic	loamy	no	organic over loam
Naumburg	214	6.0	20.0	6.00	20.0	C	5	Outwash and Stream Terraces	frigid	sandy	yes	
Newfields	444	0.6	2.0	0.60	2.0	B	3	Loose till, sandy textures	mesic	loamy over sandy	no	sandy or sandy-skeletal
Nicholville	632	0.6	2.0	0.60	2.0	C	3	Terraces and glacial lake plains	frigid	silty	yes	very fine sandy loam
Ninigret	513	0.6	6.0	6.00	20.0	B	3	Outwash and Stream Terraces	mesic	loamy over sandy	no	sandy or sandy-skeletal
Occum	1	0.6	2.0	6.00	20.0	B	2	Flood Plain (Bottom Land)	mesic	loamy	no	loamy over loamy sand
Ondawa	101	0.6	6.0	6.00	20.0	B	2	Flood Plain (Bottom Land)	frigid	loamy	no	loamy over loamy sand
Ondawa	201	0.6	6.0	6.00	20.0	B	2	Flood Plain (Bottom Land)	frigid	loamy	no	occ flood, loamy over l. sand
Ossipee	495			0.20	2.0	D	6	Organic Materials - Freshwater	frigid	loamy	no	organic over loam
Pawcatuck	497			20.00	100.0	D	6	Tidal Flat	mesic	sandy or sandy-skeletal	no	organic over sand
Paxton	66	0.6	2.0	0.00	0.2	C	3	Firm, platy, loamy till	mesic	loamy	no	
Peacham	549	0.6	2.0	0.00	0.2	D	6	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	organic over loam
Pemi	633	0.6	2.0	0.06	0.6	C	5	Terraces and glacial lake plains	frigid	silty	no	
Pennichuck	460	0.6	2.0	0.60	2.0	B	4	Friable till, silty, schist & phyllite	mesic	loamy-skeletal	no	20 to 40 in. deep
Peru	78	0.6	2.0	0.06	0.6	C	3	Firm, platy, loamy till	frigid	loamy	yes	
Pillsbury	646	0.6	2.0	0.06	0.2	C	5	Firm, platy, loamy till	frigid	silty	no	
Pipestone	314					B	5	Outwash and Stream Terraces	mesic	sandy	yes	
Pittstown	334	0.6	2.0	0.06	0.2	C	3	Firm, platy, silty till, schist & phyllite	mesic	loamy	no	channery silt loam in Cd
Plaisted	563	0.6	2.0	0.06	0.6	C	3	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	channery silt loam in Cd
Podunk	104	0.6	6.0	6.00	20.0	B	3	Flood Plain (Bottom Land)	frigid	loamy	no	loamy to coarse sand in C
Pondicherry	992			6.00	20.0	D	6	Organic Materials - Freshwater	frigid	sandy or sandy-skeletal	no	organic over sand
Poocham	230	0.6	2.0	0.20	2.0	B	3	Terraces and glacial lake plains	mesic	silty	no	silt loam in C
Pootatuck	4	0.6	6.0	6.00	20.0	B	3	Flood Plain (Bottom Land)	mesic	loamy	no	single grain in C
Quonset	310	2.0	20.0	20.00	100.0	A	1	Outwash and Stream Terraces	mesic	sandy-skeletal	no	shale
Rawsonville	98	0.6	6.0	0.60	6.0	C	4	Loose till, bedrock	frigid	loamy	yes	20 to 40 in. deep
Raynham	533	0.2	2.0	0.06	0.2	C	5	Terraces and glacial lake plains	mesic	silty	no	
Raypol	540	0.6	2.0	6.00	100.0	D	5	Outwash and Stream Terraces	mesic	co. loamy over sandy (skeletal)	no	
Redstone	665	2.0	6.0	6.00	20.0	A	1	Weathered Bedrock Till	frigid	fragmental	yes	loamy cap
Ricker	674	2.0	6.0	2.00	6.0	A	4	Organic over bedrock (up to 4" of mineral)	cryic	fibric to hemic	no	well drained, less than 20 in. deep
Ridgebury	656	0.6	6.0	0.00	0.2	C	5	Firm, platy, loamy till	mesic	loamy	no	
Rippowam	5	0.6	6.0	6.00	20.0	C	5	Flood Plain (Bottom Land)	mesic	loamy	no	
Roundabout	333	0.2	2.0	0.06	0.6	C	5	Terraces and glacial lake plains	frigid	silty	no	silt loam in the C
Rumney	105	0.6	6.0	6.00	20.0	C	5	Flood Plain (Bottom Land)	frigid	loamy	no	
Saco	6	0.6	2.0	6.00	20.0	D	6	Flood Plain (Bottom Land)	mesic	silty	no	strata
Saddleback	673	0.6	2.0	0.60	2.0	C/D	4	Loose till, bedrock	cryic	loamy	yes	less than 20 in. deep
Salmon	630	0.6	2.0	0.60	2.0	B	2	Terraces and glacial lake plains	frigid	silty	yes	very fine sandy loam
Saugatuck	16	0.06	0.2	6.00	20.0	C	5	Outwash and Stream Terraces	mesic	sandy	yes	ortstein
Scantic	233	0.0	0.2	0.00	0.2	D	5	Silt and Clay Deposits	frigid	fine	no	
Scarboro	115	6.0	20.0	6.00	20.0	D	6	Outwash and Stream Terraces	mesic	sandy	no	organic over sand, non stony
Scio	531	0.6	2.0	0.60	2.0	B	3	Terraces and glacial lake plains	mesic	silty	no	gravelly sand in 2C
Scitico	33	0.0	0.2	0.00	0.2	C	5	Silt and Clay Deposits	mesic	fine	no	
Scituate	448	0.6	2.0	0.06	0.2	C	3	Firm, platy, sandy till	mesic	loamy	no	loamy sand in Cd
Searsport	15	6.0	20.0	6.00	20.0	D	6	Outwash and Stream Terraces	frigid	sandy	no	organic over sand
Shaker	439	2.0	6.0	0.00	0.2	C	5	Sandy/loamy over silt/clay	mesic	co. loamy over clayey	no	
Shapleigh	136					C/D	4	Sandy Till	mesic	sandy	yes	less than 20 in. deep
Sheepscoot	14	6.0	20.0	6.00	20.0	B	3	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	gravelly coarse sand
Sisk	667	0.6	2.0	0.00	0.6	C	3	Firm, platy, loamy till	cryic	loamy	yes	sandy loam in Cd
Skerry	558	0.6	2.0	0.06	0.6	C	3	Firm, platy, sandy till	frigid	loamy	yes	loamy sand in Cd
Squamscott	538	6.0	20.0	0.06	0.6	C	5	Sandy/loamy over silt/clay	mesic	sandy over loamy	yes	
Stetson	523	0.6	6.0	6.00	20.0	B	2	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	loamy over gravelly
Stissing	340	0.6	2.0	0.06	0.2	C	5	Firm, platy, silty till, schist & phyllite	mesic	loamy	no	
Success	154	2.0	6.0	6.00	20.0	A	1	Sandy Till	frigid	sandy-skeletal	yes	cemented
Sudbury	118	2.0	6.0	2.00	20.0	B	3	Outwash and Stream Terraces	mesic	sandy	no	loam over gravelly sand

Soil Series	legend number	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Group	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Suffield	536	0.6	2.0	0.00	0.2	C	3	Sandy/loamy over silt/clay	mesic	silty over clayey	no	deep to clay C
Sunapee	168	0.6	2.0	0.60	6.0	B	3	Loose till, loamy textures	frigid	loamy	yes	
Sunapee var	269	0.6	2.0	0.60	6.0	B	3	Loose till, loamy textures	frigid	loamy	yes	frigid dystrodept
Suncook	2	6.0	20.0	6.00	20.0	A	1	Flood Plain (Bottomland)	mesic	sandy	no	occasionally flooded
Suncook	402	6.0	20.0	6.00	20.0	A	1	Flood Plain (Bottomland)	mesic	sandy	no	frequent flooding
Sunday	102	6.0	20.0	6.00	20.0	A	1	Flood Plain (Bottomland)	frigid	sandy	no	occasionally flooded
Sunday	202	6.0	20.0	6.00	20.0	A	1	Flood Plain (Bottomland)	frigid	sandy	no	frequently flooded
Surplus	669	0.6	2.0	0.00	0.6	C	3	Firm, platy, loamy till	cryic	loamy	yes	mwd, sandy loam in Cd
Sutton	68	0.6	6.0	0.60	6.0	B	3	Loose till, loamy textures	mesic	loamy	no	
Swanton	438	2.0	6.0	0.00	0.2	C	5	Sandy/loamy over silt/clay	frigid	co. loamy over clayey	no	
Telos	123	0.6	2.0	0.02	0.2	C	3	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	channery silt loam in Cd
Thorndike	84	0.6	2.0	0.60	2.0	C/D	4	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	less than 20 in. deep
Timakwa	393			6.00	100.0	D	6	Organic Materials - Freshwater	mesic	sandy or sandy-skeletal	no	organic over sand
Tunbridge	99	0.6	6.0	0.60	6.0	C	4	Loose till, bedrock	frigid	loamy	yes	20 to 40 in. deep
Unadilla	30	0.6	2.0	2.00	20.0	B	2	Terraces and glacial lake plains	mesic	silty	no	silty over gravelly
Vassalboro	150					D	6	Organic Materials - Freshwater	frigid	peat	no	deep organic
Walpole	546	2.0	6.0	6.00	20.0	C	5	Outwash and Stream Terraces	mesic	sandy	no	
Wareham	34	6.0	20.0	6.00	20.0	C	5	Outwash and Stream Terraces	mesic	sandy	no	
Warwick	210	2.0	6.0	20.00	100.0	A	1	Outwash and Stream Terraces	mesic	loamy-skeletal	no	loamy over slate gravel
Waskish	195					D	6	Organic Materials - Freshwater	frigid	peat	no	deep organic
Waumbeck	58	2.0	20.0	6.00	20.0	B	3	Loose till, sandy textures	frigid	sandy-skeletal	yes	very cobbly loamy sand
Westbrook	597			0.00	2.0	D	6	Tidal Flat	mesic	loamy	no	organic over loam
Whitman	49	0.0	0.2	0.00	0.2	D	6	Firm, platy, loamy till	mesic	loamy	no	mucky loam
Windsor	26	6.0	20.0	6.00	20.0	A	1	Outwash and Stream Terraces	mesic	sandy	no	
Winnecook	88	0.6	2.0	0.60	2.0	C	4	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	20 to 40 in. deep
Winooski	9	0.6	6.0	0.60	6.0	B		Flood Plain (Bottom Land)	mesic	silty over loamy	no	
Winooski	103	0.6	6.0	0.60	6.0	B	3	Flood Plain (Bottom Land)	mesic	silty	no	very fine sandy loam
Wonsqueak	995			0.20	2.0	D	6	Organic Materials - Freshwater	frigid	loamy	no	organic over loam
Woodbridge	29	0.6	2.0	0.00	0.6	C	3	Firm, platy, loamy till	mesic	loamy	no	sandy loam in Cd
Woodstock	93	2.0	6.0	2.00	6.0	C/D	4	Loose till, bedrock	frigid	loamy	no	less than 20 in. deep

 no longer recognized
 organic materials

TABLE C

NHDES SOIL GROUPINGS

Soil Series	number	NHDES Soil Group	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Adams	36	1	6.0	20.0	20.00	99.0	A	Outwash and Stream Terraces	frigid	sandy	yes	
Boscawen	220	1	6.0	20.0	20.00	100.0	A	Outwash and Stream Terraces	frigid	sandy-skeletal	no	loamy cap
Caesar	526	1	20.0	100.0	20.00	100.0	A	Outwash and Stream Terraces	mesic	coarse sand	no	
Champlain	35	1	6.0	20.0	20.00	100.0	A	Outwash and Stream Terraces	frigid	gravelly sand	no	
Colton	22	1	6.0	20.0	20.00	100.0	A	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	
Colton, gravelly	21	1	6.0	20.0	20.00	100.0	A	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	gravelly surface
Gloucester	11	1	6.0	20.0	6.00	20.0	A	Sandy Till	mesic	sandy-skeletal	no	loamy cap
Hermon	55	1	2.0	20.0	6.00	20.0	A	Sandy Till	frigid	sandy-skeletal	yes	loamy cap
Hinckley	12	1	6.0	20.0	20.00	100.0	A	Outwash and Stream Terraces	mesic	sandy-skeletal	no	
Hoosic	510	1	2.0	20.0	20.00	100.0	A	Outwash and Stream Terraces	mesic	sandy-skeletal	no	slate, loamy cap
Masardis	23	1	6.0	20.0	6.00	20.0	A	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	slate, loamy cap
Merrimac	10	1	2.0	20.0	6.00	20.0	A	Outwash and Stream Terraces	mesic	gravelly sand	no	loamy cap
Quonset	310	1	2.0	20.0	20.00	100.0	A	Outwash and Stream Terraces	mesic	sandy-skeletal	no	shale
Redstone	665	1	2.0	6.0	6.00	20.0	A	Weathered Bedrock Till	frigid	fragmental	yes	loamy cap
Success	154	1	2.0	6.0	6.00	20.0	A	Sandy Till	frigid	sandy-skeletal	yes	cemented
Suncook	2	1	6.0	20.0	6.00	20.0	A	Flood Plain (Bottomland)	mesic	sandy	no	occasionally flooded
Suncook	402	1	6.0	20.0	6.00	20.0	A	Flood Plain (Bottomland)	mesic	sandy	no	frequent flooding
Sunday	102	1	6.0	20.0	6.00	20.0	A	Flood Plain (Bottomland)	frigid	sandy	no	occasionally flooded
Sunday	202	1	6.0	20.0	6.00	20.0	A	Flood Plain (Bottomland)	frigid	sandy	no	frequently flooded
Warwick	210	1	2.0	6.0	20.00	100.0	A	Outwash and Stream Terraces	mesic	loamy-skeletal	no	loamy over slate gravel
Windsor	26	1	6.0	20.0	6.00	20.0	A	Outwash and Stream Terraces	mesic	sandy	no	
Abenaki	501	2	0.6	2.0	6.00	99.0	B	Outwash and Stream Terraces	frigid	loamy over sandy-skeletal	no	loamy over gravelly
Agawam	24	2	6.0	20.0	20.00	100.0	B	Outwash and Stream Terraces	mesic	loamy over sandy	no	loamy over sand/gravel
Allagash	127	2	0.6	2.0	6.00	20.0	B	Outwash and Stream Terraces	frigid	loamy over sandy	yes	loamy over sandy
Bangor	572	2	0.6	2.0	0.60	2.0	B	Friable till, silty, schist & phyllite	frigid	loamy	yes	silt loam
Berkshire	72	2	0.6	6.0	0.60	6.0	B	Loose till, loamy textures	frigid	loamy	yes	fine sandy loam
Bice	226	2	0.6	6.0	0.60	6.0	B	Loose till, loamy textures	frigid	loamy	no	sandy loam
Canton	42	2	2.0	6.0	6.00	20.0	B	Loose till, sandy textures	mesic	loamy over sandy	no	loamy over loamy sand
Charlton	62	2	0.6	6.0	0.60	6.0	B	Loose till, loamy textures	mesic	loamy	no	fine sandy loam
Dutchess	366	2	0.6	2.0	0.60	2.0	B	Friable till, silty, schist & phyllite	mesic	loamy	no	very channery
Fryeburg	208	2	0.6	2.0	2.00	6.0	B	Flood Plain (Bottom Land)	frigid	silty	no	very fine sandy loam
Groveton	27	2	0.6	2.0	0.60	6.0	B	Outwash and Stream Terraces	frigid	loamy	yes	loamy over sandy
Hadley	8	2	0.6	2.0	0.60	6.0	B	Flood Plain (Bottom Land)	mesic	silty	no	strata of fine sand
Hadley	108	2	0.6	2.0	0.60	6.0	B	Flood Plain (Bottom Land)	mesic	silty	no	strata of fine sand, occ flooded
Hartland	31	2	0.6	2.0	0.20	2.0	B	Terraces and glacial lake plains	mesic	silty	no	very fine sandy loam
Haven	410	2	0.6	2.0	20.00	100.0	B	Outwash and Stream Terraces	mesic	loamy over sandy	no	loamy over sand/gravel
Houghtonville	795	2	0.6	6.0	0.60	6.0	B	Loose till, loamy textures	frigid	loamy	yes	cobbly fine sandy loam
Lombard	259	2	0.6	6.0	2.00	20.0	C/D	Weathered bedrock, phyllite	frigid	loamy	no	very channery
Monadnock	142	2	0.6	2.0	2.00	6.0	B	Loose till, sandy textures	frigid	loamy over sandy, sandy-skeletal	yes	gravelly loamy sand in C
Occum	1	2	0.6	2.0	6.00	20.0	B	Flood Plain (Bottom Land)	mesic	loamy	no	loamy over loamy sand
Ondawa	101	2	0.6	6.0	6.00	20.0	B	Flood Plain (Bottom Land)	frigid	loamy	no	loamy over loamy sand
Ondawa	201	2	0.6	6.0	6.00	20.0	B	Flood Plain (Bottom Land)	frigid	loamy	no	occ flood, loamy over l. sand
Salmon	630	2	0.6	2.0	0.60	2.0	B	Terraces and glacial lake plains	frigid	silty	yes	very fine sandy loam
Stetson	523	2	0.6	6.0	6.00	20.0	B	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	loamy over gravelly
Unadilla	30	2	0.6	2.0	2.00	20.0	B	Terraces and glacial lake plains	mesic	silty	no	silty over gravelly
Chichester	442	2	0.6	2.0	2.00	6.0	B	Loose till, sandy textures	frigid	loamy over sandy	no	loamy over loamy sand
Acton	146	3	2.0	20.0	2.00	20.0	B	Loose till, sandy textures	mesic	sandy-skeletal	no	cobbly loamy sand
Becket	56	3	0.6	2.0	0.06	0.6	C	Firm, platy, sandy till	frigid	loamy	yes	gravelly sandy loam in Cd
Belgrade	532	3	0.6	2.0	0.06	2.0	B	Terraces and glacial lake plains	mesic	silty	no	strata of fine sand
Bernardston	330	3	0.6	2.0	0.06	0.2	C	Firm, platy, silty till, schist & phyllite	mesic	loamy	no	channery silt loam in Cd
Boxford	32	3	0.1	0.2	0.00	0.2	C	Silt and Clay Deposits	mesic	fine	no	silty clay loam

Soil Series	number	NHDES Soil Group	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Buckland	237	3	0.6	2.0	0.06	0.2	C	Firm, platy, loamy till	frigid	loamy	no	loam in Cd
Buxton	232	3	0.1	0.6	0.00	0.2	C	Silt and Clay Deposits	frigid	fine	no	silty clay
Canterbury	166	3	0.6	2.0	0.06	0.6	C	Firm, platy, loamy till	frigid	loamy	no	loam in Cd
Chatfield Var.	289	3	0.6	6.0	0.60	6.0	B	Loose till, bedrock	mesic	loamy	no	mwd to swpd
Chesuncook	126	3	0.6	2.0	0.02	0.2	C	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	channery silt loam in Cd
Colonel	927	3	0.6	2.0	0.06	0.6	C	Firm, platy, loamy till	frigid	loamy	yes	loam in Cd
Croghan	613	3	20.0	100.0	20.00	100.0	B	Outwash and Stream Terraces	frigid	sandy	yes	single grain in C
Dartmouth	132	3	0.6	2.0	0.06	0.6	B	Terraces and glacial lake plains	mesic	silty	no	thin strata silty clay loam
Deerfield	313	3	6.0	20.0	20.00	100.0	B	Outwash and Stream Terraces	mesic	sandy	no	single grain in C
Dixfield	378	3	0.6	2.0	0.06	0.6	C	Firm, platy, loamy till	frigid	loamy	yes	fine sandy loam in Cd
Dixmont	578	3	0.6	2.0	0.60	2.0	C	Friable till, silty, schist & phyllite	frigid	loamy	yes	silt loam, platy in C
Duane	413	3	6.0	20.0	6.00	20.0	B	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	cemented (ortstein)
Eldridge	38	3	6.0	20.0	0.06	0.6	C	Sandy/loamy over silt/clay	mesic	sandy over loamy	no	
Elmridge	238	3	2.0	6.0	0.00	0.2	C	Sandy/loamy over silt/clay	mesic	loamy over clayey	no	
Elmwood	338	3	2.0	6.0	0.00	0.2	C	Sandy/loamy over silt/clay	frigid	loamy over clayey	no	
Finch	116	3					C	Outwash and Stream Terraces	frigid	sandy	yes	cemented (ortstein)
Gilmanton	478	3	0.6	2.0	0.06	0.6	C	Firm, platy, loamy till	frigid	loamy	no	fine sandy loam in Cd
Henniker	46	3	0.6	2.0	0.06	0.6	C	Firm, platy, sandy till	frigid	loamy	no	loamy sand in Cd
Hitchcock	130	3	0.6	2.0	0.06	0.6	B	Terraces and glacial lake plains	mesic	silty	no	silt loam to silt in C
Howland	566	3	0.6	2.0	0.06	0.2	C	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	silt loam, platy in Cd
Lanesboro	228	3	0.6	2.0	0.06	0.2	C	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	channery silt loam in Cd
Lovewell	307	3	0.6	2.0	0.60	2.0	B	Flood Plain (Bottom Land)	frigid	silty	no	very fine sandy loam
Machias	520	3	2.0	6.0	6.00	20.0	B	Outwash and Stream Terraces	frigid	sandy or sandy-skeletal	yes	strata sand/gravel in C
Madawaska	28	3	0.6	2.0	6.00	20.0	B	Outwash and Stream Terraces	frigid	loamy over sandy	yes	sandy or sandy-skeletal
Madawaska, aqued	48	3	0.6	2.0	6.00	20.0	B	Outwash and Stream Terraces	frigid	loamy over sandy	yes	sandy or sandy-skeletal
Marlow	76	3	0.6	2.0	0.06	0.6	C	Firm, platy, loamy till	frigid	loamy	yes	fine sandy loam in Cd
Melrose	37	3	2.0	6.0	0.00	0.2	C	Sandy/loamy over silt/clay	frigid	loamy over clayey	no	silty clay loam in C
Metacomet	458	3	0.6	2.0	0.06	0.6	C	Firm, platy, sandy till	frigid	loamy	no	loamy sand in Cd
Metallak	404	3	6.0	100.0	6.00	100.0	B	Flood Plain (Bottom Land)	frigid	loamy over sandy	no	sandy or sandy-skeletal
Millis	39	3					C	Firm, platy, sandy till	frigid	loamy	yes	loamy sand in Cd
Montauk	44	3	0.6	6.0	0.06	0.6	C	Firm, platy, sandy till	mesic	loamy	no	loamy sand in Cd
Mundal	610	3	0.6	2.0	0.06	0.6	C	Firm, platy, loamy till	frigid	loamy	yes	gravely sandy loam in Cd
Newfields	444	3	0.6	2.0	0.60	2.0	B	Loose till, sandy textures	mesic	loamy over sandy	no	sandy or sandy-skeletal
Nicholville	632	3	0.6	2.0	0.60	2.0	C	Terraces and glacial lake plains	frigid	silty	yes	very fine sandy loam
Ninigret	513	3	0.6	6.0	6.00	20.0	B	Outwash and Stream Terraces	mesic	loamy over sandy	no	sandy or sandy-skeletal
Paxton	66	3	0.6	2.0	0.00	0.2	C	Firm, platy, loamy till	mesic	loamy	no	
Peru	78	3	0.6	2.0	0.06	0.6	C	Firm, platy, loamy till	frigid	loamy	yes	
Pittstown	334	3	0.6	2.0	0.06	0.2	C	Firm, platy, silty till, schist & phyllite	mesic	loamy	no	channery silt loam in Cd
Plaisted	563	3	0.6	2.0	0.06	0.6	C	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	channery silt loam in Cd
Podunk	104	3	0.6	6.0	6.00	20.0	B	Flood Plain (Bottom Land)	frigid	loamy	no	loamy to coarse sand in C
Poocham	230	3	0.6	2.0	0.20	2.0	B	Terraces and glacial lake plains	mesic	silty	no	silt loam in C
Pootatuck	4	3	0.6	6.0	6.00	20.0	B	Flood Plain (Bottom Land)	mesic	loamy	no	single grain in C
Scio	531	3	0.6	2.0	0.60	2.0	B	Terraces and glacial lake plains	mesic	silty	no	gravely sand in 2C
Scituate	448	3	0.6	2.0	0.06	0.2	C	Firm, platy, sandy till	mesic	loamy	no	loamy sand in Cd
Sheepscot	14	3	6.0	20.0	6.00	20.0	B	Outwash and Stream Terraces	frigid	sandy-skeletal	yes	gravely coarse sand
Sisk	667	3	0.6	2.0	0.00	0.6	C	Firm, platy, loamy till	cryic	loamy	yes	sandy loam in Cd
Skerry	558	3	0.6	2.0	0.06	0.6	C	Firm, platy, sandy till	frigid	loamy	yes	loamy sand in Cd
Sudbury	118	3	2.0	6.0	2.00	20.0	B	Outwash and Stream Terraces	mesic	sandy	no	loam over gravely sand
Suffield	536	3	0.6	2.0	0.00	0.2	C	Sandy/loamy over silt/clay	mesic	silty over clayey	no	deep to clay C
Sunapee	168	3	0.6	2.0	0.60	6.0	B	Loose till, loamy textures	frigid	loamy	yes	
Sunapee var	269	3	0.6	2.0	0.60	6.0	B	Loose till, loamy textures	frigid	loamy	yes	frigid dystrodept
Surplus	669	3	0.6	2.0	0.00	0.6	C	Firm, platy, loamy till	cryic	loamy	yes	mwd, sandy loam in Cd
Sutton	68	3	0.6	6.0	0.60	6.0	B	Loose till, loamy textures	mesic	loamy	no	
Telos	123	3	0.6	2.0	0.02	0.2	C	Firm, platy, silty till, schist & phyllite	frigid	loamy	yes	channery silt loam in Cd

Sorted by DES Soil Group for Establishing Lot Size
K_{sat} B and C horizons
SSSNNE pub no. 5

Soil Series	number	NHDES Soil Group	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Waumbeck	58	3	2.0	20.0	6.00	20.0	B	Loose till, sandy textures	frigid	sandy-skeletal	yes	very cobbly loamy sand
Winooski	103	3	0.6	6.0	0.60	6.0	B	Flood Plain (Bottom Land)	mesic	silty	no	very fine sandy loam
Woodbridge	29	3	0.6	2.0	0.00	0.6	C	Firm, platy, loamy till	mesic	loamy	no	sandy loam in Cd
Winooski	9	3	0.6	6.0	0.60	6.0	B	Flood Plain (Bottom Land)	mesic	silty over loamy	no	
Canaan	663	4	2.0	20.0	2.00	20.0	C	Weathered Bedrock Till	frigid	loamy-skeletal	yes	less than 20 in. deep
Cardigan	357	4	0.6	2.0	0.60	2.0	B	Friable till, silty, schist & phyllite	mesic	loamy	no	20 to 40 in. deep
Chatfield	89	4	0.6	6.0	0.60	6.0	B	Loose till, bedrock	mesic	loamy	no	20 to 40 in. deep
Elliottsville	128	4	0.6	2.0	0.60	2.0	B	Friable till, silty, schist & phyllite	frigid	loamy	yes	20 to 40 in. deep
Glebe	671	4	2.0	6.0	2.00	6.0	C	Loose till, bedrock	cryic	loamy	yes	20 to 40 in. deep
Glover	NA	4	0.6	2.0	0.60	2	D	Friable till, silty, schist & phyllite	frigid	loamy	no	less than 20 in. deep
Hogback	91	4	2.0	6.0	2.00	6.0	C	Loose till, bedrock	frigid	loamy	yes	less than 20 in. deep
Hollis	86	4	0.6	6.0	0.60	6.0	C/D	Loose till, bedrock	mesic	loamy	no	less than 20 in. deep
Kearsarge	359	4	0.6	2.0	0.60	2.0	B	Friable till, silty, schist & phyllite	mesic	loamy	no	less than 20 in. deep
Lyman	92	4	2.0	6.0	2.00	6.0	A/D	Loose till, bedrock	frigid	loamy	yes	less than 20 in. deep
Macomber	252	4	0.6	2.0	0.60	2.0	C	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	20 to 40 in. deep
Millsite	251	4	0.6	6.0	0.60	6.0	C	Loose till, bedrock	frigid	loamy	no	20 to 40 in. deep
Monson	133	4	0.6	2.0	0.60	2.0	D	Friable till, silty, schist & phyllite	frigid	loamy	yes	less than 20 in. deep
Pennichuck	460	4	0.6	2.0	0.60	2.0	B	Friable till, silty, schist & phyllite	mesic	loamy-skeletal	no	20 to 40 in. deep
Rawsonville	98	4	0.6	6.0	0.60	6.0	C	Loose till, bedrock	frigid	loamy	yes	20 to 40 in. deep
Ricker	674	4	2.0	6.0	2.00	6.0	A	rganic over bedrock (up to 4" of mineral)	cryic	fibric to hemic	no	well drained, less than 20 in. deep
Saddleback	673	4	0.6	2.0	0.60	2.0	C/D	Loose till, bedrock	cryic	loamy	yes	less than 20 in. deep
Shapleigh	136	4					C/D	Sandy Till	mesic	sandy	yes	less than 20 in. deep
Thorndike	84	4	0.6	2.0	0.60	2.0	C/D	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	less than 20 in. deep
Tunbridge	99	4	0.6	6.0	0.60	6.0	C	Loose till, bedrock	frigid	loamy	yes	20 to 40 in. deep
Winnecook	88	4	0.6	2.0	0.60	2.0	C	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	20 to 40 in. deep
Woodstock	93	4	2.0	6.0	2.00	6.0	C/D	Loose till, bedrock	frigid	loamy	no	less than 20 in. deep
Au Gres	516	5					B	Outwash and Stream Terraces	frigid	sandy	yes	single grain, loose
Bemis	224	5	0.6	0.2	0.00	0.2	C	Firm, platy, loamy till	cryic	loamy	no	
Binghamville	534	5	0.2	2.0	0.06	0.2	D	Terraces and glacial lake plains	mesic	silty	no	
Brayton	240	5	0.6	2.0	0.06	0.6	C	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Cabot	589	5	0.6	2.0	0.06	0.2	D	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Charles	209	5	0.6	100.0	0.60	100.0	C	Flood Plain (Bottom Land)	frigid	silty	no	
Cohas	505	5	0.6	2.0	0.60	100.0	C	Flood Plain (Bottom Land)	frigid	co. loamy over sandy (skeletal)	no	
Grange	433	5	0.6	2.0	0.60	2.0	C	Outwash and Stream Terraces	frigid	co. loamy over sandy (skeletal)	no	
Kinsman	614	5	6.0	20.0	6.00	20.0	C	Outwash and Stream Terraces	frigid	sandy	yes	
Leicester	514	5	0.6	6.0	0.60	20.0	C	Loose till, loamy textures	mesic	loamy	no	
Lim	3	5	0.6	2.0	6.00	20.0	C	Flood Plain (Bottom Land)	mesic	loamy	no	
Limerick	109	5	0.6	2.0	0.60	2.0	C	Flood Plain (Bottom Land)	mesic	silty	no	
Lyme	246	5	0.6	6.0	0.60	6.0	C	Loose till, sandy textures	frigid	loamy	no	
Mashpee	315	5	6.0	20.0	6.00	20.0	B	Outwash and Stream Terraces	mesic	sandy	yes	
Monarda	569	5	0.2	2.0	0.02	0.2	D	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Moosilauke	414	5	6.0	20.0	6.00	20.0	C	Loose till, sandy textures	frigid	sandy	no	
Naumburg	214	5	6.0	20.0	6.00	20.0	C	Outwash and Stream Terraces	frigid	sandy	yes	
Pemi	633	5	0.6	2.0	0.06	0.6	C	Terraces and glacial lake plains	frigid	silty	no	
Pillsbury	646	5	0.6	2.0	0.06	0.2	C	Firm, platy, loamy till	frigid	silty	no	
Pipestone	314	5					B	Outwash and Stream Terraces	mesic	sandy	yes	
Raynham	533	5	0.2	2.0	0.06	0.2	C	Terraces and glacial lake plains	mesic	silty	no	
Raypol	540	5	0.6	2.0	6.00	100.0	D	Outwash and Stream Terraces	mesic	co. loamy over sandy (skeletal)	no	
Ridgebury	656	5	0.6	6.0	0.00	0.2	C	Firm, platy, loamy till	mesic	loamy	no	
Rippowam	5	5	0.6	6.0	6.00	20.0	C	Flood Plain (Bottom Land)	mesic	loamy	no	
Roundabout	333	5	0.2	2.0	0.06	0.6	C	Terraces and glacial lake plains	frigid	silty	no	silt loam in the C
Rumney	105	5	0.6	6.0	6.00	20.0	C	Flood Plain (Bottom Land)	frigid	loamy	no	

Sorted by DES Soil Group for Establishing Lot Size
K_{sat} B and C horizons
SSSNNE pub no. 5

Soil Series	number	NHDES Soil Group	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Land Form	Temp.	Soil Textures	Spodosol ?	Other
Saugatuck	16	5	0.06	0.2	6.00	20.0	C	Outwash and Stream Terraces	mesic	sandy	yes	ortstein
Scantic	233	5	0.0	0.2	0.00	0.2	D	Silt and Clay Deposits	frigid	fine	no	
Scitico	33	5	0.0	0.2	0.00	0.2	C	Silt and Clay Deposits	mesic	fine	no	
Shaker	439	5	2.0	6.0	0.00	0.2	C	Sandy/loamy over silt/clay	mesic	co. loamy over clayey	no	
Squamscott	538	5	6.0	20.0	0.06	0.6	C	Sandy/loamy over silt/clay	mesic	sandy over loamy	yes	
Stissing	340	5	0.6	2.0	0.06	0.2	C	Firm, platy, silty till, schist & phyllite	mesic	loamy	no	
Swanton	438	5	2.0	6.0	0.00	0.2	C	Sandy/loamy over silt/clay	frigid	co. loamy over clayey	no	
Walpole	546	5	2.0	6.0	6.00	20.0	C	Outwash and Stream Terraces	mesic	sandy	no	
Wareham	34	5	6.0	20.0	6.00	20.0	C	Outwash and Stream Terraces	mesic	sandy	no	
Biddeford	234	6	0.0	0.2	0.00	0.2	D	Silt and Clay Deposits	frigid	fine	no	organic over clay
Bucksport	895	6					D	Organic Materials - Freshwater	frigid	sapric	no	deep organic
Burnham	131	6	0.2	6.0	0.02	0.2	D	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	organic over silt
Catden	296	6					A/D	Organic Materials - Freshwater	mesic	sapric	no	deep organic
Chocorua	395	6			6.00	20.0	D	Organic Materials - Freshwater	frigid	sandy or sandy-skeletal	no	organic over sand
Greenwood	295	6					A/D	Organic Materials - Freshwater	frigid	hemic	no	deep organic
Ipswich	397	6					D	Tidal Flat	mesic	hemic/sapric	no	deep organic
Matunuck	797	6			20.00	100.0	D	Tidal Flat	mesic	sandy	no	organic over sand
Maybid	134	6	0.0	0.2	0.00	0.2	D	Silt and Clay Deposits	mesic	fine	no	silt over clay
Meadowsedge	894	6					D	Organic Materials - Freshwater	frigid	peat	no	deep organic
Medomak	406	6	0.6	2.0	0.60	2.0	D	Flood Plain (Bottom Land)	frigid	silty	no	organic over silt
Natchaug	496	6			0.20	2.0	D	Organic Materials - Freshwater	mesic	loamy	no	organic over loam
Ossipee	495	6			0.20	2.0	D	Organic Materials - Freshwater	frigid	loamy	no	organic over loam
Pawcatuck	497	6			20.00	100.0	D	Tidal Flat	mesic	sandy or sandy-skeletal	no	organic over sand
Peacham	549	6	0.6	2.0	0.00	0.2	D	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	organic over loam
Pondicherry	992	6			6.00	20.0	D	Organic Materials - Freshwater	frigid	sandy or sandy-skeletal	no	organic over sand
Saco	6	6	0.6	2.0	6.00	20.0	D	Flood Plain (Bottom Land)	mesic	silty	no	strata
Scarboro	115	6	6.0	20.0	6.00	20.0	D	Outwash and Stream Terraces	mesic	sandy	no	organic over sand, non stony
Searsport	15	6	6.0	20.0	6.00	20.0	D	Outwash and Stream Terraces	frigid	sandy	no	organic over sand
Timakwa	393	6			6.00	100.0	D	Organic Materials - Freshwater	mesic	sandy or sandy-skeletal	no	organic over sand
Vassalboro	150	6					D	Organic Materials - Freshwater	frigid	peat	no	deep organic
Waskish	195	6					D	Organic Materials - Freshwater	frigid	peat	no	deep organic
Westbrook	597	6			0.00	2.0	D	Tidal Flat	mesic	loamy	no	organic over loam
Whitman	49	6	0.0	0.2	0.00	0.2	D	Firm, platy, loamy till	mesic	loamy	no	mucky loam
Wonsqueak	995	6			0.20	2.0	D	Organic Materials - Freshwater	frigid	loamy	no	organic over loam

no longer recognized organic materials denotes break between Soil Group

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SWPPP Cut Sheet:

Filtrex[®] Sediment Control

Sediment & Perimeter Control Technology

PURPOSE & DESCRIPTION

Filtrex[®] Sediment control is a three-dimensional tubular sediment control and storm water runoff filtration device typically used for **perimeter control** of sediment and other soluble pollutants (such as phosphorus and petroleum hydrocarbons), on and around construction activities.

APPLICATION

Filtrex[®] Sediment control is to be installed down slope of any disturbed area requiring erosion and sediment control and filtration of soluble pollutants from runoff. Sediment control is effective when installed perpendicular to sheet or low concentrated flow. Acceptable applications include:

- Site perimeters
- Above and below disturbed areas subject to sheet runoff, interrill and rill erosion
- Above and below exposed and erodable slopes
- Around area drains or inlets located in a 'sump'
- On compacted soils where trenching of silt fence is difficult or impossible
- Around sensitive trees where trenching of silt fence is not beneficial for tree survival or may unnecessarily disturb established vegetation.
- On frozen ground where trenching of silt fence is impossible.
- On paved surfaces where trenching of silt fence is impossible.

INSTALLATION

1. Sediment control used for perimeter control of sediment and soluble pollutants in storm runoff shall meet Filtrex[®] Soxx[™] Material Specifications and use Certified Filtrex[®] FilterMedia[™].
2. Contractor is required to be Filtrex[®] Certified[™], or use pre-filled Filtrex[®] Sediment control

products manufactured by a Filtrex[®] Certified Manufacturer[™] as determined by Filtrex[®] International, LLC (440-926-2607 or visit www.filtrex.com). Certification shall be considered current if appropriate identification is shown during time of bid or at time of application. Look for the Filtrex[®] Certified[™] Seal.

3. Sediment control will be placed at locations indicated on plans as directed by the Engineer.
4. Sediment control should be installed parallel to the base of the slope or other disturbed area. In extreme conditions (i.e., 2:1 slopes), a second Sediment control shall be constructed at the top of the slope.
5. Effective Soxx[™] height in the field should be as follows: 8" Diameter Sediment control = 6.5" high, 12" Diameter Sediment control = 9.5" high, 18" Diameter SiltSoxx[™] = 14.5" high, 24" Diameter Sediment control = 19" high.
6. Stakes shall be installed through the middle of the Sediment control on 10 ft (3m) centers, using 2 in (50mm) by 2 in (50mm) by 3 ft (1m) hard wood stakes. In the event staking is not possible, i.e., when Sediment control is used on pavement, heavy concrete blocks shall be used behind the Sediment control to help stabilize during rainfall/runoff events.
7. Staking depth for sand and silt loam soils shall be 12 in (300mm), and 8 in (200mm) for clay soils.
8. Loose compost may be backfilled along the upslope side of the Sediment control, filling the seam between the soil surface and the device, improving filtration and sediment retention.
9. If the Sediment control is to be left as a permanent filter or part of the natural landscape, it may be seeded at time of installation for



establishment of permanent vegetation. The Engineer will specify seed requirements.

10. Filtrex[®] Sediment control is not to be used in perennial, ephemeral, or intermittent streams.

See design drawing schematic for correct Filtrex[®] Sediment control installation (Figure 1.1).

INSPECTION AND MAINTENANCE

Routine inspection should be conducted within 24 hrs of a runoff event or as designated by the regulating authority. Sediment control should be regularly inspected to make sure they maintain their shape and are producing adequate hydraulic flow-through. If ponding becomes excessive, additional Sediment control may be required to reduce effective slope length or sediment removal may be necessary. Sediment control shall be inspected until area above has been permanently stabilized and construction activity has ceased

1. The Contractor shall maintain the Sediment control in a functional condition at all times and it shall be routinely inspected.
2. If the Sediment control has been damaged, it shall be repaired, or replaced if beyond repair.

3. The Contractor shall remove sediment at the base of the upslope side of the Sediment control when accumulation has reached 1/2 of the effective height of the Sediment control, or as directed by the Engineer. Alternatively, a new Sediment control can be placed on top of and slightly behind the original one creating more sediment storage capacity without soil disturbance.
4. Sediment control shall be maintained until disturbed area above the device has been permanently stabilized and construction activity has ceased.
5. The FilterMedia[™] will be dispersed on site once disturbed area has been permanently stabilized, construction activity has ceased, or as determined by the Engineer.
6. For long-term sediment and pollution control applications, Sediment control can be seeded at the time of installation to create a vegetative filtering system for prolonged and increased filtration of sediment and soluble pollutants (contained vegetative filter strip). The appropriate seed mix shall be determined by the Engineer.

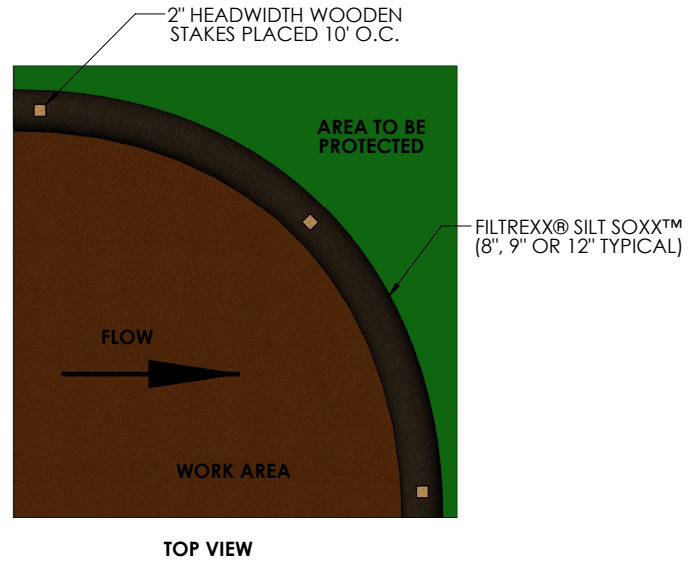
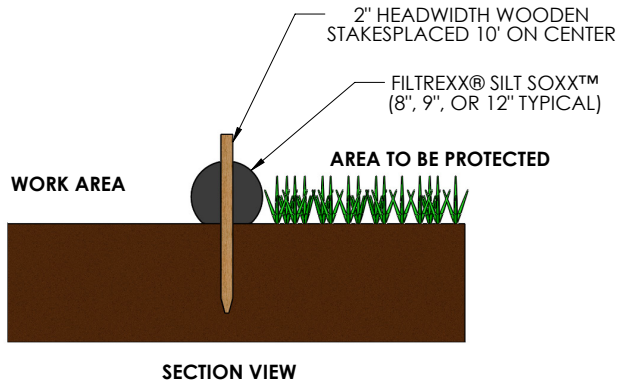
Slope Percent	Maximum Slope Length Above Sediment Control in Feet (meters)*				
	8 in (200 mm) Sediment control	12 in (300 mm) Sediment control	18 in (450 mm) Sediment control	24 in (600mm) Sediment control	32 in (800mm) Sediment control
	6.5 in (160 mm)**	9.5 in (240 mm) **	14.5 in (360 mm) **	19 in (480 mm) **	26 in (650 mm) **
2 (or less)	600 (180)	750 (225)	1000 (300)	1300 (400)	1650 (500)
5	400 (120)	500 (150)	550 (165)	650 (200)	750 (225)
10	200 (60)	250 (75)	300 (90)	400 (120)	500 (150)
15	140 (40)	170 (50)	200 (60)	325 (100)	450 (140)
20	100 (30)	125 (38)	140 (42)	260 (80)	400 (120)
25	80 (24)	100 (30)	110 (33)	200 (60)	275 (85)
30	60 (18)	75 (23)	90 (27)	130 (40)	200 (60)
35	60 (18)	75 (23)	80 (24)	115 (35)	150 (45)
40	60 (18)	75 (23)	80 (24)	100 (30)	125 (38)
45	40 (12)	50 (15)	60 (18)	80 (24)	100 (30)
50	40 (12)	50 (15)	55 (17)	65 (20)	75 (23)

* Based on a failure point of 36 in (0.9 m) super silt fence (wire reinforced) at 1000 ft (303 m) of slope, watershed width equivalent to receiving length of sediment control device, 1 in/ 24 hr (25 mm/24 hr) rain event.

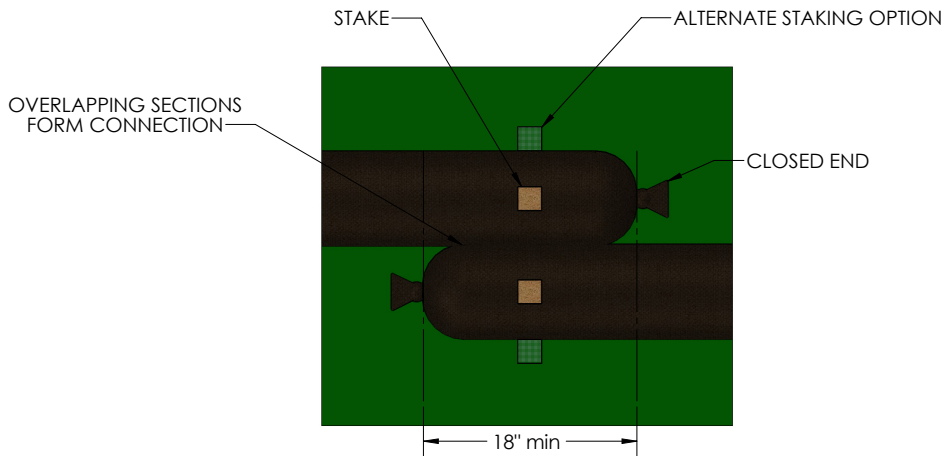
** Effective height of Sediment control after installation and with constant head from runoff as determined by Ohio State University.



FILTREXX® SILT SOXX™



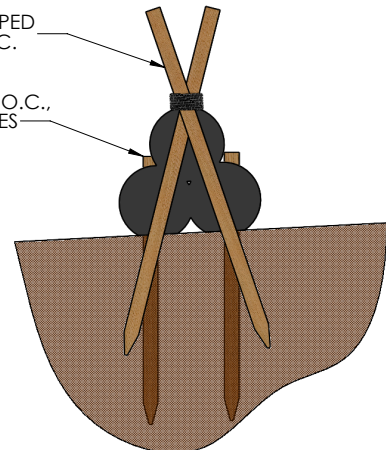
COMPOST SOCK CONNECTION/ATTACHMENT DETAIL



FILTREXX® PYRAMID STAKING DETAIL

(2) 2"x2"x48+" HARDWOOD STAKES, WRAPPED TOGETHER WITH 16 GAUGE WIRE, 10' O.C.

2"x2"x36" HARDWOOD STAKE, 10' O.C., STARTING 5' FROM ANGLED STAKES



- NOTES:**
1. ALL MATERIAL TO MEET FILTREXX® SPECIFICATIONS.
 2. SILT SOXX™ FILL TO MEET APPLICATION REQUIREMENTS.
 3. COMPOST MATERIAL TO BE DISPERSED ON SITE, AS DETERMINED BY ENGINEER.



SWPPP Cut Sheet:

Filtrex[®] Inlet Protection *Sediment & Perimeter Control Technology*

PURPOSE & DESCRIPTION

Filtrex[®] Inlet protection is a three-dimensional tubular sediment control and storm water runoff filtration device typically used for storm drain **inlet protection** of sediment and soluble pollutants (such as phosphorus and petroleum hydrocarbons) on and around construction activities.

APPLICATION

Drain inlets are located in areas that receive runoff from surrounding lands, often exposed and disturbed soils, and are located at a low point, or in a sump. Inlet protection used around drain inlets (or *Drain Inlet protection*) should completely enclose the circumference of the drain and where possible should not be placed on a grade or slope. Inlet protection used around drain inlets should never be the only form of site sediment control and should be accompanied by erosion control/slope stabilization practices, such as Slope protection or rolled erosion control blankets (RECB). Inlet protection should never be placed where they divert runoff flow from the drain inlet, or on top of the inlet, which can cause flooding. Under high runoff and sediment loading conditions placement of 1-2 in (25-50 mm) diameter rock (AASHTO #2) may be placed around the outer circumference of the Inlet protection up to ½ the height of the Inlet protection. This will slow runoff velocity as it contacts the Inlet protection and will reduce sediment build-up and clogging of the Inlet protection.

Curb inlets are generally located on paved surfaces and are designed to rapidly drain storm runoff from roadways to prevent flooding that poses a hazard to vehicular traffic. Inlet protection devices should be placed in a manner which intercepts runoff prior to entering the inlet, but does not block or divert runoff from the inlet. To prevent diversion of runoff, Inlet protection used around curbs (or *Curb*

inlet protection) should be used in low points, or sumps, and minor slopes or grades. Inlet protection should never be placed in or on the curb inlet drain, or placed in a manner than obstructs vehicular traffic. Inlet protection height should be at least 1 in (25 mm) lower than top of curb inlet to allow for overflow into the drain and not over the curb. Maximum sediment removal efficiency occurs when minor ponding exists behind Inlet protection but should never lead to flooding.

Curb sediment containment systems are used to reduce the sediment and pollutant load flowing to a curb inlet. They are generally placed on paved surfaces perpendicular to runoff flow and should be lower than the height of the curb. Curb sediment containment systems should never cause flooding or placed where they are a hazard to vehicular traffic. Inlet protection used for curb sediment containment (or *Curb Sediment Containment Inlet protection*) can be placed on a grade but should never be placed directly upslope from curb inlet where it may inadvertently divert runoff from entering curb inlet.

INSTALLATION

1. Inlet protection used for inlet protection to reduce sediment and soluble pollutants entering storm drains shall meet Filtrex[®] FilterSoxx[™] Material Specifications and use Certified Filtrex[®] FilterMedia[™].
2. Contractor is required to be a Filtrex[®] Certified[™] Installer as determined by Filtrex[®] International, LLC (440-926-2607 or visit web site at Filtrex.com). Certification shall be considered current if appropriate identification is shown during time of bid or at time of application (current list of installers can be found at www.filtrex.com). Look for the Filtrex[®] Certified[™] Installer Seal.



3. Filtrexx® Inlet protection shall be placed at locations indicated on plans as directed by the Engineer. Inlet protection should be installed in a pattern that allows complete protection of the inlet area.
4. Installation of curb Inlet protection will ensure a minimal overlap of at least 1 ft (300mm) on either side of the opening being protected. The Inlet protection will be anchored to the soil behind the curb using staples, stakes or other devices capable of holding the Inlet protection in place.
5. Standard Inlet protection for curb inlet protection and curb sediment containment will use 8 in (200mm) diameter Inlet protection, and drain inlets on soil will use 12 in (300mm) or 18 in (450mm) diameter Inlet protection. In severe flow situations, larger Inlet protection may be specified by the Engineer. During curb installation, Inlet protection shall be compacted to be slightly shorter than curb height.
6. If Inlet protection becomes clogged with debris and sediment, they shall be maintained so as to assure proper drainage and water flow into the storm drain. In severe storm events, overflow of the Inlet protection may be acceptable in order to keep the area from flooding.
7. Curb and drain Inlet protection shall be positioned so as to provide a permeable physical barrier to the drain itself, allowing sediment to collect on the outside of the Inlet protection.
8. For drains and inlets that have only curb cuts, without street grates, a spacer is required in order to keep the Inlet protection away from the drain opening. This spacer should be a hog wire screen bent to overlap the grate opening and keep the sock from falling into the opening. Use at least one spacer for every 4 ft (1.2m) of curb drain opening. The wire grid also prevents other floatable waste from passing over the Inlet protection.
9. Stakes shall be installed through the middle of the drain Inlet protection on 5 ft (1.5m) centers, using 2 in (50mm) x 2 in (50mm) x 3 ft (1m) wood stakes.
10. Staking depth for sand and silt loam soils shall be 12 in (300mm), and 8 in (200mm) for clay soils.

INSPECTION AND MAINTENANCE

Routine inspection should be conducted within 24 hrs of a runoff event or as designated by the regulating authority. Inlet protection should be regularly inspected to make sure they maintain their

shape and are producing adequate hydraulic flow-through. If ponding becomes excessive, additional Inlet protection may be required or sediment removal may be necessary. Inlet protection shall be inspected until contributing drainage area has been permanently stabilized and construction activity has ceased

1. The Contractor shall maintain the Inlet protection in a functional condition at all times and it shall be routinely inspected.
2. If the Inlet protection has been damaged, it shall be repaired, or replaced if beyond repair.
3. The Contractor shall remove sediment at the base of the upslope side of the Inlet protection when accumulation has reached 1/2 of the effective height of the Inlet protection, or as directed by the Engineer. Alternatively, for drain Inlet protection a new Soxx™ may be placed on top of the original increasing the sediment storage capacity without soil disturbance.
4. Inlet protection shall be maintained until disturbed area above or around the device has been permanently stabilized and construction activity has ceased.
5. Regular maintenance includes lifting the Inlet protection and cleaning around and under them as sediment collects.
6. The FilterMedia™ will be removed from paved areas or dispersed on site soil or behind curb once disturbed area has been permanently stabilized, construction activity has ceased, or as determined by the Engineer.

Table 2.4 Spacing for Curb Sediment Containment Systems.

Grade (%)	Spacing (ft)	Spacing (mm)
0.5	100	30
1.0	50	15
2.0	25	8
3.0	16	5
4.0	13	4
5.0	10	3

Source: Fifield, 2001.



Figure 2.1. Engineering Design Drawing for Curb and Drain Inlet Protection

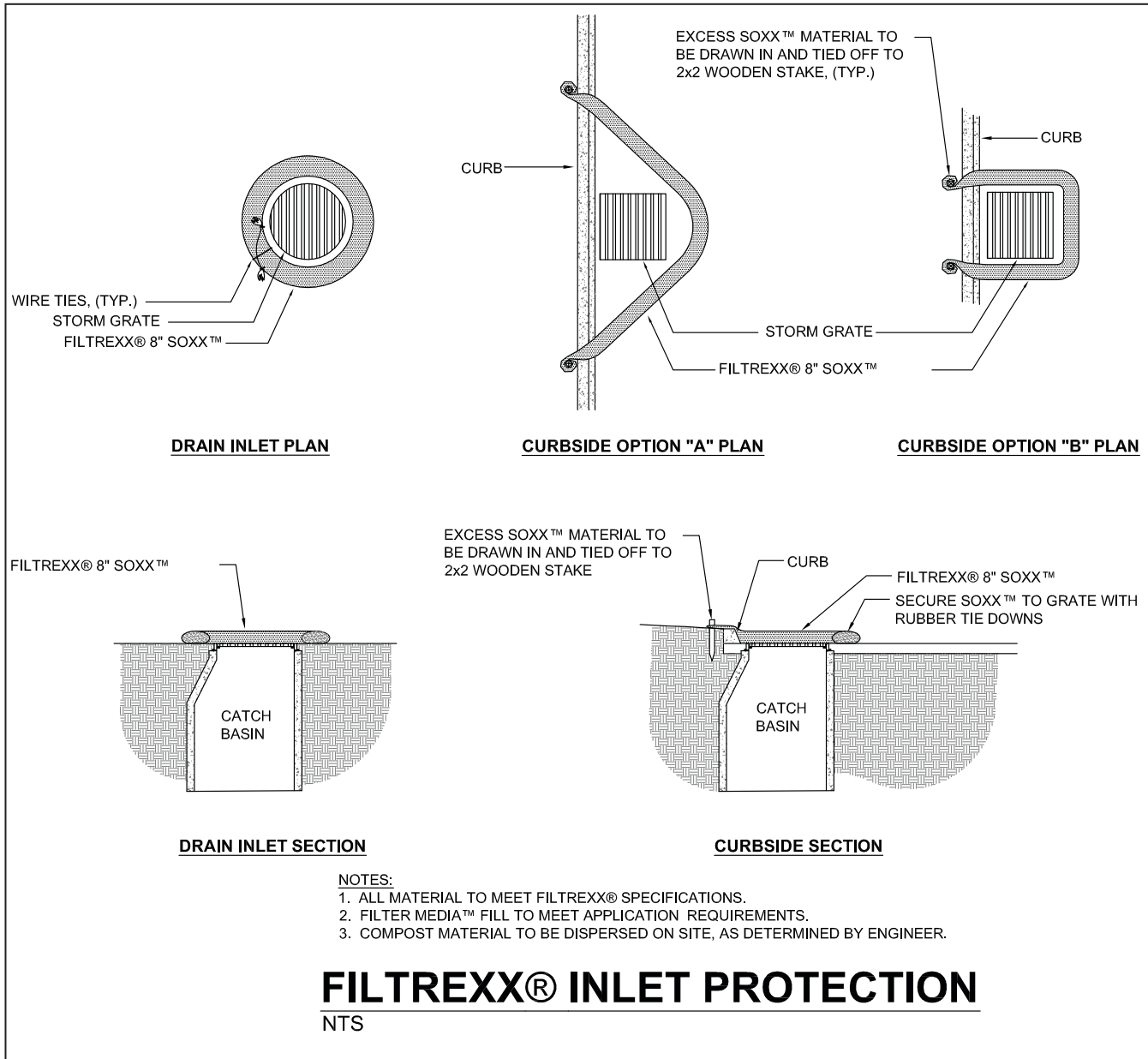


Figure 2.2. Engineering Design Drawing for Curb Sediment Containment Inlet Protection

