

*Town of Barrington  
Site Plan Application*

**STORMWATER MANAGEMENT SUBMISSION**

**BARRINGTON TOWN OFFICE BUILDING**  
Calef Highway (Route 125)  
Barrington, New Hampshire

Prepared for

**Town of Barrington  
335 Calef Highway  
Barrington, NH 03825  
March 2020**

**RECEIVED**

**MAR 17 2020**

**LAND USE OFFICE**



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**CIVIL  
CONSULTANTS**

*Engineers*

*Planners*

*Surveyors*

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***Stormwater Management Narrative***

**RECEIVED**

MAR 17 2020

**LAND USE OFFICE**

**TOWN OF BARRINGTON  
SITE PLAN APPLICATION  
STORMWATER MANAGEMENT PLAN**

Site Development  
Barrington Town Office Building

Calef Highway, NH Route 125  
Barrington, New Hampshire

Prepared for:

Town of Barrington  
335 Calef Highway  
Barrington, NH 03825

March, 2020

**INTRODUCTION:**

Stormwater runoff conditions have been evaluated for the proposed site development to construct new Town Offices with associated parking and stormwater management facilities. This report includes a review of the 1-, 2-, 10-, 25- and 50-yr storm events, as well as a description of treatment and groundwater recharge methods proposed.

The development proposed creates approximately 84,000 sf of disturbance, with 36,700 sf of impervious area. The entire area included in this application is currently woodland or existing pavement/road swale area. The remaining 47,300 sf consists of new disturbance for grading, stormwater management facilities, and the subsurface effluent disposal system.

While the proposed work does not trigger the requirement to obtain an Alteration of Terrain permit from the NH DES, the lot to be developed is part of a subdivision that will need to submit for an AoT permit. It is the intention of the proposed design to meet all of the requirements of an AoT project to allow the associated subdivision to utilize this design and submission when applying for that permit.

The analysis was performed to assess the influence of the proposed project area on future runoff and to recommend measures to control or mitigate runoff increases due to development, and to address ground water recharge as required by the current standards presented in Env-Wq 1500 and the Town of Barrington requirements of §4.7 of the Site Plan Review Regulations.

**METHODOLOGY:**

All runoff calculations were performed using the methods based on USDA-SCS Technical Release No. 20 (also known as TR-20). The one-, two-, ten-, twenty five-, and fifty-year, twenty-four hour storm event (Type III rainfall distribution) were used for the site specific analysis to determine pre- and post-development peak discharge rates. Runoff curve numbers (CN) and times of concentration (Tc) were determined by the methods outlined in USDA-SCS Technical Release No. 55 (better known as TR-55). Watershed areas were determined from the topographic map prepared for the site by on the ground survey.

**SITE & SOIL INFORMATION:**

The area to be developed is primarily Woodbridge soils as determined by a Site-Specific Soil Survey, with a small amount of Ridgebury soil adjacent to the nearby wetland.

Per the SSSNNE Special Publication No. 5 (2009), the Ksat range in the B horizon where the proposed infiltration will be located is listed as 0.6-2.0 in/hour.

Flow from the site currently flow to Rt 125, either through a wetland to the south or roadside swale to the north. All flows eventually reach the Cocheco River via Green Hill Brook.

There are no wetlands and/or streams that will be directly impacted by the proposed work.



Soil information was obtained from a Site Specific Soil Survey prepared by Luke Hurley of Gove Environmental based upon field investigations conducted in March 2019. Conditions at specific stormwater pond locations and septic sites were investigated by Michael Mariano in March 2020. The soils information has been provided in the attached supporting materials.

#### **ANALYSIS:**

As noted above, all surface waters within the site flow north to the Isinglass River. Flows exit the site at two separate locations. The watershed that will be altered by the proposed development has been evaluated in the following analysis. Property areas not influenced by the project have been ignored for the remainder of this report.

#### **Pre-Development Areas**

Two subcatchments were used to model the existing drainage conditions.

Subcatchment 1 includes the area at Route 125 and the majority of the project area. Flow from this subcatchment drains north along the roadway. The land outside of the road ROW is densely wooded, with an existing gravel entrance to the road.

Subcatchment 2 is the area further into the lot that drains to the on-site wetland. This area is densely wooded throughout.

The subcatchments were modeled to collect at two outlet locations. The first is the runoff that flows directly to the abutter to the south prior to reaching Route 125 (OUT 1) and the second is outletting to the drainage swale to the north along Route 125 (OUT 2).

#### **Post-Development Areas**

Six sub-areas were identified for the post development analysis. These reflect the intended separation of flows due to new building area and modified land cover.

There are two infiltration basins proposed that will treat the new impervious area. The

basins will also control flows from proposed entrance area.

The north basin (11P) will be located directly south of the proposed entrance, and will handle those flows generated by the new impervious area as well as a small area of woodland to remain along Route 125. This basin will outlet to a swale along Route 125.

The south basin (21P) will treat the proposed parking lot and area east of the new building. This basin will outlet to the southern wetland.

Test pits and observation holes were evaluated to determine the soil types for a site specific soil survey, as well as to provide information on expected infiltration rates of the existing soils. It is the opinion of the soil scientist that the Ksat of the soils in the area will be ranges given in SSSNNE Pub #5 for Woodbridge soils. This publication gives an infiltration rate of 0.6-2.0 in/hour. The design infiltration rate utilized for design was  $0.6/2 = 0.3$  in/hour.

Refer to the attached soil report prepared by Michael Mariano, NH CSS #76 for further information.

The BMPs have been designed per the 2008 NH DES BMP Manual Vol. II. The design also meets the intent of the Stormwater Management and Erosion and Sediment Control Handbook for Urban and Developing Areas in New Hampshire, August 1992, as required in the Town of Northwood Zoning Ordinance and Site Review Regulations.

#### **RESULTS:**

Pre- and post- development runoff rates were computed for the project as outlined above.

The detailed analysis for this project was performed by computer utilizing "HYDROCAD". The computer print-outs are attached. The following table summarizes the results of the analysis:



**SITE RUNOFF RATES - 2 Year Storm**

Outlet	Runoff Rate (CFS)		
	Pre	Post	Change
OUT 1	2.58	2.28	-0.30
Volume (ac-ft)	0.31	0.20	-0.11
OUT 2	4.42	4.36	-0.06
Volume (ac-ft)	0.50	0.52	+0.02

**SITE RUNOFF RATES - 10 Year Storm**

Outlet	Site Runoff Rates (CFS)		
	Pre	Post	Change
OUT 1	5.62	4.49	-1.13
Volume (ac-ft)	0.65	0.45	-0.20
OUT 2	10.46	10.46	+/-0.0
Volume (ac-ft)	1.09	1.16	+0.07

**SITE RUNOFF RATES - 25 Year Storm**

Outlet	Site Runoff Rates (CFS)		
	Pre	Post	Change
OUT 1	8.22	7.48	-0.74
Volume (ac-ft)	0.95	0.68	-0.27
OUT 2	15.74	15.72	-0.02
Volume (ac-ft)	1.62	1.73	+0.11

**SITE RUNOFF RATES - 50 Year Storm**

Outlet	Site Runoff Rates (CFS)		
	Pre	Post	Change
OUT 1	10.73	10.61	-0.12
Volume (ac-ft)	1.23	0.91	-0.32
OUT 2	20.89	20.82	-0.07
Volume (ac-ft)	2.15	2.29	+0.14

See the attached plans and HydroCAD reports for details and calculations.

**STORMWATER TREATMENT:**

The development will be treated using two infiltration basins (Pond 11P and 21P).

The basis will provide the required groundwater recharge for the proposed development. The total groundwater recharge capacity of the system has been tabulated and is included on the BMP worksheet for GRV.

**CONCLUSIONS:**

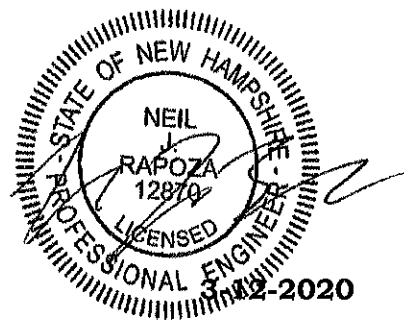
The project is designed to capture and infiltrate storm water from the new paved parking areas and roofs to eliminate adverse impacts to abutting lots and wetlands.

The results of the analysis predict post-development flows will remain at or below existing rates to the project outlet point for the 2-, 10-, 25- and 50-year events.

The overall flow volume off of the site to the receiving Green Hill Brook watershed has been reduced in all storms, and therefore meets the intent of Env-Wq 1500-1507.5 (b)(1)(a) and 1507.6. The stormwater management plan as presented also meets the requirements of the Town of Barrington Site Plan Review Regulation §4.7.

In our opinion, implementation of the facilities described on the plan will not adversely affect downstream property owners or the receiving swale and associated waterways.

A stormwater maintenance plan has also been attached to indicate the procedures and requirements to maintain the stormwater management system.



The seal affixed above applies to this report which consists of 3 pages of text and attached calculations.

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**CIVIL CONSULTANTS**

P.O. Box 100 South Berwick, Maine 03908 207-384-2550



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**CIVIL  
CONSULTANTS**

*Engineers*

*Planners*

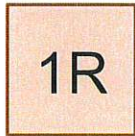
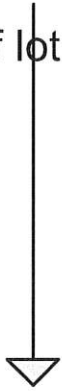
*Surveyors*

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***Pre-Development Calculations***



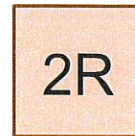
Portion of lot at Rt 125



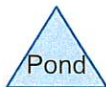
OUT 1



Area adjacent to wetland



OUT 2



**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
0.528	92	Paved roads w/open ditches, 50% imp, HSG C (1S)
9.499	73	Woods, Fair, HSG C (1S, 2S)
<b>10.027</b>	<b>74</b>	<b>TOTAL AREA</b>



**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
10.027	HSG C	1S, 2S
0.000	HSG D	
0.000	Other	
<b>10.027</b>		<b>TOTAL AREA</b>

**20200310-1933600-PRE**

Type III 24-hr 2-YR Rainfall=3.08"

Prepared by Civil Consultants

Printed 3/12/2020

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Portion of lot at Rt 125** Runoff Area=3.478 ac 7.59% Impervious Runoff Depth=1.07"  
Flow Length=595' Tc=24.4 min CN=76 Runoff=2.58 cfs 0.310 af

**Subcatchment 2S: Area adjacent to wetland** Runoff Area=6.549 ac 0.00% Impervious Runoff Depth=0.91"  
Flow Length=634' Slope=0.0190 '/' Tc=18.7 min CN=73 Runoff=4.42 cfs 0.495 af

**Reach 1R: OUT 1** Inflow=2.58 cfs 0.310 af  
Outflow=2.58 cfs 0.310 af

**Reach 2R: OUT 2** Inflow=4.42 cfs 0.495 af  
Outflow=4.42 cfs 0.495 af

**Total Runoff Area = 10.027 ac Runoff Volume = 0.805 af Average Runoff Depth = 0.96"**  
**97.37% Pervious = 9.763 ac 2.63% Impervious = 0.264 ac**

**20200310-1933600-PRE**

*Type III 24-hr 10-YR Rainfall=4.64"*

Prepared by Civil Consultants

Printed 3/12/2020

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Portion of lot at Rt 125** Runoff Area=3.478 ac 7.59% Impervious Runoff Depth=2.24"  
Flow Length=595' Tc=24.4 min CN=76 Runoff=5.62 cfs 0.650 af

**Subcatchment 2S: Area adjacent to wetland** Runoff Area=6.549 ac 0.00% Impervious Runoff Depth=2.00"  
Flow Length=634' Slope=0.0190 '/' Tc=18.7 min CN=73 Runoff=10.46 cfs 1.093 af

**Reach 1R: OUT 1**

Inflow=5.62 cfs 0.650 af  
Outflow=5.62 cfs 0.650 af

**Reach 2R: OUT 2**

Inflow=10.46 cfs 1.093 af  
Outflow=10.46 cfs 1.093 af

**Total Runoff Area = 10.027 ac Runoff Volume = 1.742 af Average Runoff Depth = 2.09"**  
**97.37% Pervious = 9.763 ac 2.63% Impervious = 0.264 ac**

**20200310-1933600-PRE**

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Type III 24-hr 25-YR Rainfall=5.86"

Printed 3/12/2020

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Portion of lot at Rt 125** Runoff Area=3.478 ac 7.59% Impervious Runoff Depth=3.26"  
Flow Length=595' Tc=24.4 min CN=76 Runoff=8.22 cfs 0.945 af

**Subcatchment 2S: Area adjacent to wetland** Runoff Area=6.549 ac 0.00% Impervious Runoff Depth=2.97"  
Flow Length=634' Slope=0.0190 '/' Tc=18.7 min CN=73 Runoff=15.74 cfs 1.622 af

**Reach 1R: OUT 1**

Inflow=8.22 cfs 0.945 af  
Outflow=8.22 cfs 0.945 af

**Reach 2R: OUT 2**

Inflow=15.74 cfs 1.622 af  
Outflow=15.74 cfs 1.622 af

**Total Runoff Area = 10.027 ac Runoff Volume = 2.567 af Average Runoff Depth = 3.07"**  
**97.37% Pervious = 9.763 ac 2.63% Impervious = 0.264 ac**

**Summary for Subcatchment 1S: Portion of lot at Rt 125**

Runoff = 8.22 cfs @ 12.34 hrs, Volume= 0.945 af, Depth= 3.26"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs  
Type III 24-hr 25-YR Rainfall=5.86"

Area (ac)	CN	Description
2.950	73	Woods, Fair, HSG C
0.528	92	Paved roads w/open ditches, 50% imp, HSG C
3.478	76	Weighted Average
3.214		92.41% Pervious Area
0.264		7.59% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.1	50	0.0180	0.06		<b>Sheet Flow, 1.1</b> Woods: Light underbrush n= 0.400 P2= 3.08"
5.1	205	0.0180	0.67		<b>Shallow Concentrated Flow, 1.2</b> Woodland Kv= 5.0 fps
6.2	340	0.0330	0.91		<b>Shallow Concentrated Flow, 1.3</b> Woodland Kv= 5.0 fps
24.4	595	Total			

**Summary for Subcatchment 2S: Area adjacent to wetland**

Runoff = 15.74 cfs @ 12.26 hrs, Volume= 1.622 af, Depth= 2.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs  
Type III 24-hr 25-YR Rainfall=5.86"

Area (ac)	CN	Description
6.549	73	Woods, Fair, HSG C
6.549		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.8	50	0.0190	0.06		<b>Sheet Flow, 2.1</b> Woods: Light underbrush n= 0.400 P2= 3.08"
3.5	143	0.0190	0.69		<b>Shallow Concentrated Flow, 2.2</b> Woodland Kv= 5.0 fps
2.4	441	0.0190	3.06	18.34	<b>Trap/Vee/Rect Channel Flow, 2.3</b> Bot.W=4.00' D=0.50' Z= 12.0 & 20.0 ' Top.W=20.00' n= 0.030 Stream, clean & straight
18.7	634	Total			

### Summary for Reach 1R: OUT 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.478 ac, 7.59% Impervious, Inflow Depth = 3.26" for 25-YR event  
Inflow = 8.22 cfs @ 12.34 hrs, Volume= 0.945 af  
Outflow = 8.22 cfs @ 12.34 hrs, Volume= 0.945 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

### Summary for Reach 2R: OUT 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 6.549 ac, 0.00% Impervious, Inflow Depth = 2.97" for 25-YR event  
Inflow = 15.74 cfs @ 12.26 hrs, Volume= 1.622 af  
Outflow = 15.74 cfs @ 12.26 hrs, Volume= 1.622 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

20200310-1933600-PRE

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Type III 24-hr 50-YR Rainfall=7.00"

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 1S: Portion of lot at Rt 125** Runoff Area=3.478 ac 7.59% Impervious Runoff Depth=4.26"  
Flow Length=595' Tc=24.4 min CN=76 Runoff=10.73 cfs 1.234 af

**Subcatchment 2S: Area adjacent to wetland** Runoff Area=6.549 ac 0.00% Impervious Runoff Depth=3.94"  
Flow Length=634' Slope=0.0190 ' / ' Tc=18.7 min CN=73 Runoff=20.89 cfs 2.148 af

Reach 1R: OUT 1

Inflow=10.73 cfs 1.234 af  
Outflow=10.73 cfs 1.234 af

Reach 2R: OUT 2

Inflow=20.89 cfs 2.148 af  
Outflow=20.89 cfs 2.148 af

**Total Runoff Area = 10.027 ac Runoff Volume = 3.382 af Average Runoff Depth = 4.05"**  
**97.37% Pervious = 9.763 ac 2.63% Impervious = 0.264 ac**



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*Engineers*

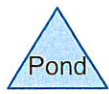
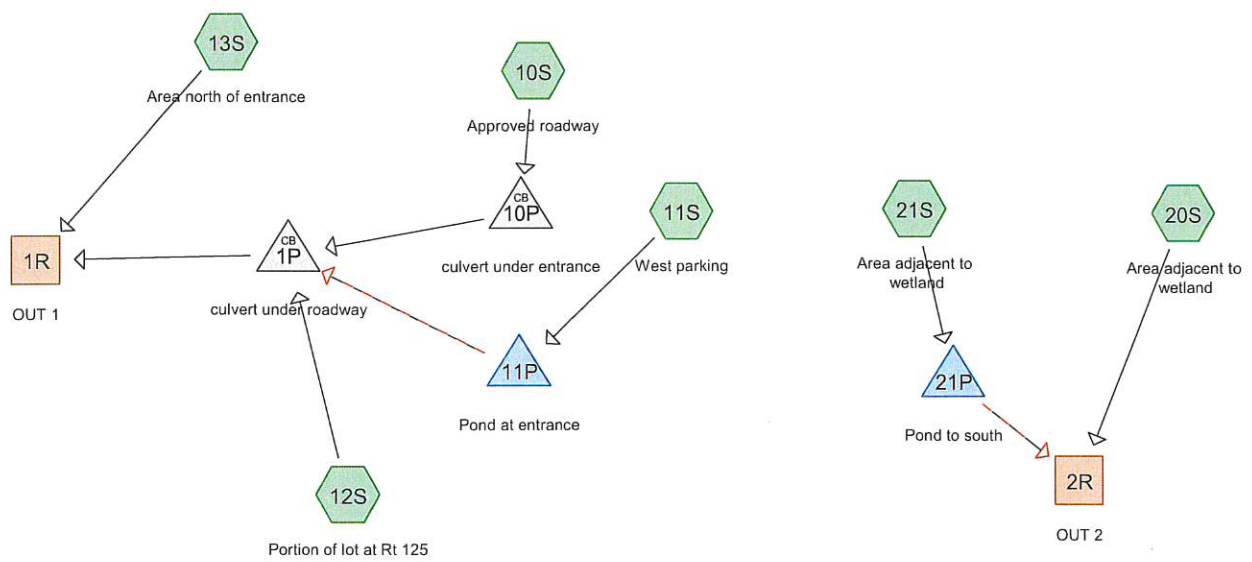
*Planners*

*Surveyors*

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***Post-Development Calculations***





**Routing Diagram for 20200317-1933600-POST**  
 Prepared by Civil Consultants, Printed 3/17/2020  
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**20200317-1933600-POST**

Prepared by Civil Consultants

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Printed 3/17/2020

**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
1.100	74	>75% Grass cover, Good, HSG C (10S, 11S, 13S, 20S, 21S)
0.286	98	Paved parking, HSG C (10S, 20S, 21S)
0.379	92	Paved roads w/open ditches, 50% imp, HSG C (13S)
0.594	98	Unconnected pavement, HSG C (11S, 12S)
7.668	73	Woods, Fair, HSG C (10S, 11S, 12S, 13S, 20S, 21S)
<b>10.027</b>	<b>76</b>	<b>TOTAL AREA</b>

**20200317-1933600-POST**

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**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
10.027	HSG C	10S, 11S, 12S, 13S, 20S, 21S
0.000	HSG D	
0.000	Other	
<b>10.027</b>		<b>TOTAL AREA</b>

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points x 5  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 10S: Approved roadway** Runoff Area=0.128 ac 12.50% Impervious Runoff Depth=1.13"  
 Flow Length=125' Tc=6.8 min CN=77 Runoff=0.16 cfs 0.012 af

**Subcatchment 11S: West parking** Runoff Area=1.325 ac 29.81% Impervious Runoff Depth=1.13"  
 Flow Length=155' Tc=12.8 min UI Adjusted CN=77 Runoff=1.34 cfs 0.124 af

**Subcatchment 12S: Portion of lot at Rt 125** Runoff Area=0.224 ac 88.84% Impervious Runoff Depth=2.53"  
 Flow Length=110' Tc=8.1 min CN=95 Runoff=0.58 cfs 0.047 af

**Subcatchment 13S: Area north of entrance** Runoff Area=1.422 ac 13.33% Impervious Runoff Depth=1.19"  
 Flow Length=365' Tc=11.1 min CN=78 Runoff=1.61 cfs 0.141 af

**Subcatchment 20S: Area adjacent to wetland** Runoff Area=6.400 ac 0.08% Impervious Runoff Depth=0.91"  
 Flow Length=634' Slope=0.0190 '/' Tc=18.7 min CN=73 Runoff=4.32 cfs 0.484 af

**Subcatchment 21S: Area adjacent to** Runoff Area=0.528 ac 50.19% Impervious Runoff Depth=1.73"  
 Flow Length=50' Slope=0.0300 '/' Tc=7.1 min CN=86 Runoff=1.02 cfs 0.076 af

**Reach 1R: OUT 1** Inflow=2.28 cfs 0.200 af  
 Outflow=2.28 cfs 0.200 af

**Reach 2R: OUT 2** Inflow=4.36 cfs 0.522 af  
 Outflow=4.36 cfs 0.522 af

**Pond 1P: culvert under roadway** Peak Elev=223.86' Inflow=0.74 cfs 0.059 af  
 18.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.74 cfs 0.059 af

**Pond 10P: culvert under entrance** Peak Elev=223.96' Inflow=0.16 cfs 0.012 af  
 18.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.16 cfs 0.012 af

**Pond 11P: Pond at entrance** Peak Elev=226.38' Storage=1,470 cf Inflow=1.34 cfs 0.124 af  
 Discarded=0.30 cfs 0.124 af Primary=0.00 cfs 0.000 af Secondary=0.00 cfs 0.000 af Outflow=0.30 cfs 0.124 af

**Pond 21P: Pond to south** Peak Elev=230.70' Storage=1,703 cf Inflow=1.02 cfs 0.076 af  
 Discarded=0.02 cfs 0.038 af Primary=0.08 cfs 0.038 af Secondary=0.00 cfs 0.000 af Outflow=0.10 cfs 0.076 af

**Total Runoff Area = 10.027 ac Runoff Volume = 0.884 af Average Runoff Depth = 1.06"**  
**89.33% Pervious = 8.958 ac 10.67% Impervious = 1.070 ac**

**20200317-1933600-POST**

Type III 24-hr 10-YR Rainfall=4.64"

Prepared by Civil Consultants

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points x 5  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 10S: Approved roadway** Runoff Area=0.128 ac 12.50% Impervious Runoff Depth=2.32"  
 Flow Length=125' Tc=6.8 min CN=77 Runoff=0.33 cfs 0.025 af

**Subcatchment 11S: West parking** Runoff Area=1.325 ac 29.81% Impervious Runoff Depth=2.32"  
 Flow Length=155' Tc=12.8 min UI Adjusted CN=77 Runoff=2.86 cfs 0.257 af

**Subcatchment 12S: Portion of lot at Rt 125** Runoff Area=0.224 ac 88.84% Impervious Runoff Depth=4.06"  
 Flow Length=110' Tc=8.1 min CN=95 Runoff=0.91 cfs 0.076 af

**Subcatchment 13S: Area north of entrance** Runoff Area=1.422 ac 13.33% Impervious Runoff Depth=2.41"  
 Flow Length=365' Tc=11.1 min CN=78 Runoff=3.36 cfs 0.285 af

**Subcatchment 20S: Area adjacent to wetland** Runoff Area=6.400 ac 0.08% Impervious Runoff Depth=2.00"  
 Flow Length=634' Slope=0.0190 '/' Tc=18.7 min CN=73 Runoff=10.22 cfs 1.068 af

**Subcatchment 21S: Area adjacent to** Runoff Area=0.528 ac 50.19% Impervious Runoff Depth=3.13"  
 Flow Length=50' Slope=0.0300 '/' Tc=7.1 min CN=86 Runoff=1.82 cfs 0.138 af

**Reach 1R: OUT 1** Inflow=4.49 cfs 0.453 af  
 Outflow=4.49 cfs 0.453 af

**Reach 2R: OUT 2** Inflow=10.46 cfs 1.162 af  
 Outflow=10.46 cfs 1.162 af

**Pond 1P: culvert under roadway** Peak Elev=224.15' Inflow=1.77 cfs 0.168 af  
 18.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=1.77 cfs 0.168 af

**Pond 10P: culvert under entrance** Peak Elev=224.16' Inflow=0.33 cfs 0.025 af  
 18.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.33 cfs 0.025 af

**Pond 11P: Pond at entrance** Peak Elev=227.06' Storage=2,527 cf Inflow=2.86 cfs 0.257 af  
 Discarded=0.30 cfs 0.190 af Primary=1.30 cfs 0.067 af Secondary=0.00 cfs 0.000 af Outflow=1.60 cfs 0.257 af

**Pond 21P: Pond to south** Peak Elev=231.10' Storage=2,899 cf Inflow=1.82 cfs 0.138 af  
 Discarded=0.02 cfs 0.043 af Primary=0.28 cfs 0.095 af Secondary=0.00 cfs 0.000 af Outflow=0.30 cfs 0.138 af

**Total Runoff Area = 10.027 ac Runoff Volume = 1.848 af Average Runoff Depth = 2.21"**  
**89.33% Pervious = 8.958 ac 10.67% Impervious = 1.070 ac**

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points x 5  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 10S: Approved roadway** Runoff Area=0.128 ac 12.50% Impervious Runoff Depth=3.36"  
 Flow Length=125' Tc=6.8 min CN=77 Runoff=0.48 cfs 0.036 af

**Subcatchment 11S: West parking** Runoff Area=1.325 ac 29.81% Impervious Runoff Depth=3.36"  
 Flow Length=155' Tc=12.8 min UI Adjusted CN=77 Runoff=4.14 cfs 0.371 af

**Subcatchment 12S: Portion of lot at Rt 125** Runoff Area=0.224 ac 88.84% Impervious Runoff Depth=5.27"  
 Flow Length=110' Tc=8.1 min CN=95 Runoff=1.16 cfs 0.098 af

**Subcatchment 13S: Area north of entrance** Runoff Area=1.422 ac 13.33% Impervious Runoff Depth=3.46"  
 Flow Length=365' Tc=11.1 min CN=78 Runoff=4.83 cfs 0.409 af

**Subcatchment 20S: Area adjacent to wetland** Runoff Area=6.400 ac 0.08% Impervious Runoff Depth=2.97"  
 Flow Length=634' Slope=0.0190 '/ Tc=18.7 min CN=73 Runoff=15.38 cfs 1.586 af

**Subcatchment 21S: Area adjacent to** Runoff Area=0.528 ac 50.19% Impervious Runoff Depth=4.28"  
 Flow Length=50' Slope=0.0300 '/ Tc=7.1 min CN=86 Runoff=2.46 cfs 0.188 af

**Reach 1R: OUT 1** Inflow=7.48 cfs 0.682 af  
 Outflow=7.48 cfs 0.682 af

**Reach 2R: OUT 2** Inflow=15.72 cfs 1.727 af  
 Outflow=15.72 cfs 1.727 af

**Pond 1P: culvert under roadway** Peak Elev=224.44' Inflow=3.13 cfs 0.272 af  
 18.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/ Outflow=3.13 cfs 0.272 af

**Pond 10P: culvert under entrance** Peak Elev=224.45' Inflow=0.48 cfs 0.036 af  
 18.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/ Outflow=0.48 cfs 0.036 af

**Pond 11P: Pond at entrance** Peak Elev=227.54' Storage=3,389 cf Inflow=4.14 cfs 0.371 af  
 Discarded=0.30 cfs 0.233 af Primary=2.46 cfs 0.138 af Secondary=0.00 cfs 0.000 af Outflow=2.76 cfs 0.371 af

**Pond 21P: Pond to south** Peak Elev=231.44' Storage=3,993 cf Inflow=2.46 cfs 0.188 af  
 Discarded=0.02 cfs 0.046 af Primary=0.38 cfs 0.142 af Secondary=0.00 cfs 0.000 af Outflow=0.40 cfs 0.188 af

**Total Runoff Area = 10.027 ac Runoff Volume = 2.688 af Average Runoff Depth = 3.22"**  
**89.33% Pervious = 8.958 ac 10.67% Impervious = 1.070 ac**

**Summary for Subcatchment 10S: Approved roadway**

Runoff = 0.48 cfs @ 12.10 hrs, Volume= 0.036 af, Depth= 3.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 25-YR Rainfall=5.86"

Area (ac)	CN	Description
0.016	98	Paved parking, HSG C
0.032	73	Woods, Fair, HSG C
0.080	74	>75% Grass cover, Good, HSG C
0.128	77	Weighted Average
0.112		87.50% Pervious Area
0.016		12.50% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.6	30	0.0360	0.08		<b>Sheet Flow, 10.1</b> Woods: Light underbrush n= 0.400 P2= 3.08"
0.1	30	0.2600	3.57		<b>Shallow Concentrated Flow, 10.2</b> Short Grass Pasture Kv= 7.0 fps
0.1	65	0.0880	14.26	71.32	<b>Trap/Vee/Rect Channel Flow, 10.3</b> Bot.W=2.00' D=1.00' Z= 3.0 ' Top.W=8.00' n= 0.022 Earth, clean & straight
6.8	125	Total			

**Summary for Subcatchment 11S: West parking**

Runoff = 4.14 cfs @ 12.18 hrs, Volume= 0.371 af, Depth= 3.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 25-YR Rainfall=5.86"

Area (ac)	CN	Adj	Description
0.401	73		Woods, Fair, HSG C
0.529	74		>75% Grass cover, Good, HSG C
0.395	98		Unconnected pavement, HSG C
1.325	81	77	Weighted Average, UI Adjusted
0.930			70.19% Pervious Area
0.395			29.81% Impervious Area
0.395			100.00% Unconnected

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Type III 24-hr 25-YR Rainfall=5.86"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.7	50	0.0300	0.08		<b>Sheet Flow, 11.1</b> Woods: Light underbrush n= 0.400 P2= 3.08"
1.3	65	0.0300	0.87		<b>Shallow Concentrated Flow, 11.2</b> Woodland Kv= 5.0 fps
0.8	40	0.0280	0.84		<b>Shallow Concentrated Flow, 11.3</b> Woodland Kv= 5.0 fps
12.8	155	Total			

**Summary for Subcatchment 12S: Portion of lot at Rt 125**

Runoff = 1.16 cfs @ 12.11 hrs, Volume= 0.098 af, Depth= 5.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs  
Type III 24-hr 25-YR Rainfall=5.86"

Area (ac)	CN	Description
0.025	73	Woods, Fair, HSG C
0.091	98	Unconnected pavement, HSG C
0.108	98	Unconnected pavement, HSG C
0.224	95	Weighted Average
0.025		11.16% Pervious Area
0.199		88.84% Impervious Area
0.199		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.0	45	0.0500	0.09		<b>Sheet Flow, 12.1</b> Woods: Light underbrush n= 0.400 P2= 3.08"
0.1	65	0.0400	8.20	26.13	<b>Trap/Vee/Rect Channel Flow, 12.2</b> Bot.W=2.00' D=0.75' Z= 3.0 ' Top.W=6.50' n= 0.022 Earth, clean & straight
8.1	110	Total			

**Summary for Subcatchment 13S: Area north of entrance**

Runoff = 4.83 cfs @ 12.16 hrs, Volume= 0.409 af, Depth= 3.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs  
Type III 24-hr 25-YR Rainfall=5.86"

Area (ac)	CN	Description
0.379	92	Paved roads w/open ditches, 50% imp, HSG C
0.155	74	>75% Grass cover, Good, HSG C
0.888	73	Woods, Fair, HSG C
1.422	78	Weighted Average
1.232		86.67% Pervious Area
0.190		13.33% Impervious Area



Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.1	50	0.0600	0.10		<b>Sheet Flow, 13.1</b> Woods: Light underbrush n= 0.400 P2= 3.08"
1.3	110	0.0850	1.46		<b>Shallow Concentrated Flow, 13.2</b> Woodland Kv= 5.0 fps
0.8	50	0.0400	1.00		<b>Shallow Concentrated Flow, 13.2</b> Woodland Kv= 5.0 fps
0.4	125	0.0100	5.66	62.31	<b>Trap/Vee/Rect Channel Flow, 13.4</b> Bot.W=8.00' D=1.00' Z= 3.0 ' ' Top.W=14.00' n= 0.022 Earth, clean & straight
0.5	30	0.0400	1.00	3.45	<b>Trap/Vee/Rect Channel Flow, 13.5</b> Bot.W=10.00' D=0.25' Z= 15.0 ' ' Top.W=17.50' n= 0.100 Heavy timber, flow below branches
11.1	365	Total			

**Summary for Subcatchment 20S: Area adjacent to wetland**

Runoff = 15.38 cfs @ 12.26 hrs, Volume= 1.586 af, Depth= 2.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs  
Type III 24-hr 25-YR Rainfall=5.86"

Area (ac)	CN	Description
0.094	74	>75% Grass cover, Good, HSG C
6.301	73	Woods, Fair, HSG C
0.005	98	Paved parking, HSG C
6.400	73	Weighted Average
6.395		99.92% Pervious Area
0.005		0.08% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.8	50	0.0190	0.06		<b>Sheet Flow, 20.1</b> Woods: Light underbrush n= 0.400 P2= 3.08"
3.5	143	0.0190	0.69		<b>Shallow Concentrated Flow, 20.2</b> Woodland Kv= 5.0 fps
2.4	441	0.0190	3.06	18.34	<b>Trap/Vee/Rect Channel Flow, 20.3</b> Bot.W=4.00' D=0.50' Z= 12.0 & 20.0 ' ' Top.W=20.00' n= 0.030 Stream, clean & straight
18.7	634	Total			

**Summary for Subcatchment 21S: Area adjacent to wetland**

Runoff = 2.46 cfs @ 12.10 hrs, Volume= 0.188 af, Depth= 4.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs  
Type III 24-hr 25-YR Rainfall=5.86"

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Type III 24-hr 25-YR Rainfall=5.86"

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Area (ac)	CN	Description
0.021	73	Woods, Fair, HSG C
0.242	74	>75% Grass cover, Good, HSG C
0.265	98	Paved parking, HSG C
0.528	86	Weighted Average
0.263		49.81% Pervious Area
0.265		50.19% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.1	50	0.0300	0.12		<b>Sheet Flow, 21.1</b> Grass: Dense n= 0.240 P2= 3.08"

**Summary for Reach 1R: OUT 1**

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.099 ac, 25.80% Impervious, Inflow Depth = 2.64" for 25-YR event  
 Inflow = 7.48 cfs @ 12.17 hrs, Volume= 0.682 af  
 Outflow = 7.48 cfs @ 12.17 hrs, Volume= 0.682 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 5

**Summary for Reach 2R: OUT 2**

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 6.928 ac, 3.90% Impervious, Inflow Depth = 2.99" for 25-YR event  
 Inflow = 15.72 cfs @ 12.26 hrs, Volume= 1.727 af  
 Outflow = 15.72 cfs @ 12.26 hrs, Volume= 1.727 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 5

**Summary for Pond 1P: culvert under roadway**

Inflow Area = 1.677 ac, 36.37% Impervious, Inflow Depth = 1.95" for 25-YR event  
 Inflow = 3.13 cfs @ 12.35 hrs, Volume= 0.272 af  
 Outflow = 3.13 cfs @ 12.35 hrs, Volume= 0.272 af, Atten= 0%, Lag= 0.0 min  
 Primary = 3.13 cfs @ 12.35 hrs, Volume= 0.272 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 5

Peak Elev= 224.44' @ 12.35 hrs  
 Flood Elev= 227.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	223.40'	<b>18.0" Round Culvert</b> L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 223.40' / 223.20' S= 0.0050 ' / Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf

**Primary OutFlow** Max=3.13 cfs @ 12.35 hrs HW=224.44' TW=0.00' (Dynamic Tailwater)

↑1=Culvert (Barrel Controls 3.13 cfs @ 3.37 fps)

**Summary for Pond 10P: culvert under entrance**

Inflow Area = 0.128 ac, 12.50% Impervious, Inflow Depth = 3.36" for 25-YR event  
 Inflow = 0.48 cfs @ 12.10 hrs, Volume= 0.036 af  
 Outflow = 0.48 cfs @ 12.10 hrs, Volume= 0.036 af, Atten= 0%, Lag= 0.0 min  
 Primary = 0.48 cfs @ 12.10 hrs, Volume= 0.036 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 5

Peak Elev= 224.45' @ 12.35 hrs

Flood Elev= 227.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	223.70'	<b>18.0" Round Culvert</b> L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 223.70' / 223.50' S= 0.0050 ' / Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf

**Primary OutFlow** Max=0.48 cfs @ 12.10 hrs HW=224.26' TW=224.19' (Dynamic Tailwater)

↑1=Culvert (Outlet Controls 0.48 cfs @ 1.19 fps)

**Summary for Pond 11P: Pond at entrance**

Inflow Area = 1.325 ac, 29.81% Impervious, Inflow Depth = 3.36" for 25-YR event  
 Inflow = 4.14 cfs @ 12.18 hrs, Volume= 0.371 af  
 Outflow = 2.76 cfs @ 12.36 hrs, Volume= 0.371 af, Atten= 33%, Lag= 10.9 min  
 Discarded = 0.30 cfs @ 11.45 hrs, Volume= 0.233 af  
 Primary = 2.46 cfs @ 12.36 hrs, Volume= 0.138 af  
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 5

Peak Elev= 227.54' @ 12.36 hrs Surf.Area= 1,941 sf Storage= 3,389 cf

Plug-Flow detention time= 34.3 min calculated for 0.370 af (100% of inflow)

Center-of-Mass det. time= 34.2 min ( 863.2 - 828.9 )

Volume	Invert	Avail.Storage	Storage Description
#1	225.00'	9,988 cf	<b>Custom Stage Data (Conic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
225.00	770	0	0	770
226.00	1,210	982	982	1,224
227.00	1,680	1,439	2,420	1,713
228.00	2,182	1,926	4,346	2,238
229.00	2,962	2,562	6,908	3,038
230.00	3,200	3,080	9,988	3,347

Device	Routing	Invert	Outlet Devices
#1	Primary	224.90'	<b>12.0" Round Culvert</b> L= 50.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 224.90' / 224.50' S= 0.0080 ' /' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	226.35'	<b>8.0" Vert. Orifice/Grate</b> C= 0.600
#3	Device 1	226.50'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600
#4	Device 1	227.45'	<b>24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#5	Discarded	225.00'	<b>0.30 cfs Exfiltration at all elevations</b> Phase-In= 0.10'
#6	Secondary	227.75'	<b>4.0' long x 7.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65 2.65 2.66 2.65 2.66 2.68 2.70 2.73 2.78

**Discarded OutFlow** Max=0.30 cfs @ 11.45 hrs HW=225.10' (Free Discharge)

↑5=Exfiltration (Exfiltration Controls 0.30 cfs)

**Primary OutFlow** Max=2.42 cfs @ 12.36 hrs HW=227.53' TW=224.43' (Dynamic Tailwater)

↑1=Culvert (Passes 2.42 cfs of 4.36 cfs potential flow)

↑2=Orifice/Grate (Orifice Controls 1.55 cfs @ 4.44 fps)

↑3=Orifice/Grate (Orifice Controls 0.39 cfs @ 4.48 fps)

↑4=Orifice/Grate (Weir Controls 0.48 cfs @ 0.94 fps)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=225.00' TW=223.40' (Dynamic Tailwater)

↑6=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

### Summary for Pond 21P: Pond to south

Inflow Area =	0.528 ac, 50.19% Impervious, Inflow Depth = 4.28" for 25-YR event
Inflow =	2.46 cfs @ 12.10 hrs, Volume= 0.188 af
Outflow =	0.40 cfs @ 12.61 hrs, Volume= 0.188 af, Atten= 84%, Lag= 30.2 min
Discarded =	0.02 cfs @ 12.61 hrs, Volume= 0.046 af
Primary =	0.38 cfs @ 12.61 hrs, Volume= 0.142 af
Secondary =	0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 5

Peak Elev= 231.44' @ 12.61 hrs Surf.Area= 3,362 sf Storage= 3,993 cf

Plug-Flow detention time= 249.1 min calculated for 0.188 af (100% of inflow)

Center-of-Mass det. time= 248.8 min ( 1,048.4 - 799.6 )

Volume	Invert	Avail.Storage	Storage Description	
#1	230.00'	5,991 cf	<b>Custom Stage Data (Conic)</b> Listed below (Recalc)	
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
230.00	2,123	0	0	2,123
231.00	3,075	2,584	2,584	3,092
232.00	3,750	3,407	5,991	3,798

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Type III 24-hr 25-YR Rainfall=5.86"

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Device	Routing	Invert	Outlet Devices
#1	Primary	230.00'	<b>12.0" Round Culvert</b> L= 115.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 230.00' / 229.00' S= 0.0087 ' / ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	230.30'	<b>2.0" Vert. Orifice/Grate</b> C= 0.600
#3	Device 1	230.60'	<b>3.5" Vert. Orifice/Grate</b> C= 0.600
#4	Discarded	230.00'	<b>0.300 in/hr Exfiltration over Surface area</b> Phase-In= 0.10'
#5	Secondary	231.85'	<b>8.0' long x 5.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65 2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88
#6	Device 1	231.60'	<b>24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Discarded OutFlow** Max=0.02 cfs @ 12.61 hrs HW=231.44' (Free Discharge)

↳4=Exfiltration (Exfiltration Controls 0.02 cfs)

**Primary OutFlow** Max=0.38 cfs @ 12.61 hrs HW=231.44' TW=0.00' (Dynamic Tailwater)

↳1=Culvert (Passes 0.38 cfs of 2.89 cfs potential flow)

↳2=Orifice/Grate (Orifice Controls 0.11 cfs @ 4.94 fps)

↳3=Orifice/Grate (Orifice Controls 0.27 cfs @ 4.00 fps)

↳6=Orifice/Grate ( Controls 0.00 cfs)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=230.00' TW=0.00' (Dynamic Tailwater)

↳5=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points x 5  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 10S: Approved roadway** Runoff Area=0.128 ac 12.50% Impervious Runoff Depth=4.37"  
 Flow Length=125' Tc=6.8 min CN=77 Runoff=0.63 cfs 0.047 af

**Subcatchment 11S: West parking** Runoff Area=1.325 ac 29.81% Impervious Runoff Depth=4.37"  
 Flow Length=155' Tc=12.8 min UI Adjusted CN=77 Runoff=5.37 cfs 0.482 af

**Subcatchment 12S: Portion of lot at Rt 125** Runoff Area=0.224 ac 88.84% Impervious Runoff Depth=6.41"  
 Flow Length=110' Tc=8.1 min CN=95 Runoff=1.39 cfs 0.120 af

**Subcatchment 13S: Area north of entrance** Runoff Area=1.422 ac 13.33% Impervious Runoff Depth=4.47"  
 Flow Length=365' Tc=11.1 min CN=78 Runoff=6.23 cfs 0.530 af

**Subcatchment 20S: Area adjacent to wetland** Runoff Area=6.400 ac 0.08% Impervious Runoff Depth=3.94"  
 Flow Length=634' Slope=0.0190 '/' Tc=18.7 min CN=73 Runoff=20.42 cfs 2.099 af

**Subcatchment 21S: Area adjacent to** Runoff Area=0.528 ac 50.19% Impervious Runoff Depth=5.37"  
 Flow Length=50' Slope=0.0300 '/' Tc=7.1 min CN=86 Runoff=3.05 cfs 0.236 af

**Reach 1R: OUT 1** Inflow=10.61 cfs 0.911 af  
 Outflow=10.61 cfs 0.911 af

**Reach 2R: OUT 2** Inflow=20.82 cfs 2.286 af  
 Outflow=20.82 cfs 2.286 af

**Pond 1P: culvert under roadway** Peak Elev=224.92' Inflow=5.58 cfs 0.380 af  
 18.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=5.58 cfs 0.380 af

**Pond 10P: culvert under entrance** Peak Elev=224.92' Inflow=0.63 cfs 0.047 af  
 18.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.63 cfs 0.047 af

**Pond 11P: Pond at entrance** Peak Elev=227.69' Storage=3,692 cf Inflow=5.37 cfs 0.482 af  
 Discarded=0.30 cfs 0.268 af Primary=4.49 cfs 0.214 af Secondary=0.00 cfs 0.000 af Outflow=4.79 cfs 0.482 af

**Pond 21P: Pond to south** Peak Elev=231.67' Storage=4,801 cf Inflow=3.05 cfs 0.236 af  
 Discarded=0.02 cfs 0.049 af Primary=0.83 cfs 0.187 af Secondary=0.00 cfs 0.000 af Outflow=0.86 cfs 0.236 af

**Total Runoff Area = 10.027 ac Runoff Volume = 3.513 af Average Runoff Depth = 4.20"**  
**89.33% Pervious = 8.958 ac 10.67% Impervious = 1.070 ac**



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**CIVIL  
CONSULTANTS**

*Engineers*

*Planners*

*Surveyors*

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***APPENDICES***

**A – Location & Topographic Plan**

**B – Soils Report**

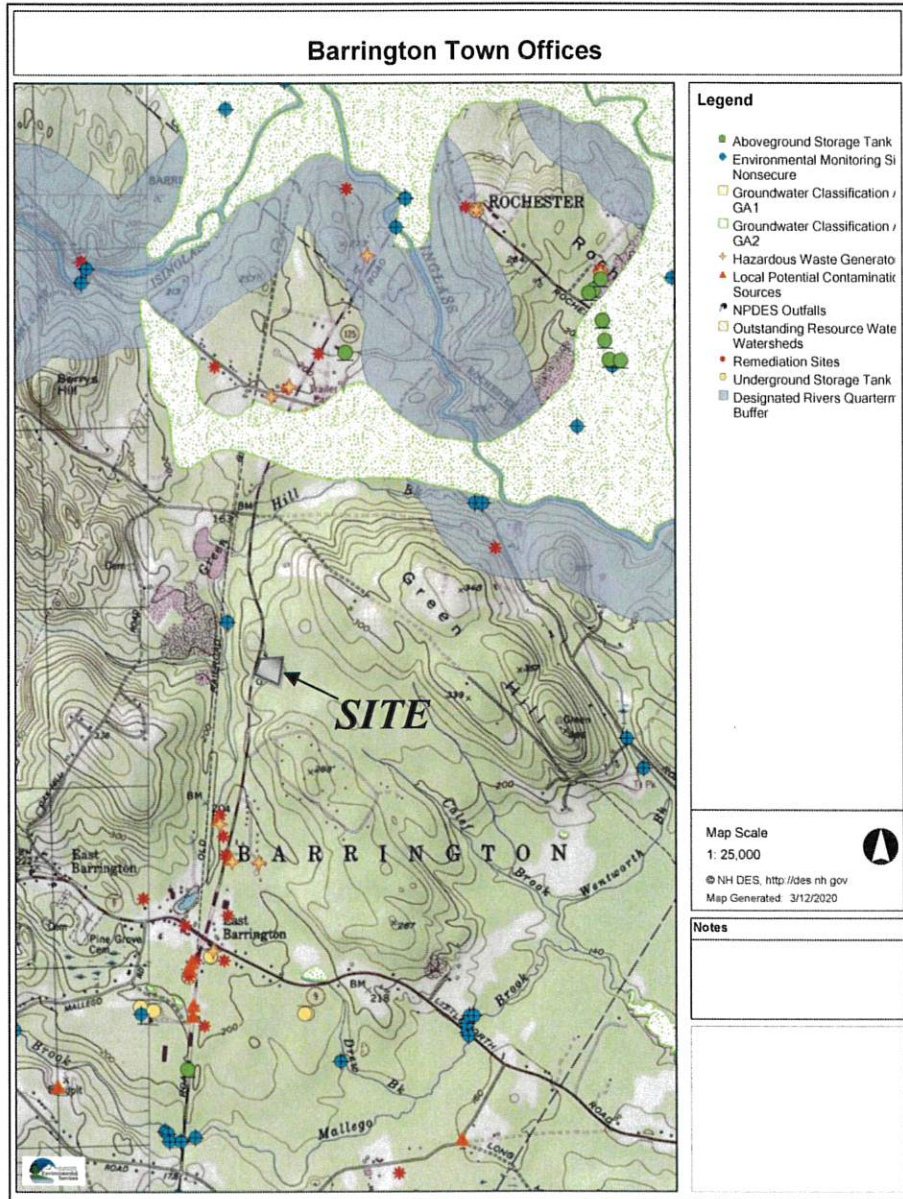
**C – Supplemental Calculations**

**D – Stormwater Maintenance Plan and Inspection Log**

**E – Drainage & Site Plans**

## APPENDIX A

# LOCATION AND TOPOGRAPHIC PLAN



<i>Portion of USGS Maps Dover West</i>		<i>PREPARED FOR:</i> <i>Town of Barrington</i>	
<i>JOB NO: 19-336.00</i>	<i>Reduced scale</i>	<i>DATE: March 2020</i>	



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## APPENDIX B

# Medium Intensity Soil Survey Plan



Obtained from NRCS Web Soil Survey		PREPARED FOR: <i>Town of Barrington</i>	
JOB NO: 19-336.00	Reduced scale	DATE: March 2020	



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## APPENDIX C

# Supplemental Stormwater Calculations

**Conveyance Systems.** Calculations for sizing on-site conveyance structures, including culverts are included in the HydroCad print outs included in this report. Stabilization calculations are included here. Ditch stabilization is per NHDOT Highway design manual. Riprap sizing and erosion control measures are shown and noted on the Site Plans. These plans also show scaled drawings and cross sections of these conveyance systems and associated practices.

**Stormwater BMP Designs.** See attached stormwater facility design spreadsheets developed by NH DES for sizing of proposed BMPs, as well as evaluation of existing BMP's that are proposed to remain.



# Extreme Precipitation Tables

## Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing	Yes
State	New Hampshire
Location	
Longitude	70.991 degrees West
Latitude	43.227 degrees North
Elevation	0 feet
Date/Time	Thu, 09 Jan 2020 08:15:13 -0500

### Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.49	0.65	0.81	1.02	1yr	0.70	0.98	1.19	1.53	1.97	2.56	3.82	1yr	2.26	2.71	3.12	3.85	4.41	1yr
2yr	0.32	0.49	0.61	0.80	1.01	1.28	2yr	0.87	1.16	1.49	1.89	2.41	3.08	4.44	2yr	2.73	3.30	3.80	4.53	5.16	2yr
5yr	0.37	0.57	0.72	0.96	1.23	1.57	5yr	1.06	1.44	1.84	2.36	3.03	3.89	4.39	5yr	3.44	4.22	4.84	5.71	6.45	5yr
10yr	0.40	0.63	0.80	1.09	1.42	1.84	10yr	1.22	1.69	2.17	2.80	3.60	4.64	5.29	10yr	4.11	5.09	5.82	6.80	7.65	10yr
25yr	0.46	0.74	0.94	1.30	1.73	2.27	25yr	1.49	2.08	2.69	3.50	4.53	5.86	6.77	25yr	5.19	6.51	7.43	8.57	9.57	25yr
50yr	0.52	0.83	1.07	1.49	2.01	2.67	50yr	1.73	2.45	3.17	4.15	5.40	7.00	8.17	50yr	6.19	7.85	8.94	10.22	11.35	50yr
100yr	0.58	0.94	1.21	1.72	2.33	3.13	100yr	2.01	2.88	3.74	4.92	6.42	8.36	9.85	100yr	7.40	9.48	10.75	12.20	13.47	100yr
200yr	0.65	1.06	1.37	1.97	2.72	3.68	200yr	2.35	3.39	4.43	5.85	7.66	9.99	11.89	200yr	8.84	11.43	12.94	14.56	15.99	200yr
500yr	0.76	1.25	1.64	2.38	3.33	4.56	500yr	2.87	4.21	5.50	7.32	9.65	12.64	15.25	500yr	11.19	14.67	16.55	18.40	20.08	500yr

### Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.24	0.36	0.44	0.60	0.73	0.90	1yr	0.63	0.88	0.91	1.25	1.51	1.95	2.48	1yr	1.73	2.39	2.93	3.28	3.97	1yr
2yr	0.31	0.48	0.59	0.81	0.99	1.18	2yr	0.86	1.15	1.35	1.81	2.34	2.99	3.34	2yr	2.65	3.21	3.69	4.41	5.03	2yr
5yr	0.35	0.54	0.67	0.91	1.16	1.40	5yr	1.00	1.37	1.61	2.14	2.77	3.61	4.06	5yr	3.20	3.90	4.52	5.34	6.04	5yr
10yr	0.38	0.59	0.73	1.02	1.32	1.60	10yr	1.14	1.56	1.81	2.43	3.12	4.14	4.70	10yr	3.66	4.52	5.25	6.17	6.92	10yr
25yr	0.44	0.67	0.83	1.19	1.56	1.91	25yr	1.35	1.87	2.12	2.83	3.62	4.95	5.70	25yr	4.38	5.48	6.41	7.44	8.22	25yr
50yr	0.49	0.74	0.92	1.33	1.78	2.19	50yr	1.54	2.14	2.37	3.20	4.05	5.66	6.58	50yr	5.01	6.33	7.46	8.58	9.47	50yr
100yr	0.54	0.82	1.03	1.49	2.04	2.52	100yr	1.76	2.46	2.67	3.59	4.51	6.45	7.59	100yr	5.71	7.30	8.69	9.89	10.81	100yr
200yr	0.61	0.91	1.16	1.68	2.34	2.89	200yr	2.02	2.82	3.00	4.04	5.03	7.36	8.77	200yr	6.51	8.43	10.13	11.40	12.36	200yr
500yr	0.71	1.06	1.36	1.98	2.82	3.49	500yr	2.43	3.42	3.51	4.72	5.82	8.71	10.60	500yr	7.71	10.20	12.41	13.77	14.70	500yr

### Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.28	0.43	0.53	0.71	0.87	1.07	1yr	0.75	1.05	1.23	1.72	2.18	2.76	3.01	1yr	2.44	2.90	3.34	4.14	4.73	1yr
2yr	0.33	0.50	0.62	0.84	1.03	1.24	2yr	0.89	1.21	1.46	1.94	2.50	3.19	3.55	2yr	2.82	3.41	3.92	4.67	5.32	2yr
5yr	0.39	0.60	0.75	1.02	1.30	1.57	5yr	1.12	1.53	1.83	2.47	3.16	4.17	4.71	5yr	3.69	4.53	5.18	6.07	6.83	5yr
10yr	0.45	0.70	0.87	1.21	1.56	1.90	10yr	1.35	1.86	2.21	3.01	3.80	5.14	5.85	10yr	4.55	5.63	6.42	7.41	8.29	10yr
25yr	0.55	0.84	1.05	1.49	1.97	2.44	25yr	1.70	2.38	2.84	3.91	4.88	6.80	7.81	25yr	6.02	7.51	8.50	9.79	10.75	25yr
50yr	0.64	0.97	1.21	1.74	2.34	2.93	50yr	2.02	2.87	3.44	4.75	5.92	8.40	9.73	50yr	7.44	9.36	10.54	12.01	13.18	50yr
100yr	0.74	1.13	1.41	2.04	2.79	3.53	100yr	2.41	3.45	4.17	5.81	7.19	10.39	12.13	100yr	9.20	11.66	13.04	14.76	16.09	100yr
200yr	0.87	1.30	1.65	2.39	3.33	4.27	200yr	2.87	4.17	5.06	7.09	8.71	12.89	15.14	200yr	11.41	14.56	16.15	18.13	19.67	200yr
500yr	1.06	1.57	2.02	2.94	4.18	5.46	500yr	3.61	5.33	6.53	9.25	11.26	17.18	20.29	500yr	15.20	19.51	21.43	23.83	25.67	500yr



Soil Series	number	NHDES Soil Group	Ksat low - B in/hr	Ksat high - B in/hr	Ksat low - C in/hr	Ksat high - C in/hr	Hyd. Grp.	Land Form	Temp.	Soil Textures	Spodosol	Other
Waubesa	402	2	0.6	6.0	0.60	6.0	D	Flood plain (bottom land)	mesic	loamy-skeletal	no	very cobbly loamy sand
Woodbridge	29	3	0.6	2.0	0.00	0.6	C	Firm, platy, loamy till	mesic	loamy	no	sandy loam in Cd
Wymoussi	9	3	0.0	6.0	0.00	6.0	D	Flood plain (bottom land)	mesic	silty over loamy	no	
Canaan	663	4	2.0	20.0	2.00	20.0	C	Weathered Bedrock Till	frigid	loamy-skeletal	yes	less than 20 in. deep
Cardigan	357	4	0.6	2.0	0.60	2.0	B	Friable till, silty, schist & phyllite	mesic	loamy	no	20 to 40 in. deep
Chaffield	89	4	0.6	6.0	0.60	6.0	B	Loose till, bedrock	mesic	loamy	no	20 to 40 in. deep
Elliottsville	128	4	0.6	2.0	2.00	2.0	B	Friable till, silty, schist & phyllite	frigid	loamy	yes	20 to 40 in. deep
Glebe	671	4	2.0	6.0	2.00	6.0	C	Loose till, bedrock	cr/cv	loamy	yes	20 to 40 in. deep
Glover	NA	4	0.6	2.0	0.60	2	D	Friable till, silty, schist & phyllite	frigid	loamy	no	less than 20 in. deep
Hogback	91	4	2.0	6.0	2.00	6.0	C	Loose till, bedrock	frigid	loamy	yes	less than 20 in. deep
Hollis	86	4	0.6	6.0	0.60	6.0	C/D	Loose till, bedrock	mesic	loamy	no	less than 20 in. deep
Kearsarge	359	4	0.6	2.0	0.60	2.0	B	Friable till, silty, schist & phyllite	mesic	loamy	no	less than 20 in. deep
Lyman	92	4	2.0	6.0	2.00	6.0	A/D	Loose till, bedrock	frigid	loamy	yes	less than 20 in. deep
Macomber	252	4	0.6	2.0	0.60	2.0	C	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	20 to 40 in. deep
Milliste	251	4	0.6	6.0	0.60	6.0	C	Loose till, bedrock	frigid	loamy	no	20 to 40 in. deep
Monson	133	4	0.6	2.0	0.60	2.0	D	Friable till, silty, schist & phyllite	frigid	loamy	yes	less than 20 in. deep
Pennichuck	460	4	0.6	2.0	0.60	2.0	B	Friable till, silty, schist & phyllite	mesic	loamy-skeletal	no	20 to 40 in. deep
Rawsonville	98	4	0.6	6.0	0.60	6.0	C	Loose till, bedrock	frigid	loamy	yes	20 to 40 in. deep
Ricker	674	4	2.0	6.0	2.00	6.0	A	gamic over bedrock (up to 4" of minerz	cr/cv	fibric to hemic	no	well drained, less than 20 in. deep
Saddleback	673	4	0.6	2.0	0.60	2.0	C/D	Loose till, bedrock	cr/cv	loamy	yes	less than 20 in. deep
Shapleigh	136	4					C/D	Sandy Till	mesic	sandy	yes	less than 20 in. deep
Thornlike	84	4	0.6	2.0	0.60	2.0	C/D	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	less than 20 in. deep
Turnbridge	99	4	0.6	6.0	0.60	6.0	C	Loose till, bedrock	frigid	loamy	yes	20 to 40 in. deep
Winnecock	88	4	0.6	2.0	0.60	2.0	C	Friable till, silty, schist & phyllite	frigid	loamy-skeletal	yes	20 to 40 in. deep
Woodstock	93	4	2.0	6.0	2.00	6.0	C/D	Loose till, bedrock	frigid	loamy	no	less than 20 in. deep
Au Gres	516	5					B	Outwash and Stream Terraces	frigid	sandy	yes	single grain, loose
Beimis	224	5	0.6	0.2	0.00	0.2	C	Firm, platy, loamy till	cr/cv	loamy	no	
Binghamville	534	5	0.2	2.0	0.06	0.2	D	Terraces and glacial lake plains	mesic	silty	no	
Brayton	240	5	0.6	2.0	0.06	0.6	C	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Cabot	589	5	0.6	2.0	0.06	0.2	D	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Charles	209	5	0.6	100.0	0.60	100.0	C	Flood Plain (Bottom Land)	frigid	silty	no	
Cohas	505	5	0.6	2.0	0.60	2.0	C	Flood Plain (Bottom Land)	frigid	co. loamy over sandy (skeletal)	no	
Grange	433	5	0.6	2.0	0.60	2.0	C	Outwash and Stream Terraces	frigid	loamy	no	
Kinsman	614	5	6.0	20.0	6.00	20.0	C	Outwash and Stream Terraces	mesic	loamy	no	
Leicester	514	5	0.6	6.0	0.60	6.0	C	Loose till, loamy textures	mesic	loamy	no	
Lim	3	5	0.6	2.0	6.00	2.0	C	Flood Plain (Bottom Land)	mesic	loamy	no	
Limerick	109	5	0.6	2.0	0.60	2.0	C	Flood Plain (Bottom Land)	mesic	silty	no	
Lyme	246	5	0.6	6.0	0.60	6.0	C	Loose till, sandy textures	frigid	loamy	no	
Mashpee	315	5	6.0	20.0	6.00	20.0	B	Outwash and Stream Terraces	mesic	sandy	yes	
Moranda	569	5	0.2	2.0	0.02	0.2	D	Firm, platy, silty till, schist & phyllite	frigid	loamy	no	
Mooslukie	414	5	6.0	20.0	6.00	20.0	C	Loose till, sandy textures	frigid	sandy	no	
Naumburg	214	5	6.0	20.0	6.00	20.0	C	Outwash and Stream Terraces	frigid	sandy	yes	
Perrin	633	5	0.6	2.0	0.06	0.6	C	Terraces and glacial lake plains	frigid	silty	no	
Pillsbury	646	5	0.6	2.0	0.06	0.2	C	Firm, platy, loamy till	frigid	silty	no	
Pipestone	314	5					B	Outwash and Stream Terraces	mesic	sandy	yes	
Raynham	533	5	0.2	2.0	0.06	0.2	C	Terraces and glacial lake plains	mesic	silty	no	
Raypol	540	5	0.6	2.0	6.00	100.0	D	Outwash and Stream Terraces	mesic	co. loamy over sandy (skeletal)	no	
Ridgetbury	656	5	0.6	6.0	0.00	0.2	C	Firm, platy, loamy till	mesic	loamy	no	
Rippowam	5	5	0.6	6.0	6.00	20.0	C	Flood Plain (Bottom Land)	mesic	loamy	no	
Roundabout	333	5	0.2	2.0	0.06	0.6	C	Terraces and glacial lake plains	frigid	silty	no	
Runney	105	5	0.6	6.0	6.00	20.0	C	Flood Plain (Bottom Land)	frigid	loamy	no	silt loam in the C

Sorted by DES Soil Group for Establishing Lot Size  
K<sub>sat</sub> B and C horizons  
SSSNNE pub no. 5

**DRAINAGE CULVERT & RIPRAP SIZING**

Based on Manning's "n" = 0.012,  $Q = K \cdot S^{1/2} \cdot (0.5)$

Culvert	Diam. (in)	Slope (ft/ft)	Capacity (cfs)	Design flow (cfs) (25 year event)	Velocity (fps)	Tailwater (feet)	Apron Length (feet)	Width W1 (feet)	Width W2 (feet)	Min d50 (inches)	Spec d50 (inches)	Notes
CB 2 out	12	0.015	4.73	2.46	4.1	0.40	9	3.00	10	1.9	5	
CB 3 out	12	0.004	2.44	0.38	6.6	0.40	9	3.00	10	0.2	5	Conservatively assume velo from 2" orifice
CB 4 out	18	0.005	8.05	2.00	1.5	0.60	14	4.50	15	0.7	5	
CB 5 out	12	0.006	2.99	2.33	6.38	0.40	9	3.00	10	1.8	8	Conservatively assume velo from 4" orifice
Road Culvert	18	0.004	7.20	3.13	3.37	0.60	14	4.50	15	1.2	5	
Drive Culvert	18	0.005	8.05	0.48	0.93	0.60	Not needed			N/A	5	Outlet to adjacent riprap

NOTE: Where amount or velocity of flow from the culvert is not know/evaluated, a conservative flow has been assumed as well as a velocity that will require the installation of outlet protection.

Apron sizing determined using Maine Erosion & Sediment Control BMP Manual for high flow pipes





## STORMWATER POND DESIGN CRITERIA (Env-Wq 1508.03)

**Type/Node Name:** Pond 11P - Detention Pond w/Infiltration

Enter the type of stormwater pond (e.g., Wet Pond) and the node name in the drainage analysis, if applicable

1.33	ac	A = Area draining to the practice	
0.39	ac	$A_I$ = Impervious area draining to the practice	
0.29	decimal	I = percent impervious area draining to the practice, in decimal form	
0.31	unitless	$R_v$ = Runoff coefficient = $0.05 + (0.9 \times I)$	
0.42	ac-in	$WQV = 1'' \times R_v \times A$	
1,516	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
152	cf	10% x WQV (check calc for sediment forebay and micropool volume)	
758	cf	50% x WQV (check calc for extended detention volume)	
234	cf	$V_{SED}$ = sediment forebay volume	← $\geq 10\%WQV$
-	cf	$V_{PP}$ = permanent pool volume (volume below the lowest invert of the outlet structure)	
1,516	cf	$V_{ED} = WQV - V_{PP}$ = extended detention volume	← $\leq X\%^1 WQV$
225.85		$E_{ED}$ = elevation of $V_{ED}$ (attach stage-storage table)	
0.04	cfs	$2Q_{avg} = 2 * V_{ED} / 24 \text{ hrs} * (1 \text{ hr} / 3600 \text{ sec})$ (used to check against $Q_{EDmax}$ below)	
0.02	cfs	$Q_{EDmax}$ = discharge at the $E_{ED}$ (attach stage-discharge table)	← $< 2Q_{avg}$
42.10	hours	$T_{ED}$ = drawdown time of extended detention = $2V_{ED}/Q_{EDmax}$	← $\geq 24\text{-hrs}$
3.00	:1	Pond side slopes	← $\geq 3:1$
	ft	Average permanent pool depth	← 3 - 6 ft
	ft	Maximum depth of permanent pool	← $\leq 8 \text{ ft}$
	ft	Length of the flow path between the inlet and outlet at mid-depth	
	ft	Average Width ([average of the top width + average bottom width]/2)	
-	:1	Length to Average Width ratio	← $\geq 3:1$
Yes	Yes/No	The perimeter should be curvilinear.	
No	Yes/No	The inlet and outlet should be located as far apart as possible.	
No	Yes/No	Is there a manually-controlled drain provided to dewater the pond over a 24hr period?	
If no state why:		Continuous drain currently installed, cleanout as necessary to provide dewatering.	
Nilex Georidge to be installed over outlets	What mechanism is proposed to prevent the outlet structure from clogging (applicable for orifices/weirs with a dimension of $\leq 6''$ )?		
227.45	ft	Peak elevation of the 50-year storm event	
228.50	ft	Berm elevation of the pond	
YES		50 peak elevation $\leq$ the berm elevation?	← yes
Qualified professional that developed the planting plan:			
Name, Profession:		Existing vegetation to remain	

1. "X" varies depending on type of stormwater pond design. See NH Stormwater Manual, Vol.2, Ch.4-3, Section 1, for the design permanent pool volumes and extended detention volumes.

Designer's Notes:

This pond will detain runoff and allow for a small amount of infiltration and to control peak flows from the site.

Stage-Area-Storage for Pond 11P: Pond at entrance

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
225.00	770	0	227.60	1,973	3,515
225.05	790	39	227.65	1,999	3,614
225.10	810	79	227.70	2,025	3,715
225.15	830	120	227.75	2,050	3,817
225.20	850	162	227.80	2,076	3,920
225.25	871	205	227.85	2,103	4,025
225.30	892	249	227.90	2,129	4,130
225.35	913	294	227.95	2,155	4,237
225.40	934	340	228.00	2,182	4,346
225.45	956	388	228.05	2,218	4,456
225.50	978	436	228.10	2,255	4,568
225.55	1,000	485	228.15	2,291	4,681
225.60	1,022	536	228.20	2,328	4,797
225.65	1,045	588	228.25	2,366	4,914
225.70	1,068	640	228.30	2,404	5,033
225.75	1,091	694	228.35	2,441	5,155
225.80	1,114	749	228.40	2,480	5,278
225.85	1,138	806	228.45	2,518	5,403
225.90	1,162	863	228.50	2,557	5,529
225.95	1,186	922	228.55	2,596	5,658
226.00	1,210	982	228.60	2,636	5,789
226.05	1,232	1,043	228.65	2,675	5,922
226.10	1,254	1,105	228.70	2,716	6,057
226.15	1,276	1,168	228.75	2,756	6,193
226.20	1,298	1,232	228.80	2,796	6,332
226.25	1,320	1,298	228.85	2,837	6,473
226.30	1,343	1,365	228.90	2,879	6,616
226.35	1,366	1,432	228.95	2,920	6,761
226.40	1,389	1,501	229.00	2,962	6,908
226.45	1,412	1,571	229.05	2,974	7,056
226.50	1,435	1,642	229.10	2,985	7,205
226.55	1,459	1,715	229.15	2,997	7,355
226.60	1,483	1,788	229.20	3,009	7,505
226.65	1,507	1,863	229.25	3,021	7,656
226.70	1,531	1,939	229.30	3,032	7,807
226.75	1,555	2,016	229.35	3,044	7,959
226.80	1,580	2,094	229.40	3,056	8,112
226.85	1,605	2,174	229.45	3,068	8,265
226.90	1,630	2,255	229.50	3,080	8,418
226.95	1,655	2,337	229.55	3,092	8,573
227.00	1,680	2,420	229.60	3,104	8,728
227.05	1,704	2,505	229.65	3,116	8,883
227.10	1,727	2,591	229.70	3,128	9,039
227.15	1,751	2,678	229.75	3,140	9,196
227.20	1,775	2,766	229.80	3,152	9,353
227.25	1,799	2,855	229.85	3,164	9,511
227.30	1,824	2,946	229.90	3,176	9,669
227.35	1,848	3,038	229.95	3,188	9,828
227.40	1,873	3,131	230.00	<b>3,200</b>	<b>9,988</b>
227.45	1,898	3,225			
227.50	1,923	3,320			
227.55	1,948	3,417			

Head=226.42

Ved=1516 cf



**Stage-Discharge for Pond 11P: Pond at entrance**

Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)
225.00	0.00	0.00	0.00	0.00
225.10	0.30	<b>0.30</b>	0.00	0.00
225.20	0.30	<b>0.30</b>	0.00	0.00
225.30	0.30	0.30	0.00	0.00
225.40	0.30	0.30	0.00	0.00
225.50	0.30	0.30	0.00	0.00
225.60	0.30	0.30	0.00	0.00
225.70	0.30	0.30	0.00	0.00
225.80	0.30	0.30	0.00	0.00
225.90	0.30	0.30	0.00	0.00
226.00	0.30	0.30	0.00	0.00
226.10	0.30	0.30	0.00	0.00
226.20	0.30	0.30	0.00	0.00
226.30	0.30	0.30	0.00	0.00
226.40	0.31	0.30	0.01	0.00
226.50	0.38	0.30	0.08	0.00
226.60	0.53	0.30	0.23	0.00
226.70	0.76	0.30	0.46	0.00
226.80	1.03	0.30	0.73	0.00
226.90	1.28	0.30	0.98	0.00
227.00	1.49	0.30	1.19	0.00
227.10	1.66	0.30	1.36	0.00
227.20	1.81	0.30	1.51	0.00
227.30	1.95	0.30	1.65	0.00
227.40	2.08	0.30	1.78	0.00
227.50	2.43	0.30	2.13	0.00
227.60	3.51	0.30	3.21	0.00
227.70	4.83	0.30	4.53	0.00
227.80	5.03	0.30	4.63	0.11
227.90	5.58	0.30	4.72	0.56
228.00	6.33	0.30	4.81	1.21
228.10	7.27	0.30	4.91	2.06
228.20	8.39	0.30	5.00	3.10
228.30	9.72	0.30	5.08	4.33
228.40	11.12	0.30	5.17	5.65
228.50	12.53	0.30	5.26	6.98
228.60	14.04	0.30	5.34	8.40
228.70	15.65	0.30	5.42	9.93
228.80	17.33	0.30	5.51	11.52
228.90	19.07	0.30	5.59	13.18
229.00	20.88	0.30	5.66	14.91
229.10	22.75	0.30	5.74	16.71
229.20	24.68	0.30	5.82	18.56
229.30	26.67	0.30	5.90	20.47
229.40	28.74	0.30	5.97	22.47
229.50	30.88	0.30	6.05	24.54
229.60	33.09	0.30	6.12	26.67
229.70	35.36	0.30	6.19	28.86
229.80	37.69	0.30	6.26	31.12
229.90	40.09	0.30	6.33	33.45
230.00	<b>42.55</b>	0.30	<b>6.40</b>	<b>35.84</b>

wd=226.42

Qed=0.02 cfs

## STORMWATER POND DESIGN CRITERIA (Env-Wq 1508.03)

**Type/Node Name:** Pond 21P - Detention Pond w/Infiltration

Enter the type of stormwater pond (e.g., Wet Pond) and the node name in the drainage analysis, if applicable

0.53	ac	A = Area draining to the practice	
0.26	ac	$A_I$ = Impervious area draining to the practice	
0.50	decimal	I = percent impervious area draining to the practice, in decimal form	
0.50	unitless	$R_v$ = Runoff coefficient = $0.05 + (0.9 \times I)$	
0.26	ac-in	$WQV = 1'' \times R_v \times A$	
958	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
96	cf	10% x WQV (check calc for sediment forebay and micropool volume)	
479	cf	50% x WQV (check calc for extended detention volume)	
195	cf	$V_{SED}$ = sediment forebay volume	← ≥ 10%WQV
-	cf	$V_{PP}$ = permanent pool volume (volume below the lowest invert of the outlet structure)	
958	cf	$V_{ED} = WQV - V_{PP}$ = extended detention volume	← ≤ X% <sup>1</sup> WQV
229.45		$E_{ED}$ = elevation of $V_{ED}$ (attach stage-storage table)	
0.02	cfs	$2Q_{avg} = 2 * V_{ED} / 24 \text{ hrs} * (1 \text{ hr} / 3600 \text{ sec})$ (used to check against $Q_{EDmax}$ below)	
0.02	cfs	$Q_{EDmax}$ = discharge at the $E_{ED}$ (attach stage-discharge table)	← < $2Q_{avg}$
26.62	hours	$T_{ED}$ = drawdown time of extended detention = $2V_{ED}/Q_{EDmax}$	← ≥ 24-hrs
3.00	:1	Pond side slopes	← ≥ 3:1
	ft	Average permanent pool depth	← 3 - 6 ft
	ft	Maximum depth of permanent pool	← ≤ 8 ft
	ft	Length of the flow path between the inlet and outlet at mid-depth	
	ft	Average Width ([average of the top width + average bottom width]/2)	
-	:1	Length to Average Width ratio	← ≥ 3:1
Yes	Yes/No	The perimeter should be curvilinear.	
Yes	Yes/No	The inlet and outlet should be located as far apart as possible.	
No	Yes/No	Is there a manually-controlled drain provided to dewater the pond over a 24hr period?	
If no state why:		Continuous drain currently installed, cleanout as necessary to provide dewatering.	
Nilex Georidge to be installed over outlets	What mechanism is proposed to prevent the outlet structure from clogging (applicable for orifices/weirs with a dimension of ≤ 6")?		
231.21	ft	Peak elevation of the 50-year storm event	
231.50	ft	Berm elevation of the pond	
YES		50 peak elevation ≤ the berm elevation?	← yes
Qualified professional that developed the planting plan:			
Name, Profession:		Existing vegetation to remain	

1. "X" varies depending on type of stormwater pond design. See NH Stormwater Manual, Vol.2, Ch.4-3, Section 1, for the design permanent pool volumes and extended detention volumes.

Designer's Notes:

This pond will detain runoff and allow for a small amount of infiltration and to control peak flows from the site.



**20200310-1933600-POST-TEST**

Type III 24-hr 1-YR Rainfall=2.56"

Prepared by Civil Consultants

Printed 3/16/2020

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**Stage-Area-Storage for Pond 21P: Pond to south**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
230.00	2,123	0	231.04	3,101	2,708
230.02	2,140	43	231.06	3,114	2,770
230.04	2,158	86	231.08	3,127	2,832
230.06	2,175	129	231.10	3,139	2,895
230.08	2,193	173	231.12	3,152	2,958
230.10	2,210	217	231.14	3,165	3,021
230.12	2,228	261	231.16	3,179	3,085
230.14	2,246	306	231.18	3,192	3,148
230.16	2,264	351	231.20	3,205	3,212
230.18	2,281	396	231.22	3,218	3,276
230.20	2,299	442	231.24	3,231	3,341
230.22	2,317	488	231.26	3,244	3,406
230.24	2,335	535	231.28	3,257	3,471
230.26	2,354	582	231.30	3,270	3,536
230.28	2,372	629	231.32	3,284	3,602
230.30	2,390	677	231.34	3,297	3,667
230.32	2,409	725	231.36	3,310	3,733
230.34	2,427	773	231.38	3,324	3,800
230.36	2,445	822	231.40	3,337	3,866
230.38	2,464	871	231.42	3,350	3,933
230.40	2,483	920	Ved=958 cf	3,364	4,000
230.42	2,501	970	231.44	3,377	4,068
230.44	2,520	1,020	231.48	3,391	4,135
230.46	2,539	1,071	231.50	3,404	4,203
230.48	2,558	1,122	231.52	3,418	4,272
230.50	2,577	1,173	231.54	3,431	4,340
230.52	2,596	1,225	231.56	3,445	4,409
230.54	2,615	1,277	231.58	3,458	4,478
230.56	2,634	1,330	231.60	3,472	4,547
230.58	2,654	1,382	231.62	3,486	4,617
230.60	2,673	1,436	231.64	3,499	4,687
230.62	2,693	1,489	231.66	3,513	4,757
230.64	2,712	1,543	231.68	3,527	4,827
230.66	2,732	1,598	231.70	3,540	4,898
230.68	2,751	1,653	231.72	3,554	4,969
230.70	2,771	1,708	231.74	3,568	5,040
230.72	2,791	1,763	231.76	3,582	5,112
230.74	2,811	1,819	231.78	3,596	5,183
230.76	2,830	1,876	231.80	3,610	5,255
230.78	2,850	1,933	231.82	3,624	5,328
230.80	2,871	1,990	231.84	3,638	5,400
230.82	2,891	2,048	231.86	3,651	5,473
230.84	2,911	2,106	231.88	3,665	5,546
230.86	2,931	2,164	231.90	3,679	5,620
230.88	2,951	2,223	231.92	3,694	5,694
230.90	2,972	2,282	231.94	3,708	5,768
230.92	2,992	2,342	231.96	3,722	5,842
230.94	3,013	2,402	231.98	3,736	5,916
230.96	3,034	2,462	232.00	<b>3,750</b>	<b>5,991</b>
230.98	3,054	2,523			
231.00	3,075	2,584			
231.02	3,088	2,646			

**20200310-1933600-POST-TEST**

Type III 24-hr 1-YR Rainfall=2.56"

Prepared by Civil Consultants

Printed 3/16/2020

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**Stage-Discharge for Pond 21P: Pond to south**

Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)	
230.00	0.00	0.00	0.00	0.00	
230.05	0.01	0.01	0.00	0.00	
230.10	0.02	0.02	0.00	0.00	
230.15	0.02	0.02	0.00	0.00	
230.20	0.02	0.02	0.00	0.00	
230.25	0.02	0.02	0.00	0.00	
230.30	0.02	0.02	0.00	0.00	
230.35	0.02	0.02	0.00	0.00	
230.40	0.03	0.02	0.01	0.00	Qed=0.02 cfs
230.45	0.04	0.02	0.03	0.00	
230.50	0.05	0.02	0.04	0.00	
230.55	0.06	0.02	0.04	0.00	
230.60	0.07	0.02	0.05	0.00	
230.65	0.08	0.02	0.06	0.00	
230.70	0.10	0.02	0.08	0.00	
230.75	0.13	0.02	0.11	0.00	
230.80	0.16	0.02	0.14	0.00	
230.85	0.20	0.02	0.18	0.00	
230.90	0.22	0.02	0.20	0.00	
230.95	0.25	0.02	0.22	0.00	
231.00	0.27	0.02	0.24	0.00	
231.05	0.28	0.02	0.26	0.00	
231.10	0.30	0.02	0.28	0.00	
231.15	0.32	0.02	0.30	0.00	
231.20	0.33	0.02	0.31	0.00	
231.25	0.35	0.02	0.33	0.00	
231.30	0.36	0.02	0.34	0.00	
231.35	0.38	0.02	0.35	0.00	
231.40	0.39	0.02	0.37	0.00	
231.45	0.40	0.02	0.38	0.00	
231.50	0.41	0.02	0.39	0.00	
231.55	0.43	0.02	0.40	0.00	
231.60	0.44	0.02	0.41	0.00	
231.65	0.68	0.02	0.65	0.00	
231.70	1.11	0.02	1.08	0.00	
231.75	1.66	0.02	1.64	0.00	
231.80	2.32	0.03	2.29	0.00	
231.85	3.06	0.03	3.03	0.00	
231.90	4.09	0.03	3.85	0.21	
231.95	5.03	0.03	4.41	0.59	
232.00	<b>5.57</b>	<b>0.03</b>	<b>4.45</b>	<b>1.09</b>	

## APPENDIX D

# Stormwater Maintenance & Inspection Plan

During the construction of the Barrington Town Office Building, maintenance of all erosion, sedimentation, and stormwater flow control structures and devices will be the responsibility of the Contractor. Upon final stabilization of the site, all maintenance will be the responsibility of the Town of Barrington (Owner).

The Owner will be responsible for the maintenance of all erosion, sedimentation, and stormwater flow control structures and devices within the limits of the development and will retain that responsibility until such time as another individual and/or agency (acceptable to the NH DES and the Town) accepts the responsibility.

The Owner will be responsible for the continued maintenance of the stormwater treatment system.

During construction all erosion control devices and structures shall be checked monthly and after each "significant rainfall"\*\*. Necessary repairs will be made to correct undermining or deterioration of the devices and/or structures. Sediment in the stormwater detention basins will be removed annually or as needed to maintain functionality of the facility.

The Owner shall maintain inspection logs (attached) of all stormwater and erosion control measures. The log shall reflect the dates of the inspections and describe actions taken. The log shall be kept on file for a minimum of 5 years and be made available to the Town upon request.

The activities listed in the inspection log will be accomplished in early spring and in late fall.

A major storm event is classified as a rainfall exceeding 2.9 inches (2yr) storm event.

\*\* Significant rainfall is ½" in 24 hr



**Sweeping**

Paved surfaces shall be swept or vacuumed at least annually in the Spring to remove all Winter sand, and periodically during the year on an as-needed basis to minimize transportation of sediment during rainfall events.

<b>Roadways and Parking Surfaces</b>	Spring	Fall or Yearly	After a Major Storm	Every 2-5 Years
Clear accumulated winter sand in parking lots and along roadways	X			
Sweep pavement to remove sediment	X			
Grade road shoulders and remove excess sand either manually or by a front-end loader	X			
Grade gravel roads and gravel shoulders	X			
Clean-out the sediment within water bars or open top culverts	X			
Ensure that stormwater is not impeded by accumulations of material or false ditches in the shoulder	X			

**Catch Basins and Culverts**

All catch basins, and any other field inlets throughout the collection system, need to be inspected on a monthly basis to assure that the inlet entry point is clear of debris and will allow the intended water entry. These will be cleared, if necessary on a yearly basis or when sediment reaches two thirds of total sump volume. Catch basins need to be vacuumed and cleaned of all accumulated sediment. This work must be done by a vacuum truck. The removed material must be disposed of in accordance with the New Hampshire Solid Waste Disposal Rules.

	Spring	Fall or Yearly	After a Major Storm	Every 2-5 Years
Remove and legally dispose of accumulated sediments and debris from the bottom of the basin, inlet grates, inflow channels to the basin, and pipes between basins.	X	X		
Remove floating debris and floating oils (using oil absorptive pads) from any trap designed for such	X	X		
Remove accumulated sediments and debris at the inlet, at the outlet, and within the culvert.	X	X	X	
Repair any erosion damage at the culvert's inlet and outlet	X	X	X	

**Vegetated Areas**

All areas of maintained lawn are to be inspected regularly for signs of erosions and channelization. Areas where erosion is occurring or areas of sparse growth shall be replanted and stabilized. Channelized flows from the eroded land shall be diverted to buffers or other areas able to withstand the high sediment load in the erosive runoff.

<b>Vegetated Areas</b>	Spring	Fall or Yearly	After a Major Storm	Every 2-5 Years
Inspect all slopes and embankments	X		X	
Replant bare areas or areas with sparse growth	X		X	
Armor areas with fill erosions with an appropriate lining or divert the erosive flows to on-site areas able to withstand concentrated flows	X		X	



## **Infiltration Facilities**

**Monitoring and Inspections:** The infiltration area should be inspected several times in the first year of operation and at least annually thereafter. Conduct inspections after large storms to check for surface ponding at the inlet that may indicate clogging. Water levels in the observation wells (if applicable) should be recorded over several days after the storm to ensure that the system drains as designed. Records should be kept of all maintenance operations to help plan future work and identify problem areas.

**Inspecting Embankments for Instability and Erosion:** Embankments should be inspected annually for erosion, destabilization of side slopes, embankment settling, and other signs of structural failure. Corrective action should be taken immediately upon identification of problems.

**Sediment Forebay Maintenance:** The sediment forebay shall be inspected at least annually for deterioration and accumulation of sediment and debris. The forebay will be cleaned out when accumulated sediment and debris occupies more than 10% of the available capacity.

**Pretreatment Buffer Strips:** If a grass buffer strip is used in conjunction with the infiltration BMP it should be inspected regularly. Growth should be vigorous and dense. Bare spots or eroded areas should be repaired and/or re-seeded or re-sodded. Watering and/or fertilization should be provided during the first few months after the strip is established, and may periodically be needed in times of drought. Grass filter strips should be mowed regularly to prevent the uncontrolled growth of briars and weeds. Filter strips in residential or commercial areas will need to be mowed more frequently, but filter strip performance will be impaired if the grass is cut too short. Lawn clippings should be removed to prevent them from clogging the BMP.

**Observation Wells, Measure of Sediment Accumulation, and Points of Access for Sediment Removal:** Observation wells will be installed in the basins to determine the system's overall performance and infiltration rate. The observation well shall be a 4-inch diameter perforated PVC pipe with a removable and securable well cap, foot plate and rebar anchor. If impounded water drains at a rate of less than 2.41 in/hour, sediment at the surface of the basin shall be removed and disposed of appropriately. Marked rods shall be installed to determine the amount of sediment accumulation at the surface of the basins. Access to the basins shall be provided over the roadway and individual lots as needed.

**Clearing Outlet Structures:** The outlet structures should be checked periodically to ensure that they are not blocked by debris. Inspections should be conducted monthly during wet weather conditions from March to November.

**Mowing:** Basins with grass cover should be mowed at least twice per year. Clippings should be removed to minimize the amount of organic material accumulating in the basin.

**Fertilization:** Fertilization of the infiltration area should be avoided unless absolutely necessary to establish vegetation.

**Harvesting and Weeding:** Harvesting and pruning of excessive growth will need to be done occasionally. Weeding to control unwanted or invasive plants may also be necessary.

**Snow Storage:** Snow removed from any on-site or off-site areas may not be stored over an infiltration area.



<b>Infiltration Facilities –Infiltration Basin</b>				
	Spring	Fall or Yearly	After a Major Storm	Every 2- 5 Years
Inspect the embankments for destabilization, slope erosion, internal piping, and downstream swamping. A professional engineer must review these immediately.		X	X	
Mow the embankment and basin surface to control woody vegetation.		X		
Inspect the sediment control areas (forebays) for accumulation of debris and sediment. Removed when more than 10% of available capacity is occupied, or when sediment is no longer contained to the forebay (at least annually).		X		X
Remove and dispose of sediments and debris upstream of the basin		X		X
The basin should be inspected several times in the first several months and at least annually thereafter		X		
Confirm infiltration rates via observation wells (if applicable) and monitor sediment accumulation on the basin surface via marked rods, remove sediment as needed (see below)		X	X	
The top several inches of the basin shall be replaced with fresh material when water ponds on the surface of the bed for more than 72 hours. The removed sediments should be disposed in an acceptable manner. A professional engineer shall review the condition of the facility to determine if additional actions are necessary to restore infiltration function.				X
Basins should be mowed at least 2 times per year, with clippings removed	X	X		
Fertilization of the basins should be avoided unless absolutely necessary to establish vegetation				
Harvesting and pruning of excessive growth will need to be done occasionally. Weeding to control unwanted or invasive plants may also be necessary		X		





### **Road Salt and Deicing Minimization**

The intent should be to minimize the amount of salt and other deicing agents utilized to the extent practical. Efforts shall be made to avoid the use of dry salt and winter sand and other abrasive materials.

A table provided by the NH DES for Deicing Application Rate Guidelines has been included for reference with regard to the type and rate of deicing agents to be used.

Use of deicers for each storm event shall be tracked using the log sheet provided.

**NO WINTER SANDING OF POROUS ASPHALT IS PERMITTED.**

### **Control of Invasive Plants**

During maintenance activities, check for the presence of invasive plants and remove in a safe manner as described on the following pages. They should be controlled as described on the following pages.

Invasive plants are introduced, alien, or non-native plants, which have been moved by people from their native habitat to a new area. Some exotic plants are imported for human use such as landscaping, erosion control, or food crops. They also can arrive as "hitchhikers" among shipments of other plants, seeds, packing materials, or fresh produce. Some exotic plants become invasive and cause harm by:

- becoming weedy and overgrown;
- killing established shade trees;
- obstructing pipes and drainage systems;
- forming dense beds in water;
- lowering water levels in lakes, streams, and wetlands;
- destroying natural communities;
- promoting erosion on stream banks and hillsides; and
- resisting control except by hazardous chemical.



### Deicing Application Rate Guidelines

24' of pavement (typical two-lane road)

These rates are not fixed values, but rather the middle of a range to be selected and adjusted by an agency according to its local conditions and experience.

Pavement Temp. (°F) and Trend (↑↓)	Weather Condition	Maintenance Actions	Pounds per two-lane mile			
			Salt Prewetted / Pretreated with Salt Brine	Salt Prewetted / Pretreated with Other Blends	Dry Salt*	Winter Sand (abrasives)
> 30° ↑	Snow	Plow, treat intersections only	80	70	100*	Not recommended
	Freezing Rain	Apply Chemical	80 - 160	70 - 140	100 - 200*	Not recommended
30° ↓	Snow	Plow and apply chemical	80 - 160	70 - 140	100 - 200*	Not recommended
	Freezing Rain	Apply Chemical	150 - 200	130 - 180	180 - 240*	Not recommended
25° - 30° ↑	Snow	Plow and apply chemical	120 - 160	100 - 140	150 - 200*	Not recommended
	Freezing Rain	Apply Chemical	150 - 200	130 - 180	180 - 240*	Not recommended
25° - 30° ↓	Snow	Plow and apply chemical	120 - 160	100 - 140	150 - 200*	Not recommended
	Freezing Rain	Apply Chemical	160 - 240	140 - 210	200 - 300*	400
20° - 25° ↑	Snow or Freezing Rain	Plow and apply chemical	160 - 240	140 - 210	200 - 300*	400
20° - 25° ↓	Snow	Plow and apply chemical	200 - 280	175 - 250	250 - 350*	Not recommended
	Freezing Rain	Apply Chemical	240 - 320	210 - 280	300 - 400*	400
15° - 20° ↑	Snow	Plow and apply chemical	200 - 280	175 - 250	250 - 350*	Not recommended
	Freezing Rain	Apply Chemical	240 - 320	210 - 280	300 - 400*	400
15° - 20° ↓	Snow or Freezing Rain	Plow and apply chemical	240 - 320	210 - 280	300 - 400*	500 for freezing rain
0° - 15° ↑↓	Snow	Plow, treat with blends, sand hazardous areas	Not recommended	300 - 400	Not recommended	500 - 750 spot treatment as needed
< 0°	Snow	Plow, treat with blends, sand hazardous areas	Not recommended	400 - 600**	Not recommended	500 - 750 spot treatment as needed

\* Dry salt is not recommended. It is likely to blow off the road before it melts ice.

\*\* A blend of 6 - 8 gal/ton MgCl<sub>2</sub> or CaCl<sub>2</sub> added to NaCl can melt ice as low as -10°.

Figure 4-1. Deicing Application Rate Guidelines



Anti-icing Route Data Form				
Truck Station:				
Date:				
Air Temperature	Pavement Temperature	Relative Humidity	Dew Point	Sky
Reason for applying:				
Route:				
Chemical:				
Application Time:				
Application Amount:				
Observation (first day):				
Observation (after event):				
Observation (before next application):				
Name:				

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**Stormwater Maintenance  
Barrington Town Office Building  
Maintenance Log**

This log is intended to accompany the Stormwater Management Facilities Maintenance Plan for Barrington Town Office Building. The following items shall be checked, cleaned and maintained on regular basis as specified in the Maintenance Plan and as described in the table below. This log shall be kept on file for a minimum of five years. Qualified personnel familiar with drainage systems and soils shall perform all inspections.

Item	Maintenance Required & Frequency				Date Completed	Maintenance Personnel	Comments
	Spring	Fall or Yearly	After a Major Storm	Every 2-5 Years			
<b>Sweeping of Roads</b>	Clear accumulated winter sand in parking lots and along roadways	X					
	Sweep pavement to remove sediment	X					
	Grade road shoulders and remove excess sand either manually or by a front-end loader	X					
	Grade gravel roads and gravel shoulders	X					
	Clean-out the sediment within water bars or open top culverts	X					
	Ensure that stormwater is not impeded by accumulations of material or false ditches in the shoulder	X					



Item	Maintenance Required & Frequency					Date Completed	Maintenance Personnel	Comments
	Vegetated Areas	Spring	Fall or Yearly	After a Major Storm	Every 2-5 Years			
Vegetated Areas	Inspect all slopes and embankments	X		X				
	Replant bare areas or areas with sparse growth	X		X				
	Armor areas with fill erosions with an appropriate lining or divert the erosive flows to on-site areas able to withstand concentrated flows	X		X				
Catch Basins (Item "1" on Plan)	Remove and legally dispose of accumulated sediments and debris from the bottom of the basin, inlet grates, inflow channels to the basin, and pipes between basins.	X	X					
	Remove floating debris and floating oils (using oil absorptive pads) from any trap designed for such	X	X					
	Remove accumulated sediments and debris at the inlet, at the outlet, and within the culvert.	X	X	X				
	Repair any erosion damage at the culvert's inlet and outlet	X	X	X				



Item	Maintenance Required & Frequency								Date Completed	Maintenance Personnel	Comments
<p><b>Roadway                      Ditches,                      Swales and                      Culverts                      (Item "2"                      on plan)</b></p>	Inspect ditches, swales and other open stormwater channels	X	X	X	X						
	Remove any obstructions and accumulated sediments or debris	X	X								
	Control vegetated growth and woody vegetation		X								
	Repair any erosion of the ditch lining		X								
	Mow vegetated ditches		X								
	Remove woody vegetation growing through riprap		X								
	Repair any slumping side slopes	X	X								
	Replace riprap where underlying filter fabric or underdrain gravel is showing or where stones have dislodge	X								X	

Item	Maintenance Required & Frequency					Date Completed	Maintenance Personnel	Comments	
	Infiltration Facilities – Infiltration Basin								
	Spring	Fall or Yearly	After a Major Storm	Every 2-5 Years					
<b>Infiltration BMPs</b>  <b>Infiltration Basin (Item “3” on plan)</b>	Inspect the embankments for destabilization, slope erosion, internal piping, and downstream swamping. A professional engineer must review these immediately.	X	X						
	Mow the embankment and basin surface to control woody vegetation.	X							
	Inspect the sediment control areas (forebays) for accumulation of debris and sediment. Removed when more than 10% of available capacity is occupied, or when sediment is no longer contained to the forebay (at least annually).		X		X				
	Remove and dispose of sediments and debris upstream of the basin		X		X				
	The basin should be inspected several times in the first several months and at least annually thereafter		X						
	Confirm infiltration rates via observation wells (if applicable) and monitor sediment accumulation on the basin surface via marked rods, remove sediment as needed (see below)		X	X					
	The top several inches of the basin shall be replaced with fresh material when water ponds on the surface of the bed for more than 72 hours. The removed sediments should be disposed in an acceptable manner. A professional engineer shall review the condition of the facility to determine if additional actions are necessary to restore infiltration function.				X				
	Basins should be mowed at least 2 times per year, with clippings removed	X	X						



CIVIL CONSULTANTS

P.O. Box 100 South Berwick, Maine 03908 207-364-2550

STORMWATER MANAGEMENT SUBMISSION  
 Barrington Town Office Building

March 2020

Appendix D  
 SITE DEVELOPMENT

	Fertilization of the basins should be avoided unless absolutely necessary to establish vegetation Harvesting and pruning of excessive growth will need to be done occasionally. Weeding to control unwanted or invasive plants may also be necessary		X							
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CIVIL  
 CONSULTANTS

P.O. Box 100 South Berwick, Maine 03908 207-364-2550

Maintenance Log.









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**CIVIL  
CONSULTANTS**

*Engineers*

*Planners*

*Surveyors*

---

***APPENDIX E***

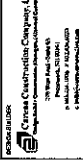
**L1 – Site Plan**

**L2 - Notes and Details**

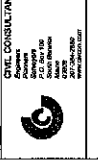
**D1 – Pre-Development Stormwater Plan**

**D2 – Post-Development Stormwater Plan**





**PORTONE ARCHITECTS**  
 100 Main Street  
 Barrington, NH 03021  
 Telephone: 603.888.8888  
 Fax: 603.888.8889  
 www.portone.com



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DATE: 08/17/2020  
 PROJECT: BARRINGTON TOWN HALL

**Barrington Town Hall**

**CONSTRUCTION DETAILS**

PROJECT NO: CCI193300 PORT19-002  
 DATE: 08/17/2020  
 SCALE: AS NOTED  
 SHEET NO: L-2

**EROSION AND SEDIMENT CONTROL PRACTICES**

- NO SOIL SHALL BE DISTURBED DURING THE PERIOD OF MARCH 1 THROUGH APRIL 15, UNLESS THE DISTURBANCE IS NECESSARY FOR THE INSTALLATION OF EROSION CONTROL MEASURES. ALL EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO EARTH MOVING.
- ALL EROSION CONTROL MEASURES SHALL BE MAINTAINED THROUGHOUT CONSTRUCTION.
- STABILIZED SOILS SHALL BE STABILIZED WITHIN ONE (1) WEEK FROM THE DATE IT WAS LAST EXPOSED TO WEATHER. EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO EARTH MOVING.
- NO EROSION CONTROL MEASURES SHALL BE REMOVED AT A RATE OF AT LEAST ONE (1) TON PER 100 SQUARE FEET (10' x 10' AREA).
- IF A SLOPE IS EXPOSED TO WEATHER IN EXCESSIVE WINDS, IT SHALL BE PROTECTED WITH NETTING, PILES OF STRAW, OR OTHER EROSION CONTROL MEASURES AND SHALL BE MAINTAINED THROUGHOUT CONSTRUCTION.
- IN ADDITION TO PLACEMENT OF EROSION CONTROL MEASURES, EROSION CONTROL MEASURES SHALL BE MAINTAINED THROUGHOUT CONSTRUCTION. EROSION CONTROL MEASURES SHALL BE MAINTAINED THROUGHOUT CONSTRUCTION. EROSION CONTROL MEASURES SHALL BE MAINTAINED THROUGHOUT CONSTRUCTION.
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**SEEDING MATERIALS AND SCHEDULE**

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**CONSTRUCTION SEQUENCE NOTES**

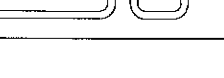
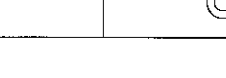
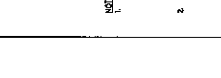
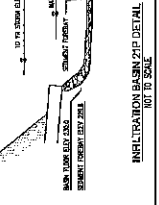
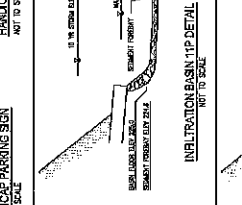
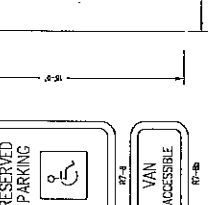
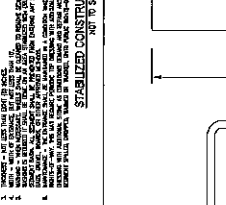
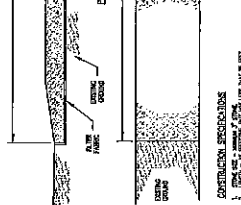
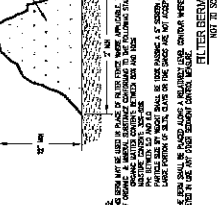
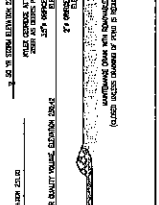
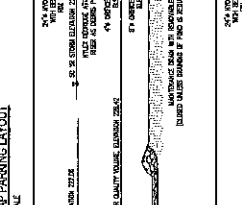
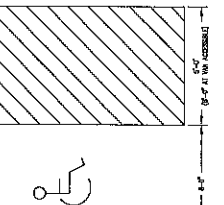
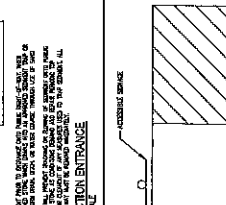
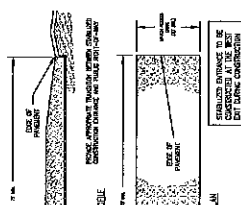
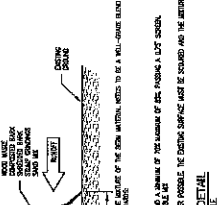
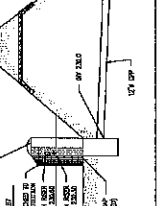
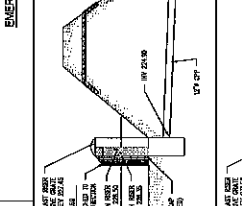
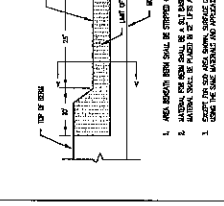
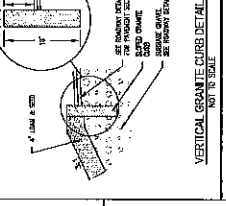
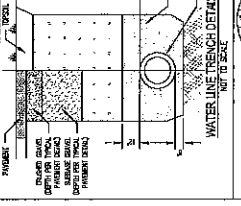
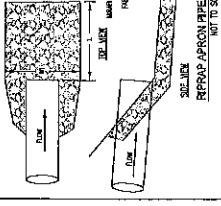
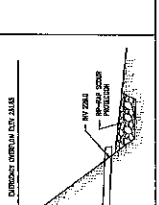
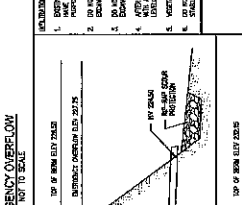
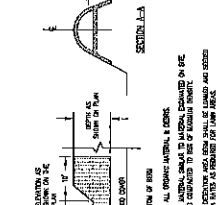
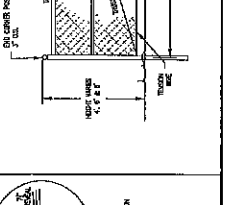
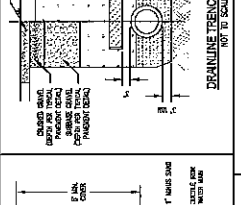
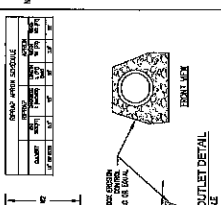
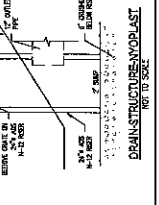
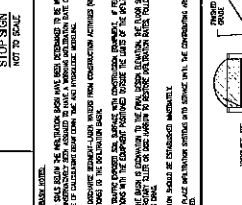
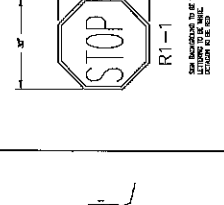
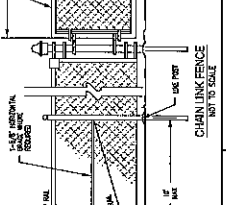
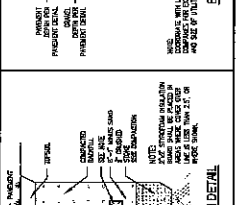
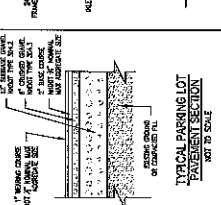
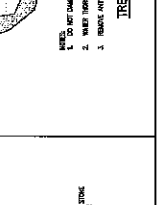
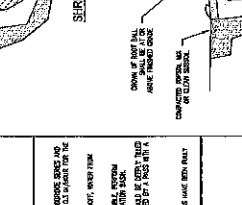
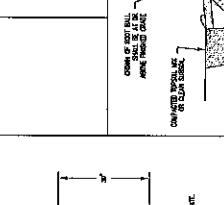
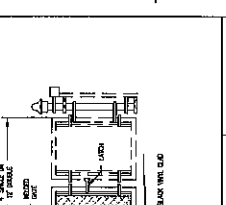
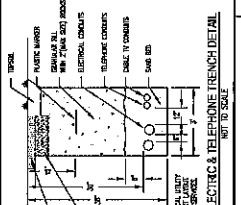
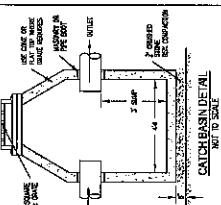
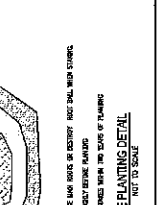
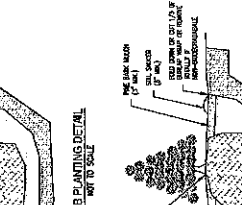
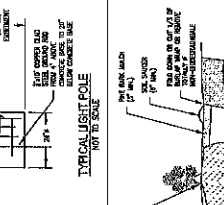
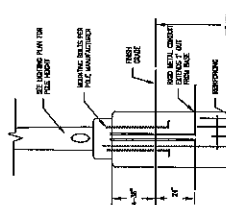
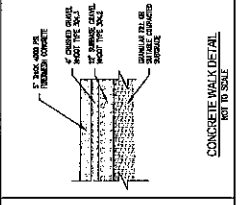
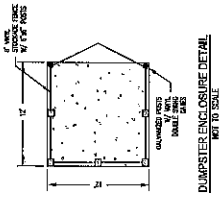
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**EROSION CONTROL MEASURES**

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DATE: 3/17/2020

PROJECT NAME: Barrington Town Hall

PROJECT NO: CC1933600

DATE: 3/17/2020

SHEET NUMBER: 17 OF 40 FT

NO DIBET INFO

TAX MAP 223

NO DIBET INFO

NO DIBET INFO

NO DIBET INFO

NO DIBET INFO

NO DIBET INFO

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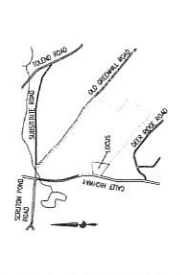
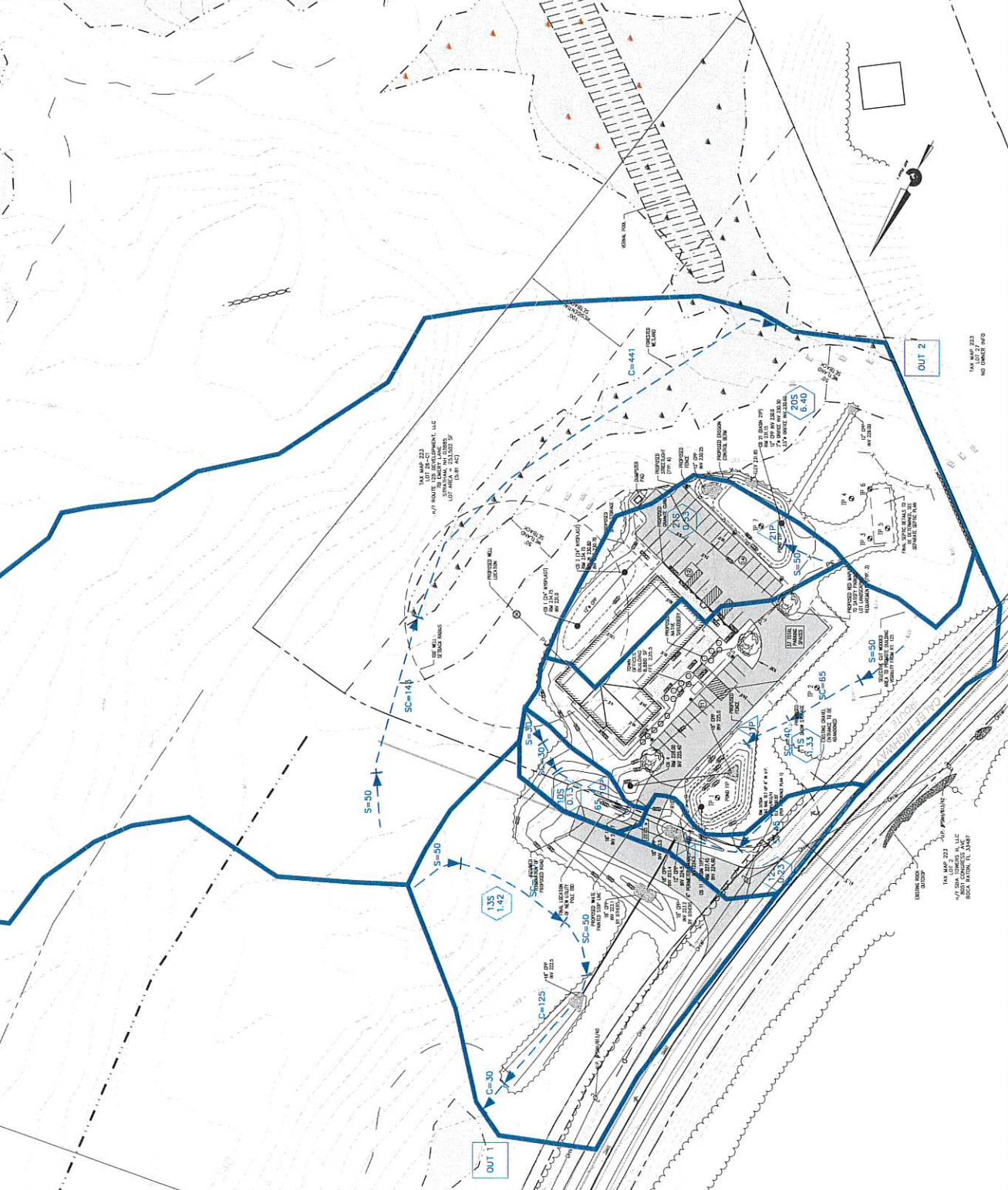
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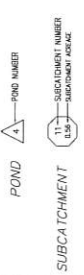


**VICINITY PLAN**  
UNIMPROVED SCALE: 1"=50'

**REFERENCE PLANS:**

1. PLAN FIELD "OPEN SPACE SUBDIVISION" PLAN FOR ESSENTIAL DEVELOPMENT, S. 125 / OLD GREEN HILL RD., BARRINGTON, NH. DATED 10/15/19. PREPARED BY: G. J. FALGOUTE, INC. (GJF) FOR: G. J. FALGOUTE, INC. ASSOCIATES, P.L.L.C. (LOR #NH-1144)
2. INFORMATION INDICATED HEREON IS BASED ON DATA OBTAINED FROM THE RECORD DRAWINGS PROVIDED BY THE TOWN OF BARRINGTON IN A DATA SET OF RECORDS PLAN 1.

- POND** POND NUMBER
- SUBCATCHMENT** SUBCATCHMENT NUMBER  
 SUBCATCHMENT PREFIX
- REACH** REACH NUMBER
- COMPONENTS**
- SOILS LEGEND**  
(NOT SHOWN ON QUANTITY SHEET B1)
- 1.0% SAND
  - 2.0% SAND
  - 3.0% SAND
  - 4.0% SAND
  - 5.0% SAND
  - 6.0% SAND
  - 7.0% SAND
  - 8.0% SAND
  - 9.0% SAND
- STRUCTURES**
- Stormwater Structures
  - Subcatchment Boundaries
  - 60% SLOPE
  - 60% SLOPE
  - High Intensity Soil Line
  - 1/2 Pipe Pitch & Direction
  - 1/2 Pipe Pitch & Direction Post-Development



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