# TRAFFIC IMPACT STUDY <br> PROPOSED MIXED-USE DEVELOPMENT <br> CALEF HIGHWAY (NH ROUTE 125) <br> BARRINGTON, NEW HAMPSHIRE 

Prepared for:
HARBOR STREET LIMITED PARTNERSHIP
Stratham, New Hampshire

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Prepared by:
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## Dear Reviewer:

This letter shall certify that this Traffic Impact Study has been prepared under my direct supervision and responsible charge. I am a Registered Professional Engineer (P.E.) in the State of New Hampshire (NH P.E. No. 9822) and hold Certification as a Professional Traffic Operations Engineer (PTOE) from the Transportation Professional Certification Board, Inc. (TPCB), an affiliate of the Institute of Transportation Engineers (ITE) (PTOE Certificate No. 993). I am also a Fellow of the Institute of Transportation Engineers (FITE).

Sincerely,
VANASSE \& ASSOCIATES, INC.

refry S. Dirk P.E., PTOE, FITE
Principal

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## EXECUTIVE SUMMARY

Vanasse \& Associates, Inc. (VAI) has conducted a Traffic Impact Study (TIS) in order to determine the potential impacts on the transportation infrastructure associated with the proposed construction of a mixed-use development to be located along the east side of NH Route 125 (Calef Highway) and south of Scruton Pond Road in Barrington, New Hampshire (hereafter referred to as the "Project"). This study was prepared in consultation with the Town of Barrington, the New Hampshire Department of Transportation (NHDOT) and the Strafford Regional Planning Commission (SRPC); was performed in general accordance with the NHDOT guidelines for the preparation of Traffic Impact Studies (TISs) and the standards of the Traffic Engineering and Transportation Planning Professions for the preparation of such reports; and is responsive to the scoping determination issued by issued by NHDOT for the Project.

Based on the analyses presented herein, we have concluded the following with respect to the Project:

1. Using trip-generation statistics published by the Institute of Transportation Engineers (ITE) ${ }^{1}$ and with adjustment to account for pass-by trips, the Project is expected to generate approximately 1,732 new vehicle trips on an average weekday and 1,064 new vehicle trips on a Saturday (both two-way volumes over the operational day of the Project), with approximately 179 new vehicle trips expected during the weekday morning peak-hour, 219 new vehicle trips expected during the weekday evening peak-hour, and 160 new vehicle trips expected during the Saturday midday peak-hour;
2. In general, the Project will not have a significant impact (increase) on motorist delays or vehicle queuing over Existing or anticipated future conditions without the Project (NoBuild conditions); however, it was noted that one or more movements at the intersection of NH Route 125 at NH Route 9 (Franklin Pierce Highway/Littleworth Road) are currently operating at or over capacity (defined as a level-of-service (LOS) of "E" or "F", respectively) independent of the Project;
3. Similar to other unsignalized intersections along the NH Route 125 corridor, motorists exiting the Project site are expected to experience delays during the peak traffic volume periods, with residual vehicle queues of up to six (6) vehicles predicted which can be

[^0]contained within the Project site without impeding access or circulation, or the movement of vehicles, pedestrians and bicyclists along NH Route 125;
4. Lines of sight at the Project site roadway intersections with NH Route 125 were found to exceed or could be made to exceed the required minimum distance for the intersections to function in a safe manner; and
5. A review of the criteria for the installation of auxiliary turn lanes at the Project site roadway intersections with NH Route 125 indicates that the addition of both a left-turn lane and a right-turn deceleration lane are justified based on the applicable criteria.

In consideration of the above, we have concluded that the Project can be accommodated within the confines of the existing transportation infrastructure in a safe and efficient manner with implementation of the recommendations that follow.

## RECOMMENDATIONS

A series of recommendations have been developed that are designed to provide safe and efficient access to the Project site and address any deficiencies identified at off-site locations evaluated in conjunction with this study. The following improvements have been recommended as a part of this evaluation and, where applicable, will be completed in conjunction with the Project subject to receipt of all necessary rights, permits and approvals.

## Project Access

Access to the Project will be provided by way of two (2) new roadways that will intersect the east side of NH Route 125 as follows: the north roadway will be situated opposite the driveway to 246-248 Calef Highway (Casella Sales \& Marketing Inc. and 603 Self-Storage); the south roadway will be located approximately 2,175 feet south of Scruton Pond Road. An access easement will also be established to allow for a future connection between the Project site and property to the north of Old Green Hill Road. The following recommendations are offered with respect to the design and operation of the Project site access and internal circulation, many of which are reflected on the Site Plans:
> The Project site roadways and internal circulating roads should be 24 -feet in width and designed to accommodate the turning and maneuvering requirements of the largest anticipated responding emergency vehicle as defined by the Barrington Fire Department.
> Vehicles exiting the Project site should be placed under STOP-sign control with a marked STOP-line provided.
> Let-turn lanes should be provided on NH Route 125 approaching both the north and south Project site roadways, with the turn lane accommodations at the north Project site roadway to include a left-turn lane in both the north and southbound directions to facilitate access to the driveway serving the driveway to 246-248 Calef Highway. The existing shoulder width along NH Route 125 (nine (9) to 10 feet) combined with properly designed corner radii for the Project site roadways will accommodate vehicles decelerating to enter the Project site without impeding the flow of traffic along NH Route 125. As such, separate right-turn deceleration lanes are not recommended at this time.
> Where perpendicular parking is proposed, the drive aisle behind the parking should be a minimum of 23 -feet in order to facilitate parking maneuvers.
> All signs and pavement markings to be installed within the Project site should conform to the applicable standards of the Manual on Uniform Traffic Control Devices (MUTCD). ${ }^{2}$
> A sidewalk should be provided along at least one side of the Project site roadways and along circulating roads within the Project site.
> Americans with Disabilities Act (ADA) compliant wheelchair ramps should be provided at all pedestrian crossings internal to the Project site.
> The embankment situated along the east side of NH Route 125 and north of the north Project site roadway should be regraded in order to provide the recommended minimum line of sight to and from the north along NH Route 125.
> Signs and landscaping to be installed as a part of the Project within intersection sight triangle areas should be designed and maintained so as not to restrict lines of sight.
> Snow windrows within sight triangle areas shall be promptly removed where such accumulations would impede sight lines.
> Bicycle parking should be provided at appropriate locations within the Project site to serve the municipal, retail and bank uses.

## Off-Site

## NH Route 125/Scruton Pond Road

The intersection of NH Route 125 at Scruton Pond Road has been identified by the Town as a priority location for a Road Safety Audit (RSA) in order to identify potential safety-related improvements at the intersection. In order to advance this effort, the Project proponent will facilitate the completion of a RSA in order to identify improvements for this intersection.

## NH Route 125/NH Route 9

One or more movements at the intersection of NH Route 125 at NH Route 9 were identified to be operating at or over capacity during the weekday and Saturday peak hours independent of the Project, with Project-related impacts defined as a predicted increase in motorist delay that resulted in a corresponding increase in vehicle queuing of up to five (5) vehicles. In an effort to reduce overall motorist delay and vehicle queuing at the intersection, the Project proponent will design and implement an optimal traffic signal timing and phasing plan subject to receipt of all necessary rights, permits and approvals.

## Transportation Demand Management Measures

Public transportation services are not currently provided in the vicinity of the Project site. In an effort to encourage the use of alternative modes of transportation to single-occupant vehicles, the following Transportation Demand Management (TDM) measures will be implemented as a part of the Project:

[^1]> Information regarding public transportation services, maps, schedules and fare information will be posted in a central location and/or otherwise made available to residents and employees;
> Tenants of the commercial components of the Project will be encouraged to offer specific amenities to discourage off-site trips, including providing a break-room equipped with a microwave and refrigerator; offering direct deposit of paychecks; coordinating with a drycleaning service for on-site pick-up and delivery; allowing telecommuting or flexible work schedules; and other such measures to reduce overall traffic volumes and travel during peak traffic volume periods;
> Pedestrian and bicycle accommodations will be incorporated into the Project including sidewalks and bicycle parking in appropriate locations; and
$>$ To the extent that public transportation services are provided along NH Route 125 in the future, an area should be reserved for a bus stop to be established.

With implementation of the above recommendations, safe and efficient vehicular, pedestrian and bicycle access will be provided to the Project site and the Project can be accommodated within the confines of the existing and improved transportation system.

## INTRODUCTION

Vanasse \& Associates, Inc. (VAI) has conducted a Traffic Impact Study (TIS) in order to determine the potential impacts on the transportation infrastructure associated with the proposed construction of a mixed-use development to be located along the east side of NH Route 125 (Calef Highway) and south of Scruton Pond Road in Barrington, New Hampshire (hereafter referred to as the "Project"). This study evaluates the following specific areas as they relate to the Project: i) access requirements; ii) potential off-site improvements; and iii) safety considerations; and identifies and analyzes existing traffic conditions and future traffic conditions, both with and without the Project, along NH Route 25 and at the following intersections defined in consultation with NHDOT: NH Route 125 at Greenhill Road and Tolend Road; NH Route 125 at Scruton Pond Road; and NH Route 125 at Franklin Pierce Highway and Littleworth Road (NH Route 9).

## PROJECT DESCRIPTION

The Project will entail the phased construction of a mixed-use development that will include: 55 single-family homes; $53,200 \pm$ square feet (sf) of commercial space that may include retail and office space, a bank with a drive-through teller facility, contractor's storage and warehouse space; and donation of a parcel of land to the Town of Barrington for a municipal use. The Project site is located on two parcels of land situated along the east side of NH Route 125 and south of Scruton Pond Road (Town of Barrington Tax Map 223, Lots 24 and 26), and contains areas of open and wooded space and low-lying wetland areas. Figure 1 depicts the Project site location in relation to the existing roadway network.

Access to the Project will be provided by way of two (2) new roadways that will intersect the east side of NH Route 125 as follows: the north roadway will be situated opposite the driveway to 246-248 Calef Highway (Casella Sales \& Marketing Inc. and 603 Self-Storage); the south roadway will be located approximately 2,175 feet south of Scruton Pond Road. An access easement will also be established to allow for a future connection between the Project site and property to the north of Old Green Hill Road.

On-site parking will be provided for the individual land uses in accordance with the requirements of the Town of Barrington Zoning Ordinance.


## STUDY METHODOLOGY

This study was prepared in consultation with the Town of Barrington, the New Hampshire Department of Transportation (NHDOT) and the Strafford Regional Planning Commission (SRPC); was performed in general accordance with: i) the NHDOT guidelines for the preparation of Traffic Impact Studies (TISs); ii) the standards of the Traffic Engineering and Transportation Planning Professions for the preparation of such reports; and iii) the scoping determination issued by NHDOT for the Project; and was conducted in three distinct stages.

The first stage of the study involved an assessment of existing conditions in the study area and included an inventory of roadway geometrics, pedestrian and bicycle facilities and public transportation services; observations of traffic flow; and the collection of daily and peak-period traffic counts.

In the second stage of the study, future conditions on the transportation system were projected and analyzed. Specific travel demand forecasts for the Project were assessed along with future demands on the transportation system that are expected due to growth independent of the Project. In accordance with NHDOT guidelines for the preparation of TISs and the scoping determination issued by NHDOT for the Project, four (4) future conditions were evaluated: 1) 2020 No-Build conditions without the Project; 2) 2020 Opening-Year Build conditions with the Project; 3) 2030 No-Build conditions without the Project; and 4) 2030 Build conditions (ten-year projection from opening-year) with the Project. The analyses conducted in stage two of the study identify existing or projected future roadway capacity and traffic safety issues.

The third stage of the study presents and evaluates measures to address roadway and intersection capacity issues and safety concerns, if any, identified in stages one and two of the study.

## EXISTING CONDITIONS

A comprehensive field inventory of existing conditions on the study area roadways was conducted in March 2019. The field investigation consisted of an inventory of existing roadway geometrics; pedestrian and bicycle facilities; traffic volumes; and operating characteristics; as well as posted speed limits and land use information within the study area. The study area that was evaluated for the Project was defined as a part of the scoping determination issued by NHDOT for the preparation of this study and included NH Route 25 and the following intersections: NH Route 125 at Greenhill Road and Tolend Road; NH Route 125 at Scruton Pond Road; and NH Route 125 at Franklin Pierce Highway (NH Route 9).

The following describes the study area roadway and intersections.

## GEOMETRY

## Roadway

## NH Route 125 (Calef Highway)

NH Route 125 (Calef Highway) is a two-lane arterial roadway (Tier 2, Class II) under NHDOT jurisdiction that traverses the study area in a general north-south direction and provides access to the City of Rochester and NH Route 16 to the north of the study area and to US Route 4 to the south. Within the study area, NH Route 125 provides two 12 to 13 -foot wide travel lanes separated by a double-yellow centerline with 2 to 10 -foot wide marked shoulders and additional travel lanes provided at major intersections. Sidewalks are not provided along NH Route 125 within the study area. Illumination is provided intermittently by street lights mounted on wood or steel poles. The posted speed limit along NH Route 125 varies from 35 to 50 miles per hour (mph). Land use along NH Route 125 within the study area consists of residential, commercial and municipal properties, and areas of open and wooded space.

## Intersections

Table 1 and Figure 2 summarize lane use, traffic control, and pedestrian and bicycle accommodations at the study area intersections as observed in March 2019.

Table 1 STUDY AREA INTERSECTION DESCRIPTION

| Intersection | Traffic Control Type ${ }^{\text {a }}$ | No. of Travel Lanes Provided | Shoulder Provided? (Yes/No/Width) | Pedestrian <br> Accommodations? <br> (Yes/No/Description) | Bicycle <br> Accommodations? <br> (Yes/No/Description) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NH Rte. 125/ Greenhill Rd./ Tolend Rd. | TS | 1 left-turn lane, 1 through lane and 1 right-turn lane on NH Rte. 125 approaches; 1 general-purpose travel lane on Greenhill Rd. and Tolend Rd. | Yes; 2-4-feet on all approaches | No | Yes; Shared traveledway ${ }^{\text {b }}$ |
| NH Rte. 125/ <br> Scruton Pond Rd. | S | 1 general purpose travel lane on all approaches | Yes; 1-foot on Scruton Pond Rd. and 8 to 10 -feet on NH Rte. 125 | No | Yes; Shared traveledway on NH Rte. 125 |
| NH Rte. 125/ NH Rte. 9 | TS | 1 left-turn lane, 1 through lane and 1 right-turn lane on NH Rte. 125 northbound approach; 1 left-turn lane, 1 through lane and 1 through/right-turn lane on NH Rte. 125 southbound approach; 1 left-turn lane, 1 through lane and 1 rightturn lane on NH Rte. 9 approaches | Yes; 5 to 6-feet on NH Rte. 125 and 2 to 10 feet on NH Rte. 9 | No | Yes; Shared traveledway |

${ }^{\text {a }}$ TS $=$ traffic signal control; $\mathrm{S}=$ STOP-sign control; $\mathrm{Y}=$ YIELD-sign control; $\mathrm{R}=$ rotary/roundabout control; NC = no control present. ${ }^{\mathrm{b}}$ Combined shoulder and travel lane width equal to or exceed 14 feet.

## EXISTING TRAFFIC VOLUMES

In order to determine existing traffic-volume demands and flow patterns within the study area, automatic traffic recorder (ATR) counts, manual turning movement counts (TMCs) and vehicle classification counts were completed in March 2019. The ATR counts were conducted on NH Route 125 south of Scruton Pond Road over a continuous 72 -hour period from March $7^{\text {th }}$ (Thursday) through $9^{\text {th }}$ (Saturday) in order to record weekday daily and Saturday traffic conditions along this roadway over an extended period, with weekday morning (7:00 to 9:00 AM) and evening (4:00 to 6:00 PM) peak period manual TMCs performed at the study intersections on March 7, 2019 (Thursday), and during the Saturday midday peak period (11:00 AM to 2:00 PM) on March 9, 2019 in accordance with the scoping determination issued by NHDOT for the preparation of this study. These time periods were selected for analysis purposes as they are representative of the peak traffic volume hours for both the Project and the adjacent roadway network.

## Legend:

(S) Signalized Intersection
(1) Unsignalized Intersection
= - Unpaved Gravel Roadway
$x x^{-}-\quad$ Lane Use and Travel Lane
Width


## Seasonal Adjustments

In order to evaluate the potential for seasonal fluctuation of traffic volumes within the study area, 2018 peak-hour and average daily traffic count data were reviewed for NHDOT count station No. 02389090 , which is located on Spaulding Turnpike (NH Route 16), south of NH Route 125 (Exit 12), in Rochester. Based on a review of this data, it was determined that traffic volumes for the month of March are approximately 33 percent below peak-month conditions and, therefore, the raw traffic count data that forms the basis of this assessment was adjusted upward accordingly to represent peak-month conditions.

The 2019 Existing weekday morning, weekday evening and Saturday midday peak-month, peakhour traffic volumes are depicted on Figure 3 and are summarized in Table 1. Note that the peakhour traffic volumes referenced in Table 1 were obtained from the TMCs and are reflected on the aforementioned figure.

Table 1
2019 EXISTING PEAK-MONTH TRAFFIC VOLUMES

| Location/Peak Hour |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

${ }^{a}$ Average weekday traffic in vehicles per day.
${ }^{\mathrm{b}}$ Vehicles.
${ }^{\mathrm{c}}$ Vehicles per hour.
${ }^{\text {d Percent }}$ of daily traffic occurring during the peak hour.
${ }^{\text {e }}$ Percent traveling in peak direction.
$\mathrm{NB}=$ northbound; $\mathrm{SB}=$ southbound.

As can be seen in Table 2, NH Route 125 in the vicinity of the Project site was found to accommodate approximately 20,230 vehicles on an average weekday and 17,050 vehicles on a Saturday (two-way, 24 -hour volumes), with approximately 1,720 vehicles per hour (vph) during the weekday morning peak-hour, $1,733 \mathrm{vph}$ during the weekday evening peak-hour and $1,415 \mathrm{vph}$ during the Saturday midday peak-hour.

## PEDESTRIAN AND BICYCLE FACILITIES

A comprehensive field inventory of pedestrian and bicycle facilities within the study area was undertaken in March 2019. The field inventory consisted of a review of the location of sidewalks and pedestrian crossing locations along the study roadway and at the study intersection, as well as the location of existing and planned future bicycle facilities. Sidewalks and formal bicycle facilities are not currently provided within the study area. That being said, the study area roadways generally provide sufficient width (combined travel lane and shoulder) to support bicycle travel in a shared traveled-way condition ${ }^{3}$ and NH Route 125 is designated as a bike route.

[^2]WEEKDAY MORNING PEAK HOUR (7:00-8:00 AM)

## WEEKDAY EVENING PEAK HOUR

 (4:00-5:00 PM)SATURDAY MIDDAY PEAK HOUR (11:00 AM - 12:00 PM)




## Not To Scale

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## Figure 3

## 2019 Existing

Peak Month
Peak Hour Traffic Volumes

## PUBLIC TRANSPORTATION

Regularly scheduled public transportation services are not currently provided within the study area. The closest public transportation options are available in the Cities of Dover and Rochester, where bus services are provided by the Cooperative Alliance For Seacoast Transportation (COAST). Regional bus services are available at the Portsmouth Transportation Center and air transportation is available at the Portsmouth International Airport.

## SPOT SPEED MEASUREMENTS

Vehicle travel speed measurements were performed on NH Route 125 in the vicinity of the Project site over a continuous 72 -hour period (Thursday through Saturday) in conjunction with the ATR counts. Table 3 summarizes the results of the vehicle travel speed measurements.

Table 3
VEHICLE TRAVEL SPEED MEASUREMENTS

|  | NH Route 125 |  |
| :--- | :---: | :---: |
|  | Northbound | Southbound |
| Mean Travel Speed (mph) | 55 | 53 |
| $85^{\text {th }}$ Percentile Speed (mph) | 59 | 58 |
| Posted Speed Limit (mph) | 50 | 50 |

$\mathrm{mph}=$ miles per hour.

As can be seen in Table 3, the mean vehicle travel speed along NH Route 125 in the vicinity of the Project site was found to be approximately 55 mph in the northbound direction and 53 mph southbound. The average measured $85^{\text {th }}$ percentile vehicle travel speed, or the speed at which 85 percent of the observed vehicles traveled at or below, was found to be approximately 59 mph northbound and 58 mph southbound, which is 8 to 9 mph above the posted speed limit in the vicinity of the Project site ( 50 mph ). The $85^{\text {th }}$ percentile speed is used as the basis of engineering design and in the evaluation of sight distances, and is often used in establishing posted speed limits.

## MOTOR VEHICLE CRASH DATA

A town-wide assessment of motor vehicle crashes was completed by the Barrington Police Department in 2018 in order to prioritize funding for Road Safety Audits (RSAs). This assessment identified that three roadways accounted for 62 percent of the total number of motor vehicle crashes that were reported within the Town: NH Route 125, NH Route 9 and Washington Street (NH Route 202). For the 10-year period 2008 through 2017, NH Route 125 was reported to have experienced an average of approximately 42 crashes per year, with 76 crashes reported to have occurred at the NH Route $125 / \mathrm{NH}$ Route 9 intersection and 13 crashes reported at the NH Route 125/Scruton Pond Road intersection (one of which resulted in a fatality). The NH Route 125 /Greenhill Road/Tolend Road intersection was not directly included in the
assessment; however, a 2012 Conference Report prepared by NHDOT in reference to the then planned (and subsequently completed) installation of a traffic control signal and associated intersection geometric improvements was included in the attachments. At that time, a total of 21 motor vehicle crashes were reported at the NH Route 125/Greenhill Road/Tolend Road intersection, one of which resulted in a fatality. A review of NHDOT crash mapping for the period 2002 through 2016 indicates that 35 crashes were reported at or in the vicinity of the NH Route 125/Greenhill Road/Tolend Road intersection.

The crash assessment concluded that while the NH Route $125 / \mathrm{NH}$ Route 9 intersection experienced the highest number of motor vehicle crashes, the improvements that have been completed at the intersection have reduced the severity of the crashes. A similar conclusion was inferred for the NH Route 125/Greenhill Road/Tolend Road intersection, as this intersection was also the subject of recently completed improvements. The NH Route $125 /$ Scruton Pond Road intersection was specifically identified by the Police Department as a priority location for a RSA, with identified concerns relating to approach speeds and the horizontal and vertical alignment of NH Route 125 approaching the intersection. Specific recommendations to advance safety-related improvements at this intersection have been identified and are detailed in the Recommendations section of this assessment.

## FUTURE CONDITIONS

Traffic volumes in the study area were projected to the years 2020 and 2030, which reflect the anticipated opening-year of the Project and a ten-year planning horizon from opening-year, respectively, consistent with NHDOT traffic study guidelines and the scoping determination issued by NHDOT for the preparation of this study. The future condition traffic-volume projections incorporate identified specific development projects by others, as well as general background traffic growth as a result of development external to the study area and presently unforeseen projects. Anticipated Project-generated traffic volumes superimposed upon the 2020 and 2030 No-Build traffic volumes reflect the Build conditions with the Project.

## FUTURE TRAFFIC GROWTH

Future traffic growth is a function of the expected land development in the immediate area and the surrounding region. Several methods can be used to estimate this growth. A procedure frequently employed estimates an annual percentage increase in traffic growth and applies that percentage to all traffic volumes under study. The drawback to such a procedure is that some turning volumes may actually grow at either a higher or a lower rate at particular intersections.

An alternative procedure identifies the location and type of planned development, estimates the traffic to be generated, and assigns it to the area roadway network. This procedure produces a more realistic estimate of growth for local traffic. However, the drawback of this procedure is that the potential growth in population and development external to the study area would not be accounted for in the traffic projections.

To provide a conservative analysis framework, both procedures were used, the salient components of which are described below.

## Specific Development By Others

The Town of Barrington Land Use Department and NHDOT were contacted in order to determine if there were any projects planned within the study area that would have an impact on future traffic volumes at the study intersections. Based on these discussions, the following project was identified for review in conjunction with this assessment:
>Convenience Store/Gas Station, 491 Calef Highway, Barrington, New Hampshire. This project is currently under construction and includes a $5,000 \pm$ sf convenience store and an associated gasoline fueling facility.

Traffic volumes associated with the aforementioned specific development project by others were obtained from the Traffic Impact and Site Access Study that was prepared by Pernaw \& Company, Inc. in support of the project and using trip-generation information available from the Institute of Transportation Engineers (ITE) ${ }^{4}$ for the appropriate land use, and were assigned onto the study area roadway network based on existing traffic patterns where no other information was available. No other developments were identified at this time that are expected to result in an increase in traffic within the study area beyond the general background traffic growth rate.

## General Background Traffic Growth

A review of historic traffic growth information compiled by NHDOT for the Town of Barrington was undertaken in order to determine general traffic growth trends. Based on a review of this data and consistent with the scoping determination issued by NHDOT for the preparation of this study, a 1.0 percent per year compounded annual background traffic growth rate was used in order to account for future traffic growth and presently unforeseen development within the study area.

## Roadway Improvement Projects

The Town of Barrington and NHDOT were contacted in order to determine if there were any planned roadway improvement projects expected to be completed within the study area. Based on these discussions, no roadway improvement projects aside from routine maintenance activities were identified to be planned within the study area at this time.

## No-Build Traffic Volumes

The 2020 and 2030 No-Build peak-month peak-hour traffic volumes were developed by applying the 1.0 percent per year compounded annual background traffic growth rate to the 2019 Existing peak-month peak-hour traffic volumes and then adding the traffic associated with the identified specific development project by others. The resulting 2020 No-Build weekday morning, weekday evening and Saturday midday peak-month peak-hour traffic volumes are shown on Figure 4, with the corresponding 2030 No-Build peak-month peak-hour traffic volumes shown on Figure 5.

## PROJECT-GENERATED TRAFFIC

Design year (2020 and 2030) Build traffic volumes for the study area roadways were determined by estimating Project-generated traffic volumes and assigning these volumes on the study roadways. The following sections describe the procedures used to develop the Build condition traffic volume networks.

The Project will entail the phased construction of a mixed-use development that will include: 55 single-family homes; $53,200 \pm$ sf of commercial space that may include retail and office space, a bank with a drive-through teller facility, contractor's storage and warehouse space; and donation of a parcel of land to the Town of Barrington for a municipal use. In order to develop the traffic

[^3]WEEKDAY MORNING PEAK HOUR (7:00-8:00 AM)

## WEEKDAY EVENING PEAK HOUR

(4:00-5:00 PM)

(11:00 AM - 12:00 PM)


Note: Imbalances exist due to numerous curb cuts and side streets that are not shown.

## Not To Scale

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## Figure 4

2020 No-Build
Peak Month
Peak Hour Traffic Volumes

WEEKDAY MORNING PEAK HOUR (7:00-8:00 AM)

WEEKDAY EVENING PEAK HOUR
(4:00-5:00 PM)
SATURDAY MIDDAY PEAK HOUR (11:00 AM - 12:00 PM)




Note: Imbalances exist due to numerous curb cuts and side streets that are not shown.

## Not To Scale

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## Figure 5

2030 No-Build
Peak Month
Peak Hour Traffic Volumes
characteristics of the Project, trip-generation statistics published by the ITE ${ }^{5}$ for similar land uses as those proposed were used. ITE Land Use Codes (LUCs) 150, Warehousing; 180, Specialty Trade Contractor; 210, Single-Family Detached Housing; 710, General Office; 730, Government Office Building; 820, Shopping Center; and 912, Drive-In Bank; were used to establish the base trip-generation calculations for the Project.

## Internal Trips

It is expected that a portion of the residents, employees and customers of the Project may visit one or more of the uses that are proposed within the development, such as a resident that visits the municipal building, shops at the retail store or patronizes the bank. Such trips remain "internal" to the Project site and do not constitute additional traffic "external" to the site. This interaction between uses is not accounted for when the traffic volume projections are completed on an individual land use basis. Given that the exact uses other than the municipal building are not yet defined, an internal trip credit (reduction) was not applied to the base trip-generation calculations for the Project.

## Pass-By Trips

Not all of the trips expected to be generated by the retail and bank components of the Project will be new trips on the roadway network. A significant portion of these trips will consist of pass-by trips or vehicles already traveling along NH Route 125 for other purposes that will patronize the Project in conjunction with their trip and then continue on to their original destination. These trips are not new trips on the roadway network as a result of the Project. Statistics published by the ITE ${ }^{6}$ indicate that on average, up to 34 percent of the trips generated by retail uses and 38 percent of the trips generated by a bank with drive-through window may consist of pass-by trips. As such and pursuant to scoping determination issued by NHDOT for the preparation of this study, a pass-by trip rate of up to 34 percent was applied to the trip-generation calculations for the retail component of the Project and pass-by trip rate of up to 38 percent was applied to the bank component.

Table 4 summarizes the anticipated traffic characteristics of the Project using the above methodology.

[^4]Table 4
TRIP GENERATION SUMMARY

| Time Period/Direction |  |  | (C) <br> $\begin{array}{l}\text { Municipal } \\ \text { Building } \\ (10,000 \text { sf) }\end{array}$ | $\begin{gathered} \text { (D) } \\ \begin{array}{c} \text { (Darehouse } \\ (8,000 \\ \text { sf })^{d} \end{array} \\ \hline \end{gathered}$ | (E) <br> Contractor/Trade Storage Building (14,000 sf) | $\begin{gathered} \text { (F) } \\ \text { Retail Space } \\ (8,000 \text { sf) } \\ \hline \end{gathered}$ | $\begin{gathered} \text { (G) } \\ \text { Bank } \\ (3,200 \mathrm{sf})^{\mathrm{g}} \end{gathered}$ | $\begin{gathered} (\mathrm{H}=\mathrm{A}+\mathrm{B}+\mathrm{C}+ \\ \mathrm{D}+\mathrm{E}+\mathrm{E}+\mathrm{F}+\mathrm{G}) \\ \text { Total } \\ \text { Trips } \\ \hline \end{gathered}$ | $\begin{gathered} \text { (I) } \\ \begin{array}{c} \text { Pass-By } \\ \text { Trips } \\ \hline \end{array} \\ \hline \end{gathered}$ | $\begin{aligned} & (\mathrm{J}=\mathrm{H}-\mathrm{I}) \\ & \text { New Trips } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Average Weekday Daily |  |  |  |  |  |  |  |  |  |  |
| Entering | 300 | 112 | 113 | 29 | 72 | 151 | 191 | 968 | 102 | 866 |
| Exiting | 300 | 112 | $\frac{113}{26}$ | $\underline{29}$ | 72 | 151 | 191 | 968 | 102 | 866 |
| Total | 600 | 224 | 226 | 58 | 144 | 302 | 382 | 1,936 | 204 | 1,732 |
| Weekday Morning Peak Hour |  |  |  |  |  |  |  |  |  |  |
| Entering | 11 | 20 | 25 | 20 | 17 | 5 | 17 | 115 | 4 | 111 |
| Exiting | 33 | 3 | 8 | 6 | 6 | 3 | 13 | 72 | 4 | 68 |
| Total | 44 | 23 | 33 | 26 | 23 | 8 | 30 | 187 | 8 | 179 |
| Weekday Evening Peak Hour |  |  |  |  |  |  |  |  |  |  |
| Entering | 36 | 4 | 4 | 8 | 9 | 14 | 32 | 107 | 16 | 91 |
| Exiting | $\frac{21}{57}$ | $\frac{21}{25}$ | $\frac{13}{17}$ | 21 | 19 | 16 | $\frac{33}{6}$ | 144 | 16 | 128 |
| Total | 57 | 25 | 17 | 29 | 28 | 30 | 65 | 251 | 32 | 219 |
| Saturday |  |  |  |  |  |  |  |  |  |  |
| Entering | 280 | 22 | 0 | 1 | 6 | 185 | 139 | 633 | 101 | 532 |
| Exiting | 280 | $\underline{22}$ | $\underline{0}$ | $\frac{1}{2}$ | 6 | $\frac{185}{370}$ | $\frac{139}{}$ | 633 | $\frac{101}{}$ | 532 |
| Total | 560 | 44 | 0 | 2 | 12 | 370 | 278 | 1,266 | 202 | 1,064 |
| Saturday Midday Peak Hour |  |  |  |  |  |  |  |  |  |  |
| Entering | 35 | 6 | 0 | 0 | 2 | 19 | 43 | 105 | 21 | 84 |
| Exiting | $\frac{29}{64}$ | $\frac{5}{11}$ | $\underline{0}$ | $\underline{0}$ | 5 | 17 | 41 | 97 | 21 | 76 |
| Total | 64 | 11 | 0 | 0 | 7 | 36 | 84 | 202 | 42 | 160 |

Based on ITE LUC 210, Single-Family Detached
Based on ITE LUC 710, General Office Building.
Based on ITE LUC 730, Goverrment Office Building. Closed on Saturday
'Based on ITE LUC 150, Warehousing.
'Based on ITE LUC 180, Specialty Trade Contractor. Saturday trip projections were developed using a proportionate ratio of the Saturday trip rate to the average weekday trip rate and the weekday evening peak-hour trip Based on ITE LUC 820, Shopping Center.
Based on ITE LUC 912, Drive-in Bank.
A Pass-by trip rate was applied to the traffic volumes associated with the retail and bank uses as follows: Retail- average weekday daily - 30 percent; weekday morning peak-hour -0 percent; weekday evening peak-hour -
34 percent; Saturday and Saturday midday peak-hour -26 percent; Bank- average weekday daily -30 percent; weekday morning peak-hour -29 percent; weekday evening peak-hour -35 percent; Saturday and Saturday midday peak-hour- 38 percent.

## Project-Generated Traffic Summary

As can be seen in Table 4, using the aforementioned methodology and after applying reductions to account for pass-by trips, the Project is expected to generate approximately 1,732 new vehicle trips on an average weekday and 1,064 new vehicle trips on a Saturday (both two-way volumes over the operational day of the Project), with approximately 179 new vehicle trips ( 111 vehicles entering and 68 exiting) expected during the weekday morning peak-hour, 219 new vehicle trips ( 91 vehicles entering and 128 exiting) expected during the weekday evening peak-hour, and 160 new vehicle trips ( 84 vehicles entering and 76 exiting) expected during the Saturday midday peak-hour.

## TRIP DISTRIBUTION AND ASSIGNMENT

Separate trip-distribution patterns were developed for the residential and commercial components of the Project given the differing nature and purpose of the trips associated with these uses. For the residential component of the Project, the directional distribution was determined based on a review of Journey-to-Work data obtained from the U.S. Census for persons residing in the Town of Barrington and then refined based on a review of existing traffic patterns within the study area during the peak periods. For the commercial component of the Project, the directional distribution was determined based on a review of existing traffic patterns within the study area. The general trip distribution for the commercial and residential components for the Project are graphically depicted on Figures 6 and 7, respectively. Traffic volumes expected to be generated by the Project were assigned onto the study area roadway network as shown on Figure 8.

## FUTURE TRAFFIC VOLUMES - BUILD CONDITION

The 2020 Opening-Year and 2030 Build condition traffic-volumes were developed by adding Project-generated traffic to the corresponding 2020 and 2030 No-Build peak-month peak-hour traffic-volumes. The resulting 2020 Opening-Year Build condition weekday morning, weekday evening and Saturday midday peak-month peak-hour traffic volumes are graphically depicted on Figure 9, with the corresponding 2030 Build condition peak-month peak-hour traffic volumes depicted on Figure 10.

A summary of peak-hour projected traffic-volume increases outside of the study area that is the subject of this assessment is shown in Table 5. These volumes are based on the expected increases from the Project.




WEEKDAY MORNING PEAK HOUR (7:00-8:00 AM)

WEEKDAY EVENING PEAK HOUR
(4:00-5:00 PM)
SATURDAY MIDDAY PEAK HOUR
(11:00-12:00 PM)



$\quad$| SITE  <br> In 105 <br> Out 97 <br> Total $\frac{902}{202}$ |
| :--- |


| SIE |
| ---: | ---: |
| ln 105 <br> Out 97 <br> Total 202 |


| SIE |  |
| :--- | :--- |
| In | 105 |
| Out | 97 |
| Total | 202 |



Note: Imbalances exist due to numerous curb cuts and side streets that are not shown.

WEEKDAY MORNING PEAK HOUR (7:00-8:00 AM)



SITE

## Not To Scale

Vanasse \& Associates, Inc.
Transportation Engineers \& Planners

WEEKDAY EVENING PEAK HOUR
(4:00-5:00 PM)
SATURDAY MIDDAY PEAK HOUR (11:00-12:00 PM)





Note: Imbalances exist due to numerous curb cuts and side streets that are not shown.

## Figure 10

2030 Opening-Year Build Peak Hour Traffic Volumes Peak Month Conditions

Table 5
PEAK-HOUR TRAFFIC-VOLUME INCREASES

| Location/Peak Hour | $2019$ <br> Existing | $\begin{gathered} 2020 / 2030 \\ \text { No-Build } \end{gathered}$ | $\begin{gathered} 2020 / 2030 \\ \text { Build } \\ \hline \end{gathered}$ | Traffic <br> Volume <br> Increase <br> Over <br> No-Build <br> $(2020 / 2030)$ | Percent Increase Over No-Build (2020/2030) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NH Route 125, north of Greenhill Road/ |  |  |  |  |  |
| Tolend Road: |  |  |  |  |  |
| Weekday Morning | 1,591 | 1,605/1,801 | 1,676/1,872 | 71 | 4.4/3.9 |
| Weekday Evening | 1,674 | 1,711/1,890 | 1,796/1,975 | 85 | 5.0/4.5 |
| Saturday Midday | 1,348 | 1,376/1,519 | 1,430/1,573 | 54 | 3.9/3.6 |
| NH Route 125, south of NH Route 9: |  |  |  |  |  |
| Weekday Morning | 1,933 | 1,978/2,181 | 2,028/2,231 | 50 | 2.5/2.3 |
| Weekday Evening | 2,042 | 2,085/2,400 | 2,146/2,461 | 61 | 2.9/2.5 |
| Saturday Midday | 1,566 | 1,597/1,762 | 1,642/1,807 | 45 | 2.8/2.6 |
| Tolend Road, east of NH Route 125: |  |  |  |  |  |
| Weekday Morning | 136 | 136/152 | 146/162 | 10 | 7.4/6.6 |
| Weekday Evening | 183 | 184/206 | 195/217 | 11 | 6.0/5.3 |
| Saturday Midday | 137 | 137/152 | 148/163 | 11 | 8.0/7.2 |
| Greenhill Road, west of NH Route 125: |  |  |  |  |  |
| Weekday Morning | 224 | 227/252 | 236/261 | 9 | 4.0/3.6 |
| Weekday Evening | 249 | 253/282 | 265/294 | 12 | 4.7/4.3 |
| Saturday Midday | 198 | 202/222 | 208/228 | 6 | 3.0/2.7 |
| NH Route 9, east of NH Route 125: |  |  |  |  |  |
| Weekday Morning | 1,344 | 1,382/1,523 | 1,397/1,538 | 15 | 1.1/1.0 |
| Weekday Evening | 1,203 | 1,236/1,408 | 1,253/1,425 | 17 | 12.2/11.3 |
| Saturday Midday | 904 | 926/1,023 | 941/1,038 | 15 | 1.6/1.5 |
| NH Route 9, west of NH Route 125: |  |  |  |  |  |
| Weekday Morning | 1,121 | 1,070/1,179 | 1,091/1,200 | 21 | 2.0/1.8 |
| Weekday Evening | 1,108 | 1,136/1,251 | 1,165/1,280 | 29 | 2.6/2.3 |
| Saturday Midday | 951 | 972/1,073 | 997/1,098 | 25 | 2.6/2.3 |
| Scruton Pond Road, west of NH Route 125: |  |  |  |  |  |
| Weekday Morning | 115 | 115/129 | 118/132 | 3 | 2.6/2.3 |
| Weekday Evening | 116 | 116/130 | 120/134 | 4 | 3.4/3.1 |
| Saturday Midday | 133 | 134/148 | 138/152 | 4 | 3.0/2.7 |

As shown in Table 5, Project-related traffic-volume increases outside of the study area relative to 2020 and 2030 No-Build conditions are anticipated to range from 1.0 to 12.2 percent during the peak periods, with vehicle increases shown to range from 3 to 85 vehicles. When dispersed over the peak-hour, such increases would not result in a significant impact (increase) on motorist delays or vehicle queuing outside of the immediate study area that is the subject of this assessment.

## TRAFFIC OPERATIONS ANALYSIS

Measuring existing and future traffic volumes quantifies traffic flow within the study area. To assess quality of flow, roadway capacity and vehicle queue analyses were conducted under Existing, No-Build and Build traffic volume conditions. Capacity analyses provide an indication of how well the roadway facilities serve the traffic demands placed upon them, with vehicle queue analyses providing a secondary measure of the operational characteristics of an intersection or section of roadway under study.

## METHODOLOGY

## Levels of Service

A primary result of capacity analyses is the assignment of level of service to traffic facilities under various traffic-flow conditions. ${ }^{7}$ The concept of level of service is defined as a qualitative measure describing operational conditions within a traffic stream and their perception by motorists and/or passengers. A level-of-service definition provides an index to quality of traffic flow in terms of such factors as speed, travel time, freedom to maneuver, traffic interruptions, comfort, convenience, and safety.

Six levels of service are defined for each type of facility. They are given letter designations from A to F , with level-of-service (LOS) A representing the best operating conditions and LOS F representing congested or constrained operating conditions.

Since the level of service of a traffic facility is a function of the traffic flows placed upon it, such a facility may operate at a wide range of levels of service, depending on the time of day, day of week, or period of year.

[^5]
## Signalized Intersections

The six levels of service for signalized intersections may be described as follows:

- LOS A describes operations with very low control delay; most vehicles do not stop at all.
- LOS B describes operations with relatively low control delay. However, more vehicles stop than LOS A.
- LOS C describes operations with higher control delays. Individual cycle failures may begin to appear. The number of vehicles stopping is significant at this level, although many still pass through the intersection without stopping.
- LOS D describes operations with control delay in the range where the influence of congestion becomes more noticeable. Many vehicles stop and individual cycle failures are noticeable.
- LOS $E$ describes operations with high control delay values. Individual cycle failures are frequent occurrences.
- LOS $F$ describes operations with high control delay values that often occur with oversaturation. Poor progression and long cycle lengths may also be major contributing causes to such delay levels.

Levels of service for signalized intersections are calculated using the operational analysis methodology of the 2000 Highway Capacity Manual and implemented as a part of the Synchro ${ }^{\circledR} 10$ software. This method assesses the effects of signal type, timing, phasing, and progression; vehicle mix; and geometrics on delay. Level-of-service designations are based on the criterion of control or signal delay per vehicle. Control or signal delay is a measure of driver discomfort, frustration, and fuel consumption, and includes initial deceleration delay approaching the traffic signal, queue move-up time, stopped delay and final acceleration delay. Table 6 summarizes the relationship between level of service and control delay. The tabulated control delay criterion may be applied in assigning level-of-service designations to individual lane groups, to individual intersection approaches, or to entire intersections.

Table 6
LEVEL-OF-SERVICE CRITERIA FOR SIGNALIZED INTERSECTIONS ${ }^{\text {a }}$

|  | Control (Signal) Delay <br> Per Vehicle (Seconds) |
| :---: | :---: |
| A | $\leq 10.0$ |
| B | 10.1 to 20.0 |
| C | 20.1 to 35.0 |
| D | 35.1 to 55.0 |
| E | 55.1 to 80.0 |
| F | $>80.0$ |

${ }^{\text {a Source: }}$ Highway Capacity Manual, Transportation Research Board;
Washington, DC; 2000; page 16-2.

## Unsignalized Intersections

The six levels of service for unsignalized intersections may be described as follows:

- $\operatorname{LOS} A$ represents a condition with little or no control delay to minor street traffic.
- LOS B represents a condition with short control delays to minor street traffic.
- LOS C represents a condition with average control delays to minor street traffic.
- LOS D represents a condition with long control delays to minor street traffic.
- LOS E represents operating conditions at or near capacity level, with very long control delays to minor street traffic.
- LOS F represents a condition where minor street demand volume exceeds capacity of an approach lane, with extreme control delays resulting.

The levels of service of unsignalized intersections are determined by application of a procedure described in the 2010 Highway Capacity Manual. ${ }^{8}$ Level of service is measured in terms of average control delay. Mathematically, control delay is a function of the capacity and degree of saturation of the lane group and/or approach under study and is a quantification of motorist delay associated with traffic control devices such as traffic signals and STOP signs. Control delay includes the effects of initial deceleration delay approaching a STOP sign, stopped delay, queue move-up time, and final acceleration delay from a stopped condition. Definitions for level of service at unsignalized intersections are also given in the 2010 Highway Capacity Manual. Table 7 summarizes the relationship between level of service and average control delay for two way stop controlled and all-way stop controlled intersections.

[^6]Table 7
LEVEL-OF-SERVICE CRITERIA FOR
UNSIGNALIZED INTERSECTIONS ${ }^{\text {a }}$

| Level-Of-Service by Volume-to-Capacity Ratio |  | Average Control Delay <br> (Seconds Per Vehicle) |
| :---: | :---: | :---: |
| $\mathrm{V} / \mathrm{c} \leq 1.0$ | $\mathrm{v} / \mathrm{c}>1.0$ |  |
| B | F | $\leq 10.0$ |
| B | F | 10.1 to 15.0 |
| D | F | 15.1 to 25.0 |
| E | F | 25.1 to 35.0 |
| F | F | 35.1 to 50.0 |
|  | F | $>50.0$ |

${ }^{\text {a Source: Highway Capacity Manual; Transportation Research Board; Washington, DC; 2010; }}$ page 19-2.

## Vehicle Queue Analysis

Vehicle queue analyses are a direct measurement of an intersection's ability to process vehicles under various traffic control and volume scenarios and lane use arrangements. The vehicle queue analysis was performed using the Synchro® intersection capacity analysis software which is based upon the methodology and procedures presented in the 2010 Highway Capacity Manual. The Synchro ${ }^{\circledR}$ vehicle queue analysis methodology is a simulation based model which reports the number of vehicles that experience a delay of six seconds or more at an intersection. For signalized intersections, Synchro ${ }^{\circledR}$ reports both the average ( $50^{\text {th }}$ percentile) the $95^{\text {th }}$ percentile vehicle queue. For unsignalized intersections, Synchro ${ }^{\circledR}$ reports the $95^{\text {th }}$ percentile vehicle queue. Vehicle queue lengths are a function of the capacity of the movement under study and the volume of traffic being processed by the intersection during the analysis period. The $95^{\text {th }}$ percentile vehicle queue is the vehicle queue length that will be exceeded only 5 percent of the time, or approximately three minutes out of sixty minutes during the peak one hour of the day (during the remaining fifty-seven minutes, the vehicle queue length will be less than the $95^{\text {th }}$ percentile queue length).

## ANALYSIS RESULTS

Level-of-service and vehicle queue analyses were conducted for 2019 Existing, 2020 and 2030 NoBuild, and 2020 Opening-Year and 2030 Build peak-month conditions for the study area intersections. The results of the intersection capacity and vehicle queue analyses are summarized in Tables 8 and 9 , with detailed analysis results presented in the Appendix.

The following is a summary of the level-of-service and vehicle queue analysis results. For context, we note that an LOS of " $D$ " or better is generally defined as "acceptable" operating conditions.

## Signalized Intersections

## NH Route 125 at Greenhill Road and Tolend Road

Under 2019 Existing and 2020 No-Build peak-month conditions, this signalized intersection was shown to operate at an overall LOS B during the weekday morning, weekday evening, and Saturday
midday peak hours. Under 2030 No-Build peak-month conditions, overall operating conditions were shown to degrade from LOS B to LOS C during the weekday morning and evening peak hours as a result of traffic volume increases independent of the Project, and to remain operating at LOS B during the Saturday midday peak-hour.

Under 2020 Opening-Year Build peak-month conditions with the addition of Project-related traffic, overall operating conditions were shown to degrade from LOS B to LOS C during the weekday morning and evening peak-hours as a result of an increase in overall average motorist delay of up to 4.4 seconds, and to remain at operating at an overall LOS B during the Saturday midday peakhour, with no movement reported to be operating below LOS D (as previously mentioned, generally defined as the limit of acceptable traffic operations). Under 2030 Build peak-month conditions with the addition of project-related traffic, overall operating conditions were shown to degrade from LOS C to LOS D during the weekday morning peak-hour as a result of an increase in average motorist delay of 8.2 seconds, and to remain operating at LOS C during the weekday evening peakhour and at LOS B during the Saturday midday peak-hour. One movement (through movements along NH Route 125 southbound) was shown to operate below LOS D during the weekday morning peak-hour as a result of the addition of Project-related traffic. Vehicle queues at the intersection were shown to range from 0 to 38 vehicles during the peak periods. The Project was shown to result in a predicted increase in vehicle queuing at the intersection of up to 3 vehicles.

## NH Route 125 at Greenhill Road and Tolend Road

Under 2019 Existing, 2020 No-Build and 2030 No-Build peak-month conditions, this signalized intersection was shown to operate at an overall LOS F during the weekday morning and evening peak hours, and at LOS D during the Saturday midday peak-hour. Under 2020 Opening-Year Build peak-month conditions with the addition of project-related traffic, overall operating conditions were shown to remain at LOS F during the weekday morning and evening peak hours, and at LOS D during the Saturday midday peak-hour (no change over No-Build conditions). Under 2030 Build peak-month conditions with the addition of project related traffic, overall operating conditions were shown to remain at LOS F during the weekday morning and evening peak hours, and to degrade from LOS D to LOS E during the Saturday midday peak-hour as a result of a predicted increase in overall average motorist delay of 5.0 seconds. Vehicle queues at the intersection were shown to range from 0 to 87 vehicles during the peak periods. The Project was shown to result in a predicted increase in vehicle queuing at the intersection of up to 5 vehicles.

## Unsignalized Intersections

## NH Route 125 at Scruton Pond Road

Under 2019 Existing, 2020 No-Build, 2020 Opening-Year Build, 2030 No-Build and 2030 Build peak-month conditions, the critical movements at this unsignalized intersection (all movements from Scrunton Pond Road) were shown to operate at LOS F during the weekday morning, weekday evening and Saturday midday peak hours as a result of the relatively large volume of conflicting traffic on NH Route 125 during the peak hours independent of the Project. Vehicle queues on the Scruton Pond Road approach were shown to range from 3 to 13 vehicles during the peak periods. The project was shown to result in a predicted increase in vehicle queuing at the intersection of up to two (2) vehicles.

## NH Route 125 at the North Project Site Roadway

Under 2020 Opening-Year Build and 2030 Build peak-month conditions, the critical movements at this unsignalized intersection (all movements exiting the Project site) were shown to operate at LOS F during the weekday morning and evening peak hours, and at LOS E during the Saturday midday peak-hour. Vehicle queues exiting the Project site were shown to range from 1 to 5 vehicles during the peak periods, with negligible vehicle queuing predicted along NH Route 125.

## NH Route 125 at the South Project Site Roadway

Under 2020 Opening-Year Build peak-month conditions, the critical movements at this unsignalized intersection (all movements exiting the Project site) were shown to operate at LOS F during the weekday morning and evening peak hours, and at LOS E during the Saturday midday peak hour. Under 2030 Build peak-month conditions, the critical movement were shown to remain operating at LOS F during the weekday morning and evening peak hours, and to degrade to LOS F during the Saturday midday peak hour. Vehicle queues exiting the Project site were shown to range from 2 to 6 vehicles during the peak periods, with negligible vehicle queuing predicted along NH Route 125.

| Signalized Intersection/ Peak Hour/Movement | 2019 Existing |  |  |  | 2020 No-Build |  |  |  | 2020 Opening Year Build |  |  |  | 2030 No-Build |  |  |  | 2030 Build |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C ${ }^{\text {a }}$ | Delay ${ }^{\text {b }}$ | LOS $^{\text {c }}$ | $\begin{gathered} \hline \begin{array}{c} \text { Queue }{ }^{\mathrm{d}} \\ 50^{\mathrm{th}} / 95^{\mathrm{th}} \end{array} \end{gathered}$ | V/C | Delay | LOS | $\begin{gathered} \hline \begin{array}{c} \text { Queue } \\ 50^{1 /} \\ \hline 155^{\text {h }} \end{array} \\ \hline \end{gathered}$ | V/C | Delay | LOS | $\begin{gathered} \text { Queue } \\ 50^{\text {th }} / 95^{\mathrm{hb}} \end{gathered}$ | V/C | Delay | LOS | $\begin{gathered} \hline \text { Queue } \\ 50^{\text {th }} / 95^{\text {th }} \\ \hline \end{gathered}$ | V/C | Delay | LOS | $\begin{gathered} \text { Queue } \\ 50^{\text {th }} / 95^{\text {th }} \\ \hline \end{gathered}$ |
| NH Route 125 at Greenhill Road and Tolend Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Greenhill Road EB LT/TH/RT | 0.52 | 32.3 | C | 2/5 | 0.52 | 32.2 | C | 2/5 | 0.53 | 32.3 | C | 2/5 | 0.59 | 33.0 | , | 2/6 ${ }^{\text {f }}$ | 0.60 | 33.5 | C | 2/6 ${ }^{\text {f }}$ |
| Tolend Road WB LT/TH/RT | 0.35 | 31.5 | c | 1/2 | 0.35 | 31.4 | c | 1/2 | 0.45 | 32.9 | c | 1/2 | 0.41 | 31.1 | c | 1/2 | 0.52 | 33.5 | c | $1 / 3^{\text {f }}$ |
| NH Route 125 NB LT | 0.10 | 10.9 | B | 0/1 | 0.11 | 12.0 | B | 0/1 | 0.13 | 14.6 | B | 0/1 | 0.13 | 16.6 | B | 0/1 | 0.14 | 16.6 | B | 0/1 |
| NH Route 125 NB TH | 0.50 | 6.8 | A | 4/11 | 0.50 | 6.8 | A | 4/10 | 0.52 | 7.0 | A | 4/11 | 0.60 | 8.9 | A | 5/13 | 0.62 | 9.2 | A | 5/14 |
| NH Route 125 NB RT | 0.02 | 4.4 | A | 0/0 | 0.02 | 4.4 | A | 0/0 | 0.03 | 4.5 | A | 0/0 | 0.03 | 5.0 | A | $0 / 0$ | 0.03 | 5.1 | A | 0/0 |
| NH Route 125 SB LT | 0.03 | 4.2 | A | 0/1 | 0.03 | 4.2 | A | 0/1 | 0.04 | 4.3 | A | 0/1 | 0.04 | 4.8 | A | 0/1 | 0.05 | 4.9 | A | 0/1 |
| NH Route 125 SB TH | 0.89 | 20.2 | c | $10 / 30^{r}$ | 0.91 | 22.7 | c | $10 / 31^{\text {f }}$ | 0.96 | 30.8 | c | $11 / 34^{\text {f }}$ | 1.02 | 46.4 | D | 13/36 ${ }^{\text {r }}$ | 1.07 | 61.9 | E | 15/38 ${ }^{\text {r }}$ |
| NH Route 125 SB RT | 0.00 | 4.8 | A | 0/0 | 0.00 | 4.8 | A | 0/0 | 0.00 | 4.8 | A | 0/0 | 0.00 | 5.0 | A | 0/0 | 0.00 | 5.0 | A | 0/0 |
| Weekday Evening: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Greenhill Road EB LT/TH/RT | 0.18 | 28.0 | ${ }^{\text {c }}$ | $1 / 2$ | 0.18 | 28.9 | ${ }^{\text {c }}$ | $1 / 2$ | 0.18 | 29.0 | C | $1 / 2$ | 0.20 | 28.9 | C | $1 / 2$ | 0.21 | 29.5 | C | 1/2 |
| Tolend Road WB LT/TH/RT | 0.55 | 32.1 | c | $2 / 4$ | 0.58 | 33.8 | c | $2 / 4$ | 0.62 | 35.8 | D | 3/4 | 0.66 | 37.1 | D | 3/5 | 0.72 | 42.5 | D | $3 / 5^{\text {r }}$ |
| NH Route 125 NB LT | 0.29 | 6.5 | A | 1/1 | 0.30 | 6.8 | A | 1/1 | 0.33 | 7.3 | A | 1/1 | 0.38 | 9.7 | A | 1/1 | 0.42 | 11.2 | B | 1/2 |
| NH Route 125 NB TH | 0.88 | 18.8 | B | $9 / 30^{\text {f }}$ | 0.89 | 19.5 | B | 10/31 ${ }^{\text {f }}$ | 0.94 | 26.0 | C | 11/33 ${ }^{\text {r }}$ | 0.98 | 35.7 | D | 12/36 ${ }^{\text {r }}$ | 1.03 | 46.8 | D | 14/38 ${ }^{\text {r }}$ |
| NH Route 125 NB RT | 0.02 | 5.1 | A | $0 / 0$ | 0.02 | 5.0 | A | 0/0 | 0.02 | 5.1 | A | 0/0 | 0.02 | 5.1 | A | 0/0 | 0.02 | 5.1 | A | 0/0 |
| NH Route 125 SB LT | 0.13 | 11.2 | B | 0/1 | 0.13 | 11.8 | B | 0/1 | 0.14 | 14.6 | B | 0/1 | 0.15 | 16.2 | B | 0/1 | 0.16 | 16.7 | B | 0/1 |
| NH Route 125 SB TH | 0.67 | 12.0 | B | 9/14 | 0.67 | 12.1 | B | 10/15 | 0.69 | 12.6 | B | 10/15 | 0.77 | 16.2 | B | 12/17 | 0.80 | 17.3 | B | 13/19 |
| NH Route 125 SB RT | 0.02 | 6.5 | A | $0 / 0$ | 0.02 | 6.3 | A | 00 | 0.02 | 6.5 | ${ }^{\text {A }}$ | 00 | 0.02 | 7.1 | ${ }^{\text {A }}$ | $0 / 0$ | 0.02 | 7.1 | ${ }^{\text {A }}$ | $0 / 0$ |
| Saturday Midday: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Greenhill Road EB LT/TH/RT | 0.20 | 28.0 | C | 1/3 | 0.20 | 28.3 | C | 1/3 | 0.20 | 29.1 | C | 1/3 | 0.22 | 30.2 | C | 1/3 | 0.22 | 30.7 | C | 1/3 |
| Tolend Road WB LT/TH/RT | 0.33 | 29.1 | c | 1/3 | 0.33 | 29.4 | c | 1/3 | 0.41 | 31.1 | c | 1/3 | 0.43 | 32.3 | c | 1/3 | 0.51 | 33.9 | c | 2/3 |
| NH Route 125 NB LT | 0.19 | 6.4 | A | 1/1 | 0.20 | 6.9 | A | 1/1 | 0.22 | 7.7 | A | 1/1 | 0.25 | 9.2 | A | 1/1 | 0.28 | 10.6 | в | 1/1 |
| NH Route 125 NB TH | 0.55 | 6.9 | A | 4/12 | 0.56 | 7.1 | A | 4/12 | 0.57 | 7.3 | A | 4/13 | 0.60 | 7.6 | A | 5/14 | 0.62 | 8.0 | A | 5/15 |
| NH Route 125 NB RT | 0.02 | 4.2 | A | $0 / 0$ | 0.02 | 4.2 | A | 0/0 | 0.02 | 4.2 | A | 0/0 | 0.02 | 4.1 | A | 0/0 | 0.02 | 4.2 | A |  |
| NH Route 125 SB LT | 0.05 | 4.4 | A | 0/1 | 0.05 | 4.4 | A | 0/1 | 0.05 | 4.6 | A | 0/1 | 0.06 | 4.7 | A | 0/1 | 0.07 | 5.0 | A | 0/1 |
| NH Route 125 SB TH | 0.73 | 11.9 | в | 11/14 | 0.74 | 12.4 | в | 11/14 | 0.76 | 13.1 | B | 13/16 | 0.80 | 14.3 | B | 14/18 | 0.82 | 15.5 | B | 16/19 |
| NH Route 125 SB RT | 0.01 | 5.4 | A | 0/0 | 0.01 | 5.4 | A | $0 / 0$ | 0.01 | 5.4 | A | $0 / 0$ | 0.01 | 5.3 | ${ }^{\text {A }}$ | 0/0 | 0.01 | 5.3 | ${ }^{\text {A }}$ | $0 / 0$ |
| Overall | - | 11.4 | B | -- | 0.62 | 11.7 | B | -- | 0.65 | 12.3 | B | -- | 0.68 | 13.1 | B | -- | 0.72 | 14.0 | B | -- |


| Signalized Intersection/ Peak Hour/Movement | 2019 Existing |  |  |  | 2020 No-Build |  |  |  | 2020 Opening Year Build |  |  |  | 2030 No-Build |  |  |  | 2030 Build |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C ${ }^{\text {a }}$ | Delay ${ }^{\text {b }}$ | $\underline{\text { LOS }}$ | $\begin{gathered} \hline \text { Queue }{ }^{\mathrm{d}} \\ 50^{\mathrm{th}} / 95^{\mathrm{hb}} \\ \hline \end{gathered}$ | V/C | Delay | LOS | $\begin{gathered} \text { Queue } \\ 50^{\text {th }} / 95^{\text {th }} \\ \hline \end{gathered}$ | V/C | Delay | LOS | $\begin{gathered} \text { Queue } \\ 50^{\mathrm{th}} / 95^{\text {th }} \\ \hline \end{gathered}$ | V/C | $\underline{\text { Delay }}$ | LOS | $\begin{gathered} \text { Queue } \\ 50^{\text {th }} / 95^{\text {th }} \\ \hline \end{gathered}$ | V/C | $\underline{\text { Delay }}$ | LOS | $\begin{gathered} \text { Queue } \\ 50^{\text {th }} / 95^{\text {th }} \\ \hline \end{gathered}$ |
| NH Route 125 at NH Route 9 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NH Route 135 NB LT | 0.47 | 70.4 | E | 3/5 | 0.47 | 72.4 | E | 3/5 | 0.47 | 72.7 | E | 3/5 | 0.50 | 73.9 | E | 3/5 | 0.50 | 74.0 | E | 3/5 |
| NH Route 135 NB TH | 1.27 | >80.0 | F | $27^{7 / 38^{8}}$ | 1.40 | >80.0 | F | $32^{\circ} / 41^{\text {f }}$ | 1.49 | >80.0 | F | $35^{\text {c/4 }} 44^{\text {f }}$ | 1.56 | >80.0 | F | $36^{6} / 46^{6}$ | 1.66 | >80.0 | F | 399\%49 |
| NH Route 135 NB RT | 0.38 | 51.2 | D | 4/8 | 0.36 | 52.8 | D | 4/8 | 0.36 | 53.0 | D | 4/8 | 0.43 | 55.4 | E | 5/9 | 0.44 | 55.6 | E | 5/9 |
| NH Route 135 SB LT | 0.72 | 70.2 | E | 8/11 | 0.82 | 77.9 | E | 10/15 ${ }^{\text {f }}$ | 0.84 | 79.2 | E | 11/16 ${ }^{\text {f }}$ | 0.87 | >80.0 | F | 11/17 ${ }^{\text {f }}$ | 0.88 | >80.0 | F | 12/118 |
| NH Route 135 SB TH/RT | 0.93 | 64.8 | E | $21 / 28$ | 0.93 | 64.1 | E | 23/30 ${ }^{\text {r }}$ | 0.95 | 68.3 | E | $24 / 32^{\text {r }}$ | 1.03 | >80.0 | F | $28^{\circ} / 36^{\text {r }}$ | 1.05 | >80.0 |  | $29^{9} / 37^{7}$ |
| NH Route 9 SEb LT | 0.46 | 67.9 | E | 3/5 | 0.61 | 70.2 | E | 5/8 | 0.63 | 70.7 | E | $6 / 8$ | 0.63 | 72.2 | E | 6/8 | 0.65 | 72.4 | E | 6/8 |
| NH Route 9 SEB TH | 1.08 | >80.0 | F | 30\%/40 | 1.07 | >80.0 | F | $30^{\circ} / 37^{7}$ | 1.07 | >80.0 | , | $30 \% 37^{\text {f }}$ | 1.20 | >80.0 | F | $36^{6 / 43^{\text {f }}}$ | 1.21 | >80.0 | F | $36^{6} / 43^{\text {f }}$ |
| NH Route 9 SEB RT | 0.24 | 38.0 | D | 3/5 | 0.23 | 39.7 | D | 3/5 | 0.23 | 39.9 | D | 3/5 | 0.28 | 41.8 | D | 3/6 | 0.28 | 41.9 | D | 3/6 |
| NH Route 9 NWB LT | 0.85 | 78.6 | E | 11/11 | 0.85 | >80.0 | F | 11/11 | 0.85 | >80.0 | F | 11/11 | 0.90 | >80.0 | F | 12/12 | 0.91 | >80.0 | F | 12/12 |
| NH Route 9 NWB TH | 0.29 | 28.8 | c | 6/7 | 0.31 | 33.9 | c | 6/7 | 0.32 | 34.8 | c | $6 / 7$ | 0.34 | 35.2 | D | 7/8 | 0.35 | 36.1 | D | $7 / 8$ |
| NH Route 9 NWB RT | 0.08 | 26.0 | c | 0/1 | 0.14 | 31.5 | C | 1/2 | 0.16 | 32.4 | c | 1/2 | 0.17 | 32.5 | c | 2/2 | 0.18 | 33.5 | c | 2/2 |
| Overall | 1.02 | >80.0 | F | -- | 1.05 | >80.0 | F | -- | 1.08 | >80.0 | F | -- | 1.16 | >80.0 | F | -- | 1.19 | >80.0 | F | -- |
| Weekday Evening: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NH Route 135 NB LT | 0.66 | 53.3 | D | $7 / 11$ | 0.66 | 54.7 | E | $7 / 11$ | 0.67 | 55.7 | E | $7 / 11$ | 0.72 | 61.1 | , | $8 / 13$ | 0.72 | 61.9 | E | $8 / 13$ |
| NH Route 135 NB TH | 1.67 | >80.0 | F | $51^{1 / 67^{7}}$ | 1.78 | >80.0 | F | $54^{6 / 73^{\text {f }}}$ | 1.87 | >80.0 | F | $57^{7} / 77^{\text {P }}$ | 2.04 | >80.0 | F | $64^{1 / 82^{\text {r }}}$ | 2.15 | >80.0 | F | $67^{\circ} / 87^{\text {f }}$ |
| NH Route 135 NB RT | 0.09 | 31.0 | C | 1/3 | 0.09 | 32.3 | C | 1/3 | 0.09 | 33.4 | C | 1/3 | 0.35 | 38.9 | D | 4/8 | 0.36 | 40.3 | D | 4/8 |
| NH Route 135 SB LT | 0.45 | 54.7 | D | 3/6 | 0.52 | 55.1 | E | $4 / 7$ | 0.54 | 56.1 | E | 4/7 | 0.56 | 60.0 | E | 4/7 | 0.58 | 61.1 | E | 5/8 |
| NH Route 135 SB TH/RT | 0.72 | 47.2 | D | 11/15 | 0.78 | 49.5 | D | 12/118 ${ }^{\text {f }}$ | 0.84 | 54.4 | D | $13 / 21^{\text {f }}$ | 0.91 | 64.8 | E | 14/22 ${ }^{\text {f }}$ | 0.98 | >80.0 | F | 16/25 ${ }^{\text {f }}$ |
| NH Route 9 SEB LT | 0.45 | 54.6 | D | 3/6 | 0.51 | 55.1 | E | 4/7 | 0.55 | 56.1 | E | 5/8 | 0.55 | 59.9 | E | 4/7 | 0.58 | 60.9 | E | 5/8 |
| NH Route 9 SEB TH | 0.39 | 40.9 | D | 5/9 | 0.37 | 41.0 | D | 5/9 | 0.36 | 40.9 | D | 5/9 | 0.39 | 42.1 | D | 6/10 | 0.38 | 41.9 | D | $6 / 10$ |
| NH Route 9 SEB RT | 0.07 | 37.3 | D | 0/2 | 0.07 | 37.5 | D | 0/2 | 0.07 | 37.4 | D | 0/2 | 0.09 | 38.4 | D | 0/3 | 0.09 | 38.2 | D | 0/2 |
| NH Route 9 NWB LT | 0.74 | 54.2 | D | 9/15 | 0.74 | 55.6 | E | 9/15 | 0.75 | 57.1 | E | 9/15 | 0.80 | 63.4 | E | 10/17 ${ }^{\text {r }}$ | 0.81 | 64.7 | E | 10/17 ${ }^{\text {f }}$ |
| NH Route 9 NWB TH | 0.81 | 46.0 | D | 16/26 ${ }^{\text {f }}$ | 0.82 | 48.5 | D | 16/26 ${ }^{\text {f }}$ | 0.83 | 50.3 | D | 16/26 ${ }^{\text {f }}$ | 0.85 | 52.0 | D | 18/30 $0^{\text {f }}$ | 0.86 | 53.9 | D | 19/31 $1^{\text {f }}$ |
| NH Route 9 NWB RT | 0.12 | 28.8 | c | 1/3 | 0.20 | 31.1 | c | $2 / 5$ | 0.22 | 32.2 | c | 2/5 | 0.11 | 30.1 | c | 1/3 | 0.12 | 31.0 | c | 1/3 |
| Saturday Midday: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NH Route 135 NB LT | 0.47 | 43.3 | D | 3/6 | 0.46 | 43.8 | D | 3/6 | 0.46 | 44.2 | D | 3/6 | 0.50 | 46.5 | F | 4/7 | 0.51 | 47.0 | D | 4/7 |
| NH Route 135 NB TH | 0.85 | 45.1 | D | 12/28 ${ }^{\text {f }}$ | 0.89 | 51.2 | D | 13/29 ${ }^{\text {f }}$ | 0.94 | 60.4 | E | $14 / 32^{\text {f }}$ | 1.03 | >80.0 | F | $18^{0} / 37^{\text {f }}$ | 1.09 | >80.0 | F | 20 ${ }^{\text {c/39 }}$ |
| NH Route 135 NB RT | 0.08 | 26.0 | C | 0/2 | 0.08 | 26.4 | C | 0/2 | 0.08 | 26.8 | c | 0/2 | 0.10 | 29.4 | c | 1/3 | 0.10 | 29.9 | C | 1/3 |
| NH Route 135 SB LT | 0.50 | 42.9 | D | 4/6 | 0.55 | 43.4 | D | 4/7 | 0.57 | 43.7 | D | 4/7 | 0.58 | 46.3 | D | 5/8 | 0.60 | ${ }_{5}^{46.7}$ | D | 5/8 |
| NH Route 135 SB TH/RT | 0.78 | 36.4 | D | 11/17 ${ }^{\text {f }}$ | 0.80 | 36.4 | D | 12/17 | 0.83 | 38.2 | D | 13/19 ${ }^{\text {f }}$ | 0.92 | 49.1 | D | 15/24 ${ }^{\text {f }}$ | 0.95 | 53.7 | D | 16/25 ${ }^{\text {f }}$ |
| NH Route 9 SEB LT | 0.48 | 43.0 | D | 3/7 | 0.53 | 43.2 | D | 4/8 | 0.56 | 43.6 | D | 4/8 | 0.57 | 46.3 | D | 5/9 | 0.59 | 46.7 | D | 5/10 |
| NH Route 9 SEB TH | 0.65 | 40.5 | D | 7/12 | 0.65 | 41.4 | D | 7/12 | 0.65 | 41.7 | D | $7 / 12$ | 0.67 | 43.4 | D | $8 / 14$ | 0.67 | 43.8 | D | $8 / 14$ |
| NH Route 9 SEB RT | 0.25 | 33.9 | c | 2/4 | 0.24 | 34.7 | c | 2/4 | 0.24 | 35.0 | D | 2/4 | 0.28 | 35.9 | D | $2 / 5$ | 0.28 | 36.3 | D | 2/5 |
| NH Route 9 NWB LT | 0.55 | 42.7 | D | 4/8 | 0.54 | 43.2 | D | 4/8 | 0.54 | 43.6 | D | 4/8 | 0.58 | 46.2 | D | 5/9 | 0.58 | 46.8 | D | 5/9 |
| NH Route 9 NWB TH | 0.49 | 35.1 | D | 5/9 | 0.53 | 37.9 | D | 5/10 | 0.55 | 39.2 | D | 5/10 | 0.55 | 39.0 | D | 6/11 | 0.57 | 40.7 | D | $6 / 11$ |
| NH Route 9 NWB RT | 0.07 | 30.7 | C | 0/2 | 0.14 | 33.6 | C | 1/3 | 0.17 | 34.7 | C | 1/3 | 0.17 | 34.3 | C | 1/4 | 0.20 | 35.7 | ${ }^{\text {D }}$ | 1/4 |
| Overall | 0.67 | 38.7 | D | -- | 0.69 | 40.3 | D | -- | 0.72 | 42.9 | D | -- | 0.75 | 51.8 | D | -- | 0.78 | 56.8 | E | -- |

$\overline{\text { avolume-to-capacity ratio. }}$
Conl(siz) delay per vehicle in seconds
Level-of-Service.
Volume exceeds capacity, queue is theoretically infinite. Queue shown is maximum after two cycles
$95^{\text {th }}$ percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.
$\mathrm{NB}=$ northbound; $\mathrm{SB}=$ southbound; $\mathrm{EB}=$ eastbound; $\mathrm{WB}=$ westbound; $\mathrm{SEB}=$ south-eastbound; $\mathrm{NWB}=$ north-westbound; $\mathrm{LT}=$ left-turning movements; $\mathrm{TH}=$ through movements; $\mathrm{RT}=$ right-turning movements.

## UNSIGNALIZED INTERSECTION LEVEL-OF-SERVICE AND VEHICLE QUEUE SUMMARY

|  | 2019 Existing |  |  |  | 2020 No-Build |  |  |  | 2020 Opening-Year Build |  |  |  | 2030 No-Build |  |  |  | 2030 Build |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Unsignalized Intersection/Peak Hour/Movement | $\underline{\text { Demand }}$ | Delay ${ }^{\text {b }}$ | LOS $^{\text {c }}$ | $\begin{gathered} \text { Queue } \mathrm{a}^{\mathrm{a}} \\ 95^{\mathrm{h}} \end{gathered}$ | Demand | Delay | $\underline{L O S}$ | $\begin{gathered} \text { Queue } \\ \hline 95 \mathrm{bb} \end{gathered}$ | Demand | $\xrightarrow{\text { Delay }}$ | LOS | $\begin{gathered} \text { Queue } \\ 95^{\mathrm{h}} \\ \hline \end{gathered}$ | Demand | Delay | LOS | $\begin{gathered} \text { Queue } \\ \hline 95 \mathrm{bl} \end{gathered}$ | Demand | Delay | LOS | $\begin{gathered} \text { Queue } \\ \hline 95 \mathrm{bl} \\ \hline \end{gathered}$ |
| NH Route 125 at Scrunton Pond Road Weekday Morning: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Scrunton Pond Road EB LT/RT | 98 | >50.0 | F | 8 | 98 | >50.0 | F | 8 | 99 | >50.0 | F | 9 | 110 | >50.0 | F | 11 | 111 | >50.0 | F | 13 |
| NH Route 125 NB LT/TH | 580 | 0.1 | A | 0 | 598 | 0.1 | A | 0 | 629 | 0.1 | A | 0 | 659 | 0.1 | A | 0 | 690 | 0.1 | A | 0 |
| NH Route 125 SB TH/RT | 1,115 | 0.0 | A | 0 | 1,140 | 0.0 | A | 0 | 1,201 | 0.0 | A | 0 | 1,258 | 0.0 | A | 0 | 1,319 | 0.0 | A | 0 |
| Weekday Evening: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Scrunton Pond Road EB LT/RT | 33 | >50.0 | F | 3 | 33 | >50.0 | F | 3 | 35 | $>50.0$ | F | 4 | 37 | >50.0 | F | 5 | 39 | >50.0 | F | 6 |
| NH Route 125 NB LT/TH | 1,106 | 0.1 | A | 0 | 1,130 | 0.1 | A | 0 | 1,199 | 0.1 | A | 0 | 1,247 | 0.1 | A | 0 | 1,216 | 0.2 | A | 0 |
| Saturday Midday: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Scrunton Pond Road EB LT/RT | 71 | >50.0 | F | 5 | 72 | >50.0 | F | 5 | 74 | >50.0 | F | 6 | 79 | >50.0 | F | 7 | 81 | >50.0 | F | 8 |
| NH Route 125 NB LT/TH | 671 | 0.3 | A | 0 | 686 | 0.3 | A | 0 | 722 | 0.3 | A | 0 | 756 | 0.3 | A | 0 | 792 | 0.3 | A | 0 |
| NH Route 125 SB TH/RT | 772 | 0.0 | A | 0 | 788 | 0.0 | A | 0 | 825 | 0.0 | A | 0 | 870 | 0.0 | A | 0 | 907 | 0.0 | A | 0 |
| NH Route 125 at North Project Site Driveway Weekday Morning: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| North Project Site Driveway WB LT/RT | -- | -- | -- | -- | -- | -- | - | -- | 29 | >50.0 | F | 2 | -- | -- | - | -- | 29 | >50.0 | F | 2 |
| NH Route 125 NB TH/RT | -- | -- | -- | -- | -- | -- | -- | -- | ${ }_{6} 63$ | 0.0 | A | 0 | -- | -- | -- | -- | 698 | 0.0 | A | 0 |
| NH Route 125 SB LT/TH | -- | -- | -- | -- | -- | -- | -- | -- | 1,229 | 0.2 | A | 0 | -- | -- | -- | -- | 1,351 | 0.2 | A | 0 |
| Weekday Evening: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| North Project Site Driveway WB LT/RT | -- | -- | -- | -- | -- | -- | -- | -- | ${ }_{6}$ | $>50.0$ | F | 4 | -- | -- | -- | -- | 66 | >50.0 | F | 5 |
| NH Route 125 NB TH/RT | -- | -- | -- | -- | -- | -- | -- | -- | 1,183 | 0.0 | A | 0 | -- | -- | -- | -- | 1,200 | 0.0 | A | 0 |
| NH Route 125 SB LT/TH | -- | -- | -- | -- | -- | -- | -- | -- | 689 | 0.4 | A | 0 | -- | -- | -- | -- | 755 | 0.4 | A | 0 |
| Saturday Midday: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| North Project Site Driveway WB LT/RT | -- | -- | -- | -- | -- | -- | -- | -- | 41 | 35.4 | E | 1 | -- | -- | -- | - | 41 | 45.6 | E | 2 |
| NH Route 125 NB TH/RT | -- | -- | -- | -- | -- | -- | -- | -- | 722 | 0.0 | A | 0 | -- | -- | -- | -- | 788 | 0.0 | A | 0 |
| NH Route 125 SB LT/TH | -- | -- | -- | -- | -- | -- | -- | -- | 799 | 0.3 | A | 0 | -- | -- | -- | -- | 878 | 0.3 | , | 0 |
| NH Route 125 at South Project Site Driveway Weekday Morning: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| South Project Site Driveway WB LT/RT | -- | -- | -- | -- | -- | -- | -- | -- | 43 | >50.0 | F | 3 | -- | -- | -- | -- | 43 | >50.0 | F | 4 |
| NH Route 125 NB TH/RT | -- | -- | -- | -- | -- | -- | -- | -- | 647 | 0.0 | A | 0 | -- | -- | -- | -- | 708 | 0.0 | A | 0 |
| NH Route 125 SB LT/TH | -- | -- | -- | -- | -- | -- | -- | -- | 1,211 | 0.2 | A | 0 | -- | -- | -- | -- | 1,333 | 0.2 | A | 0 |
| Weekday Evening: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| South Project Site Driveway WB LT/RT | -- | -- | -- | -- | -- | -- | -- | -- | 78 | $>50.0$ | F | 6 | -- | -- | -- | -- | 78 | $>50.0$ | F | 6 |
| NH Route 125 NB TH/RT | -- | -- | -- | -- | -- | -- | -- | -- | 1,178 | 0.0 | A | 0 | -- | -- | -- | -- | 1,195 | 0.0 | A | 0 |
| NH Route 125 SB LT/TH | -- | -- | -- | -- | -- | -- | -- | -- | 694 | 0.5 | A | 0 | -- | -- | -- | -- | 760 | 0.4 | A | 0 |
| Saturday Midday: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| South Project Site Driveway WB LT/RT | -- | -- | -- | -- | -- | -- | -- | -- | 56 | 44.9 | E | 2 | -- | -- | - | - | 56 | $>50.0$ | , | 3 |
| NH Route 125 NB TH/RT | -- | -- | -- | -- | -- | -- | -- | -- | ${ }_{795} 71$ | 0.0 | A | ${ }^{0}$ | -- | -- | -- | -- | 881 | ${ }_{0}^{0.0}$ | A | ${ }_{0}$ |
| NH Route 125 SB LT/TH | -- | -- | -- | -- | -- | -- | -- | -- | 795 | 0.3 | A | 0 | -- | -- | -- | -- | 874 | 0.3 | A | 0 |

${ }^{\text {and Demand in vehicles per hour. }}{ }^{\text {andverage control delay per vehicle (in seconds). }}$

Cueue length in vehicles.
$\mathrm{NB}=$ northbound; $\mathrm{SB}=$ southbound; $\mathrm{EB}=$ eastbound; $\mathrm{WB}=$ westbound; $\mathrm{LT}=$ left-turning movements; $\mathrm{TH}=$ through movement; $\mathrm{RT}=$ right-turning movements.

## SIGHT DISTANCE EVALUATION

Sight distance measurements were performed at the Project site roadway intersections with NH Route 125 in accordance with American Association of State Highway and Transportation Officials (AASHTO) ${ }^{9}$ standards. Both stopping sight distance (SSD) and intersection sight distance (ISD) measurements were performed. In brief, SSD is the distance required by a vehicle traveling at the design speed of a roadway, on wet pavement, to stop prior to striking an object in its travel path. ISD or corner sight distance (CSD) is the sight distance required by a driver entering or crossing an intersecting roadway to perceive an on-coming vehicle and safely complete a turning or crossing maneuver with on-coming traffic. In accordance with AASHTO standards, if the measured ISD is at least equal to the required SSD value for the appropriate design speed, the intersection can operate in a safe manner. Table 10 presents the measured SSD and ISD at the subject intersections.

[^7]Table 10

## SIGHT DISTANCE MEASUREMENTS ${ }^{\text {a }}$

| Intersection/Sight Distance Measurement | Feet |  |  |
| :---: | :---: | :---: | :---: |
|  | Required <br> Minimum (SSD) | ISD ${ }^{\text {b }}$ | Measured |
| NH Route 125 at the North Project Site Roadway |  |  |  |
| Stopping Sight Distance: |  |  |  |
| NH Route 125 approaching from the north | 570 | -- | 562/600+ ${ }^{\text {c }}$ |
| NH Route 125 approaching from the south | 570 | -- | $650+$ |
| Intersection Sight Distance: |  |  |  |
| Looking to the north from the Project site roadway | 570 | 665 | 509/600+ ${ }^{\text {c }}$ |
| Looking to the south from the Project site roadway | 570 | 575 | $650+$ |
| NH Route 125 at the North Project Site Roadway |  |  |  |
| Stopping Sight Distance: |  |  |  |
| NH Route 125 approaching from the north | 570 | -- | 600+ |
| NH Route 125 approaching from the south | 570 | -- | 595 |
| Intersection Sight Distance: |  |  |  |
| Looking to the north from the Project site roadway | 570 | 665 | 600+ |
| Looking to the south from the Project site roadway | 570 | 575 | $600+$ |

[^8]As can be seen in Table 10, the available lines of sight at the Project site roadway intersections with NH Route 125 were found to exceed or could be made to exceed the recommended minimum requirements (SSD) to function in a safe manner based on a 60 mph approach speed along NH Route 125 , which is slightly above the measured $85^{\text {th }}$ percentile vehicle travel speed ( 58 59 mph ) and 10 mph above the posted speed limit ( 50 mph ).

## TURN LANE WARRANTS ANALYSIS

An auxiliary turn lane warrants analysis was conducted for the NH Route 125 approaches to the Project site roadways in accordance with the methodology and procedures outlined in NCHRP Report $457^{10}$ published by National Cooperative Highway Research Program (NCHRP).

## Left-Turn Lane

Determination of the need for a left-turn lane of adequate storage length is a function of the volume of left-turning vehicles at the intersection under study and the magnitude of opposing or conflicting traffic volumes along the roadway. Based on a review of this criteria under 2020 Opening Year and 2030 Build conditions, provision of a left-turn lane on the NH Route 125 southbound approach to the north and south Project site roadways appears to be warranted. The detailed analysis of the left-turn lane criteria is presented in the Appendix.

## Right-Turn Lane

Consideration of the need for a right-turn lane is a function of the volume of right-turning vehicles at the intersection and the total volume of traffic on the same approach (advancing volume). Based on a review of this criteria under 2020 Opening Year and 2030 Build conditions, provision of a right-turn lane on the NH Route 125 northbound approach to the north and south Project site roadways appears to be warranted. The detailed analysis of the right-turn lane criteria is presented in the Appendix.

A review of the motor vehicle crash history at the nearby intersection of NH Route 125 at Scrunton Pond Road as documented by the Barrington Police Department in the town-wide safety assessment indicated the presence of safety deficiencies along the NH Route 125 corridor due in part to the high travel speeds along the roadway. As such and based on the results of the auxiliary turn lane warrants analysis, it is recommended that left-turn lanes be provided on the NH Route 125 approaches to the Project site roadways. The existing shoulder width along NH Route 125 (nine (9) to 10 feet) combined with properly designed corner radii for the Project site roadways will accommodate vehicles decelerating to enter the Project site without impeding the flow of traffic along NH Route 125. As such, separate right-turn deceleration lanes are not recommended at this time.

[^9]
## CONCLUSIONS AND RECOMMENDATIONS

## CONCLUSIONS

VAI has completed a detailed assessment of the potential impacts on the transportation infrastructure associated with the proposed construction of a mixed-use development to be located along the east side of NH Route 125 (Calef Highway) and south of Scruton Pond Road in Barrington, New Hampshire. This study was prepared in consultation with the Town of Barrington, NHDOT and the SRPC, and is responsive to the scoping determination issued by NHDOT for the preparation of this study. The following specific areas have been evaluated as they relate to the Project: i) access requirements; ii) potential off-site improvements; and iii) safety considerations; under existing and future conditions, both with and without the Project.

As a result of this assessment, we have concluded the following with respect to the Project:

1. Using trip-generation statistics published by the ITE ${ }^{11}$ and with adjustment to account for pass-by trips, the Project is expected to generate approximately 1,732 new vehicle trips on an average weekday and 1,064 new vehicle trips on a Saturday (both two-way volumes over the operational day of the Project), with approximately 179 new vehicle trips expected during the weekday morning peak-hour, 219 new vehicle trips expected during the weekday evening peak-hour, and 160 new vehicle trips expected during the Saturday midday peak-hour;
2. In general, the Project will not have a significant impact (increase) on motorist delays or vehicle queuing over Existing or anticipated future conditions without the Project (NoBuild conditions); however, it was noted that one or more movements at the intersection of NH Route 125 at NH Route 9 are currently operating at or over capacity (defined as a LOS of "E" or "F", respectively) independent of the Project;
3. Similar to other unsignalized intersections along the NH Route 125 corridor, motorists exiting the Project site are expected to experience delays during the peak traffic volume periods, with residual vehicle queues of up to six (6) vehicles predicted which can be contained within the Project site without impeding access or circulation, or the movement of vehicles, pedestrians and bicyclists along NH Route 125;

[^10]4. Lines of sight at the Project site roadway intersections with NH Route 125 were found to exceed or could be made to exceed the required minimum distance for the intersections to function in a safe manner; and
5. A review of the criteria for the installation of auxiliary turn lanes at the Project site roadway intersections with NH Route 125 indicates that the addition of both a left-turn lane and a right-turn deceleration lane are justified based on the applicable criteria.

In consideration of the above, we have concluded that the Project can be accommodated within the confines of the existing transportation infrastructure in a safe and efficient manner with implementation of the recommendations that follow.

## RECOMMENDATIONS

A series of recommendations have been developed that are designed to provide safe and efficient access to the Project site and address any deficiencies identified at off-site locations evaluated in conjunction with this study. The following improvements have been recommended as a part of this evaluation and, where applicable, will be completed in conjunction with the Project subject to receipt of all necessary rights, permits and approvals.

## Project Access

Access to the Project will be provided by way of two (2) new roadways that will intersect the east side of NH Route 125 as follows: the north roadway will be situated opposite the driveway to 246-248 Calef Highway (Casella Sales \& Marketing Inc. and 603 Self-Storage); the south roadway will be located approximately 2,175 feet south of Scruton Pond Road. An access easement will also be established to allow for a future connection between the Project site and property to the north of Old Green Hill Road. The following recommendations are offered with respect to the design and operation of the Project site access and internal circulation, many of which are reflected on the Site Plans:
> The Project site roadways and internal circulating roads should be 24 -feet in width and designed to accommodate the turning and maneuvering requirements of the largest anticipated responding emergency vehicle as defined by the Barrington Fire Department.
> Vehicles exiting the Project site should be placed under STOP-sign control with a marked STOP-line provided.
> Let-turn lanes should be provided on NH Route 125 approaching both the north and south Project site roadways, with the turn lane accommodations at the north Project site roadway to include a left-turn lane in both the north and southbound directions to facilitate access to the driveway serving the driveway to 246-248 Calef Highway. The existing shoulder width along NH Route 125 (nine (9) to 10 feet) combined with properly designed corner radii for the Project site roadways will accommodate vehicles decelerating to enter the Project site without impeding the flow of traffic along NH Route 125. As such, separate right-turn deceleration lanes are not recommended at this time.
> Where perpendicular parking is proposed, the drive aisle behind the parking should be a minimum of 23 -feet in order to facilitate parking maneuvers.
$>$ All signs and pavement markings to be installed within the Project site should conform to the applicable standards of the Manual on Uniform Traffic Control Devices (MUTCD). ${ }^{12}$
$>$ A sidewalk should be provided along at least one side of the Project site roadways and along circulating roads within the Project site.
$>$ Americans with Disabilities Act (ADA) compliant wheelchair ramps should be provided at all pedestrian crossings internal to the Project site.
$>$ The embankment situated along the east side of NH Route 125 and north of the north Project site roadway should be regraded in order to provide the recommended minimum line of sight to and from the north along NH Route 125.
$>$ Signs and landscaping to be installed as a part of the Project within intersection sight triangle areas should be designed and maintained so as not to restrict lines of sight.
$>$ Snow windrows within sight triangle areas shall be promptly removed where such accumulations would impede sight lines.
$>$ Bicycle parking should be provided at appropriate locations within the Project site to serve the municipal, retail and bank uses.

## Off-Site

## NH Route 125/Scruton Pond Road

The intersection of NH Route 125 at Scruton Pond Road has been identified by the Town as a priority location for a RSA in order to identify potential safety-related improvements at the intersection. In order to advance this effort, the Project proponent will facilitate the completion of a RSA in order to identify improvements for this intersection.

## NH Route 125/NH Route 9

One or more movements at the intersection of NH Route 125 at NH Route 9 were identified to be operating at or over capacity during the weekday and Saturday peak hours independent of the Project, with Project-related impacts defined as a predicted increase in motorist delay that resulted in a corresponding increase in vehicle queuing of up to five (5) vehicles. In an effort to reduce overall motorist delay and vehicle queuing at the intersection, the Project proponent will design and implement an optimal traffic signal timing and phasing plan subject to receipt of all necessary rights, permits and approvals.

## Transportation Demand Management Measures

Public transportation services are not currently provided in the vicinity of the Project site. In an effort to encourage the use of alternative modes of transportation to single-occupant vehicles, the following Transportation Demand Management (TDM) measures will be implemented as a part of the Project:

[^11]> Information regarding public transportation services, maps, schedules and fare information will be posted in a central location and/or otherwise made available to residents and employees;
> Tenants of the commercial components of the Project will be encouraged to offer specific amenities to discourage off-site trips, including providing a break-room equipped with a microwave and refrigerator; offering direct deposit of paychecks; coordinating with a drycleaning service for on-site pick-up and delivery; allowing telecommuting or flexible work schedules; and other such measures to reduce overall traffic volumes and travel during peak traffic volume periods;
> Pedestrian and bicycle accommodations will be incorporated into the Project including sidewalks and bicycle parking in appropriate locations; and
$>$ To the extent that public transportation services are provided along NH Route 125 in the future, an area should be reserved for a bus stop to be established.

With implementation of the above recommendations, safe and efficient vehicular, pedestrian and bicycle access will be provided to the Project site and the Project can be accommodated within the confines of the existing and improved transportation system.


## APPENDIX

PROJECT SITE PLAN
AUTOMATIC TRAFFIC RECORDER COUNT DATA
MANUAL TURNING MOVEMENT COUNT DATA
SEASONAL ADJUSTMENT DATA
VEHICLE TRAVEL SPEED DATA
BARRINGTON POLICE DEPARTMENT SAFETY ASSESSMENT
BACKGROUND DEVELOPMENT TRAFFIC-VOLUME NETWORKS
TRIP-GENERATION CALCULATIONS
JOURNEY TO WORK TRIP DISTRIBUTION
CAPACITY ANALYSIS WORKSHEETS
TURN LANE WARRANTS ANALYSIS





| Start | 3/7/2019 | SB |  | Hour Totals |  | NB |  | Hour Totals |  | Combined Totals |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Thu | Morning | Afternoon | Morning | Afternoon | Morning | Afternoon | Morning | Afternoon | Morning | Afternoon |
| 12:00 |  | 7 | 84 |  |  | 8 | 85 |  |  |  |  |
| 12:15 |  | 2 | 87 |  |  | 10 | 101 |  |  |  |  |
| 12:30 |  | 3 | 92 |  |  | 18 | 96 |  |  |  |  |
| 12:45 |  | 4 | 90 | 16 | 353 | 7 | 96 | 43 | 378 | 59 | 731 |
| 01:00 |  | 1 | 117 |  |  | 9 | 110 |  |  |  |  |
| 01:15 |  | 3 | 85 |  |  | 6 | 110 |  |  |  |  |
| 01:30 |  | 5 | 108 |  |  | 1 | 123 |  |  |  |  |
| 01:45 |  | 2 | 117 | 11 | 427 | 6 | 124 | 22 | 467 | 33 | 894 |
| 02:00 |  | 3 | 118 |  |  | 5 | 100 |  |  |  |  |
| 02:15 |  | 5 | 119 |  |  | 1 | 128 |  |  |  |  |
| 02:30 |  | 2 | 100 |  |  | 5 | 124 |  |  |  |  |
| 02:45 |  | 4 | 127 | 14 | 464 | 3 | 172 | 14 | 524 | 28 | 988 |
| 03:00 |  | 9 | 113 |  |  | 3 | 171 |  |  |  |  |
| 03:15 |  | 11 | 113 |  |  | 4 | 161 |  |  |  |  |
| 03:30 |  | 10 | 139 |  |  | 13 | 201 |  |  |  |  |
| 03:45 |  | 16 | 130 | 46 | 495 | 9 | 172 | 29 | 705 | 75 | 1200 |
| 04:00 |  | 19 | 138 |  |  | 16 | 217 |  |  |  |  |
| 04:15 |  | 35 | 125 |  |  | 11 | 201 |  |  |  |  |
| 04:30 |  | 34 | 126 |  |  | 7 | 189 |  |  |  |  |
| 04:45 |  | 48 | 129 | 136 | 518 | 15 | 212 | 49 | 819 | 185 | 1337 |
| 05:00 |  | 61 | 104 |  |  | 16 | 227 |  |  |  |  |
| 05:15 |  | 93 | 119 |  |  | 24 | 208 |  |  |  |  |
| 05:30 |  | 98 | 96 |  |  | 22 | 180 |  |  |  |  |
| 05:45 |  | 112 | 94 | 364 | 413 | 39 | 180 | 101 | 795 | 465 | 1208 |
| 06:00 |  | 139 | 100 |  |  | 41 | 133 |  |  |  |  |
| 06:15 |  | 164 | 78 |  |  | 88 | 157 |  |  |  |  |
| 06:30 |  | 198 | 87 |  |  | 95 | 113 |  |  |  |  |
| 06:45 |  | 236 | 83 | 737 | 348 | 97 | 116 | 321 | 519 | 1058 | 867 |
| 07:00 |  | 199 | 43 |  |  | 86 | 90 |  |  |  |  |
| 07:15 |  | 257 | 52 |  |  | 123 | 70 |  |  |  |  |
| 07:30 |  | 209 | 38 |  |  | 112 | 60 |  |  |  |  |
| 07:45 |  | 208 | 36 | 873 | 169 | 122 | 69 | 443 | 289 | 1316 | 458 |
| 08:00 |  | 163 | 43 |  |  | 105 | 46 |  |  |  |  |
| 08:15 |  | 150 | 54 |  |  | 95 | 56 |  |  |  |  |
| 08:30 |  | 128 | 30 |  |  | 116 | 53 |  |  |  |  |
| 08:45 |  | 121 | 28 | 562 | 155 | 110 | 70 | 426 | 225 | 988 | 380 |
| 09:00 |  | 110 | 39 |  |  | 111 | 51 |  |  |  |  |
| 09:15 |  | 88 | 24 |  |  | 94 | 58 |  |  |  |  |
| 09:30 |  | 122 | 27 |  |  | 85 | 36 |  |  |  |  |
| 09:45 |  | 105 | 17 | 425 | 107 | 91 | 33 | 381 | 178 | 806 | 285 |
| 10:00 |  | 74 | 28 |  |  | 90 | 33 |  |  |  |  |
| 10:15 |  | 94 | 22 |  |  | 84 | 37 |  |  |  |  |
| 10:30 |  | 90 | 19 |  |  | 96 | 24 |  |  |  |  |
| 10:45 |  | 96 | 24 | 354 | 93 | 93 | 25 | 363 | 119 | 717 | 212 |
| 11:00 |  | 93 | 11 |  |  | 90 | 36 |  |  |  |  |
| 11:15 |  | 106 | 12 |  |  | 107 | 16 |  |  |  |  |
| 11:30 |  | 88 | 8 |  |  | 108 | 21 |  |  |  |  |
| 11:45 |  | 96 | 5 | 383 | 36 | 109 | 14 | 414 | 87 | 797 | 123 |
| Total |  | 3921 | 3578 |  |  | 2606 | 5105 |  |  | 6527 | 8683 |
| Percent |  | 52.3\% | 47.7\% |  |  | 33.8\% | 66.2\% |  |  | 42.9\% | 57.1\% |

Location : South of Scruton Pond Road
City/State: Barrington, NH

| Start | 3/8/2019 | SB |  | Hour Totals |  | NB |  | Hour Totals |  | Combined Totals |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Fri | Morning | Afternoon | Morning | Afternoon | Morning | Afternoon | Morning | Afternoon | Morning | Afternoon |
| 12:00 |  | 5 | 84 |  |  | 9 | 121 |  |  |  |  |
| 12:15 |  | 10 | 100 |  |  | 11 | 115 |  |  |  |  |
| 12:30 |  | 3 | 121 |  |  | 21 | 127 |  |  |  |  |
| 12:45 |  | 3 | 115 | 21 | 420 | 7 | 120 | 48 | 483 | 69 | 903 |
| 01:00 |  | 1 | 97 |  |  | 8 | 140 |  |  |  |  |
| 01:15 |  | 4 | 101 |  |  | 7 | 146 |  |  |  |  |
| 01:30 |  | 5 | 138 |  |  | 7 | 163 |  |  |  |  |
| 01:45 |  | 3 | 120 | 13 | 456 | 7 | 128 | 29 | 577 | 42 | 1033 |
| 02:00 |  | 5 | 127 |  |  | 3 | 129 |  |  |  |  |
| 02:15 |  | 3 | 115 |  |  | 2 | 158 |  |  |  |  |
| 02:30 |  | 4 | 142 |  |  | 6 | 171 |  |  |  |  |
| 02:45 |  | 8 | 121 | 20 | 505 | 5 | 163 | 16 | 621 | 36 | 1126 |
| 03:00 |  | 12 | 128 |  |  | 9 | 204 |  |  |  |  |
| 03:15 |  | 12 | 126 |  |  | 3 | 198 |  |  |  |  |
| 03:30 |  | 17 | 143 |  |  | 12 | 205 |  |  |  |  |
| 03:45 |  | 18 | 128 | 59 | 525 | 9 | 189 | 33 | 796 | 92 | 1321 |
| 04:00 |  | 20 | 149 |  |  | 20 | 201 |  |  |  |  |
| 04:15 |  | 27 | 146 |  |  | 13 | 228 |  |  |  |  |
| 04:30 |  | 28 | 123 |  |  | 7 | 205 |  |  |  |  |
| 04:45 |  | 36 | 101 | 111 | 519 | 16 | 205 | 56 | 839 | 167 | 1358 |
| 05:00 |  | 61 | 116 |  |  | 6 | 211 |  |  |  |  |
| 05:15 |  | 79 | 120 |  |  | 29 | 206 |  |  |  |  |
| 05:30 |  | 98 | 117 |  |  | 33 | 188 |  |  |  |  |
| 05:45 |  | 104 | 95 | 342 | 448 | 39 | 180 | 107 | 785 | 449 | 1233 |
| 06:00 |  | 111 | 87 |  |  | 59 | 162 |  |  |  |  |
| 06:15 |  | 176 | 87 |  |  | 59 | 156 |  |  |  |  |
| 06:30 |  | 207 | 93 |  |  | 98 | 124 |  |  |  |  |
| 06:45 |  | 189 | 79 | 683 | 346 | 103 | 111 | 319 | 553 | 1002 | 899 |
| 07:00 |  | 219 | 56 |  |  | 79 | 112 |  |  |  |  |
| 07:15 |  | 214 | 57 |  |  | 109 | 80 |  |  |  |  |
| 07:30 |  | 199 | 43 |  |  | 136 | 78 |  |  |  |  |
| 07:45 |  | 232 | 53 | 864 | 209 | 139 | 61 | 463 | 331 | 1327 | 540 |
| 08:00 |  | 160 | 37 |  |  | 101 | 71 |  |  |  |  |
| 08:15 |  | 157 | 36 |  |  | 114 | 58 |  |  |  |  |
| 08:30 |  | 146 | 30 |  |  | 111 | 54 |  |  |  |  |
| 08:45 |  | 125 | 35 | 588 | 138 | 129 | 57 | 455 | 240 | 1043 | 378 |
| 09:00 |  | 120 | 33 |  |  | 98 | 62 |  |  |  |  |
| 09:15 |  | 134 | 40 |  |  | 91 | 61 |  |  |  |  |
| 09:30 |  | 90 | 25 |  |  | 101 | 46 |  |  |  |  |
| 09:45 |  | 102 | 20 | 446 | 118 | 97 | 47 | 387 | 216 | 833 | 334 |
| 10:00 |  | 98 | 28 |  |  | 87 | 37 |  |  |  |  |
| 10:15 |  | 89 | 39 |  |  | 106 | 35 |  |  |  |  |
| 10:30 |  | 96 | 28 |  |  | 105 | 26 |  |  |  |  |
| 10:45 |  | 97 | 20 | 380 | 115 | 104 | 42 | 402 | 140 | 782 | 255 |
| 11:00 |  | 107 | 15 |  |  | 108 | 39 |  |  |  |  |
| 11:15 |  | 86 | 15 |  |  | 114 | 28 |  |  |  |  |
| 11:30 |  | 101 | 17 |  |  | 103 | 39 |  |  |  |  |
| 11:45 |  | 138 | 5 | 432 | 52 | 114 | 11 | 439 | 117 | 871 | 169 |
| Total |  | 3959 | 3851 |  |  | 2754 | 5698 |  |  | 6713 | 9549 |
| Percent |  | 50.7\% | 49.3\% |  |  | 32.6\% | 67.4\% |  |  | 41.3\% | 58.7\% |


| Start | 3/9/2019 | SB |  | Hour Totals |  | NB |  | Hour Totals |  | Combined Totals |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Sat | Morning | Afternoon | Morning | Afternoon | Morning | Afternoon | Morning | Afternoon | Morning | Afternoon |
| 12:00 |  | 10 | 128 |  |  | 15 | 114 |  |  |  |  |
| 12:15 |  | 9 | 137 |  |  | 17 | 125 |  |  |  |  |
| 12:30 |  | 3 | 115 |  |  | 20 | 137 |  |  |  |  |
| 12:45 |  | 10 | 118 | 32 | 498 | 11 | 143 | 63 | 519 | 95 | 1017 |
| 01:00 |  | 7 | 104 |  |  | 10 | 137 |  |  |  |  |
| 01:15 |  | 5 | 112 |  |  | 6 | 122 |  |  |  |  |
| 01:30 |  | 1 | 124 |  |  | 5 | 125 |  |  |  |  |
| 01:45 |  | 5 | 118 | 18 | 458 | 6 | 131 | 27 | 515 | 45 | 973 |
| 02:00 |  | 3 | 104 |  |  | 5 | 113 |  |  |  |  |
| 02:15 |  | 5 | 114 |  |  | 9 | 122 |  |  |  |  |
| 02:30 |  | 10 | 96 |  |  | 3 | 104 |  |  |  |  |
| 02:45 |  | 2 | 125 | 20 | 439 | 8 | 105 | 25 | 444 | 45 | 883 |
| 03:00 |  | 0 | 119 |  |  | 3 | 145 |  |  |  |  |
| 03:15 |  | 8 | 92 |  |  | 5 | 142 |  |  |  |  |
| 03:30 |  | 7 | 124 |  |  | 5 | 110 |  |  |  |  |
| 03:45 |  | 11 | 124 | 26 | 459 | 9 | 132 | 22 | 529 | 48 | 988 |
| 04:00 |  | 7 | 121 |  |  | 5 | 117 |  |  |  |  |
| 04:15 |  | 12 | 131 |  |  | 7 | 103 |  |  |  |  |
| 04:30 |  | 18 | 118 |  |  | 2 | 152 |  |  |  |  |
| 04:45 |  | 19 | 119 | 56 | 489 | 8 | 104 | 22 | 476 | 78 | 965 |
| 05:00 |  | 21 | 103 |  |  | 6 | 112 |  |  |  |  |
| 05:15 |  | 20 | 94 |  |  | 8 | 132 |  |  |  |  |
| 05:30 |  | 27 | 114 |  |  | 14 | 125 |  |  |  |  |
| 05:45 |  | 32 | 102 | 100 | 413 | 23 | 140 | 51 | 509 | 151 | 922 |
| 06:00 |  | 44 | 62 |  |  | 26 | 100 |  |  |  |  |
| 06:15 |  | 44 | 104 |  |  | 30 | 92 |  |  |  |  |
| 06:30 |  | 51 | 100 |  |  | 33 | 121 |  |  |  |  |
| 06:45 |  | 58 | 92 | 197 | 358 | 34 | 93 | 123 | 406 | 320 | 764 |
| 07:00 |  | 39 | 70 |  |  | 47 | 82 |  |  |  |  |
| 07:15 |  | 62 | 63 |  |  | 41 | 64 |  |  |  |  |
| 07:30 |  | 72 | 35 |  |  | 55 | 62 |  |  |  |  |
| 07:45 |  | 83 | 67 | 256 | 235 | 76 | 60 | 219 | 268 | 475 | 503 |
| 08:00 |  | 78 | 43 |  |  | 77 | 40 |  |  |  |  |
| 08:15 |  | 73 | 46 |  |  | 59 | 46 |  |  |  |  |
| 08:30 |  | 101 | 40 |  |  | 79 | 40 |  |  |  |  |
| 08:45 |  | 94 | 32 | 346 | 161 | 87 | 54 | 302 | 180 | 648 | 341 |
| 09:00 |  | 106 | 37 |  |  | 86 | 53 |  |  |  |  |
| 09:15 |  | 115 | 39 |  |  | 102 | 66 |  |  |  |  |
| 09:30 |  | 90 | 30 |  |  | 117 | 58 |  |  |  |  |
| 09:45 |  | 121 | 26 | 432 | 132 | 110 | 47 | 415 | 224 | 847 | 356 |
| 10:00 |  | 108 | 29 |  |  | 91 | 36 |  |  |  |  |
| 10:15 |  | 96 | 20 |  |  | 101 | 36 |  |  |  |  |
| 10:30 |  | 126 | 22 |  |  | 116 | 27 |  |  |  |  |
| 10:45 |  | 124 | 24 | 454 | 95 | 130 | 29 | 438 | 128 | 892 | 223 |
| 11:00 |  | 104 | 21 |  |  | 144 | 18 |  |  |  |  |
| 11:15 |  | 129 | 21 |  |  | 136 | 28 |  |  |  |  |
| 11:30 |  | 177 | 16 |  |  | 113 | 31 |  |  |  |  |
| 11:45 |  | 141 | 14 | 551 | 72 | 127 | 18 | 520 | 95 | 1071 | 167 |
| Total |  | 2488 | 3809 |  |  | 2227 | 4293 |  |  | 4715 | 8102 |
| Percent |  | 39.5\% | 60.5\% |  |  | 34.2\% | 65.8\% |  |  | 36.8\% | 63.2\% |
| Grand Total |  | 10368 | 11238 |  |  | 7587 | 15096 |  |  | 17955 | 26334 |
| Percent |  | 48.0\% | 52.0\% |  |  | 33.4\% | 66.6\% |  |  | 40.5\% | 59.5\% |
| ADT |  | T 14,763 |  | T 14,763 |  |  |  |  |  |  |  |

Location: Route 125
Location: South of Scruton Pond Road
City/State: Barrington, NH


MANUAL TURNING MOVEMENT COUNT DATA.

| Accurate Counts <br> 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 <br> ENW Street: Route 9 <br> City/State : Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Star Page | $\begin{aligned} & : 81880001 \\ & : 81880001 \\ & : 3 / 7 / 2019 \\ & : 1 \end{aligned}$ |
| Groups Printed-Cars - Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 <br> From North |  |  | Route 9 <br> From East |  |  | Route 125 From South |  |  | Route 9 From West |  |  |  |
| Start Time | Left | Thru | Right | Left |  | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 07:00 AM | 50 | 151 | 10 | 21 | 15 | 13 | 10 | 73 | 39 | 5 | 99 | 25 | 511 |
| 07:15 AM | 24 | 165 | 8 | 48 | 43 | 23 | 7 | 89 | 50 | 15 | 119 | 21 | 612 |
| 07:30 AM | 34 | 176 | 9 | 36 | 30 | 16 | 8 | 91 | 27 | 15 | 109 | 51 | 602 |
| 07:45 AM | 28 | 166 | 10 | 30 | 19 | 8 | 15 | 93 | 31 | 12 | 98 | 30 | 540 |
| Total | 136 | 658 | 37 | 135 | 107 | 60 | 40 | 346 | 147 | 47 | 425 | 127 | 2265 |
| 08:00 AM | 24 | 136 | 8 | 32 | 34 | 12 | 9 | 76 | 33 | 18 | 63 | 53 | 498 |
| 08:15 AM | 17 | 113 | 9 | 29 | 25 | 15 | 31 | 84 | 31 | 6 | 49 | 62 | 471 |
| 08:30 AM | 19 | 103 | 10 | 22 | 20 | 23 | 10 | 80 | 31 | 14 | 58 | 34 | 424 |
| 08:45 AM | 21 | 92 | 13 | 17 | 23 | 14 | 16 | 79 | 20 | 11 | 48 | 25 | 379 |
| Total | 81 | 444 | 40 | 100 | 102 | 64 | 66 | 319 | 115 | 49 | 218 | 174 | 1772 |
| Grand Total | 217 | 1102 | 77 | 235 | 209 | 124 | 106 | 665 | 262 | 96 | 643 | 301 | 4037 |
| Apprch \% | 15.5 | 78.9 | 5.5 | 41.4 | 36.8 | 21.8 | 10.3 | 64.4 | 25.4 | 9.2 | 61.8 | 28.9 |  |
| Total \% | 5.4 | 27.3 | 1.9 | 5.8 | 5.2 | 3.1 | 2.6 | 16.5 | 6.5 | 2.4 | 15.9 | 7.5 |  |
| Cars | 205 | 1061 | 69 | 228 | 204 | 100 | 103 | 642 | 257 | 94 | 632 | 287 | 3882 |
| \% Cars | 94.5 | 96.3 | 89.6 | 97 | 97.6 | 80.6 | 97.2 | 96.5 | 98.1 | 97.9 | 98.3 | 95.3 | 96.2 |
| Trucks | 12 | 41 | 8 | 7 | 5 | 24 | 3 | 23 | 5 | 2 | 11 | 14 | 155 |
| \% Trucks | 5.5 | 3.7 | 10.4 | 3 | 2.4 | 19.4 | 2.8 | 3.5 | 1.9 | 2.1 | 1.7 | 4.7 | 3.8 |

File Name: $: 81880001$
Site Code : 81880001
Start Date : $3 / 7 / 2019$
Page No : 2

|  | Route 125 <br> From North |  |  |  | Route 9 <br> From East |  |  |  | Route 125 <br> From South |  |  |  | Route 9 <br> From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 07:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:00 AM | 50 | 151 | 10 | 211 | 21 | 15 | 13 | 49 | 10 | 73 | 39 | 122 | 5 | 99 | 25 | 129 | 511 |
| 07:15 AM | 24 | 165 | 8 | 197 | 48 | 43 | 23 | 114 | 7 | 89 | 50 | 146 | 15 | 119 | 21 | 155 | 612 |
| 07:30 AM | 34 | 176 | 9 | 219 | 36 | 30 | 16 | 82 | 8 | 91 | 27 | 126 | 15 | 109 | 51 | 175 | 602 |
| 07:45 AM | 28 | 166 | 10 | 204 | 30 | 19 | 8 | 57 | 15 | 93 | 31 | 139 | 12 | 98 | 30 | 140 | 540 |
| Total Volume | 136 | 658 | 37 | 831 | 135 | 107 | 60 | 302 | 40 | 346 | 147 | 533 | 47 | 425 | 127 | 599 | 2265 |
| \% App. Total | 16.4 | 79.2 | 4.5 |  | 44.7 | 35.4 | 19.9 |  | 7.5 | 64.9 | 27.6 |  | 7.8 | 71 | 21.2 |  |  |
| PHF | . 680 | . 935 | . 925 | . 949 | . 703 | . 622 | . 652 | . 662 | . 667 | . 930 | . 735 | . 913 | . 783 | . 893 | . 623 | . 856 | . 925 |
| Cars | 129 | 635 | 31 | 795 | 131 | 103 | 52 | 286 | 37 | 330 | 145 | 512 | 46 | 419 | 126 | 591 | 2184 |
| \% Cars | 94.9 | 96.5 | 83.8 | 95.7 | 97.0 | 96.3 | 86.7 | 94.7 | 92.5 | 95.4 | 98.6 | 96.1 | 97.9 | 98.6 | 99.2 | 98.7 | 96.4 |
| Trucks | 7 | 23 | 6 | 36 | 4 | 4 | 8 | 16 | 3 | 16 | 2 | 21 | 1 | 6 | 1 | 8 | 81 |
| \% Trucks | 5.1 | 3.5 | 16.2 | 4.3 | 3.0 | 3.7 | 13.3 | 5.3 | 7.5 | 4.6 | 1.4 | 3.9 | 2.1 | 1.4 | 0.8 | 1.3 | 3.6 |

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| Accurate Counts 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 <br> E/W Street: Route 9 <br> City/State: Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Sta Pag | $\begin{aligned} & : 81880001 \\ & : 81880001 \\ & : 3 / 7 / 2019 \\ & : 5 \end{aligned}$ |
| Groups Printed-Cars |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  Route 125 <br> From North <br> Left Thru |  |  | Route 9 <br> From East |  |  | Route 125 From South |  |  | Route 9 From West |  |  |  |
| Start Time |  |  | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 07:00 AM | 47 | 147 | 7 | 21 | 15 | 12 | 10 | 71 | 38 | 4 | 96 | 25 | 493 |
| 07:15 AM | 23 | 158 | 8 | 45 | 40 | 21 | 6 | 84 | 50 | 15 | 117 | 21 | 588 |
| 07:30 AM | 33 | 169 | 7 | 35 | 29 | 12 | 7 | 85 | 27 | 15 | 109 | 51 | 579 |
| 07:45 AM | 26 | 161 | 9 | 30 | 19 | 7 | 14 | 90 | 30 | 12 | 97 | 29 | 524 |
| Total | 129 | 635 | 31 | 131 | 103 | 52 | 37 | 330 | 145 | 46 | 419 | 126 | 2184 |
| 08:00 AM | 21 | 127 | 7 | 32 | 33 | 11 | 9 | 75 | 31 | 18 | 61 | 51 | 476 |
| 08:15 AM | 16 | 108 | 8 | 28 | 25 | 11 | 31 | 82 | 31 | 6 | 47 | 56 | 449 |
| 08:30 AM | 18 | 103 | 10 | 22 | 20 | 16 | 10 | 76 | 31 | 14 | 57 | 30 | 407 |
| 08:45 AM | 21 | 88 | 13 | 15 | 23 | 10 | 16 | 79 | 19 | 10 | 48 | 24 | 366 |
| Total | 76 | 426 | 38 | 97 | 101 | 48 | 66 | 312 | 112 | 48 | 213 | 161 | 1698 |
| Grand Total | 205 | 1061 | 69 | 228 | 204 | 100 | 103 | 642 | 257 | 94 | 632 | 287 | 3882 |
| Apprch \% | 15.4 | 79.5 | 5.2 | 42.9 | 38.3 | 18.8 | 10.3 | 64.1 | 25.6 | 9.3 | 62.4 | 28.3 |  |
| Total \% | 5.3 | 27.3 | 1.8 | 5.9 | 5.3 | 2.6 | 2.7 | 16.5 | 6.6 | 2.4 | 16.3 | 7.4 |  |


| Accurate Counts 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 <br> EN Street: Route 9 <br> City/State : Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Start Page | $\begin{aligned} & : 81880001 \\ & : 81880001 \\ & : 3 / 7 / 2019 \\ & 9 \end{aligned}$ |
| Groups Printed- Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 From North |  |  | Route 9 From East |  |  | Route 125 <br> From South |  |  | Route 9 From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 07:00 AM | 3 | 4 | 3 | 0 | 0 | 1 | 0 | 2 | 1 | 1 | 3 | 0 | 18 |
| 07:15 AM | 1 | 7 | 0 | 3 | 3 | 2 | 1 | 5 | 0 | 0 | 2 | 0 | 24 |
| 07:30 AM | 1 | 7 | 2 | 1 | 1 | 4 | 1 | 6 | 0 | 0 | 0 | 0 | 23 |
| 07:45 AM | 2 | 5 | 1 | 0 | 0 | 1 | 1 | 3 | 1 | 0 | 1 | 1 | 16 |
| Total | 7 | 23 | 6 | 4 | 4 | 8 | 3 | 16 | 2 | 1 | 6 | 1 | 81 |
| 08:00 AM | 3 | 9 | 1 | 0 | 1 | 1 | 0 | 1 | 2 | 0 | 2 | 2 | 22 |
| 08:15 AM | 1 | 5 | 1 | 1 | 0 | 4 | 0 | 2 | 0 | 0 | 2 | 6 | 22 |
| 08:30 AM | 1 | 0 | 0 | 0 | 0 | 7 | 0 | 4 | 0 | 0 | 1 | 4 | 17 |
| 08:45 AM | 0 | 4 | 0 | 2 | 0 | 4 | 0 | 0 | 1 | 1 | 0 | 1 | 13 |
| Total | 5 | 18 | 2 | 3 | 1 | 16 | 0 | 7 | 3 | 1 | 5 | 13 | 74 |
| Grand Total | 12 | 41 | 8 | 7 | 5 | 24 | 3 | 23 | 5 | 2 | 11 | 14 | 155 |
| Apprch \% | 19.7 | 67.2 | 13.1 | 19.4 | 13.9 | 66.7 | 9.7 | 74.2 | 16.1 | 7.4 | 40.7 | 51.9 |  |
| Total \% | 7.7 | 26.5 | 5.2 | 4.5 | 3.2 | 15.5 | 1.9 | 14.8 | 3.2 | 1.3 | 7.1 | 9 |  |



|  | Route 125 <br> From North |  |  |  | Route 9 <br> From East |  |  |  | Route 125 <br> From South |  |  |  | Route 9 From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 07:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| \% App. Total | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |
| PHF | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 |

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| :---: |
| $\varepsilon$ |
| 8 |

File Name


| Accurate Counts 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 ENW Street: Route 9 City/State : Barrington, NH Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Star Sag | 81880001 81880001 3/7/2019 : 1 |
| Groups Printed-Cars - Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 <br> From North |  |  | Route 9 <br> From East |  |  | Route 125 From South |  |  | Route 9 From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thus | Right | Int. Total |
| 04:00 PM | 24 | 92 | 22 | 30 | 71 | 35 | 32 | 167 | 21 | 9 | 35 | 32 | 570 |
| 04:15 PM | 19 | 105 | 13 | 35 | 80 | 29 | 30 | 139 | 31 | 20 | 30 | 21 | 552 |
| 04:30 PM | 14 | 98 | 16 | 42 | 80 | 22 | 25 | 152 | 23 | 18 | 28 | 20 | 538 |
| 04:45 PM | 15 | 99 | 20 | 54 | 92 | 28 | 36 | 182 | 20 | 19 | 31 | 13 | 609 |
| Total | 72 | 394 | 71 | 161 | 323 | 114 | 123 | 640 | 95 | 66 | 124 | 86 | 2269 |
| 05:00 PM | 12 | 86 | 19 | 41 | 89 | 28 | 57 | 175 | 17 | 12 | 30 | 20 | 586 |
| 05:15 PM | 20 | 80 | 18 | 54 | 92 | 18 | 28 | 170 | 20 | 12 | 35 | 24 | 571 |
| 05:30 PM | 21 | 72 | 9 | 37 | 65 | 22 | 33 | 139 | 20 | 10 | 41 | 16 | 485 |
| 05:45 PM | 13 | 68 | 10 | 28 | 67 | 18 | 27 | 129 | 22 | 7 | 38 | 16 | 443 |
| Total | 66 | 306 | 56 | 160 | 313 | 86 | 145 | 613 | 79 | 41 | 144 | 76 | 2085 |
| Grand Total | 138 | 700 | 127 | 321 | 636 | 200 | 268 | 1253 | 174 | 107 | 268 | 162 | 4354 |
| Apprch \% | 14.3 | 72.5 | 13.2 | 27.7 | 55 | 17.3 | 15.8 | 73.9 | 10.3 | 19.9 | 49.9 | 30.2 |  |
| Total \% | 3.2 | 16.1 | 2.9 | 7.4 | 14.6 | 4.6 | 6.2 | 28.8 | 4 | 2.5 | 6.2 | 3.7 |  |
| Cars | 136 | 686 | 127 | 320 | 633 | 199 | 267 | 1243 | 174 | 106 | 268 | 158 | 4317 |
| \% Cars | 98.6 | 98 | 100 | 99.7 | 99.5 | 99.5 | 99.6 | 99.2 | 100 | 99.1 | 100 | 97.5 | 99.2 |
| Trucks | 2 | 14 | 0 | 1 | 3 | 1 | 1 | 10 | 0 | 1 | 0 | 4 | 37 |
| \% Trucks | 1.4 | 2 | 0 | 0.3 | 0.5 | 0.5 | 0.4 | 0.8 | 0 | 0.9 | 0 | 2.5 | 0.8 |



|  | Route 125 <br> From North |  |  |  | Route 9 <br> From East |  |  |  | Route 125 <br> From South |  |  |  | Route 9 From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 04:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:30 PM | 14 | 98 | 16 | 128 | 42 | 80 | 22 | 144 | 25 | 152 | 23 | 200 | 18 | 28 | 20 | 66 | 538 |
| 04:45 PM | 15 | 99 | 20 | 134 | 54 | 92 | 28 | 174 | 36 | 182 | 20 | 238 | 19 | 31 | 13 | 63 | 609 |
| 05:00 PM | 12 | 86 | 19 | 117 | 41 | 89 | 28 | 158 | 57 | 175 | 17 | 249 | 12 | 30 | 20 | 62 | 586 |
| 05:15 PM | 20 | 80 | 18 | 118 | 54 | 92 | 18 | 164 | 28 | 170 | 20 | 218 | 12 | 35 | 24 | 71 | 571 |
| Total Volume | 61 | 363 | 73 | 497 | 191 | 353 | 96 | 640 | 146 | 679 | 80 | 905 | 61 | 124 | 77 | 262 | 2304 |
| \% App. Total | 12.3 | 73 | 14.7 |  | 29.8 | 55.2 | 15 |  | 16.1 | 75 | 8.8 |  | 23.3 | 47.3 | 29.4 |  |  |
| PHF | . 763 | . 917 | . 913 | . 927 | . 884 | . 959 | . 857 | . 920 | . 640 | . 933 | . 870 | . 909 | . 803 | . 886 | . 802 | . 923 | . 946 |
| Cars | 61 | 360 | 73 | 494 | 190 | 352 | 95 | 637 | 146 | 677 | 80 | 903 | 61 | 124 | 77 | 262 | 2296 |
| \% Cars | 100 | 99.2 | 100 | 99.4 | 99.5 | 99.7 | 99.0 | 99.5 | 100 | 99.7 | 100 | 99.8 | 100 | 100 | 100 | 100 | 99.7 |
| Trucks | 0 | 3 | 0 | 3 | 1 | 1 | 1 | 3 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 8 |
| \% Trucks | 0 | 0.8 | 0 | 0.6 | 0.5 | 0.3 | 1.0 | 0.5 | 0 | 0.3 | 0 | 0.2 | 0 | 0 | 0 | 0 | 0.3 |

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Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 Peak Hour for Each Approach Begins at

| Accurate Counts 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 EN Street: Route 9 City/State : Barrington, NH Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Star Pag | $\begin{aligned} & : 81880001 \\ & : 81880001 \\ & : 37 / 2019 \\ & : 5 \end{aligned}$ |
| Groups Printed-Cars |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 <br> From North |  |  | Route 9 <br> From East |  |  | Route 125 From South |  |  | Route 9 From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 04:00 PM | 23 | 87 | 22 | 30 | 69 | 35 | 32 | 166 | 21 | 9 | 35 | 28 | 557 |
| 04:15 PM | 19 | 102 | 13 | 35 | 80 | 29 | 29 | 134 | 31 | 20 | 30 | 21 | 543 |
| 04:30 PM | 14 | 97 | 16 | 41 | 80 | 21 | 25 | 150 | 23 | 18 | 28 | 20 | 533 |
| 04:45 PM | 15 | 98 | 20 | 54 | 91 | 28 | 36 | 182 | 20 | 19 | 31 | 13 | 607 |
| Total | 71 | 384 | 71 | 160 | 320 | 113 | 122 | 632 | 95 | 66 | 124 | 82 | 2240 |
| 05:00 PM | 12 | 85 | 19 | 41 | 89 | 28 | 57 | 175 | 17 | 12 | 30 | 20 | 585 |
| 05:15 PM | 20 | 80 | 18 | 54 | 92 | 18 | 28 | 170 | 20 | 12 | 35 | 24 | 571 |
| 05:30 PM | 20 | 70 | 9 | 37 | 65 | 22 | 33 | 138 | 20 | 9 | 41 | 16 | 480 |
| 05:45 PM | 13 | 67 | 10 | 28 | 67 | 18 | 27 | 128 | 22 | 7 | 38 | 16 | 441 |
| Total | 65 | 302 | 56 | 160 | 313 | 86 | 145 | 611 | 79 | 40 | 144 | 76 | 2077 |
| Grand Total | 136 | 686 | 127 | 320 | 633 | 199 | 267 | 1243 | 174 | 106 | 268 | 158 | 4317 |
| Apprch \% | 14.3 | 72.3 | 13.4 | 27.8 | 54.9 | 17.3 | 15.9 | 73.8 | 10.3 | 19.9 | 50.4 | 29.7 |  |
| Total \% | 3.2 | 15.9 | 2.9 | 7.4 | 14.7 | 4.6 | 6.2 | 28.8 | 4 | 2.5 | 6.2 | 3.7 |  |


| Accurate Counts 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 E/W Street: Route 9 City/State : Barrington, NH Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Star Page | $\begin{aligned} & : 81880001 \\ & : 81880001 \\ & : 3 / 7 / 2019 \\ & : 9 \end{aligned}$ |
| Groups Printed-Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 <br> From North |  |  | Route 9 <br> From East |  |  | Route 125 <br> From South |  |  | Route 9 From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 04:00 PM | 1 | 5 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 4 | 13 |
| 04:15 PM | 0 | 3 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 9 |
| 04:30 PM | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 5 |
| 04:45 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Total | 1 | 10 | 0 | 1 | 3 | 1 | 1 | 8 | 0 | 0 | 0 | 4 | 29 |
| 05:00 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 5 |
| 05:45 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| Total | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 8 |
| Grand Total | 2 | 14 | 0 | 1 | 3 | 1 | 1 | 10 | 0 | 1 | 0 | 4 | 37 |
| Apprch \% | 12.5 | 87.5 | 0 | 20 | 60 | 20 | 9.1 | 90.9 | 0 | 20 | 0 | 80 |  |
| Total \% | 5.4 | 37.8 | 0 | 2.7 | 8.1 | 2.7 | 2.7 | 27 | 0 | 2.7 | 0 | 10.8 |  |


| N/S Street : Route ENW Street: Route City/State : Barring Weather : Clear |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { File Name : } 81880001 \\ & \text { Site Code : } 81880001 \\ & \text { Start Date : } 3 / 7 / 2019 \\ & \text { Page No : } 13 \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Groups Printed- Bikes Peds |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Rout From |  |  |  | Rou From |  |  |  | Rout From | 25 |  |  | Rou |  |  |  |  |  |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Exclu. Total | Inclu. Total | Int. Total |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch \% | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |  |
| Total \% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 |  |




 Page No : 15



| Accurate Counts <br> 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 <br> E/W Street: Route 9 <br> Clity/State : Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Sta Pag | 818800S1 <br> 81880001 <br> 3/9/2019 <br> 1 |
| Groups Printed- Cars - Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 <br> From North |  |  | Route 9 <br> From East |  |  | Route 125 From South |  |  | Route 9 From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 11:00 AM | 12 | 69 | 20 | 24 | 42 | 14 | 27 | 96 | 16 | 19 | 52 | 14 | 405 |
| 11:15 AM | 10 | 103 | 15 | 17 | 33 | 18 | 27 | 90 | 20 | 20 | 37 | 28 | 418 |
| 11:30 AM | 27 | 130 | 34 | 23 | 38 | 17 | 20 | 86 | 28 | 20 | 53 | 36 | 512 |
| 11:45 AM | 16 | 103 | 20 | 28 | 39 | 26 | 24 | 88 | 23 | 21 | 54 | 27 | 469 |
| Total | 65 | 405 | 89 | 92 | 152 | 75 | 98 | 360 | 87 | 80 | 196 | 105 | 1804 |
| 12:00 PM | 20 | 109 | 18 | 27 | 34 | 16 | 14 | 83 | 13 | 19 | 35 | 32 | 420 |
| 12:15 PM | 16 | 93 | 22 | 32 | 38 | 18 | 26 | 93 | 16 | 24 | 44 | 23 | 445 |
| 12:30 PM | 10 | 88 | 18 | 25 | 39 | 26 | 22 | 87 | 22 | 19 | 32 | 26 | 414 |
| 12:45 PM | 19 | 92 | 23 | 15 | 36 | 17 | 15 | 97 | 14 | 19 | 43 | 33 | 423 |
| Total | 65 | 382 | 81 | 99 | 147 | 77 | 77 | 360 | 65 | 81 | 154 | 114 | 1702 |
| 01:00 PM | 16 | 72 | 15 | 22 | 35 | 18 | 19 | 103 | 27 | 18 | 40 | 22 | 407 |
| 01:15 PM | 15 | 79 | 15 | 27 | 41 | 23 | 24 | 88 | 16 | 23 | 45 | 26 | 422 |
| 01:30 PM | 12 | 82 | 17 | 20 | 44 | 19 | 18 | 75 | 17 | 16 | 29 | 23 | 372 |
| 01:45 PM | 16 | 90 | 15 | 25 | 28 | 20 | 24 | 101 | 8 | 17 | 24 | 27 | 395 |
| Total | 59 | 323 | 62 | 94 | 148 | 80 | 85 | 367 | 68 | 74 | 138 | 98 | 1596 |
| Grand Total | 189 | 1110 | 232 | 285 | 447 | 232 | 260 | 1087 | 220 | 235 | 488 | 317 | 5102 |
| Apprch \% | 12.3 | 72.5 | 15.2 | 29.6 | 46.4 | 24.1 | 16.6 | 69.4 | 14 | 22.6 | 46.9 | 30.5 |  |
| Total \% | 3.7 | 21.8 | 4.5 | 5.6 | 8.8 | 4.5 | 5.1 | 21.3 | 4.3 | 4.6 | 9.6 | 6.2 |  |
| Cars | 189 | 1101 | 232 | 285 | 446 | 232 | 260 | 1078 | 220 | 235 | 488 | 317 | 5083 |
| \% Cars | 100 | 99.2 | 100 | 100 | 99.8 | 100 | 100 | 99.2 | 100 | 100 | 100 | 100 | 99.6 |
| Trucks | 0 | 9 | 0 | 0 | 1 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 19 |
| \% Trucks | 0 | 0.8 | 0 | 0 | 0.2 | 0 | 0 | 0.8 | 0 | 0 | 0 | 0 | 0.4 |


|  | Route 125 <br> From North |  |  |  | Route 9 From East |  |  |  | Route 125 <br> From South |  |  |  | Route 9 From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thrs | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 11:00 AM to 01:45 PM - Peak 1 of 1 , |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 11:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:30 AM | 27 | 130 | 34 | 191 | 23 | 38 | 17 | 78 | 20 | 86 | 28 | 134 | 20 | 53 | 36 | 109 | 512 |
| 11:45 AM | 16 | 103 | 20 | 139 | 28 | 39 | 26 | 93 | 24 | 88 | 23 | 135 | 21 | 54 | 27 | 102 | 469 |
| 12:00 PM | 20 | 109 | 18 | 147 | 27 | 34 | 16 | 77 | 14 | 83 | 13 | 110 | 19 | 35 | 32 | 86 | 420 |
| 12:15 PM | 16 | 93 | 22 | 131 | 32 | 38 | 18 | 88 | 26 | 93 | 16 | 135 | 24 | 44 | 23 | 91 | 445 |
| Total Volume | 79 | 435 | 94 | 608 | 110 | 149 | 77 | 336 | 84 | 350 | 80 | 514 | 84 | 186 | 118 | 388 | 1846 |
| \% App. Total | 13 | 71.5 | 15.5 |  | 32.7 | 44.3 | 22.9 |  | 16.3 | 68.1 | 15.6 |  | 21.6 | 47.9 | 30.4 |  |  |
| PHF | . 731 | . 837 | . 691 | . 796 | . 859 | . 955 | . 740 | . 903 | . 808 | . 941 | . 714 | . 952 | . 875 | . 861 | . 819 | . 890 | . 901 |
| Cars | 79 | 432 | 94 | 605 | 110 | 148 | 77 | 335 | 84 | 348 | 80 | 512 | 84 | 186 | 118 | 388 | 1840 |
| \% Cars | 100 | 99.3 | 100 | 99.5 | 100 | 99.3 | 100 | 99.7 | 100 | 99.4 | 100 | 99.6 | 100 | 100 | 100 | 100 | 99.7 |
| Trucks | 0 | 3 | 0 | 3 | 0 | 1 | 0 | 1 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 6 |
| \% Trucks | 0 | 0.7 | 0 | 0.5 | 0 | 0.7 | 0 | 0.3 | 0 | 0.6 | 0 | 0.4 | 0 | 0 | 0 | 0 | 0.3 |

Peak Hour Analysis From 11:00 AM to 01:45 PM - Peak 1 of 1 Peak Hour for Each Approach Begins at:


| Accurate Counts 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 <br> E/N Street: Route 9 <br> City/State : Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Start Page | $\begin{aligned} & : 818800 \text { S } 1 \\ & : 8188001 \\ & : 3 / 9 / 2019 \\ & : 5 \end{aligned}$ |
| Groups Printed-Cars |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 From North |  |  |  Route 9 <br> From East <br> Left Thru |  |  | Route 125 <br> From South |  |  | Route 9 From West |  |  |  |
| Start Time | Left | Thru | Right |  |  | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 11:00 AM | 12 | 67 | 20 | 24 | 42 | 14 | 27 | 96 | 16 | 19 | 52 | 14 | 403 |
| 11:15 AM | 10 | 100 | 15 | 17 | 33 | 18 | 27 | 89 | 20 | 20 | 37 | 28 | 414 |
| 11:30 AM | 27 | 130 | 34 | 23 | 38 | 17 | 20 | 86 | 28 | 20 | 53 | 36 | 512 |
| 11:45 AM | 16 | 103 | 20 | 28 | 38 | 26 | 24 | 88 | 23 | 21 | 54 | 27 | 468 |
| Total | 65 | 400 | 89 | 92 | 151 | 75 | 98 | 359 | 87 | 80 | 196 | 105 | 1797 |
| 12:00 PM | 20 | 107 | 18 | 27 | 34 | 16 | 14 | 82 | 13 | 19 | 35 | 32 | 417 |
| 12:15 PM | 16 | 92 | 22 | 32 | 38 | 18 | 26 | 92 | 16 | 24 | 44 | 23 | 443 |
| 12:30 PM | 10 | 88 | 18 | 25 | 39 | 26 | 22 | 87 | 22 | 19 | 32 | 26 | 414 |
| 12:45 PM | 19 | 92 | 23 | 15 | 36 | 17 | 15 | 96 | 14 | 19 | 43 | 33 | 422 |
| Total | 65 | 379 | 81 | 99 | 147 | 77 | 77 | 357 | 65 | 81 | 154 | 114 | 1696 |
| 01:00 PM | 16 | 72 | 15 | 22 | 35 | 18 | 19 | 101 | 27 | 18 | 40 | 22 | 405 |
| 01:15 PM | 15 | 79 | 15 | 27 | 41 | 23 | 24 | 87 | 16 | 23 | 45 | 26 | 421 |
| 01:30 PM | 12 | 82 | 17 | 20 | 44 | 19 | 18 | 75 | 17 | 16 | 29 | 23 | 372 |
| 01:45 PM | 16 | 89 | 15 | 25 | 28 | 20 | 24 | 99 | 8 | 17 | 24 | 27 | 392 |
| Total | 59 | 322 | 62 | 94 | 148 | 80 | 85 | 362 | 68 | 74 | 138 | 98 | 1590 |
| Grand Total | 189 | 1101 | 232 | 285 | 446 | 232 | 260 | 1078 | 220 | 235 | 488 | 317 | 5083 |
| Apprch \% | 12.4 | 72.3 | 15.2 | 29.6 | 46.3 | 24.1 | 16.7 | 69.2 | 14.1 | 22.6 | 46.9 | 30.5 |  |
| Total \% | 3.7 | 21.7 | 4.6 | 5.6 | 8.8 | 4.6 | 5.1 | 21.2 | 4.3 | 4.6 | 9.6 | 6.2 |  |


| Groups Printed- Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Route 125 From North |  |  | Route 9 From East |  |  | Route 125 From South |  |  | Route 9 From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 11:00 AM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 11:15 AM | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 4 |
| 11:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 5 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 7 |
| 12:00 PM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 3 |
| 12:15 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| 12:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 6 |
| 01:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 01:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 01:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01:45 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 3 |
| Total | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 6 |
| Grand Total | 0 | 9 | 0 | 0 | 1 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 19 |
| Apprch \% | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 |  |
| Total \% | 0 | 47.4 | 0 | 0 | 5.3 | 0 | 0 | 47.4 | 0 | 0 | 0 | 0 |  |

N/S Street: Route 125 City/State : Barrington, NH Weather : Clear

 $\stackrel{\leftrightarrow}{2}$


Peak Hour Analysis From 11:00 AM to 01:45 PM - Peak 1 of 1 City/State : Barrington, NH
Weather : Clear

File Name: 81880002


|  | Route 125 <br> From North |  |  |  | Old Green Hill Rd From East |  |  |  | Roule 125 <br> From South |  |  |  | Scruton Pond Rd From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 07:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:00 AM | 0 | 203 | 2 | 205 | 0 | 0 | 0 | 0 | 0 | 92 | 0 | 92 | 8 | 0 | 8 | 16 | 313 |
| 07:15 AM | 0 | 221 | 2 | 223 | 0 | 0 | 0 | 0 | 1 | 117 | 0 | 118 | 13 | 0 | 9 | 22 | 363 |
| 07:30 AM | 0 | 211 | 5 | 216 | 0 | 0 | 0 | 0 | 1 | 98 | 0 | 99 | 9 | 0 | 5 | 14 | 329 |
| 07:45 AM | 0 | 194 | 0 | 194 | 0 | 0 | 0 | 0 | 2 | 124 | 0 | 126 | 14 | 0 | 7 | 21 | 341 |
| Total Volume | 0 | 829 | 9 | 838 | 0 | 0 | 0 | 0 | 4 | 431 | 0 | 435 | 44 | 0 | 29 | 73 | 1346 |
| \% App. Total | 0 | 98.9 | 1.1 |  | 0 | 0 | 0 |  | 0.9 | 99.1 | 0 |  | 60.3 | 0 | 39.7 |  |  |
| PHF | . 000 | . 938 | . 450 | . 939 | . 000 | . 000 | . 000 | . 000 | . 500 | . 869 | . 000 | . 863 | . 786 | . 000 | . 806 | . 830 | . 927 |
| Cars | 0 | 791 | 9 | 800 | 0 | 0 | 0 | 0 | 4 | 404 | 0 | 408 | 44 | 0 | 29 | 73 | 1281 |
| \% Cars | 0 | 95.4 | 100 | 95.5 | 0 | 0 | 0 | 0 | 100 | 93.7 | 0 | 93.8 | 100 | 0 | 100 | 100 | 95.2 |
| Trucks | 0 | 38 | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 27 | 0 | 27 | 0 | 0 | 0 | 0 | 65 |
| \% Trucks | 0 | 4.6 | 0 | 4.5 | 0 | 0 | 0 | 0 | 0 | 6.3 | 0 | 6.2 | 0 | 0 | 0 | 0 | 4.8 |


Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1


| $07: 00 \mathrm{AM}$ |
| :---: |
| 8 |
| 13 |
| 9 |
| 14 |
| 44 |


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| $07: 15$ AM |
| :---: |
| 1 |
| 1 |
| 2 |
| 1 |
| 5 |


| Accurate Counts <br> 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 <br> ENW Street: Scruton Pond R <br> City/State : Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Star Pag | $\begin{aligned} & : 81880002 \\ & : 81880002 \\ & : 3 / 7 / 2019 \\ & : 5 \end{aligned}$ |
| Groups Printed-Cars |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 <br> From North |  |  | Old Green Hill Rd From East |  |  | Route 125 From South |  |  | Scruton Pond Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 07:00 AM | 0 | 191 | 2 | 0 | 0 | 0 | 0 | 89 | 0 | 8 | 0 | 8 | 298 |
| 07:15 AM | 0 | 212 | 2 | 0 | 0 | 0 | 1 | 108 | 0 | 13 | 0 | 9 | 345 |
| 07:30 AM | 0 | 202 | 5 | 0 | 0 | 0 | 1 | 89 | 0 | 9 | 0 | 5 | 311 |
| 07:45 AM | 0 | 186 | 0 | 0 | 0 | 0 | 2 | 118 | 0 | 14 | 0 | 7 | 327 |
| Total | 0 | 791 | 9 | 0 | 0 | 0 | 4 | 404 | 0 | 44 | 0 | 29 | 1281 |
| 08:00 AM | 0 | 147 | 4 | 0 | 0 | 0 | 1 | 89 | 0 | 10 | 0 | 4 | 255 |
| 08:15 AM | 0 | 151 | 1 | 0 | 0 | 0 | 1 | 92 | 0 | 4 | 0 | 5 | 254 |
| 08:30 AM | 0 | 123 | 7 | 0 | 0 | 0 | 0 | 104 | 0 | 12 | 0 | 2 | 248 |
| 08:45 AM | 0 | 105 | 7 | 0 | 0 | 0 | 1 | 87 | 0 | 7 | 0 | 2 | 209 |
| Total | 0 | 526 | 19 | 0 | 0 | 0 | 3 | 372 | 0 | 33 | 0 | 13 | 966 |
| Grand Total | 0 | 1317 | 28 | 0 | 0 | 0 | 7 | 776 | 0 | 77 | 0 | 42 | 2247 |
| Apprch \% | 0 | 97.9 | 2.1 | 0 | 0 | 0 | 0.9 | 99.1 | 0 | 64.7 | 0 | 35.3 |  |
| Total \% | 0 | 58.6 | 1.2 | 0 | 0 | 0 | 0.3 | 34.5 | 0 | 3.4 | 0 | 1.9 |  |


N/S Street : Route 125
E/W Street: Scruton Pond Road
City/State : Barrington, NH
Weather : Clear
War :

|  | Route 125 From North |  |  |  | Old Green Hill Rd From East |  |  |  | Route 125 <br> From South |  |  |  | Scruton Pond Rd From West |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Exclu. Total | Inclu. Total | Int. Total |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch \% | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |  |
| Total \% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 |  |

File Name ： 81880002
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|  | Route 125 <br> From North |  |  |  | Old Green Hill Rd <br> From East |  |  |  | Route 125 <br> From South |  |  |  | Scruton Pond Rd From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App．Total | Left | Thru | Right | App．Total | Left | Thru | Right | App．Total | Left | Thru | Right | App．Total | Int．Total |
| Peak Hour Analysis From 07：00 AM to 08：45 AM－Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 07：00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07：00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07：15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07：30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07：45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| \％App．Total | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |
| PHF | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 | ． 000 |

G9Gz-t99-8
squno oqeans.
N/S Street : Route 125 E/W Street: Scruton Pond Road City/State : Barrington, NH
Weather : Clear
Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 Peak Hour for Each Approach Begins at:


| 0 | 0 | 0 | 0 | 0 |
| :--- | :--- | :--- | :--- | :--- |
| 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 |


| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 |
| :--- |
| Peak Hour for Each Approach Begins at: |$|$| 07:00 AM |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: |
| +0 mins. | 0 | 0 | 0 | 0 |
| +15 mins. | 0 | 0 | 0 | 0 |
| +30 mins. | 0 | 0 | 0 | 0 |
| +45 mins. | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 0 | 0 | 0 |



|  | Route 125 <br> From North |  |  |  | Old Green Hill Rd From East |  |  |  | Route 125 <br> From South |  |  |  | Scruton Pond Rd From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 04:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:30 PM | 0 | 120 | 18 | 138 | 0 | 0 | 0 | 0 | 4 | 180 | 0 | 184 | 4 | 0 | 1 | 5 | 327 |
| 04:45 PM | 0 | 122 | 12 | 134 | 0 | 0 | 0 | 0 | 3 | 216 | 0 | 219 | 1 | 0 | 2 | 3 | 356 |
| 05:00 PM | 0 | 107 | 10 | 117 | 0 | 0 | 0 | 0 | 2 | 225 | 0 | 227 | 9 | 0 | 2 | 11 | 355 |
| 05:15 PM | 0 | 116 | 10 | 126 | 0 | 0 | 0 | 0 | 4 | 198 | 0 | 202 | 4 | 0 | 2 | 6 | 334 |
| Total Volume | 0 | 465 | 50 | 515 | 0 | 0 | 0 | 0 | 13 | 819 | 0 | 832 | 18 | 0 | 7 | 25 | 1372 |
| \% App. Total | 0 | 90.3 | 9.7 |  | 0 | 0 | 0 |  | 1.6 | 98.4 | 0 |  | 72 | 0 | 28 |  |  |
| PHF | . 000 | . 953 | . 694 | . 933 | . 000 | . 000 | . 000 | . 000 | . 813 | . 910 | . 000 | . 916 | . 500 | . 000 | . 875 | . 568 | . 963 |
| Cars | 0 | 459 | 50 | 509 | 0 | 0 | 0 | 0 | 13 | 816 | 0 | 829 | 18 | 0 | 7 | 25 | 1363 |
| \% Cars | 0 | 98.7 | 100 | 98.8 | 0 | 0 | 0 | 0 | 100 | 99.6 | 0 | 99.6 | 100 | 0 | 100 | 100 | 99.3 |
| Trucks | 0 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 9 |
| \% Trucks | 0 | 1.3 | 0 | 1.2 | 0 | 0 | 0 | 0 | 0 | 0.4 | 0 | 0.4 | 0 | 0 | 0 | 0 | 0.7 |



Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 Peak Hour for Each Approach Begins at:

|  | 04:00 PM |  |  |  | 04:00 PM |  |  |  | 04:30 PM |  |  |  | 05:00 PM |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| +0 mins. | 0 | 144 | 10 | 154 | 0 | 0 | 0 | 0 | 4 | 180 | 0 | 184 | 9 | 0 | 2 | 11 |
| +15 mins. | 0 | 119 | 7 | 126 | 0 | 0 | 0 | 0 | 3 | 216 | 0 | 219 | 4 | 0 | 2 | 6 |
| +30 mins. | 0 | 120 | 18 | 138 | 0 | 0 | 0 | 0 | 2 | 225 | 0 | 227 | 3 | 0 | 6 | 9 |
| +45 mins. | 0 | 122 | 12 | 134 | 0 | 0 | 0 | 0 | 4 | 198 | 0 | 202 | 3 | 0 | 5 | 8 |
| Total Volume | 0 | 505 | 47 | 552 | 0 | 0 | 0 | 0 | 13 | 819 | 0 | 832 | 19 | 0 | 15 | 34 |


| Accurate Counts 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 E/W Street: Scruton Pond Ro City/State : Barrington, NH Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Star Pag | $\begin{aligned} & : 81880002 \\ & : 81880002 \\ & : 3 / 7 / 2019 \\ & : 5 \end{aligned}$ |
| Groups Printed-Cars |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 From North |  |  | Old Green Hill Rd From East |  |  | Route 125 <br> From South |  |  | Scruton Pond Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 04:00 PM | 0 | 138 | 10 | 0 | 0 | 0 | 5 | 210 | 0 | 1 | 0 | 4 | 368 |
| 04:15 PM | 0 | 117 | 7 | 0 | 0 | 0 | 2 | 176 | 0 | 1 | 0 | 2 | 305 |
| 04:30 PM | 0 | 119 | 18 | 0 | 0 | 0 | 4 | 178 | 0 | 4 | 0 | 1 | 324 |
| 04:45 PM | 0 | 121 | 12 | 0 | 0 | 0 | 3 | 215 | 0 | 1 | 0 | 2 | 354 |
| Total | 0 | 495 | 47 | 0 | 0 | 0 | 14 | 779 | 0 | 7 | 0 | 9 | 1351 |
| 05:00 PM | 0 | 106 | 10 | 0 | 0 | 0 | 2 | 225 | 0 | 9 | 0 | 2 | 354 |
| 05:15 PM | 0 | 113 | 10 | 0 | 0 | 0 | 4 | 198 | 0 | 4 | 0 | 2 | 331 |
| 05:30 PM | 0 | 86 | 8 | 0 | 0 | 0 | 6 | 168 | 0 | 3 | 0 | 6 | 277 |
| 05:45 PM | 0 | 88 | 9 | 0 | 0 | 0 | 4 | 165 | 0 | 3 | 0 | 5 | 274 |
| Total | 0 | 393 | 37 | 0 | 0 | 0 | 16 | 756 | 0 | 19 | 0 | 15 | 1236 |
| Grand Total | 0 | 888 | 84 | 0 | 0 | 0 | 30 | 1535 | 0 | 26 | 0 | 24 | 2587 |
| Apprch \% | 0 | 91.4 | 8.6 | 0 | 0 | 0 | 1.9 | 98.1 | 0 | 52 | 0 | 48 |  |
| Total \% | 0 | 34.3 | 3.2 | 0 | 0 | 0 | 1.2 | 59.3 | 0 | 1 | 0 | 0.9 |  |


| Accurate Counts 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 <br> ENW Street: Scruton Pond R <br> City/State : Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Star Pag | $\begin{aligned} & : 81880002 \\ & : 81880002 \\ & : 3 / 7 / 2019 \\ & : 9 \end{aligned}$ |
| Groups Printed- Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 <br> From North |  |  | Old Green Hill Rd From East |  |  | Route 125 <br> From South |  |  | Scruton Pond Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 04:00 PM | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 7 |
| 04:15 PM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 7 |
| 04:30 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 3 |
| 04:45 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| Total | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 19 |
| 05:00 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:15 PM | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 05:30 PM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 4 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 9 |
| Grand Total | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 28 |
| Apprch \% | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 0 | 0 |  |
| Total \% | 0 | 57.1 | 0 | 0 | 0 | 0 | 0 | 42.9 | 0 | 0 | 0 | 0 |  |

File Name : 81880002
Site Code $: 81880002$
Start Date $: 3 / 712019$

|  | Route 125 <br> From North |  |  |  | Old Green Hill Rd From East |  |  |  | Route 125 From South |  |  |  | Scruton Pond Rd From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 04:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:00 PM | 0 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 7 |
| 04:15 PM | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 7 |
| 04:30 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 3 |
| 04:45 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| Total Volume | 0 | 10 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 9 | 0 | 0 | 0 | 0 | 19 |
| \% App. Total | 0 | 100 | 0 |  | 0 | 0 | 0 |  | 0 | 100 | 0 |  | 0 | 0 | 0 |  |  |
| PHF | . 000 | . 417 | . 000 | . 417 | . 000 | . 000 | . 000 | . 000 | . 000 | . 450 | . 000 | . 450 | . 000 | . 000 | . 000 | . 000 | . 679 |

File Name : 81880002
6L0ZIL ル: on abed


|  |  |  |
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|  |  |  |
|  |  |  |

N/S Street : Route 125 EN Street: Scruton Pond Road
City/State: Barrington, NH
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|  | Groups Printed-Bikes Peds |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Route 125 From North |  |  |  | Old Green Hill Rd From East |  |  |  | Route 125 From South |  |  |  | Scruton Pond Rd From West |  |  |  |  |  |  |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Exclu. Total | Inclu. Total | Int. Total |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch \% | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |  |
| Total \% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 |  |

File Name: 81880002
Site Code : 81880002
Start Date : $3 / 712019$
Page No : 14

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Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of ENW Street: Scruton Pond Road
City/State : Barrington, NH
Weather : Clear :

|  | 04:00 PM |  |  |  | 04:00 PM |  |  |  | 04:00 PM |  |  |  | 04:00 PM |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| +0 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +30 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +45 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

N/S Street : Route 125
City/State : Barrington, NH

| Groups Printed- Cars - Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Route 125 From North |  |  | Old Green Hill Rd From East |  |  | Route 125 From South |  |  | Scruton Pond Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 11:00 AM | 0 | 107 | 12 | 0 | 0 | 0 | 5 | 132 | 0 | 11 | 0 | 5 | 272 |
| 11:15 AM | 0 | 134 | 6 | 0 | 0 | 0 | 3 | 124 | 0 | 15 | 0 | 3 | 285 |
| 11:30 AM | 0 | 166 | 4 | 0 | 0 | 0 | 4 | 111 | 0 | 6 | 0 | 1 | 292 |
| 11:45 AM | 0 | 141 | 10 | 0 | 0 | 0 | 2 | 123 | 0 | 10 | 0 | 2 | 288 |
| Total | 0 | 548 | 32 | 0 | 0 | 0 | 14 | 490 | 0 | 42 | 0 | 11 | 1137 |
| 12:00 PM | 0 | 124 | 10 | 0 | 0 | 0 | 2 | 111 | 0 | 6 | 0 | 4 | 257 |
| 12:15 PM | 0 | 122 | 6 | 0 | 0 | 0 | 1 | 123 | 0 | 9 | 0 | 6 | 267 |
| 12:30 PM | 0 | 112 | 7 | 0 | 0 | 0 | 2 | 132 | 0 | 7 | 0 | 4 | 264 |
| 12:45 PM | 0 | 106 | 10 | 0 | 0 | 0 | 4 | 140 | 0 | 12 | 0 | 3 | 275 |
| Total | 0 | 464 | 33 | 0 | 0 | 0 | 9 | 506 | 0 | 34 | 0 | 17 | 1063 |
| 01:00 PM | 0 | 116 | 8 | 0 | 0 | 0 | 3 | 126 | 0 | 8 | 0 | 5 | 266 |
| 01:15 PM | 0 | 103 | 11 | 0 | 0 | 0 | 3 | 118 | 0 | 5 | 0 | 2 | 242 |
| 01:30 PM | 0 | 125 | 4 | 0 | 0 | 0 | 5 | 116 | 0 | 5 | 0 | 3 | 258 |
| 01:45 PM | 0 | 109 | 8 | 0 | 0 | 0 | 1 | 123 | 0 | 3 | 0 | 2 | 246 |
| Total | 0 | 453 | 31 | 0 | 0 | 0 | 12 | 483 | 0 | 21 | 0 | 12 | 1012 |
| Grand Total | 0 | 1465 | 96 | 0 | 0 | 0 | 35 | 1479 | 0 | 97 | 0 | 40 | 3212 |
| Apprch \% | 0 | 93.9 | 6.1 | 0 | 0 | 0 | 2.3 | 97.7 | 0 | 70.8 | 0 | 29.2 |  |
| Total \% | 0 | 45.6 | 3 | 0 | 0 | 0 | 1.1 | 46 | 0 | 3 | 0 | 1.2 |  |
| Cars | 0 | 1456 | 96 | 0 | 0 | 0 | 35 | 1470 | 0 | 97 | 0 | 40 | 3194 |
| \% Cars | 0 | 99.4 | 100 | 0 | 0 | 0 | 100 | 99.4 | 0 | 100 | 0 | 100 | 99.4 |
| Trucks | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 18 |
| \% Trucks | 0 | 0.6 | 0 | 0 | 0 | 0 | 0 | 0.6 | 0 | 0 | 0 | 0 | 0.6 |


| N/S Street : Route 125 EN Street: Scruton P City/State : Barrington Weather : Clear | Road H |  |  |  |  |  |  |  |  |  |  |  |  |  |  | File Nam Site Co Start D Page | $\begin{aligned} & : 818800 \mathrm{~S} 2 \\ & : 81880002 \\ & : 3 / 9 / 2019 \\ & : 2 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Rou } \\ & \text { Fron } \end{aligned}$ |  |  |  |  | $\begin{aligned} & \text { Hill Ro } \\ & \text { ast } \end{aligned}$ |  |  |  |  |  |  | $\begin{aligned} & \text { crutor } \\ & \text { Fror } \end{aligned}$ | nd Rd /est |  |  |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis F | 11:00 | to 01: | PM - P | k 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire | sectio | egins a | 1:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM | 0 | 107 | 12 | 119 | 0 | 0 | 0 | 0 | 5 | 132 | 0 | 137 | 11 | 0 | 5 | 16 | 272 |
| 11:15 AM | 0 | 134 | 6 | 140 | 0 | 0 | 0 | 0 | 3 | 124 | 0 | 127 | 15 | 0 | 3 | 18 | 285 |
| 11:30 AM | 0 | 166 | 4 | 170 | 0 | 0 | 0 | 0 | 4 | 111 | 0 | 115 | 6 | 0 | 1 | 7 | 292 |
| 11:45 AM | 0 | 141 | 10 | 151 | 0 | 0 | 0 | 0 | 2 | 123 | 0 | 125 | 10 | 0 | 2 | 12 | 288 |
| Total Volume | 0 | 548 | 32 | 580 | 0 | 0 | 0 | 0 | 14 | 490 | 0 | 504 | 42 | 0 | 11 | 53 | 1137 |
| \% App. Total | 0 | 94.5 | 5.5 |  | 0 | 0 | 0 |  | 2.8 | 97.2 | 0 |  | 79.2 | 0 | 20.8 |  |  |
| PHF | . 000 | . 825 | . 667 | . 853 | . 000 | . 000 | . 000 | . 000 | . 700 | . 928 | . 000 | . 920 | . 700 | . 000 | . 550 | . 736 | . 973 |
| Cars | 0 | 541 | 32 | 573 | 0 | 0 | 0 | 0 | 14 | 488 | 0 | 502 | 42 | 0 | 11 | 53 | 1128 |
| \% Cars | 0 | 98.7 | 100 | 98.8 | 0 | 0 | 0 | 0 | 100 | 99.6 | 0 | 99.6 | 100 | 0 | 100 | 100 | 99.2 |
| Trucks | 0 | 7 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 9 |
| \% Trucks | 0 | 1.3 | 0 | 1.2 | 0 | 0 | 0 | 0 | 0 | 0.4 | 0 | 0.4 | 0 | 0 | 0 | 0 | 0.8 |


Peak Hour Analysis From 11：00 AM to 01：45 PM－Peak 1 of 1

|  | 11：15 AM |  |  |  | 11：00 AM |  |  |  | 12：15 PM |  |  |  | 12：15 PM |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ＋0 mins． | 0 | 134 | 6 | 140 | 0 | 0 | 0 | 0 | 1 | 123 | 0 | 124 | 9 | 0 | 6 | 15 |
| ＋15 mins． | 0 | 166 | 4 | 170 | 0 | 0 | 0 | 0 | 2 | 132 | 0 | 134 | 7 | 0 | 4 | 11 |
| ＋ 30 mins． | 0 | 141 | 10 | 151 | 0 | 0 | 0 | 0 | 4 | 140 | 0 | 144 | 12 | 0 | 3 | 15 |
| ＋45 mins． | 0 | 124 | 10 | 134 | 0 | 0 | 0 | 0 | 3 | 126 | 0 | 129 | 8 | 0 | 5 | 13 |
| Total Volume | 0 | 565 | 30 | 595 | 0 | 0 | 0 | 0 | 10 | 521 | 0 | 531 | 36 | 0 | 18 | 54 |
| \％App．Total | 0 | 95 | 5 |  | 0 | 0 | 0 |  | 1.9 | 98.1 | 0 |  | 66.7 | 0 | 33.3 |  |
| PHF | ． 000 | ． 851 | ． 750 | ． 875 | ． 000 | ． 000 | ． 000 | ． 000 | ． 625 | ． 930 | ． 000 | ． 922 | ． 750 | ． 000 | ． 750 | ． 900 |

－＋응ㅇㅆㄴ액


| 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Groups Printed-Cars |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Route 125 <br> From North |  |  | Old Green Hill Rd From East |  |  | Route 125 From South |  |  | Scruton Pond Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 11:00 AM | 0 | 104 | 12 | 0 | 0 | 0 | 5 | 131 | 0 | 11 | 0 | 5 | 268 |
| 11:15 AM | 0 | 132 | 6 | 0 | 0 | 0 | 3 | 123 | 0 | 15 | 0 | 3 | 282 |
| 11:30 AM | 0 | 166 | 4 | 0 | 0 | 0 | 4 | 111 | 0 | 6 | 0 | 1 | 292 |
| 11:45 AM | 0 | 139 | 10 | 0 | 0 | 0 | 2 | 123 | 0 | 10 | 0 | 2 | 286 |
| Total | 0 | 541 | 32 | 0 | 0 | 0 | 14 | 488 | 0 | 42 | 0 | 11 | 1128 |
| 12:00 PM | 0 | 124 | 10 | 0 | 0 | 0 | 2 | 111 | 0 | 6 | 0 | 4 | 257 |
| 12:15 PM | 0 | 120 | 6 | 0 | 0 | 0 | 1 | 122 | 0 | 9 | 0 | 6 | 264 |
| 12:30 PM | 0 | 112 | 7 | 0 | 0 | 0 | 2 | 132 | 0 | 7 | 0 | 4 | 264 |
| 12:45 PM | 0 | 106 | 10 | 0 | 0 | 0 | 4 | 140 | 0 | 12 | 0 | 3 | 275 |
| Total | 0 | 462 | 33 | 0 | 0 | 0 | 9 | 505 | 0 | 34 | 0 | 17 | 1060 |
| 01:00 PM | 0 | 116 | 8 | 0 | 0 | 0 | 3 | 124 | 0 | 8 | 0 | 5 | 264 |
| 01:15 PM | 0 | 103 | 11 | 0 | 0 | 0 | 3 | 116 | 0 | 5 | 0 | 2 | 240 |
| 01:30 PM | 0 | 125 | 4 | 0 | 0 | 0 | 5 | 115 | 0 | 5 | 0 | 3 | 257 |
| 01:45 PM | 0 | 109 | 8 | 0 | 0 | 0 | 1 | 122 | 0 | 3 | 0 | 2 | 245 |
| Total | 0 | 453 | 31 | 0 | 0 | 0 | 12 | 477 | 0 | 21 | 0 | 12 | 1006 |
| Grand Total | 0 | 1456 | 96 | 0 | 0 | 0 | 35 | 1470 | 0 | 97 | 0 | 40 | 3194 |
| Apprch \% | 0 | 93.8 | 6.2 | 0 | 0 | 0 | 2.3 | 97.7 | 0 | 70.8 | 0 | 29.2 |  |
| Total \% | 0 | 45.6 | 3 | 0 | 0 | 0 | 1.1 | 46 | 0 | 3 | 0 | 1.3 |  |


| N/S Street : Route 125 <br> EM Street: Scruton Pond R <br> City/State : Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Sta Pag |  | $\begin{aligned} & 81880052 \\ & 81880002 \\ & 3 / 9 / 2019 \\ & 9 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | rinted- |  |  |  |  |  |  |  |  |
|  |  | 125 North |  |  | $\begin{aligned} & \text { n Hill } \\ & \text { East } \end{aligned}$ |  |  | 125 <br> South |  |  | Pond West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  | Int. Total |
| 11:00 AM | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 |  | 4 |
| 11:15 AM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 |  | 3 |
| 11:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |
| 11:45 AM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 2 |
| Total | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 |  | 9 |
| 12:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |
| 12:15 PM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 |  | 3 |
| 12:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |
| 12:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |
| Total | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 |  | 3 |
| 01:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 |  | 2 |
| 01:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 |  | 2 |
| 01:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 |  | 1 |
| 01:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 |  | 1 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 |  | 6 |
| Grand Total | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 |  | 18 |
| Apprch \% | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 0 | 0 |  |  |
| Total \% | 0 | 50 | 0 | 0 | 0 | 0 | 0 | 50 | 0 | 0 | 0 | 0 |  |  |


| Groups Printed－Bikes Peds |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Exclu．Total | Inclu．Total | Int．Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Route 125 From North |  |  |  | Old Green Hill Rd From East |  |  |  | Route 125 From South |  |  |  | Scruton Pond Rd From West |  |  |  |  |  |  |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds |  |  |  |
| 11：00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11：15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11：30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11：45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12：00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12：15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12：30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12：45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01：00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01：15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01：30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01：45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch \％ | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |  |
| Total \％ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 |  |


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2命
File Name :
Site Code :
Start Date :
Page No :

 N/S Street : Route 125 R Road City/State : Barrington, NH Weather : Clear
N/S Street : Route 125 City/State : Barrington, NH Weather : Clear


[^12]|  | Route 125 <br> From North |  |  |  | Tolend Rd <br> From East |  |  |  | Route 125 From South |  |  |  | Greenhill Rd <br> From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 07:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:00 AM | 0 | 174 | 2 | 176 | 7 | 1 | 3 | 11 | 1 | 90 | 3 | 94 | 3 | 4 | 25 | 32 | 313 |
| 07:15 AM | 1 | 196 | 1 | 198 | 2 | 4 | 0 | 6 | 7 | 111 | 6 | 124 | 3 | 9 | 29 | 41 | 369 |
| 07:30 AM | 5 | 187 | 0 | 192 | 5 | 1 | 2 | 8 | 5 | 111 | 4 | 120 | 4 | 7 | 19 | 30 | 350 |
| 07:45 AM | 7 | 173 | 1 | 181 | 5 | 0 | 6 | 11 | 2 | 112 | 8 | 122 | 4 | 12 | 24 | 40 | 354 |
| Total Volume | 13 | 730 | 4 | 747 | 19 | 6 | 11 | 36 | 15 | 424 | 21 | 460 | 14 | 32 | 97 | 143 | 1386 |
| \% App. Total | 1.7 | 97.7 | 0.5 |  | 52.8 | 16.7 | 30.6 |  | 3.3 | 92.2 | 4.6 |  | 9.8 | 22.4 | 67.8 |  |  |
| PHF | . 464 | . 931 | . 500 | . 943 | . 679 | . 375 | . 458 | . 818 | . 536 | . 946 | . 656 | . 927 | . 875 | . 667 | . 836 | . 872 | . 939 |
| Cars | 13 | 689 | 4 | 706 | 19 | 6 | 10 | 35 | 14 | 402 | 16 | 432 | 14 | 32 | 96 | 142 | 1315 |
| \% Cars | 100 | 94.4 | 100 | 94.5 | 100 | 100 | 90.9 | 97.2 | 93.3 | 94.8 | 76.2 | 93.9 | 100 | 100 | 99.0 | 99.3 | 94.9 |
| Trucks | 0 | 41 | 0 | 41 | 0 | 0 | 1 | 1 | 1 | 22 | 5 | 28 | 0 | 0 | 1 | 1 | 71 |
| \% Trucks | 0 | 5.6 | 0 | 5.5 | 0 | 0 | 9.1 | 2.8 | 6.7 | 5.2 | 23.8 | 6.1 | 0 | 0 | 1.0 | 0.7 | 5.1 |



Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

|  | 07:00 AM |  |  |  | 07:30 AM |  |  |  | 07:15 AM |  |  |  | 07:00 AM |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| +0 mins. | 0 | 174 | 2 | 176 | 5 | 1 | 2 | 8 | 7 | 111 | 6 | 124 | 3 | 4 | 25 | 32 |
| +15 mins. | 1 | 196 | 1 | 198 | 5 | 0 | 6 | 11 | 5 | 111 | 4 | 120 | 3 | 9 | 29 | 41 |
| +30 mins. | 5 | 187 | 0 | 192 | 1 | 2 | 5 | 8 | 2 | 112 | 8 | 122 | 4 | 7 | 19 | 30 |
| +45 mins. | 7 | 173 | 1 | 181 | 9 | 3 | 1 | 13 | 4 | 110 | 3 | 117 | 4 | 12 | 24 | 40 |
| Total Volume | 13 | 730 | 4 | 747 | 20 | 6 | 14 | 40 | 18 | 444 | 21 | 483 | 14 | 32 | 97 | 143 |


| Accurate Counts 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 <br> ENW Street: Greenhill Rd / To <br> City/State : Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Star Pag | $\begin{aligned} & : 81880003 \\ & : 81880003 \\ & : 3 / 7 / 2019 \\ & : 5 \end{aligned}$ |
| Groups Printed-Cars |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 <br> From North |  |  | Tolend Rd From East |  |  | Route 125 From South |  |  | Greenhill Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 07:00 AM | 0 | 162 | 2 | 7 | 1 | 3 | 1 | 86 | 3 | 3 | 4 | 24 | 296 |
| 07:15 AM | 1 | 188 | 1 | 2 | 4 | 0 | 7 | 105 | 4 | 3 | 9 | 29 | 353 |
| 07:30 AM | 5 | 175 | 0 | 5 | 1 | 2 | 4 | 103 | 3 | 4 | 7 | 19 | 328 |
| 07:45 AM | 7 | 164 | 1 | 5 | 0 | 5 | 2 | 108 | 6 | 4 | 12 | 24 | 338 |
| Total | 13 | 689 | 4 | 19 | 6 | 10 | 14 | 402 | 16 | 14 | 32 | 96 | 1315 |
| 08:00 AM | 3 | 118 | 2 | 1 | 2 | 5 | 4 | 108 | 3 | 3 | 3 | 25 | 277 |
| 08:15 AM | 5 | 118 | 1 | 9 | 3 | 1 | 5 | 82 | 3 | 3 | 11 | 21 | 262 |
| 08:30 AM | 1 | 114 | 3 | 2 | 1 | 2 | 5 | 106 | 10 | 4 | 5 | 9 | 262 |
| 08:45 AM | 5 | 102 | 4 | 0 | 2 | 6 | 7 | 94 | 2 | 1 | 5 | 10 | 238 |
| Total | 14 | 452 | 10 | 12 | 8 | 14 | 21 | 390 | 18 | 11 | 24 | 65 | 1039 |
| Grand Total | 27 | 1141 | 14 | 31 | 14 | 24 | 35 | 792 | 34 | 25 | 56 | 161 | 2354 |
| Apprch \% | 2.3 | 96.5 | 1.2 | 44.9 | 20.3 | 34.8 | 4.1 | 92 | 3.9 | 10.3 | 23.1 | 66.5 |  |
| Total \% | 1.1 | 48.5 | 0.6 | 1.3 | 0.6 | 1 | 1.5 | 33.6 | 1.4 | 1.1 | 2.4 | 6.8 |  |

File Name : 81880003
Site Code : 81880003
Start Date : $3 / 7 / 2019$

| Groups Printed- Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Route 125 <br> From North |  |  | Tolend Rd From East |  |  | Route 125 <br> From South |  |  | Greenhill Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 07:00 AM | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 1 | 17 |
| 07:15 AM | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 16 |
| 07:30 AM | 0 | 12 | 0 | 0 | 0 | 0 | 1 | 8 | 1 | 0 | 0 | 0 | 22 |
| 07:45 AM | 0 | 9 | 0 | 0 | 0 | 1 | 0 | 4 | 2 | 0 | 0 | 0 | 16 |
| Total | 0 | 41 | 0 | 0 | 0 | 1 | 1 | 22 | 5 | 0 | 0 | 1 | 71 |
| 08:00 AM | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 12 |
| 08:15 AM | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 9 |
| 08:30 AM | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 14 |
| 08:45 AM | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 14 |
| Total | 1 | 21 | 0 | 0 | 0 | 0 | 0 | 26 | 0 | 0 | 0 | 1 | 49 |
| Grand Total | 1 | 62 | 0 | 0 | 0 | 1 | 1 | 48 | 5 | 0 | 0 | 2 | 120 |
| Apprch \% | 1.6 | 98.4 | 0 | 0 | 0 | 100 | 1.9 | 88.9 | 9.3 | 0 | 0 | 100 |  |
| Total \% | 0.8 | 51.7 | 0 | 0 | 0 | 0.8 | 0.8 | 40 | 4.2 | 0 | 0 | 1.7 |  |


| N/S Street : Route 1 <br> E/N Street: Greenh <br> City/State : Barringt <br> Weather : Clear | NH | d Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & 81880003 \\ & 81880003 \\ & 3 / 7 / 2019 \\ & 13 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | Grou | Printe | Bikes P |  |  |  |  |  |  |  |  |  |
|  |  | Route From |  |  |  | Tolen From |  |  |  | Rout From | $\begin{aligned} & 125 \\ & \text { outh } \end{aligned}$ |  |  | Green From | $\begin{aligned} & 1 \mathrm{Rd} \\ & \text { est } \end{aligned}$ |  |  |  |  |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Exclu. Total | Inclu. Total | Int. Total |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch \% | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |  |
| Total \% |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 |  |


|  | Route 125 <br> From North |  |  |  | Tolend Rd <br> From East |  |  |  | Route 125 <br> From South |  |  |  | Greenhill Rd From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 07:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| \% App. Total | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |
| PHF | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 |

600088 8: әpaply

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Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

|  | 07:00 AM |  |  |  | 07:00 AM |  |  |  | 07:00 AM |  |  |  | 07:00 AM |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| +0 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +30 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +45 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| Accurate Counts 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 <br> EN Street: Greenhill Rd / T <br> City/State : Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Star Page | $\begin{aligned} & : 81880003 \\ & : 81880003 \\ & : 3 / 7 / 2019 \\ & : 1 \end{aligned}$ |
| Groups Printed-Cars - Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 From North |  |  | Tolend Rd From East |  |  | Route 125From South |  |  | Greenhill Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 04:00 PM | 7 | 136 | 4 | 7 | 4 | 8 | 21 | 184 | 6 | 3 | 2 | 10 | 392 |
| 04:15 PM | 3 | 111 | 4 | 12 | 11 | 6 | 22 | 156 | 3 | 0 | 4 | 5 | 337 |
| 04:30 PM | 2 | 119 | 7 | 9 | 3 | 6 | 21 | 164 | 7 | 6 | 2 | 6 | 352 |
| 04:45 PM | 6 | 115 | 6 | 9 | 5 | 7 | 25 | 195 | 5 | 3 | 3 | 10 | 389 |
| Total | 18 | 481 | 21 | 37 | 23 | 27 | 89 | 699 | 21 | 12 | 11 | 31 | 1470 |
| 05:00 PM | 6 | 102 | 4 | 8 | 9 | 4 | 33 | 177 | 9 | 5 | 4 | 8 | 369 |
| 05:15 PM | 2 | 103 | 5 | 10 | 12 | 7 | 22 | 167 | 7 | 3 | 0 | 8 | 346 |
| 05:30 PM | 6 | 81 | 3 | 5 | 5 | 2 | 19 | 157 | 3 | 4 | 4 | 12 | 301 |
| 05:45 PM | 4 | 89 | 2 | 6 | 5 | 4 | 20 | 158 | 1 | 3 | 3 | 6 | 301 |
| Total | 18 | 375 | 14 | 29 | 31 | 17 | 94 | 659 | 20 | 15 | 11 | 34 | 1317 |
| Grand Total | 36 | 856 | 35 | 66 | 54 | 44 | 183 | 1358 | 41 | 27 | 22 | 65 | 2787 |
| Apprch \% | 3.9 | 92.3 | 3.8 | 40.2 | 32.9 | 26.8 | 11.6 | 85.8 | 2.6 | 23.7 | 19.3 | 57 |  |
| Total \% | 1.3 | 30.7 | 1.3 | 2.4 | 1.9 | 1.6 | 6.6 | 48.7 | 1.5 | 1 | 0.8 | 2.3 |  |
| Cars | 36 | 840 | 35 | 66 | 54 | 43 | 183 | 1345 | 41 | 27 | 22 | 65 | 2757 |
| \% Cars | 100 | 98.1 | 100 | 100 | 100 | 97.7 | 100 | 99 | 100 | 100 | 100 | 100 | 98.9 |
| Trucks | 0 | 16 | 0 | 0 | 0 | 1 | 0 | 13 | 0 | 0 | 0 | 0 | 30 |
| \% Trucks | 0 | 1.9 | 0 | 0 | 0 | 2.3 | 0 | 1 | 0 | 0 | 0 | 0 | 1.1 |


|  | Route 125 <br> From North |  |  |  | Tolend Rd <br> From East |  |  |  | Route 125 <br> From South |  |  |  | Greenhill Rd From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 04:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:00 PM | 7 | 136 | 4 | 147 | 7 | 4 | 8 | 19 | 21 | 184 | 6 | 211 | 3 | 2 | 10 | 15 | 392 |
| 04:15 PM | 3 | 111 | 4 | 118 | 12 | 11 | 6 | 29 | 22 | 156 | 3 | 181 | 0 | 4 | 5 | 9 | 337 |
| 04:30 PM | 2 | 119 | 7 | 128 | 9 | 3 | 6 | 18 | 21 | 164 | 7 | 192 | 6 | 2 | 6 | 14 | 352 |
| 04:45 PM | 6 | 115 | 6 | 127 | 9 | 5 | 7 | 21 | 25 | 195 | 5 | 225 | 3 | 3 | 10 | 16 | 389 |
| Total Volume | 18 | 481 | 21 | 520 | 37 | 23 | 27 | 87 | 89 | 699 | 21 | 809 | 12 | 11 | 31 | 54 | 1470 |
| \% App. Total | 3.5 | 92.5 | 4 |  | 42.5 | 26.4 | 31 |  | 11 | 86.4 | 2.6 |  | 22.2 | 20.4 | 57.4 |  |  |
| PHF | . 643 | . 884 | . 750 | . 884 | . 771 | . 523 | . 844 | . 750 | . 890 | . 896 | . 750 | . 899 | . 500 | . 688 | . 775 | . 844 | . 938 |
| Cars | 18 | 471 | 21 | 510 | 37 | 23 | 26 | 86 | 89 | 688 | 21 | 798 | 12 | 11 | 31 | 54 | 1448 |
| \% Cars | 100 | 97.9 | 100 | 98.1 | 100 | 100 | 96.3 | 98.9 | 100 | 98.4 | 100 | 98.6 | 100 | 100 | 100 | 100 | 98.5 |
| Trucks | 0 | 10 | 0 | 10 | 0 | 0 | 1 | 1 | 0 | 11 | 0 | 11 | 0 | 0 | 0 | 0 | 22 |
| \% Trucks | 0 | 2.1 | 0 | 1.9 | 0 | 0 | 3.7 | 1.1 | 0 | 1.6 | 0 | 1.4 | 0 | 0 | 0 | 0 | 1.5 |

60008818


| Accurate Counts 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 <br> ENW Street: Greenhill Rd / To <br> City/State : Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Star Pag | : 81880003 <br> 81880003 <br> 3/7/2019 <br> : 5 |
| Groups Printed-Cars |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 From North |  |  | Tolend Rd From East |  |  | Route 125 From South |  |  | Greenhill Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 04:00 PM | 7 | 130 | 4 | 7 | 4 | 7 | 21 | 182 | 6 | 3 | 2 | 10 | 383 |
| 04:15 PM | 3 | 108 | 4 | 12 | 11 | 6 | 22 | 152 | 3 | 0 | 4 | 5 | 330 |
| 04:30 PM | 2 | 119 | 7 | 9 | 3 | 6 | 21 | 160 | 7 | 6 | 2 | 6 | 348 |
| 04:45 PM | 6 | 114 | 6 | 9 | 5 | 7 | 25 | 194 | 5 | 3 | 3 | 10 | 387 |
| Total | 18 | 471 | 21 | 37 | 23 | 26 | 89 | 688 | 21 | 12 | 11 | 31 | 1448 |
| 05:00 PM | 6 | 101 | 4 | 8 | 9 | 4 | 33 | 177 | 9 | 5 | 4 | 8 | 368 |
| 05:15 PM | 2 | 101 | 5 | 10 | 12 | 7 | 22 | 167 | 7 | 3 | 0 | 8 | 344 |
| 05:30 PM | 6 | 78 | 3 | 5 | 5 | 2 | 19 | 156 | 3 | 4 | 4 | 12 | 297 |
| 05:45 PM | 4 | 89 | 2 | 6 | 5 | 4 | 20 | 157 | 1 | 3 | 3 | 6 | 300 |
| Total | 18 | 369 | 14 | 29 | 31 | 17 | 94 | 657 | 20 | 15 | 11 | 34 | 1309 |
| Grand Total | 36 | 840 | 35 | 66 | 54 | 43 | 183 | 1345 | 41 | 27 | 22 | 65 | 2757 |
| Apprch \% | 4 | 92.2 | 3.8 | 40.5 | 33.1 | 26.4 | 11.7 | 85.7 | 2.6 | 23.7 | 19.3 | 57 |  |
| Total \% | 1.3 | 30.5 | 1.3 | 2.4 | 2 | 1.6 | 6.6 | 48.8 | 1.5 | 1 | 0.8 | 2.4 |  |


| Accurate Counts <br> 978-664-2565 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/S Street : Route 125 <br> ENW Street: Greenhill Rd / T <br> City/State : Barrington, NH <br> Weather : Clear |  |  |  |  |  |  |  |  |  |  |  | File Site Star Pag | $\begin{aligned} & : 81880003 \\ & : 81880003 \\ & : 3 / 7 / 2019 \\ & : 9 \end{aligned}$ |
| Groups Printed- Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Route 125 <br> From North |  |  | Tolend Rd From East |  |  | Route 125 From South |  |  | Greenhill Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 04:00 PM | 0 | 6 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 9 |
| 04:15 PM | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 7 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 |
| 04:45 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| Total | 0 | 10 | 0 | 0 | 0 | 1 | 0 | 11 | 0 | 0 | 0 | 0 | 22 |
| 05:00 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:15 PM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 05:30 PM | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 4 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 8 |
| Grand Total | 0 | 16 | 0 | 0 | 0 | 1 | 0 | 13 | 0 | 0 | 0 | 0 | 30 |
| Apprch \% | 0 | 100 | 0 | 0 | 0 | 100 | 0 | 100 | 0 | 0 | 0 | 0 |  |
| Total \% | 0 | 53.3 | 0 | 0 | 0 | 3.3 | 0 | 43.3 | 0 | 0 | 0 | 0 |  |


| Groups Printed- Bikes Peds |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Route 125 From North |  |  |  | Tolend Rd From East |  |  |  | Route 125 From South |  |  |  | Greenhill Rd From West |  |  |  |  |  |  |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Exclu. Total | Inclu. Total | Int. Total |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 |
| Apprch \% | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 100 | 0 |  | 0 | 0 | 0 |  |  |  |  |
| Total \% | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 100 | 0 |  | 0 | 0 | 0 |  | 50 | 50 |  |

File Name: $: 81880003$
Site Code $: 81880003$
Start Date : $3 / 712019$
Page No : 14

|  | Route 125 <br> From North |  |  |  | Tolend Rd <br> From East |  |  |  | Route 125 <br> From South |  |  |  | Greenhill Rd From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 04:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| \% App. Total | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 100 | 0 |  | 0 | 0 | 0 |  |  |
| PHF | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 250 | . 000 | . 250 | . 000 | . 000 | . 000 | . 000 | . 250 |



| Groups Printed- Cars - Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Route 125 From North |  |  | Tolend Rd From East |  |  | Route 125 From South |  |  | Greenhill Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 11:00 AM | 4 | 98 | 3 | 9 | 3 | 4 | 11 | 131 | 5 | 2 | 3 | 13 | 286 |
| 11:15 AM | 1 | 121 | 1 | 5 | 3 | 6 | 18 | 113 | 6 | 2 | 2 | 15 | 293 |
| 11:30 AM | 8 | 150 | 7 | 5 | 1 | 6 | 13 | 94 | 3 | 4 | 4 | 14 | 309 |
| 11:45 AM | 2 | 129 | 2 | 6 | 1 | 10 | 9 | 115 | 5 | 1 | 1 | 16 | 297 |
| Total | 15 | 498 | 13 | 25 | 8 | 26 | 51 | 453 | 19 | 9 | 10 | 58 | 1185 |
| 12:00 PM | 5 | 113 | 4 | 5 | 2 | 9 | 11 | 110 | 4 | 2 | 2 | 12 | 279 |
| 12:15 PM | 5 | 111 | 4 | 7 | 2 | 4 | 11 | 120 | 2 | 2 | 3 | 15 | 286 |
| 12:30 PM | 2 | 105 | 3 | 3 | 1 | 9 | 12 | 119 | 3 | 4 | 3 | 9 | 273 |
| 12:45 PM | 4 | 96 | 3 | 7 | 2 | 5 | 17 | 131 | 3 | 4 | 2 | 11 | 285 |
| Total | 16 | 425 | 14 | 22 | 7 | 27 | 51 | 480 | 12 | 12 | 10 | 47 | 1123 |
| 01:00 PM | 5 | 107 | 1 | 6 | 1 | 6 | 13 | 116 | 5 | 1 | 1 | 14 | 276 |
| 01:15 PM | 4 | 91 | 3 | 3 | 1 | 2 | 9 | 114 | 4 | 1 | 1 | 14 | 247 |
| 01:30 PM | 7 | 115 | 0 | 5 | 6 | 4 | 11 | 104 | 6 | 1 | 3 | 5 | 267 |
| 01:45 PM | 8 | 101 | 3 | 4 | 4 | 7 | 10 | 104 | 11 | 1 | 3 | 10 | 266 |
| Total | 24 | 414 | 7 | 18 | 12 | 19 | 43 | 438 | 26 | 4 | 8 | 43 | 1056 |
| Grand Total | 55 | 1337 | 34 | 65 | 27 | 72 | 145 | 1371 | 57 | 25 | 28 | 148 | 3364 |
| Apprch \% | 3.9 | 93.8 | 2.4 | 39.6 | 16.5 | 43.9 | 9.2 | 87.2 | 3.6 | 12.4 | 13.9 | 73.6 |  |
| Total \% | 1.6 | 39.7 | 1 | 1.9 | 0.8 | 2.1 | 4.3 | 40.8 | 1.7 | 0.7 | 0.8 | 4.4 |  |
| Cars | 55 | 1329 | 34 | 65 | 27 | 72 | 145 | 1360 | 57 | 25 | 28 | 148 | 3345 |
| \% Cars | 100 | 99.4 | 100 | 100 | 100 | 100 | 100 | 99.2 | 100 | 100 | 100 | 100 | 99.4 |
| Trucks | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 19 |
| \% Trucks | 0 | 0.6 | 0 | 0 | 0 | 0 | 0 | 0.8 | 0 | 0 | 0 | 0 | 0.6 |


|  | Route 125 <br> From North |  |  |  | Tolend Rd From East |  |  |  | Route 125 From South |  |  |  | Greenhill Rd From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From 11:00 AM to 01:45 PM - Peak 1 of 1 A |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 11:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM | 4 | 98 | 3 | 105 | 9 | 3 | 4 | 16 | 11 | 131 | 5 | 147 | 2 | 3 | 13 | 18 | 286 |
| 11:15 AM | 1 | 121 | 1 | 123 | 5 | 3 | 6 | 14 | 18 | 113 | 6 | 137 | 2 | 2 | 15 | 19 | 293 |
| 11:30 AM | 8 | 150 | 7 | 165 | 5 | 1 | 6 | 12 | 13 | 94 | 3 | 110 | 4 | 4 | 14 | 22 | 309 |
| 11:45 AM | 2 | 129 | 2 | 133 | 6 | 1 | 10 | 17 | 9 | 115 | 5 | 129 | 1 | 1 | 16 | 18 | 297 |
| Total Volume | 15 | 498 | 13 | 526 | 25 | 8 | 26 | 59 | 51 | 453 | 19 | 523 | 9 | 10 | 58 | 77 | 1185 |
| \% App. Total | 2.9 | 94.7 | 2.5 |  | 42.4 | 13.6 | 44.1 |  | 9.8 | 86.6 | 3.6 |  | 11.7 | 13 | 75.3 |  |  |
| PHF | . 469 | . 830 | 464 | . 797 | . 694 | . 667 | . 650 | . 868 | . 708 | . 865 | . 792 | . 889 | . 563 | . 625 | . 906 | . 875 | . 959 |
| Cars | 15 | 491 | 13 | 519 | 25 | 8 | 26 | 59 | 51 | 451 | 19 | 521 | 9 | 10 | 58 | 77 | 1176 |
| \% Cars | 100 | 98.6 | 100 | 98.7 | 100 | 100 | 100 | 100 | 100 | 99.6 | 100 | 99.6 | 100 | 100 | 100 | 100 | 99.2 |
| Trucks | 0 | 7 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 9 |
| \% Trucks | 0 | 1.4 | 0 | 1.3 | 0 | 0 | 0 | 0 | 0 | 0.4 | 0 | 0.4 | 0 | 0 | 0 | 0 | 0.8 |


Peak Hour Analysis From 11:00 AM to 01:45 PM - Peak 1 of 1
Peak Hour for Each Approach Begins at:

|  | 11:15 AM |  |  |  | 11:00 AM |  |  |  | 12:15 PM |  |  |  | 11:00 AM |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| +0 mins. | 1 | 121 | 1 | 123 | 9 | 3 | 4 | 16 | 11 | 120 | 2 | 133 | 2 | 3 | 13 | 18 |
| +15 mins. | 8 | 150 | 7 | 165 | 5 | 3 | 6 | 14 | 12 | 119 | 3 | 134 | 2 | 2 | 15 | 19 |
| +30 mins. | 2 | 129 | 2 | 133 | 5 | 1 | 6 | 12 | 17 | 131 | 3 | 151 | 4 | 4 | 14 | 22 |
| +45 mins. | 5 | 113 | 4 | 122 | 6 | 1 | 10 | 17 | 13 | 116 | 5 | 134 | 1 | 1 | 16 | 18 |
| Total Volume | 16 | 513 | 14 | 543 | 25 | 8 | 26 | 59 | 53 | 486 | 13 | 552 | 9 | 10 | 58 | 77 |
| \% App. Total | 2.9 | 94.5 | 2.6 |  | 42.4 | 13.6 | 44.1 |  | 9.6 | 88 | 2.4 |  | 11.7 | 13 | 75.3 |  |
| PHF | . 500 | . 855 | . 500 | . 823 | . 694 | . 667 | . 650 | . 868 | . 779 | . 927 | . 650 | . 914 | . 563 | . 625 | . 906 | . 875 |



| Groups Printed- Trucks |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Route 125 From North |  |  | Tolend Rd From East |  |  | Route 125 From South |  |  | Greenhill Rd From West |  |  |  |
| Start Time | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Int. Total |
| 11:00 AM | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 4 |
| 11:15 AM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 3 |
| 11:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Total | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 9 |
| 12:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 12:15 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| 12:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 3 |
| 01:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 01:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 01:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 7 |
| Grand Total | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 19 |
| Apprch \% | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 0 | 0 |  |
| Total \% | 0 | 42.1 | 0 | 0 | 0 | 0 | 0 | 57.9 | 0 | 0 | 0 | 0 |  |

N/S Street: Route 125
EM Street: Greenhill Rd / Tolend Rd
City/State: Barrington, NH
Weather : Clear



| Groups Printed-Bikes Peds |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Inclu. Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Route 125 From North |  |  |  | Tolend Rd From East |  |  |  | Route 125 From South |  |  |  | Greenhill Rd From West |  |  |  | Exclu. Total |  | Int. Total |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds |  |  |  |
| 11:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 PM | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 |
| 12:45 PM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| Total | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 3 |
| 01:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 3 |
| Apprch \% | 100 | 0 | 0 |  | 0 | 100 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |  |
| Total \% | 33.3 | 0 | 0 |  | 0 | 66.7 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 100 |  |


610 Z/6
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Peak Hour Analysis From 11:00 AM to 01:45 PM - Peak 1 of 1
Peak Hour for Each Approach Begins at:
Peak Hour for Each Approach Begins at.
0000008

| +0 mins. | 0 |
| ---: | :---: |
| +15 mins. | 0 |
| +30 mins. | 0 |
| +45 mins. | 1 |
| Total Volume | 1 |
| \% App. Total | 100 |
| PHF | .250 |

























VEHICLE TRAVEL SPEED DATA

Location: Route 125
Location : South of Scruton Pond Road City/State: Barrington, NH



| NB |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Start | 1 | 16 | 21 | 26 | 31 |
| Time | 15 | 20 | 25 | 30 | 35 |
| 03/07/19 | 0 | 0 | 0 | 0 | 0 |
| $01: 00$ | 0 | 0 | 0 | 0 | 0 |
| $02: 00$ | 0 | 0 | 0 | 0 | 0 |
| $03: 00$ | 0 | 0 | 0 | 0 | 0 |
| $04: 00$ | 0 | 0 | 0 | 0 | 0 |
| $05: 00$ | 0 | 0 | 0 | 0 | 0 |
| $06: 00$ | 0 | 0 | 0 | 0 | 0 |
| $07: 00$ | 0 | 0 | 0 | 0 | 0 |
| $08: 00$ | 0 | 0 | 0 | 0 | 0 |
| $09: 00$ | 0 | 0 | 0 | 0 | 0 |
| $10: 00$ | 0 | 0 | 0 | 0 | 0 |
| $11: 00$ | 0 | 0 | 0 | 0 | 0 |
| $12 P M$ | 0 | 0 | 0 | 0 | 0 |
| $13: 00$ | 0 | 0 | 0 | 2 | 0 |
| $14: 00$ | 0 | 0 | 0 | 0 | 2 |
| $15: 00$ | 0 | 0 | 0 | 0 | 0 |
| $16: 00$ | 0 | 0 | 0 | 0 | 0 |
| $17: 00$ | 0 | 0 | 0 | 0 | 0 |
| $18: 00$ | 0 | 0 | 0 | 0 | 0 |
| $19: 00$ | 0 | 0 | 0 | 0 | 0 |
| $20: 00$ | 0 | 0 | 0 | 0 | 1 |
| $21: 00$ | 0 | 0 | 0 | 0 | 0 |
| $22: 00$ | 0 | 0 | 0 | 0 | 0 |
| $23: 00$ | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 2 | 9 |

48 MPH
54 MPH
59 MPH
62 MPH

54 MPH
$51-60 \mathrm{MPH}$
5639
$73.1 \%$
3248
$42.1 \%$ 15th Percentile :
50th Percentile :
85th Percentile :
95th Percentile :

Mean Speed(Average) :


49 MPH
54 MPH
59 MPH
62 MPH
55 MPH
$51-60 \mathrm{MPH}$
6265
$74.1 \%$
3815
$45.1 \%$ 15th Percentile :
50th Percentile
85th Percentile
95th Percentile :

Mean Speed(Average)
10 MPH Pace Speed

Location : South of Scruton Pond Road
City/State: Barrington,




Page 6 $\square$

Location : South of Scruton Pond Road City/State: Barrington, SB, NB


Location : Route 125
Location: South of Scruton Pond Road



Location：Route 125
Location：South of Scruton Pond Road
City／State：Barrington，NH
SB，NB


Kıן


BARRINGTON POLICE DEPARTMENT 774 FRANKLIN PIERCE HIGHWAY BARRINGTON, NH 03825

Chief Robert Williams
Emergency Dial 911
Phone (603) 664-7679
Fax (603) 664-5024

October 15, 2018

## Barrington Road Safety Audit

## Findings After Review of Crash Data

The Town of Barrington is approximately 48.5 square miles in size (land) and has over 125 miles of road. Most of the roadways are winding and are not equipped with street lights. This contributes to the number of crashes that occur within the town each year as well as the sheer volume of cars and trucks on the roadways every day.

Over the past ten years (2008-2017), the Barrington Police Department has covered 1640 crashes within our jurisdiction. Of those crashes, 336 resulted in non-capacitating injury, 39 resulted in serious bodily injury, and 12 resulted in fatalities. In total, the Department covers an average of 164 crashes each year and the numbers continue to increase each year.

Due to the large majority of crashes that are recorded, the focus was placed on roadways that accounted for most crashes. After review, the top three roadways for crashes include:

- Calef Highway (State Route 125) - Average of 42 crashes per year
- Franklin Pierce Highway (State Route 9) - Average of 44 crashes per year
- Washington Street (State Route 202) - Average of 16 crashes per year

The number of crashes on these roadways account for an average of $62 \%$ of the total crashes reported for the year in the Town.

Focusing on the top three roadways with the highest instance of crashes, we then reviewed the areas with the highest number of crashes. The top five areas with the highest number of crashes occur at intersections with Calef Highway (total crashes 2008-2017):

- Calef Highway at Franklin Pierce Highway - 76 Total Crashes
- Calef Highway at Newtown Plains Road - 39 Total Crashes
- Calef Highway at Beauty Hill Road - 20 Total Crashes
- Calef Highway at Mallego Road - 22 Total Crashes
- Calef Highway at Scruton Pond Road - 13 Total Crashes

Calef Highway (Route 125) is currently the most heavily traveled road in the town, in 2014 the average traffic volume recorded for the roadway was 16683 vehicles per day. The speed limit on Calef Highway where most of the intersections are located is 50 MPH , except for Calef Highway at Franklin Pierce, which is a post 35 MPH zone. Calef Highway is a major thoroughfare for people traveling within the state, including junctions with Routes 101 in Epping and the Spaulding Turnpike in Rochester.

The crashes at the above listed intersections were then reviewed for any involving serious bodily injury and/or death (2008-2017).

- Calef Highway at Franklin Pierce - 0 instances
- Calef Highway at Newtown Plains Road - 2 Instances
- Calef Highway at Beauty Hill Road - 5 Instances
- Calef Highway at Mallego Road - 2 Instances
- Calef Highway at Scruton Pond Road - 4 Instances (1 Fatal)

According to the data available on the NH DOT webpage, the intersection of Calef Highway and Franklin Pierce Highway was updated with traffic lights in the 1960's and was converted to the current traffic pattern in the 1970's. The addition of the traffic lights has completely reduced the number of crashes involving serious bodily injury/fatalities at that intersection. Though it is the intersection with the highest number of crashes per year, the last ten years of data show that none have been serious.

## Conclusion

The intersections of concern to the department is Calef Highway at Beauty Hill Road, and Calef Highway at Scruton Pond Road. Beauty Hill Road is located in a long flat section of Calef Highway where we encounter vehicles going well over the posted speed limit. There is also a considerable amount of traffic that comes off Beauty Hill Road and during peak hours, this can be very dangerous for motorists trying to enter Calef Highway. Scruton Pond Road intersects Calef Highway at a low point in the roadway. Both north and south bound traffic on Calef Highway are going downhill as they approach the intersection of Scruton Pond Road. The north bound traffic is also coming around a corner. The location of the road and speed of vehicles in the area has a significant effect on the number of crashes in that area.

## Data Source

All of the information was compiled using our in-house record system (IMC), which was the primary record system for the department until 2015, and our Strafford County records (also IMC) which has been our record system since 2015. Years 2008-2017 were used to provide a 10-year account of crash history.

At this time, I recommend that the information be provided to Colin at the Strafford Regional Planning Commission for further review.

Sincerely

Sgt. Kathleen P. O'Brien

| Total Accidents In Barrington 2008-2017 |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Year | Total Accidents | Acc w/ Non-Inc. Inj. | Acc. w/SBI | Acc. w/Fatalities |
| 2008 | 152 | 23 | 3 | 1 |
| 2009 | 163 | 34 | 8 | 1 |
| 2010 | 151 | 29 | 0 | 2 |
| 2011 | 154 | 30 | 6 | 0 |
| 2012 | 164 | 30 | 4 | 1 |
| 2013 | 179 | 39 | 6 | 2 |
| 2014 | 164 | 35 | 2 | 2 |
| 2015 | 160 | 28 | 0 | 1 |
| 2016 | 177 | 43 | 5 | 2 |
| 2017 | 176 | 45 | 5 | 0 |
| Total | $\mathbf{1 6 4 0}$ | $\mathbf{3 3 6}$ | $\mathbf{3 9}$ | $\mathbf{1 2}$ |
| Average | $\mathbf{1 6 4}$ | $\mathbf{3 4}$ | 4 | 1 |

## Roads with Highest Crash Instances

Total of All Crashes

| Traffic Crash Data Top 3 Crash Roads |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | 2017 Average |  |
| Calef Highway | 34 | 36 | 44 | 46 | 49 | 46 | 36 | 33 | 46 | 48 | 42 |
| Franklin Pierce | 46 | 56 | 35 | 39 | 47 | 41 | 47 | 43 | 47 | 41 | 44 |
| Washington St. | 10 | 13 | 19 | 12 | 23 | 21 | 15 | 19 | 19 | 12 | 16 |
| Totals | 90 | 105 | 98 | 97 | 119 | 108 | 98 | 95 | 112 | 101 | 102 |
| Percent of All Crashes | 59\% | 64\% | 65\% | 63\% | 73\% | 60\% | 60\% | 59\% | 63\% | 57\% | 62\% |

Roads w/Highest Crash Instances


## Intersection Related Crashes

| Highest Intersection Related Crashes (Includes Total Crashes for the Year) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 20082009 |  | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 20162017 |  |
| Calef @ Franklin Pierce | 5 | 10 | 10 | 12 | 4 | 8 | 14 | 4 | 5 | 4 |
| Calef @ New Town Pl. | 3 | 4 | 1 | 4 | 7 | 7 | 5 | 2 | 1 | 5 |
| Calef @ Beauty Hill | 1 | 1 | 2 | 2 | 4 | 1 | 1 | 0 | 1 | 7 |
| Calef @ Mallego | 3 | 1 | 3 | 3 | 1 | 2 | 2 | 2 | 1 | 4 |
| Calef @ Scruton Pond | 0 | 3 | 1 | 0 | 1 | 3 | 0 | 0 | 2 | 3 |
| Total | 12 | 16 | 16 | 21 | 16 | 18 | 22 | 8 | 8 | 20 |

Intersection Related Crashes


# Intersection Crash Data - SBI and Fatalities 

| Total Intersection Related Crashes w/SBI \& Fatalities Over Ten Years <br> (Utilizing Intersections/Area's with Highest Number of Total Accidents) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Road | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | 2017 | Totals |
| Calef @ Franklin Pierce | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Calef @ New Town Pl. | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 2 |
| Calef @ Beauty Hill | 0 | 1 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 5 |
| Calef @ Mallego | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 |
| Calef @ Scruton Pond | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 4 |

10 Year Total SBI/Fatalities at High Crash Intersections


| SBI/Fatal Crash List 2008-2017 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Accident Number | Accident Date | Time | Location | Injury |
| 08BAR-58-AC | 5/16/2008 | 9:42 PM | Route 125 S of Deer Ridge Road | SBI |
| 08BAR-60-AC | 5/24/2008 | 3:47 PM | Frankline Pierce, East of Stonehouse Pond | SBI |
| 08BAR-71-AC | 6/30/2008 | 1:26 PM | Greenhill @ \# 147 | SBI |
| 08BAR-81-AC | 8/4/2008 | 2:30 AM | Franklin Pierce Hwy @ Estate Drive | Fatal |
| 09BAR-30-AC | 3/2/2009 | 2:08 PM | Franklin Pierce Highway @ Kelly Ln. | SBI |
| 09BAR-57-AC | 4/24/2009 | 10:15 PM | Tolend Road @ Greenhill Road | SBI |
| 09BAR-66-AC | 5/20/2009 | 4:39 PM | Franklin Pierce Highway @ Washington | SBI |
| 09BAR-72-AC | 6/1/2009 | 4:48 PM | Tolend Road @ Carr Dr. | SBI |
| 09BAR-84-AC | 7/15/2009 | 5:00 PM | Calef Hwy @ Beauty Hill Road | SBI |
| O9BAR-101-AC | 9/3/2009 | 7:15 AM | Calef Hwy @ Province Road | SBI |
| 09BAR-114-AC | 9/28/2009 | 7:00 AM | Franklin Pierce Hwy @ Haley Dr. | SBI |
| 09BAR-116-AC | 10/6/2009 | 7:59 AM | Old Concord Tnpk. 2500 ft. East of Meadowbrook | SBI |
| O9BAR-142-AC | 12/4/2009 | 5:06 PM | Franklin Pierce Hwy. 200 ft . West Kelly Ln. | Fatal |
| 10BAR-106-AC | 10/3/2010 | 4:17 AM | Washington St. West of Mahala Way. | Fatal |
| 10BAR-111-AC | 10/18/2010 | 2:52 PM | Calef Highway 500 Ft . South Scrouton Pond Rd. | Fatal |
| 11BAR-37-AC | 3/17/2011 | 8:39 AM | Washington St. 1 mi. South of Pond Hill Rd. | SBI |
| 11BAR-50-AC | 5/2/2011 | 5:00 AM | Old Concord Tnpk. @ Truck Lanes | SBI |
| 11BAR-51-AC | 5/11/2011 | 5:05 PM | Calef Hwy. @ Beauty Hill Road | SBI |
| 11BAR-63-AC | 6/12/2011 | 7:16 AM | Franklin Pierce Highway @ Hearthside Dr. | SBI |
| 11BAR-96-AC | 8/14/2011 | 11:25 AM | Calef Highway @ Beauty Hill Rd. | SBI |
| 11BAR-123-AC | 10/30/2011 | 10:39 PM | Tolend @ Pumpkin Hollow | SBI |
| 12BAR-18-AC | 1/25/2012 | 2:16 PM | Old Concord Tnpk. 200 ft . West of Glass Ln. | SBI |
| 12BAR-27-AC | 2/8/2012 | 5:58 PM | Franklin Pierce @ Mallego Rd. | SBI |
| 12BAR-56-AC | 5/15/2012 | 2:39 PM | Franklin Pierce Hwy. East of Swain Rd. | Fatal |
| 12BAR-95-AC | 8/11/2012 | 4:21 PM | Calef Highway @ Newtown Plains Road | SBI |
| 12BAR-113-AC | 10/2/2012 | 2:13 PM | Calef Highway South of Scruton Pond | SBI |
| 13BAR-69-AC | 5/29/2013 | 11:02 AM | Franklin Pierce @ \#2143 | SBI |
| 13BAR-80-AC | 6/14/2013 | 6:54 AM | Calef Highway @ Winkley Pond Rd. | SBI |
| 13BAR-81-AC | 6/18/2013 | 10:52 AM | Old Concord Tnpk. 1500 ft . E. Warren Rd. | SBI |
| 13BAR-110-AC | 9/11/2013 | 5:08 PM | Spring Dr. @ Washington St. | SBI |
| 13BAR-120-AC | 9/25/2013 | 6:07 PM | Franklin Pierce Hwy. 100 ft . W. Ramsdell Ln. | SBI |
| 13BAR-134-AC | 10/15/2013 | 3:49 PM | Canaan Back Road (OHRV) | Fatal |
| 13BAR-135-AC | 10/16/2013 | 11:32 PM | Calef Highway 200 ft . S. Scruton Pond Rd. | SBI |
| 13BAR-143-AC | 10/31/2013 | 10:37 PM | Frankline Pierce 500 ft . East Cooper Rd | Fatal |
| 14BAR-97-AC | 8/23/2014 | 5:34 AM | Franklin Pierce Hwy. @ \# 1738 | Fatal |
| 14BAR-102-AC | 8/31/2014 | 7:28 PM | Calef Hwy. @ Newtown Plains | SBI |
| 14BAR-126-AC | 10/26/2014 | 10:00 AM | Franklin Pierce @ Calef Hwy. | SBI |
| 14BAR-165-AC | 12/26/2014 | 3:52 PM | Tolend Road 200 ft . West of Substitute Rd. | Fatal |
| 15BAR-133-AC | 11/1/2015 | 4:10 PM | Franklin Pierce @ Garnett Dr. | Fatal |
| 16BAR-25-AC | 2/2/2016 | 9:09 AM | Calef Hwy @ Barnz's Cinema | SBI |
| 16BAR-47-AC | 3/12/2016 | 10:47 AM | Old Concord Tnpk. @ \# 287 | SBI |
| 16BAR-49-AC | 3/21/2016 | 11:42 AM | Calef Highway @ Pierce Road | Fatal |
| 16BAR-54-AC | 4/14/2016 | 7:42 PM | Calef Highway @ Province | SBI |
| 16BAR-55-AC | 4/14/2016 | 5:41 PM | Calef Highway @ Scrouton Pond Road | SBI |


| SBI/Fatal Crash List 2008-2017 |  |  |  |  |  |  |
| :--- | :---: | :---: | :--- | :--- | :---: | :---: |
| Accident Number | Accident Date | Time | Location | Injury |  |  |
| 16BAR-111-AC | $8 / 15 / 2016$ | 4:50 AM | Calef Highway @ Greenhill Road | SBI |  |  |
| 16BAR-167-AC | $12 / 16 / 2016$ | $5: 11$ AM | Franklin Pierce @ Estate Drive | Fatal |  |  |
| 17BAR-5-AC | $1 / 10 / 2017$ | $12: 18$ PM | Greenhill Road 1500 ft. West Calef Hwy. | SBI |  |  |
| 17BAR-13-AC | $1 / 20 / 2017$ | $8: 20$ AM | Calef Highway @ Beauty Hill Rd. | SBI |  |  |
| 17BAR-32-AC | $2 / 16 / 2017$ | $12: 34$ PM | Franklin Pierce Hwy. @ Madbury Line | SBI |  |  |
| 17BAR-76-AC | $6 / 12 / 2017$ | $5: 02$ PM | Scrouton Pond @ Coachman Dr. | SBI |  |  |
| 17BAR-125-AC | $10 / 23 / 2017$ | 7:56 AM | Calef Hwy. North of Century Pines | SBI |  |  |
| 17BAR-132-AC | $11 / 1 / 2017$ | $7: 31$ AM | Calef Hwy 1000 ft. North Pierce Road | SBI |  |  |


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\text { LOSS }
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STATE OF NEW HAMPSHIRE, DEPARTMENT OF TRANSPORTATION - BUREAU OF TRAFFIC



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# STATE OF NEW HAMPSHIRE DEPARTMENT OF TRANSPORTATION BUREAU OF HIGHWAY DESIGN 

CONFERENCE REPORT

PROJECT: BARRINGTON<br>X-A001(181)<br>16201<br>NH 125/Tolend Rd/Greenhill Rd Intersection Safety Improvements (HSIP)

## DATE OF CONFERENCE: March 1, 2012

LOCATION OF CONFERENCE: Early Childhood Learning Center, Barrington

## ATTENDED BY:

NHDOT
Bill Oldenburg
John Butler
Doug DePorter
OTHERS
See attached sign-in sheet.
SUBJECT: Public Officials/Public Informational Meeting

## NOTES ON CONFERENCE:

Bill Oldenburg introduced this intersection safety improvement project at the intersection of NH Route 125 / Tolend Road / Greenhill Road. He explained that the intersection had been identified for improvements through the work of the Highway Safety Improvement Program (HSIP). The current Federal highway funding law, known by its acronym of SAFETEA-LU, created the Highway Safety Improvement Program to identify highway safety issues and provide for modest safety improvements that would achieve a significant reduction in traffic fatalities and serious injury accidents. New Hampshire receives $\$ 5.5$ million per year to implement modest safety improvements in locations where crash data indicates safety deficiencies. Crash data available for the intersection showed that there were 21 accidents between 2002 to 2009, including 1 fatal accident and 9 severe injury accidents.

In March of 2011 the Department met with the Board of Selectmen to get an understanding of the perceived deficiencies at the intersection, and to gain their support to investigate possible solutions to improve safety. Based on that input and an engineering study by the Department, a conceptual plan for improvements has been developed. Several important
issues were considered as the designs were developed, including safety, efficient operation, property impacts, historic resources, and natural resources.

John Butler described the existing intersection conditions and the conceptual plan for improvements. NH 125 through the intersection area has two $12^{\prime}$ wide travel lanes, $10^{\prime}$ wide paved shoulders, and a $150^{\prime}$ wide controlled access right-of-way. The posted speed limit on NH 125 is 50 mph . Environmental issues include some small pockets of wetlands scattered throughout the project area and a potentially historic house in one quadrant of the intersection. Current average daily traffic volumes are approximately 14,600 vehicles on NH 125, 2100 vehicles on Greenhill Road, and 1100 vehicles on Tolend Road.

In 2008, the Strafford Regional Planning Commission completed a NH Route 125 corridor study, which recommended signalizing the $\mathrm{NH} 125 /$ Tolend $\mathrm{Rd} /$ Greenhill Rd intersection and widening NH 125 to have two through lanes in each direction for long-term capacity needs. Concerns expressed by town officials and the public at the March 2011 meeting included the difficuity of safely pulling out of the two side roads and the speed of traffic on NH 125. The predominant recommendation at that meeting was to signalize the intersection.

Traffic data was collected at the intersection and an engineering analysis was done to determine if signalization is justified at the intersection. Based on that analysis, it was determined that signals are warranted, therefore, signalization of the intersection is proposed. The proposed design also calls for separate left turn and right turn lanes on NH 125 in both the northbound and southbound directions. Constructing the turning lanes will require widening NH 125 by approximately $10^{\circ}$ in two areas. No impacts to private property or environmental resources are anticipated. The construction cost is estimated to be $\$ 625,000$.

Bill Oldenburg noted that an environmental document will be prepared for the project which will describe all known environmental resources in the project area, and the anticipated impacts to those resources. Bill noted that owners of historic properties directly affected by the project or agencies that possess a direct interest in historical resources can become more involved in an advisory role during project development by becoming a "Consulting Party" to the Section 106 process. He also noted that several areas of invasive (non-native) plans have been identified in the project area, and measures will be taken to ensure that these plants are not spread by the construction activities.

Bill noted that funding for the project will be a combination of State and Federal funds. No Town funds are anticipated to be required. If the proposal is well received at tonight's meeting, the project could possibly be advertised for construction this coming winter, with construction in 2013.

## Discussion:

The fire chief requested that the new signals be equipped with Opticom for emergency vehicles and with a generator transfer switch so that the signals could be run off a portable generator if the power goes out. He noted that the Town might be able to provide a generator in the event of a power outage.

It was asked if the signals would operate in flashing mode during non-peak traffic times, and if there would be traffic sensors in the pavement. Bill Oldenburg responded that the signals will be fully actuated with sensors in the pavement, but they will not be put on flash mode during non-peak traffic.

It was recommended that lighting be provided at the intersection. Bill Oldenburg responded that lighting will be considered, but in general the Department has been reducing the number of active street lights statewide as a cost savings measure.

It was noted that speeding on NH 125 is a significant issue, and that tuming left from NH 125 is uncomfortable due to the fear of being rear-ended. It was asked if the speed limit on NH 125 would be reduced. Bill Oldenburg responded that the speed limit is likely to be reduced through the intersection area, but is unknown at this time what the reduced speed limit will be, and where the exact limits of the reduction will be.

It was noted that truck traffic on NH 125 is significant. In particular there has been an increase in Waste Management trucks heading north to a facility in Rochester.

It was recommended that signing could be improved on Tolend Road and Greenhill Road to alert drivers of the upcoming intersection.


```
cc: W. Cass
    D. DePorter
    W. Oldenburg
    C. Perron
    W. Lambert
        M. Dugas
    Barrington Selectmen
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PROJECT Barrington - NH $125 /$ Greenhill Rd/Tolend Rd. $^{\text {R }}$ /
location Public Officials/Public Info, meeting, Early Child hoed Learning Center, PROJECTNO. $\frac{X-A \phi \phi \not 2(181)}{\text { Federal }}-\frac{16201}{\text { State }}$


# STATE OF NEW HAMPSHIRE DEPARTMENT OF TRANSPORTATION BUREAU OF HIGHWAY DESIGN 

## CONFERENCE REPORT

PROJECT: BARRINGTON
X-A001(173)

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16178
$$

$$
\text { US } 202 \text { / NH } 9 \text { Intersection Safety Improvements (HSIP) }
$$

DATE OF CONFERENCE: July 18, 2012
LOCATION OF CONFERENCE: Early Childhood Learning Center, Barrington
ATTENDED BY: PUBLIC HEARING COMMISSION
Richard Adams, Chairperson
William Gregsak
Thomas Tatarczuch
NHDOT
Bill Oldenburg Victoria Chase John Butler Christine Perron
OTHERS
See attached sign-in sheet.

SUBJECT: Public Hearing

## NOTES ON CONFERENCE:

A public hearing was held for the above-noted project on July 18, 2012. A transcript of the hearing is available in the Bureau of Right-of-Way. The following is a summary of the questions and comments made at the hearing, and the Department's response to those comments.

1. John Scruton, Barrington Town Administrator, voiced his support for the project. He noted that his preference would be to have the left tum lane included in the design, but understood that it would require significant additional cost.
2. John Allard, Barrington resident, expressed the following comments and questions:
a. He expressed his preference for the alternative design that makes US Route 202 the free-flow movement. He is concerned with the speed of traffic on the westbound NH 9 approach coming down the hill, and felt that making them stop at the intersection would be a way to control their speed.
b. He asked if the bypass shoulder was designed to accommodate tractor trailers.
c. He wanted to know how much additional property would be required from Parcel \#2 with the left turn lane alternative.

## Response:

a. The Department has considered all the issues associated with the US 202 freeflow alternative and with the left turn lane alternative, and feels that the proposed design presented at the public hearing provides the most cost-effective solution while considering the issues of safety, efficient operations, property impacts, and impacts to cultural and natural resources.
b. The bypass shoulder will accornmodate tractor trailers going around a vehicle that is stopped to make a left hand turn.
c. There is only a small amount of additional property required from Parcel \#2 with the left turn lane alternative as compared to the proposed design, however, there are also impacts to three additional properties that are not impacted by the proposed design.
3. Steve Young, Barrington resident, asked if traffic would be routed along Gooseneck Lane during construction.
Response: US 202 and NH 9 traffic will not be detoured along any local roads, including Gooseneck Lane, during construction.
4. Terri Frank, Barrington resident, requested that measures be taken to reduce traffic speed along US 202 and NH 9. She suggested additional signage.
Response: The project area will be reviewed by the Bureau of Traffic to insure that appropriate signage is provided on the approaches to the intersection.


John D. Butler, PE
Preliminary Design Supervisor

ATTACHMENTS: Chairperson Preliminary Statement
Project Manager Statement
Design Presentation Outline
Right-of-Way Statement
Environment Statement
Meeting Sign-in Sheet

NOTED BY: W. Oldenburg

| cc: | W. Cass | D. DePorter |
| :--- | :--- | :--- |
| W. Oldenburg | C. Perron |  |
| W. Lambert | M. Dugas |  |
|  | V. Chase |  |

S:<br>(TOWNS)\Barrington\16178\Conference Reports\071812_PH_16178.doc

# PRELIMINARY STATEMENT 

BY
RICHARD ADAMS, CHAIR

## BARRINGTON 16178

THIS MEETING IS CALLED TO ORDER. I AM RICHARD ADAMS, CHAIR OF THIS COMMISSION APPOINTED BY THE GOVERNOR AND EXECUTIVE COUNCIL. WILLIAM GREGSAK AND THOMAS TATARCZUCH ARE ALSO MEMBERS OF THIS COMMISSION.

THIS HEARING IS CONCERNED WITH THE RECONSTRUCTION OF US 202 AND NH 9 TO IMPROVE SAFETY. IT IS PURSUANT TO RSA 230:14, AND THE SURFACE TRANSPORTATION AND UNIFORM RELOCATION ASSISTANCE ACT OF 1987.

THE PURPOSE OF THIS HEARING IS TO DETERMINE THE NECESSITY OF THE OCCASION OF THE LAYOUT AND TO HEAR EVIDENCE OF THE ECONOMIC AND SOCIAL EFFECTS OF SUCH A LOCATION, ITS IMPACT ON THE ENVIRONMENT, AND ITS CONSISTENCY WITH THE GOALS AND OBJECTIVES OF SUCH LOCAL PLANNING AS HAS BEEN UNDERTAKEN BY THE TOWNS.

IMMEDIATELY FOLLOWING THE HEARING, THIS COMMISSION WILL EVALUATE ALL MATTERS BROUGHT TO OUR ATTENTION, AND MAKE DEFINITE decisions relative to the layout. THE DEPARTMENT WILL CONTACT EACH OWNER WHOSE PROPERTY IS AFFECTED AND DISCUSS INDIVIDUAL CONCERNS. IT IS, THEREFORE, IMPORTANT THAT ALL INDIVIDUALS DESIRING TO MAKE REQUESTS OR SUGGESTIONS, DO SO TONIGHT.

AT THIS TIME, I WILL ASK WILLIAM OLDENBURG, PROJECT MANAGER OF THE NEW HAMPSHIRE DEPARTMENT OF TRANSPORTATION, TO PRESENT, IN A FORMAL MANNER, THE LAYOUT WHICH HE HAS PROPOSED. AFTER THIS, I WILL OPEN THE FLOOR TO THOSE WHO WISH TO ADDRESS THE COMMISSION. I WILL REQUEST THAT ALL DESIRING TO SPEAK SIGNIFY THEIR DESIRE AND UPON RECOGNITION BY ME, STEP TO THE MICROPHONE, STATE THEIR NAME AND ADDRESS, AND MAKE THEIR STATEMENTS. PLEASE PRINT YOUR NAME AND address on the sign in sheet. this hearing is being recorded and a TRANSCRIPT WILL LATER BE PREPARED.

WILLIAM OLDENBURG WILL NOW PRESENT THE LAYOUT.

THANK YOU BILL

BEFORE I OPEN THE HEARING FOR COMMENTS, CONCERNS OR QUESTIONS, I would like to know if we have any elected officials with us this evening THAT WOULD LIKE TO BE HEARD?

ANY TOWN OFFICIALS?

I WILL NOW OPEN THE MEETING TO ANYONE DESIRING TO BE HEARD. AGAIN I WOULD ASK YOU TO RAISE YOUR HAND AND, UPON RECOGNITION BY ME, COME TO THE MICROPHONE, STATE YOUR NAME AND ADDRESS AND MAKE YOUR statements. please be sure that you have printed your name and address on the sign in sheet located on the podium.

THERE BEING NO INDICATION OF ANYONE REMAINING WHO DESIRES TO BE HEARD, THIS HEARING IS ADJOURNED. THE COMMISSION WILL TAKE A 15 MINUTE RECESS AND RECONVENE FOR A MEETING TO DISCUSS THE PROPOSED PROJECT. THIS MEETING IS A PUBLIC PROCEEDING UNDER RSA CHAPTER 91-A. THE INTENT OF THIS MEETING IS NOT TO CONTINUE TAKING TESTIMONY, BUT INSTEAD THE MEETING SERVES AS DECISION-MAKING FOR THE HEARING COMMISSION. THE PUBLIC MAY OBSERVE THE PROCEEDINGS. IF THE COMMISSION REQUIRES ADDITIONAL TIME TO CONSIDER THE TESTIMONY PRESENTED HERE TONIGHT, A FINDING OF NECESSITY MEETING HAS BEEN SCHEDULED FOR WEDNESDAY, AUGUST 1, 2012.

HEARING ADJOURNED AT $\qquad$ .

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Barrington
16178
Public Hearing
7/18/12
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Thank you Mr. Chairman, members of the Commission, ladies and gentlemen good evening. It is a pleasure this evening to present what the Department of Transportation proposes for improvements to the intersection of US 202 and NH 9 in the Town of Barrington. My name is Bill Oldenburg and I'm the Project Manager for this project. Tonight's meeting is a Public Hearing to present the Department's preferred alternative to improve the safety of the intersection, and to get public comment and testimony.

Before I get started, I'd like to introduce several of my colleagues from the Department who will be helping with tonight's presentation. On my right is Victoria Chase. She is the Right-of-Way Engineer and she will be providing a brief summary of the right-of-way process for the project. On her right, is Christine Perron and she is the Environmental Manager for the project and she will provide a brief overview of the environmental study that has been completed for the project. Also at the Board is John Butler. He is one of our senior Preliminary Design engineers and he will be presenting the plans this evening and discussing the detailed aspects of the design. I would also like to acknowledge our Right-ofWay folks that are doing the recording this evening Linda Smith and Don LaBelle and transcriptionist Deb Mekula. We will try to be succinct as possible on presenting all of the information, but anticipate our presentation will take about 30 minutes. And then Commission Chairman Adams will open it up for your comments.

As everyone is aware US 202 and NH 9 are major east-west highways for the state and service many communities within the region. This project serves to provide for safety upgrades of this intersection.

The project limits where US 202 and NH 9 are combined extend approximately 400 feet from the intersection west towards Northwood. US 202 extends approximately 300 feet north from the intersection towards Rochester and NH 9 extends approximately 400 feet from the intersection towards Barrington.

This intersection came to our attention thru work we had been doing on the Highway Safety Improvement Program. The HSIP was included in the last reauthorization of the Federal Highway Program and came about from concerns by the FHWA and other agencies involved in highway safety, about the number of fatalities that were occurring on our nations highways. They set a goal to reduce fatal and serious injury crashes and as part of that initiative they provided funding for modest safety improvements, which would achieve a significant reduction in fatalities and serious injury crashes. The State receives about $\$ 6.5$ million each year to be used at various identified locations around the State. This program is also intended to be data driven, and any location where we intend to utilize these funds has to have a crash history that demonstrates a need. Our crash statistics showed that during 2002 to 2009 there were 12 crashes at this intersection, including 1 fatality and 3 severe injury accidents. $66 \%$ of the crashes involved more than 1 vehicle.

The primary purpose and need for this project is to improve the safety of the intersection. In developing the project we looked at numerous options that improved safety but also attempted to limit the impacts to the abutters. In March 2011 the Department met with the Town's Selectboard to discuss the intersection improvements. Discussions of this intersection and the various alternatives that were studied were also presented at a public informational meeting in February 2012. Several important issues were considered in the design: safety, efficient operation, property impacts and historic and natural resources. Based upon
these issues, our studies and input from the public meetings, the design that is shown on the boards and will be presented tonight is the Department's preferred alternative.

The plans you see here tonight are preliminary plans. Much more engineering work will be required to get these to a point where we can identify exactly the right-of-way impacts and to develop plans that are suitable for construction. The plans will be developed in more detail to determine the drainage needs, utility relocations, final grading, and this typically takes place if we have a positive public hearing. Based on your input tonight there may be some modifications made to the plans. Tonight's meeting is a significant milestone in the project, where it transitions from the preliminary design phase to the final design and right-of-way procurement phase.

At this time I would like to ask John Butler to present the plans in more detail. John.......

Thank you John. As this project will involve acquisitions of property and easements and I'd like to ask Victoria Chase to talk about the right-of-way process. Victoria....

Thank you Victoria. As part of this project the Department must consider and document environmental impacts as a result of the project. At this time I would like to ask Christine Perron to provide a summary of the environmental study completed for the project. Christine....

## Thank you Christine.

The Department will study all of the issues that are raised and make recommendations on how they should be addressed. These recommendations will be presented to the hearing commission at a public meeting. The hearing commission will then make a decision on the necessity for the project. If there are no substantive issues raised tonight that will change the design, or that cannot be readily addressed, the finding of necessity for this project will held tonight immediately following this hearing. An alternative date of August 1,2012 has been scheduled for this meeting, if the commission cannot make their decision tonight. If there is a positive decision by the Commission the project will move to the final design phase and the right-of-way process will begin. Once all of the necessary approvals are done, permits and right-of-way procured, the project will advertise for construction, which we are anticipating for early 2014. This project will most likely take only I construction season to complete, ending in fall of 2014.

The project cost is estimated at roughly $\$ 600,000.100 \%$ of the cost of the project will be funded by Federal HSIP funds and State funds. As designed there are no Town funds anticipated for this project.

This concludes the Department's presentation. I'd like to thank all of you for your attentiveness and patience. I know we provided a lot of information fairly quickly. I would like to thank the Town staff
for their time and effort in assisting us in this project. At this time I would like to formally request Mr. Chairman that the Commission find occasion for the necessity for the layout of the project as presented this evening. Thank you for your consideration and attention.

## Barrington 16178 Public Hearing

## Existing Conditions

- plan orientation
- colors
- speed limits: 45 mph on US 202, 40 mph on NH 9
- describe existing intersection configuration
- traffic data: 2012 ADT: US 202/NH $9=7130$ vehicles

US $202=4190$ vehicles
NH $9=3180$ vehicles

- environmental constraints:
cemetery - historic
wetlands (prime)
- issues expressed at previous meetings
- confusion over who has the ROW
- poor sight distance


## Proposed Layout

- Consolidate US 202 SB into a single leg
- Widen shoulder on US 202/NH 9 EB for bypass shoulder
- Tree clearing to improve sight distance to and from intersection
- Property impacts:
- $25^{\prime}+/$ strip acquisition from Parcel \#2 - multiple ownership
- Two small drainage easements from Parcel \#1
- 

Utility impacts: relocate 2 to 4 poles

## Other Alternatives

- Left Turn Lane
- significantly longer \& more expensive
- more property impacts
- proposed layout addresses the major safety concerns
- US 202 as Free Flow
- suggested at Feb. Public Info meeting
- curve needs to be flattened
- property impacts
- more expensive
- NH 9 WB coming down a steep grade to a STOP sign
- Operationally
- Good: US 202 SB free flow
- Bad: NH 9 WB heavy left turn must stop


## COMMISSION HEARING SPEECH FOR VICTORIA

## BARRINGTON 16178

JULY 18, 2012

THANK YOU, BILL, CHAIRMAN ADAMS, MEMBERS OF THE COMMISSION, LADIES AND GENTLEMEN. BEFORE I GO INTO THE RIGHT-OF-WAY PROCEDURES FOR THIS PROJECT, THERE ARE A COUPLE OF THINGS I'D LIKE TO MENTION. WE HAVE WITH US TONIGHT A MAP SHOWING THE PROJECT AND A HANDOUT ENTITLED "YOUR LAND AND NEW HAMPSHIRE HIGHWAYS" WHICH DESCRIBES THE RIGHT-OF-WAY ACQUISITION AND RELOCATION ASSISTANCE PROCEDURES THAT ARE UTILIZED BY THE STATE. THESE ITEMS ARE MOST USEFUL FOR THOSE PROPERTY OWNERS AFFECTED BY THIS PROPOSED PROJECT. THESE ARE AVAILABLE FROM THE DEPARTMENT'S STAFF.

IF AFTER REVIEWING THE INFORMATION RECEIVED AT THIS HEARING, CHAIRMAN ADAMS AND THE COMMISSION FIND NECESSITY FOR THIS LAYOUT, SEVERAL THINGS WILL HAPPEN. FIRST, WITH APPROVAL TO PROCEED WITH THE DESIGN OF THIS PROJECT, APPRAISALS WILL BE PREPARED FOR EACH OF THE PROPERTIES AFFECTED BY THE PROPOSED CONSTRUCTION YOU SEE ON THE PLANS. THE APPRAISALS WILL DETERMINE THE FAIR MARKET VALUE OF THE PROPERTY RIGHTS NEEDED FOR THE NEW CONSTRUCTION.

THESE APPRAISALS ARE REVIEWED SEPARATELY TO SEE THAT ALL ARE ACCURATE AND HAVE TAKEN INTO ACCOUNT ALL APPLICABLE APPROACHES TO

VALUE. ONCE THIS REVIEW IS COMPLETE, THE DEPARTMENTS' APPRAISALS ARE GIVEN TO THE COMMISSION TO BEGIN DISCUSSIONS WITH THE PROPERTY OWNERS REGARDING THE ACQUISITION. THE VALUE IN THIS APPRAISAL WILL BE THE OFFER OF COMPENSATION USED BY THE COMMISSION.

THE COMMISSION WILL CONTACT EACH PROPERTY OWNER AND DISCUSS EACH ACQUISITION SEPARATELY. WE URGE OWNERS AT THAT TIME TO ASK QUESTIONS AND BRING UP CONCERNS THAT THEY FEEL SHOULD BE CONSIDERED. IF THE PROPERTY OWNER IS SATISFIED WITH THE OFFER, DEEDS ARE PREPARED AND OWNERSHIP IS TRANSFERRED TO THE STATE. IF THE OWNER IS NOT HAPPY WITH THE FIGURES THE COMMISSION OFFERS, THEY CAN APPEAL TO THE NEW HAMPSHIRE BOARD OF TAX AND LAND APPEALS AND ARGUE FOR ADDITIONAL COMPENSATION THERE. IT IS IMPORTANT YOU UNDERSTAND THAT THIS CAN BE DONE WITH OR WITHOUT AN ATTORNEY. EITHER PARTY CAN APPEAL THE BOARD'S DECISION TO THE SUPERIOR COURT IF THEY ARE UNSATISFIED.

ANY TIME AFTER THIS HEARING OR BEFORE DESIGN APPROVAL, ALL INFORMATION IN SUPPORT OF THIS HEARING IS AVAILABLE AT THE DEPARTMENT'S HEADQUARTERS IN CONCORD FOR YOUR INSPECTION AND COPYING.

THAT'S ALL I HAVE BILL. THANK YOU.

## BARRINGTON 16178 PUBLIC HEARING STATEMENT

Good evening, members of the commission, ladies and gentlemen.

Pursuant to the National Environmental Policy Act, the Department has evaluated alternatives to the proposed project and the potential impacts this project will have on the surrounding social, economic, and natural environments. Coordination was established and input received from Federal and State environmental agencies, including the US Army Corps of Engineers, NH Department of Environmental Services, the State Historic Preservation Office, and town and regional officials. After evaluation of the information gathered, an environmental document was prepared. The following is a brief summary of the information contained in that document.

1) The proposed project will require work within areas under the jurisdiction of the DES Wetlands Bureau and the US Army Corps of Engineers. The total wetland impact is expected to be approximately $2,000 \mathrm{sq}$. ft and is associated with roadside drainage. There will be no impacts to the Hale Pond Prime Wetland or the Prime Wetland Buffer, which is defined by DES as 100 feet from the edge of the prime wetland. Anticipated impacts do not meet the State's mitigation thresholds. The Department will continue to coordinate with the appropriate agencies to ensure that all wetland impacts are minimized and all permits are secured prior to construction.
2) State regulations prohibit the spread of invasive plants listed on the NH Prohibited Species List. The project area contains Japanese barberry, Oriental bittersweet, and multiflora rose, all of which are prohibited invasive plants. Appropriate best management practices will be implemented to prevent construction activities from spreading existing invasive plants and introducing new plants into the project area.
3) Stone walls are located throughout the project area and were assessed according to the State of New Hampshire Roadside Stone Wall Reconstruction Policy. Approximately 100 linear feet of stone wall will be impacted by the Proposed Action along the south side of 202 \& 9. Following coordination with the State Historic Preservation Office, it was agreed that this impacted stone wall would be reconstructed in-kind.
4) Pursuant to Section 106 of the National Historic Preservation Act, the NH Department of Transportation, in coordination with the Federal Highway Administration and State Historic Preservation Office, must take into account the impacts of the project on cultural resources. The project area has been evaluated and reviewed for historic properties and archeological sensitivity.

The land surrounding the intersection was part of the Thomas Wright Hale farm and house site from the early 1780 s to the early 1920 s. The house stood on the north side of the road just east of the intersection until it burned down in the early 1940s. The surviving house site is an un-filled cellar hole and foundation. There are stone walls throughout the property, and along the roads and property boundaries. Most interior walls are located on the land north and northeast of the house site where farm activity would have been concentrated. The Hale family cemetery is located west of the intersection on the north side of the road.

It was determined that the Proposed Action will not impact areas of the former Hale homestead that still retain a high potential for historic archaeological information. Therefore, the project-related impacts will have no effect on cultural resources under Section 106 of the National Historic Preservation Act.

A copy of the environmental document is available for anyone who wishes to review it after the hearing.
Barrington Finding of Necessity Meeting
July 18, 2012 Early Childhood Learning Center, Bar

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WEEKDAY MORNING PEAK HOUR (7:00-8:00 AM)

$14 \longrightarrow$

WEEKDAY EVENING PEAK HOUR (4:00-5:00 PM)

(11:00 AM - 12:00 PM)


Table 1A
TRIP GENERATION
Gas Station/C-Store $^{1}$
Donut Shop $^{2}$
Less Trip Linking $^{3}$
Opening Year Generation

Trip Generation Summary - Horizon Year (2012)

AM Peak Hour

| AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Entering | Exiting | Total | Entering | Exiting | Total |
| 100 veh | 100 veh | 200 trips | 115 veh | 115 veh | 230 trips |
| 138 veh | 138 veh | 276 trips | 43 veh | 43 veh | 86 trips |
| -47 veh | -47 veh | -94 trips | -15 veh | -15 veh | -30 trips |
| 191 veh | 191 veh | 382 trips | 143 veh | 143 veh | 286 trips |

TRIP COMPOSITION

| Primary Trips | 46 veh | 46 veh | 92 trips | 42 veh | 42 veh | 84 trips |
| :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Pass-by Trips ${ }^{4}$ | $\underline{145} \underline{\text { veh }}$ | $\underline{145}$ veh | $\underline{290}$ trips | $\underline{101} \underline{\text { veh }}$ | $\underline{101} \underline{\text { veh }}$ | $\underline{202} \underline{t r i p s}$ |
| Total Trips | 191 veh | 191 veh | 382 trips | 143 veh | 143 veh | 286 trips |

Table 1B
Trip Generation Summary - Horizon Year (2022)

| AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Entering | Exiting | Total | Entering | Exiting | Total |
| 100 veh | 100 veh | 200 trips | 115 veh | 115 veh | 230 trips |
| 152 veh | 152 veh | 304 trips | 47 veh | 47 veh | 94 trips |
| -52 veh | -52 veh | -104 trips | -16 veh | -16 veh | -32 trips |
| 200 veh | 200 veh | 400 trips | 146 veh | 146 veh | 292 trips |

## TRIP COMPOSITION

| Primary Trips | 47 veh | 47 veh | 94 trips | 42 veh | 42 veh | 84 trips |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Pass-by Trips ${ }^{4}$ | $\underline{153}$ veh | $\underline{153}$ veh | $\underline{306}$ | $\underline{\text { trips }}$ | $\underline{104} \underline{\text { veh }}$ | $\underline{104} \underline{\text { veh }}$ | $\underline{208} \underline{t r i p s}$ |
| Total Trips | 200 veh | 200 veh | 400 trips | 146 veh | 146 veh | 292 trips |  |

[^13]The primary trips or "new" trips to the area are expected to be distributed in the following manner:

| To / From |  | Percentage |
| :--- | :--- | :---: |
| NH Route 125 - North |  | $30 \%$ |
| NH Route 125 - South |  | $25 \%$ |
| NH Route 9 - East |  | $25 \%$ |
| NH Route 9 - West |  | $\underline{20 \%}$ |
|  |  | $100 \%$ |

These percentages are based on an analysis of several factors, including overall regional accessibility, population densities and local knowledge of the study area. The pass-by trips are expected to be distributed in proportion to the approach volumes observed at the $\mathrm{NH} 125 / \mathrm{NH} 9$ signalized intersection.

Appendix G contains diagrams that summarize the anticipated distribution of site traffic throughout the study area for the morning and evening analysis periods.

## BUILD TRAFFIC VOLUMES

The Build traffic projections (with the proposed development) are summarized schematically on Figure 5 (2012) and Figure 6 (2022). These projections are based on the No-Build traffic volumes (Figure 3 and Figure 4), the trip generation estimates contained in Table 1B, and the anticipated trip distribution patterns described above. Since the difference between the trip generation estimates for 2012 and 2022 is not significant, the 2022 trip generation estimates were applied to both the opening year and horizon year cases.



1373A
NORTH

# Institute of Transportation Engineers (ITE) 

## Trip Generation, 9 th Edition

Land Use Code (LUC) 853 - Convenience Market with Gasoline Pumps
Average Vehicle Trips Ends vs: Vehicle Fueling Positions
Independent Variable (X): 12

Average Weekday Daily
$\mathrm{T}=542.6^{*}(\mathrm{X})$
$\mathrm{T}=542.6^{*} \quad 12$
$\mathrm{T}=6511.20$
$T=6,512 \quad$ vehicle trips
with $50 \%$ ( $3,256 \mathrm{vpd}$ ) entering and $50 \%$ ( $3,256 \mathrm{vpd}$ ) exiting
Weekday Morning Peak Hour Of Adjacent Street Traffic
$\mathrm{T}=16.57^{*}(\mathrm{X})$
$\mathrm{T}=16.57^{*} \quad 12$
$\mathrm{T}=198.84$
T = 109200 vehicle trips 100 with $50 \%$ ( 100 vph ) entering and $50 \% ~(98 \mathrm{vph})$ exiting

## Weekday Evening Peak Hour Of Adjacent Street Traffic

$\mathrm{T}=19.07$ * (X)
$\mathrm{T}=19.07$ * $\quad 12$
$\mathrm{T}=228.84$


## Saturday Daily

$\mathrm{T}=204.47^{*}$ (X)
$\mathrm{T}=204.47$ * 12
$\mathrm{T}=2453.64$
$\mathrm{T}=2,454 \quad$ vehicle trips
with $50 \%$ ( $1,227 \mathrm{vph}$ ) entering and $50 \%$ ( $1,227 \mathrm{vph}$ ) exiting

## Saturday Midday Peak Hour

```
T = 10.00* (X)
T=10.00* 12
T=120.00
T=120 vehicle trips
    with 51% ( 61 vph) entering and 49% (
\[
59 \mathrm{vph}) \text { exiting. }
\]
```

    * Assume 60 Pass-by
    \(\begin{array}{llll} & \begin{array}{l}\text { ToTAL } \\ \text { TRiPS }\end{array} & \frac{\text { PASS-By }}{61} & \frac{\text { PrimARY }}{36} \\ \text { In }_{\text {IN }} & \frac{59}{\text { TOTAL }} & \frac{59}{120} & \frac{36}{72}\end{array}\)
    

WEEKDAY MORNING PEAK HOUR (7:00-8:00 AM)


WEEKDAY EVENING PEAK HOUR (4:00 - 5:00 PM)


## Warehousing (150)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday

## Setting/Location: General Urban/Suburban

Number of Studies: 29
Avg. 1000 Sq. Ft. GFA: 285
Directional Distribution: $50 \%$ entering, $50 \%$ exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 1.74 | $0.15-16.93$ | 1.55 |

Data Plot and Equation


## Warehousing (150)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,
Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

## Setting/Location: General Urban/Suburban

Number of Studies: 34
Avg. 1000 Sq. Ft. GFA: 451
Directional Distribution: 77\% entering, 23\% exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.17 | $0.02-1.93$ | 0.20 |

Data Plot and Equation



## Warehousing

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Saturday

## Setting/Location: General Urban/Suburban

Number of Studies: 3
Avg. 1000 Sq. Ft. GFA: 226
Directional Distribution: 50\% entering, 50\% exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.15 | $0.01-1.58$ | 0.53 |




## Specialty Trade Contractor (180)

Vehlcle Trip Ends vs: 1000 Sq. Ft. GFA On a: Weekday

## Setting/Location: General Urban/Suburban

Number of Studies: 19
Avg. 1000 Sq. Ft. GFA: 6
Directional Distribution: $50 \%$ entering, $50 \%$ exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 10.22 | $3.00-43.33$ | 8.82 |

Data Plot and Equation


Trip Generation Manual, 10th Edition - Institute of Transportation Enginears

## Specialty Trade Contractor (180)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA<br>On a: Weekday,<br>Peak Hour of AdJacent Street Traffic, One Hour Between 7 and 9 a.m.<br>Setting/Location: General Urban/Suburban<br>Number of Studies: 19<br>Avg. 1000 Sq. Ft. GFA: 6<br>Directional Distribution: $73 \%$ entering, $27 \%$ exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 1.66 | $0.12-9.17$ | 2.09 |

Data Plot and Equation


## Specialty Trade Contractor (180)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,
Peak Hour of Adjacent Street Traffic,
One Hour Between 4 and 6 p.m.
Setting/Location: General Urban/Suburban
Number of Studies: 18
Avg. 1000 Sq. Ft. GFA: 6
Directional Distribution: 32\% entering, 68\% exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 1.97 | $0.38-10.83$ | 2.07 |

## Data Plot and Equation



## Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units
On a: Weekday

## Setting/Location: General Urban/Suburban

Number of Studies: 159
Avg. Num. of Dwelling Units: 264
Directional Distribution: 50\% entering, 50\% exiting
Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 9.44 | $4.81-19.39$ | 2.10 |

## Data Plot and Equation



# Single-Family Detached Housing (210) 

## Vehicle Trip Ends vs: Dwelling Units

On a: Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.
Setting/Location: General Urban/Suburban
Number of Studies: 173
Avg. Num. of Dwelling Units: 219
Directional Distribution: $25 \%$ entering, $75 \%$ exiting
Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.74 | $0.33-2.27$ | 0.27 |

Data Plot and Equation


# Single-Family Detached Housing (210) 

Vehicle Trip Ends vs: Dwelling Units
On a: Weekday,
Peak Hour of Adjacent Street Traffic,
One Hour Between 4 and 6 p.m.
Setting/Location: General Urban/Suburban
Number of Studies: 190
Avg. Num. of Dwelling Units: 242
Directional Distribution: $63 \%$ entering, $37 \%$ exiting
Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.99 | $0.44-2.98$ | 0.31 |

## Data Plot and Equation



# Single-Family Detached Housing (210) 

Vehicle Trip Ends vs: Dwelling Units
On a: Saturday

Setting/Location: General Urban/Suburban
Number of Studies: 52
Avg. Num. of Dwelling Units: 207
Directional Distribution: $50 \%$ entering, $50 \%$ exiting
Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 9.54 | $5.32-15.25$ | 2.17 |

## Data Plot and Equation



## Single-Family Detached Housing <br> (210)

Vehicle Trip Ends vs: Dwelling Units
On a: Saturday, Peak Hour of Generator

## Setting/Location: General Urban/Suburban

Number of Studies: 31
Avg. Num. of Dwelling Units: 188
Directional Distribution: 54\% entering, 46\% exiting
Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.93 | $0.64-1.75$ | 0.26 |

## Data Plot and Equation



# General Office Building (710) 

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday

## Setting/Location: General Urban/Suburban

Number of Studies: 66
Avg. 1000 Sq. Ft. GFA: 171
Directional Distribution: $50 \%$ entering, $50 \%$ exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 9.74 | $2.71-27.56$ | 5.15 |

Data Plot and Equation


## General Office Building (710)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA<br>On a: Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.<br>Setting/Location: General Urban/Suburban<br>Number of Studies: 35<br>Avg. 1000 Sq. Ft. GFA: 117<br>Directional Distribution: $86 \%$ entering, $14 \%$ exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 1.16 | $0.37-4.23$ | 0.47 |

Data Plot and Equation


Trip Generation Manual, 10th Edition - Institute of Transportation Engineers

* use rate (set weekday pm peak-hour trip calculations)


## General Office Building (710)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA<br>On a: Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.<br>Setting/Location: General Urban/Suburban<br>Number of Studies: 32<br>Avg. 1000 Sq. Ft. GFA: 114<br>Directional Distribution: 16\% entering, $84 \%$ exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 1.15 | $0.47-3.23$ | 0.42 |

## Data Plot and Equation



## General Office Building (710)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Saturday

Setting/Location: General Urban/Suburban
Number of Studies: 5
Avg. 1000 Sq. Ft. GFA: 94
Directional Distribution: $50 \%$ entering, $50 \%$ exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 2.21 | $1.24-7.46$ | 1.70 |



# General Office Building (710) 

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Saturday, Peak Hour of Generator

Setting/Location: General Urban/Suburban
Number of Studies: 3
Avg. 1000 Sq. Ft. GFA: 82
Directional Distribution: 54\% entering, 46\% exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.53 | $0.30-1.57$ | 0.52 |

Data Plot and Equation


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## Government Office Building (730)



## Data Plot and Equation



## Government Office Building <br> (730)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,
Peak Hour of Adjacent Street Traffic,
One Hour Between 7 and 9 a.m.
Setting/Location: General Urban/Suburban
Number of Studies: 7
Avg. 1000 Sq. Ft. GFA: 11
Directional Distribution: 75\% entering, 25\% exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 3.34 | $0.45-7.38$ | 2.18 |

Data Plot and Equation


## Government Office Building <br> (730)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weokday,
Peak Hour of Adjacent Street Traffic,
One Hour Between 4 and 6 p.m.
Setting/Location: General Urban/Suburban
Number of Studies: 8
Avg. 1000 Sq. Ft. GFA: 22
Directional Distribution: 25\% entering, 75\% exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 1.71 | $1.09-6.19$ | 1.24 |

Data Plot and Equation


## Shopping Center (820)

Vehicle Trip Ends vs: 1000 Sq. Ft. GLA On a: Weekday

## Setting/Location: General Urban/Suburban

Number of Studies: 147
Avg. 1000 Sq. Ft. GLA: 453
Directional Distribution: 50\% entering, 50\% exiting
Vehicle Trip Generation per 1000 Sq. Ft. GLA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 37.75 | $7.42-207.98$ | 16.41 |

Data Plot and Equation


## Shopping Center (820)

Vehicle Trip Ends vs: 1000 Sq. Ft. GLA<br>On a: Weekday,<br>Peak Hour of Adjacent Street Traffic,<br>One Hour Between 7 and 9 a.m.<br>Setting/Location: General Urban/Suburban<br>Number of Studies: 84<br>Avg. 1000 Sq. Ft. GLA: 351<br>Directional Distribution: $62 \%$ entering, $38 \%$ exiting

Vehicle Trip Generation per 1000 Sq. Ft. GLA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.94 | $0.18-23.74$ | 0.87 |

## Data Plot and Equation



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## Shopping Center (820)

|  | Vehicle Trip Ends vs: On a: <br> Setting/Location: <br> Number of Studies: Avg. 1000 Sq. Ft. GLA: Directional Distribution: | 1000 Sq. Ft. GLA <br> Weekday, <br> Peak Hour of Adjacent Street Traffic, <br> One Hour Between 4 and 6 p.m. <br> General Urban/Suburban <br> 261 <br> 327 <br> $48 \%$ entering, $52 \%$ exiting |
| :---: | :---: | :---: |
| Vehicle Trip Generation per 1000 Sq. Ft. GLA |  |  |
| Average Rate | Range o | f Rates Standard Deviation |
| 3.81 | 0.74-1 | 8.69 2.04 |

## Data Plot and Equation



## Shopping Center (820)

Vehicle Trip Ends vs: 1000 Sq. Ft. GLA<br>On a: Saturday

## Setting/Location: General Urban/Suburban

Number of Studies: 58
Avg. 1000 Sq. Ft. GLA: 602
Directional Distribution: 50\% entering, $50 \%$ exiting
Vehicle Trip Generation per 1000 Sq. Ft. GLA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :--- | :---: |
| 46.12 | $13.01-167.89$ | 17.91 |

Data Plot and Equation


## Shopping Center (820)

## Vehicle Trip Ends vs: 1000 Sq. Ft. GLA

On a: Saturday, Peak Hour of Generator

## Setting/Location: General Urban/Suburban

Number of Studies: 119
Avg. 1000 Sq. Ft. GLA: 416
Directional Distribution: $52 \%$ entering, $48 \%$ exiting
Vehicle Trip Generation per 1000 Sq. Ft. GLA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 4.50 | $1.42-15.10$ | 1.88 |

Data Plot and Equation


## Drive-in Bank

## Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday

## Setting/Location: General Urban/Suburban

Number of Studies: 21
Avg. 1000 Sq. Ft. GFA: 7
Directional Distribution: 50\% entering, $50 \%$ exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 100.03 | $32.67-408.42$ | 61.61 |

Data Plot and Equation


## Drive-in Bank

(912)

## Vehicle Trip Ends vs: 1000 Sq. Ft. GFA <br> On a: Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

## Setting/Location: General Urban/Suburban

Number of Studies: 46
Avg. 1000 Sq. Ft. GFA: 5
Directional Distribution: 58\% entering, 42\% exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 9.50 | $0.89-29.47$ | 5.85 |

## Data Plot and Equation



## Drive-in Bank <br> (912)

## Vehicle Trip Ends vs: 1000 Sq. Ft. GFA <br> On a: Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. <br> Setting/Location: General Urban/Suburban <br> Number of Studies: 115 <br> Avg. 1000 Sq. Ft. GFA: 4 <br> Directional Distribution: 50\% entering, 50\% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 20.45 | $3.04-109.91$ | 15.01 |

## Data Plot and Equation



## Drive-in Bank <br> (912)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Saturday

## Setting/Location: General Urban/Suburban

Number of Studies: 5
Avg. 1000 Sq. Ft. GFA: 3
Directional Distribution: 50\% entering, 50\% exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 86.48 | $42.46-171.78$ | 38.92 |



## Drive-in Bank

(912)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Saturday, Peak Hour of Generator

## Setting/Location: General Urban/Suburban

Number of Studies: 41
Avg. 1000 Sq. Ft. GFA: 4
Directional Distribution: $51 \%$ entering, $49 \%$ exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 26.35 | $7.18-107.00$ | 15.32 |

Data Plot and Equation


WEEKDAY MORNING PEAK HOUR (7:00-8:00 AM)


SATURDAY MIDDAY PEAK HOUR (11:00-12:00 PM)


Town of Barrington, New Hampshire
2010 U.S. Census Journey-to-Work Data


NH Route 125 at Greenhill Road and Tolend Road
NH Route 125 at Scruton Pond Road
NH Route 125 at NH Route 9
NH Route 125 at the North Project Site Roadway
NH Route 125 at the South Project Site Roadway

NH Route 125 at Greenhill Road and Tolend Road

|  | 4 | $\rightarrow$ | $\dagger$ | $\checkmark$ | $\pm$ | 4 | $4$ | 9 | \% | $t$ | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | \$ |  | 7 | + | 「 | ${ }^{7}$ | + | 「 |
| Traffic Volume (vph) | 19 | 43 | 129 | 25 | 8 | 15 | 20 | 564 | 28 | 17 | 971 | 5 |
| Future Volume (vph) | 19 | 43 | 129 | 25 | 8 | 15 | 20 | 564 | 28 | 17 | 971 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width ( ft ) | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 100 |  | 100 | 60 |  | 60 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 579 |  |  | 696 |  |  | 2249 |  |  | 626 |  |
| Travel Time (s) |  | 13.2 |  |  | 15.8 |  |  | 51.1 |  |  | 14.2 |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.82 | 0.82 | 0.82 | 0.93 | 0.93 | 0.93 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 0\% | 0\% | 2\% | 0\% | 0\% | 9\% | 7\% | 5\% | 24\% | 0\% | 6\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 219 | 0 | 0 | 58 | 0 | 22 | 606 | 30 | 18 | 1033 | 5 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% |  | 20.0\% | 20.0\% |  | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| v/c Ratio |  | 0.62 |  |  | 0.40 |  | 0.07 | 0.47 | 0.03 | 0.03 | 0.85 | 0.00 |
| Control Delay |  | 23.5 |  |  | 30.6 |  | 3.2 | 7.2 | 0.1 | 2.9 | 21.3 | 0.0 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 23.5 |  |  | 30.6 |  | 3.2 | 7.2 | 0.1 | 2.9 | 21.3 | 0.0 |
| Queue Length 50th (ft) |  | 39 |  |  | 14 |  | 2 | 86 | 0 | 2 | 231 | 0 |
| Queue Length 95th (ft) |  | 111 |  |  | 47 |  | 7 | 256 | 0 | 6 | \#751 | 0 |
| Internal Link Dist (ft) |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 387 |  |  | 162 |  | 341 | 1281 | 957 | 662 | 1209 | 1130 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.57 |  |  | 0.36 |  | 0.06 | 0.47 | 0.03 | 0.03 | 0.85 | 0.00 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## 2019 Existing Weekday Morning Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road
Area Type: Other

Cycle Length: 80
Actuated Cycle Length: 71.3
Natural Cycle: 75
Control Type: Actuated-Uncoordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 |  | $\geqslant$ | 7 | - |  | 4 | $\dagger$ | \% |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | \$ |  | \% | $\uparrow$ | 「 | \% | 4 | \% |
| Traffic Volume (voh) | 19 | 43 | 129 | 25 | 8 | 15 | 20 | 564 | 28 | 17 | 971 | 5 |
| Future Volume (vph) | 19 | 43 | 129 | 25 | 8 | 15 | 20 | 564 | 28 | 17 | 971 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.91 |  |  | 0.96 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| FIt Protected |  | 1.00 |  |  | 0.97 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1808 |  |  | 1841 |  | 1687 | 1810 | 1302 | 1805 | 1792 | 1615 |
| Flt Permitted |  | 0.96 |  |  | 0.46 |  | 0.10 | 1.00 | 1.00 | 0.37 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1744 |  |  | 871 |  | 174 | 1810 | 1302 | 698 | 1792 | 1615 |
| Peak-hour factor, PHF | 0.87 | 0.87 | 0.87 | 0.82 | 0.82 | 0.82 | 0.93 | 0.93 | 0.93 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 22 | 49 | 148 | 30 | 10 | 18 | 22 | 606 | 30 | 18 | 1033 | 5 |
| RTOR Reduction (vph) | 0 | 95 | 0 | 0 | 16 | 0 | 0 | 0 | 10 | 0 | 0 | 2 |
| Lane Group Flow (vph) | 0 | 124 | 0 | 0 | 42 | 0 | 22 | 606 | 20 | 18 | 1033 | 3 |
| Heavy Vehicles (\%) | 0\% | 0\% | 2\% | 0\% | 0\% | 9\% | 7\% | 5\% | 24\% | 0\% | 6\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 8.5 |  |  | 8.5 |  | 50.9 | 48.5 | 48.5 | 48.3 | 47.2 | 47.2 |
| Effective Green, g (s) |  | 10.5 |  |  | 10.5 |  | 54.9 | 50.5 | 50.5 | 52.3 | 49.2 | 49.2 |
| Actuated g/C Ratio |  | 0.14 |  |  | 0.14 |  | 0.72 | 0.66 | 0.66 | 0.69 | 0.65 | 0.65 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 240 |  |  | 120 |  | 213 | 1201 | 864 | 524 | 1158 | 1044 |
| v/s Ratio Prot |  |  |  |  |  |  | c0.01 | 0.33 |  | 0.00 | c0.58 |  |
| v/s Ratio Perm |  | c0.07 |  |  | 0.05 |  | 0.07 |  | 0.02 | 0.02 |  | 0.00 |
| v/c Ratio |  | 0.52 |  |  | 0.35 |  | 0.10 | 0.50 | 0.02 | 0.03 | 0.89 | 0.00 |
| Uniform Delay, d1 |  | 30.4 |  |  | 29.7 |  | 10.7 | 6.5 | 4.4 | 4.2 | 11.2 | 4.8 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 1.9 |  |  | 1.8 |  | 0.2 | 0.3 | 0.0 | 0.0 | 8.9 | 0.0 |
| Delay (s) |  | 32.3 |  |  | 31.5 |  | 10.9 | 6.8 | 4.4 | 4.2 | 20.2 | 4.8 |
| Level of Service |  | C |  |  | C |  | B | A | A | A | C | A |
| Approach Delay (s) |  | 32.3 |  |  | 31.5 |  |  | 6.8 |  |  | 19.8 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 17.2 |  | HCM 2000 | evel of | Service |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.78 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 76.1 |  | Sum of lost | time (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 69.1\% |  | CU Level | Service |  |  | C |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
AJA

|  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group Flow (vph) | 0 | 86 | 0 | 0 | 154 | 0 | 131 | 1033 | 31 | 27 | 727 | 32 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |

Switch Phase

| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum Split (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 | 16.0 | 16.0 | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% | 20.0\% | 20.0\% | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 | 10.0 | 10.0 | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None | Min | Min | None | Min | Min |
| v/c Ratio |  | 0.28 |  | 0.56 | 0.27 | 0.83 | 0.03 | 0.09 | 0.67 | 0.03 |
| Control Delay |  | 17.9 |  | 33.1 | 4.4 | 19.2 | 0.0 | 3.6 | 15.3 | 0.1 |
| Queue Delay |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 17.9 |  | 33.1 | 4.4 | 19.2 | 0.0 | 3.6 | 15.3 | 0.1 |
| Queue Length 50th ( t ) |  | 13 |  | 48 | 14 | 226 | 0 | 3 | 224 | 0 |
| Queue Length 95th ( ft ) |  | 50 |  | 95 | 26 | \#733 | 0 | 8 | 340 | 0 |
| Internal Link Dist (ft) |  | 499 |  | 616 |  | 2169 |  |  | 546 |  |
| Turn Bay Length (t) |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 327 |  | 297 | 499 | 1243 | 1118 | 358 | 1232 | 1110 |
| Starvation Cap Reductn |  | 0 |  | 0 | , | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.26 |  | 0.52 | 0.26 | 0.83 | 0.03 | 0.08 | 0.59 | 0.03 |

## Intersection Summary

## 2019 Existing Weekday Evening Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road
Area Type:
Other

Cycle Length: 80
Actuated Cycle Length: 70.6
Natural Cycle: 70
Control Type: Actuated-Uncoordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


|  | 4 | $\rightarrow$ |  | 7 | $\square$ | 4 | 4 | 4 | 1 | * | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | $\uparrow$ |  | \% | $\uparrow$ | F | ${ }_{1}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 16 | 15 | 41 | 49 | 31 | 36 | 118 | 930 | 28 | 24 | 640 | 28 |
| Future Volume (vph) | 16 | 15 | 41 | 49 | 31 | 36 | 118 | 930 | 28 | 24 | 640 | 28 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.92 |  |  | 0.96 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 0.99 |  |  | 0.98 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1850 |  |  | 1878 |  | 1805 | 1863 | 1615 | 1805 | 1863 | 1615 |
| Flt Permitted |  | 0.89 |  |  | 0.85 |  | 0.22 | 1.00 | 1.00 | 0.10 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1673 |  |  | 1622 |  | 419 | 1863 | 1615 | 182 | 1863 | 1615 |
| Peak-hour factor, PHF | 0.84 | 0.84 | 0.84 | 0.75 | 0.75 | 0.75 | 0.90 | 0.90 | 0.90 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph) | 19 | 18 | 49 | 65 | 41 | 48 | 131 | 1033 | 31 | 27 | 727 | 32 |
| RTOR Reduction (vph) | 0 | 42 | 0 | 0 | 20 | 0 | 0 | 0 | 11 | 0 | 0 | 13 |
| Lane Group Flow (vph) | 0 | 44 | 0 | 0 | 134 | 0 | 131 | 1033 | 20 | 27 | 727 | 19 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 4\% | 0\% | 2\% | 0\% | 0\% | 2\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 |  |  | 6 |
| Actuated Green, G (s) |  | 9.1 |  |  | 9.1 |  | 50.8 | 45.1 | 45.1 | 43.8 | 41.6 | 41.6 |
| Effective Green, g (s) |  | 11.1 |  |  | 11.1 |  | 54.8 | 47.1 | 47.1 | 47.8 | 43.6 | 43.6 |
| Actuated g/C Ratio |  | 0.15 |  |  | 0.15 |  | 0.74 | 0.63 | 0.63 | 0.64 | 0.59 | 0.59 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 249 |  |  | 241 |  | 452 | 1179 | 1022 | 208 | 1091 | 946 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  | c0.03 | c0.55 |  | 0.01 | 0.39 |  |
| v/s Ratio Perm |  | 0.03 |  |  | c0.08 |  | 0.18 |  | 0.01 | 0.08 |  | 0.01 |
| $v / c$ Ratio |  | 0.18 |  |  | 0.55 |  | 0.29 | 0.88 | 0.02 | 0.13 | 0.67 | 0.02 |
| Uniform Delay, d1 |  | 27.7 |  |  | 29.4 |  | 6.2 | 11.2 | 5.1 | 10.9 | 10.5 | 6.5 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.3 |  |  | 2.7 |  | 0.4 | 7.5 | 0.0 | 0.3 | 1.6 | 0.0 |
| Delay (s) |  | 28.0 |  |  | 32.1 |  | 6.5 | 18.8 | 5.1 | 11.2 | 12.0 | 6.5 |
| Level of Service |  | C |  |  | C |  | A | B | A | B | B | A |
| Approach Delay (s) |  | 28.0 |  |  | 32.1 |  |  | 17.1 |  |  | 11.8 |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 16.7 |  | CM 2000 | evel of S | ervice |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.79 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 74.4 |  | Sum of lost | ime (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 74.9\% |  | CU Level of | Service |  |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

2019 Existing Saturday Midday Peak Hour
1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ |  | 7 | $\square$ | 4 | 4 | 4 | 7 | V | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | $\dagger$ |  | 7 | $\uparrow$ | 「 | K | $\uparrow$ | F |
| Traffic Volume (vph) | 12 | 13 | 77 | 33 | 11 | 35 | 68 | 602 | 25 | 20 | 662 | 17 |
| Future Volume (vph) | 12 | 13 | 77 | 33 | 11 | 35 | 68 | 602 | 25 | 20 | 662 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width ( t ) | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 100 |  | 100 | 60 |  | 60 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (t) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (t) |  | 579 |  |  | 696 |  |  | 2249 |  |  | 626 |  |
| Travel Time (s) |  | 13.2 |  |  | 15.8 |  |  | 51.1 |  |  | 14.2 |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.87 | 0.87 | 0.87 | 0.89 | 0.89 | 0.89 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 117 | 0 | 0 | 91 | 0 | 76 | 676 | 28 | 25 | 828 | 21 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(ft) |  | 0 |  |  | 0 |  |  | 12 |  |  | 12 |  |
| Link Offsel(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(ft) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Tuming Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% |  | 20.0\% | 20.0\% |  | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| vic Ratio |  | 0.33 |  |  | 0.33 |  | 0.16 | 0.49 | 0.02 | 0.04 | 0.68 | 0.02 |
| Control Delay |  | 14.2 |  |  | 22.3 |  | 3.4 | 8.4 | 0.0 | 2.9 | 15.3 | 0.1 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 14.2 |  |  | 22.3 |  | 3.4 | 8.4 | 0.0 | 2.9 | 15.3 | 0.1 |
| Queue Length 50th (ft) |  | 11 |  |  | 20 |  | 7 | 86 | 0 | 2 | 261 | 0 |
| Queue Length 95th (ti) |  | 56 |  |  | 61 |  | 16 | 285 | 0 | 6 | 343 | 0 |
| Internal Link Dist (ft) |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | 7 | 1 | $\longleftarrow$ | 4 | 4 | $\uparrow$ | $p$ | b | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Turn Bay Length ( t ) |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 436 |  |  | 342 |  | 513 | 1413 | 1233 | 675 | 1356 | 1199 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.27 |  |  | 0.27 |  | 0.15 | 0.48 | 0.02 | 0.04 | 0.61 | 0.02 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 63.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 60 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | $\stackrel{ }{*}$ | $\rightarrow$ | $\geqslant$ | 6 | 4 | 4 | $\cdots$ | $\uparrow$ | 1 | - | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | $\uparrow$ |  | 7 | $\uparrow$ | F | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 12 | 13 | 77 | 33 | 11 | 35 | 68 | 602 | 25 | 20 | 662 | 17 |
| Future Volume (vph) | 12 | 13 | 77 | 33 | 11 | 35 | 68 | 602 | 25 | 20 | 662 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.90 |  |  | 0.94 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 0.99 |  |  | 0.98 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1810 |  |  | 1867 |  | 1805 | 1900 | 1615 | 1805 | 1881 | 1615 |
| FIt Permitted |  | 0.95 |  |  | 0.77 |  | 0.18 | 1.00 | 1.00 | 0.34 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1737 |  |  | 1470 |  | 337 | 1900 | 1615 | 644 | 1881 | 1615 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.87 | 0.87 | 0.87 | 0.89 | 0.89 | 0.89 | 0.80 | 0.80 | 0.80 |
| Adj. Flow (vph) | 14 | 15 | 88 | 38 | 13 | 40 | 76 | 676 | 28 | 25 | 828 | 21 |
| RTOR Reduction (vph) | 0 | 78 | 0 | 0 | 35 | 0 | 0 | 0 | 10 | 0 | 0 | 8 |
| Lane Group Flow (vph) | 0 | 39 | 0 | 0 | 56 | 0 | 76 | 676 | 18 | 25 | 828 | 13 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | - |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 5.9 |  |  | 5.9 |  | 48.0 | 42.8 | 42.8 | 41.4 | 39.5 | 39.5 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 7.9 |  |  | 7.9 |  | 52.0 | 44.8 | 44.8 | 45.4 | 41.5 | 41.5 |
| Actuated g/C Ratio |  | 0.12 |  |  | 0.12 |  | 0.76 | 0.65 | 0.65 | 0.66 | 0.60 | 0.60 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 200 |  |  | 169 |  | 409 | 1240 | 1054 | 492 | 1137 | 977 |
| v/s Ratio Prot |  |  |  |  |  |  | c0.02 | c0.36 |  | 0.00 | c0.44 |  |
| v/s Ratio Perm |  | 0.02 |  |  | c0.04 |  | 0.12 |  | 0.01 | 0.03 |  | 0.01 |
| v/c Ratio |  | 0.20 |  |  | 0.33 |  | 0.19 | 0.55 | 0.02 | 0.05 | 0.73 | 0.01 |
| Uniform Delay, d1 |  | 27.5 |  |  | 27.9 |  | 6.2 | 6.4 | 4.2 | 4.3 | 9.6 | 5.4 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.5 |  |  | 1.1 |  | 0.2 | 0.5 | 0.0 | 0.0 | 2.4 | 0.0 |
| Delay (s) |  | 28.0 |  |  | 29.1 |  | 6.4 | 6.9 | 4.2 | 4.4 | 11.9 | 5.4 |
| Level of Service |  | C |  |  | c |  | A | A | A | A | B | A |
| Approach Delay (s) |  | 28.0 |  |  | 29.1 |  |  | 6.8 |  |  | 11.6 |  |
| Approach LOS |  | C |  |  | c |  |  | A |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 11.4 |  | CM 2000 | evel of S | Service |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.60 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 68.6 |  | Sum of lost | lime (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 60.2\% |  | CU Level of | Service |  |  | B |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ | 7 | $t$ |  | 4 | 4 | $\dagger$ | + |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | $\uparrow$ |  | ${ }^{1}$ | $\uparrow$ | 「 | \% | $\uparrow$ | 「 |
| Traffic Volume (vph) | 19 | 43 | 132 | 25 | 8 | 15 | 20 | 556 | 28 | 17 | 993 | 5 |
| Future Volume (vph) | 19 | 43 | 132 | 25 | 8 | 15 | 20 | 556 | 28 | 17 | 993 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 100 |  | 100 | 60 |  | 60 |
| Storage Lanes |  |  | 0 | 0 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 579 |  |  | 696 |  |  | 2249 |  |  | 626 |  |
| Travel Time (s) |  | 13.2 |  |  | 15.8 |  |  | 51.1 |  |  | 14.2 |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.82 | 0.82 | 0.82 | 0.93 | 0.93 | 0.93 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 0\% | 0\% | 2\% | 0\% | 0\% | 9\% | 7\% | 5\% | 24\% | 0\% | 6\% | 0\% |


| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group Flow (vph) | 0 | 223 | 0 | 0 | 58 | 0 | 22 | 598 | 30 | 18 | 1056 | 5 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |


| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 | 16.0 | 16.0 | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% | 20.0\% | 20.0\% | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 | 10.0 | 10.0 | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None | Min | Min | None | Min | Min |
| v/c Ratio |  | 0.63 |  | 0.40 | 0.08 | 0.47 | 0.03 | 0.03 | 0.87 | 0.00 |
| Control Delay |  | 23.5 |  | 30.7 | 3.3 | 7.1 | 0.1 | 2.8 | 22.9 | 0.0 |
| Queue Delay |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 23.5 |  | 30.7 | 3.3 | 7.1 | 0.1 | 2.8 | 22.9 | 0.0 |
| Queue Length 50th (t) |  | 39 |  | 14 |  | 85 | 0 | 2 | 245 | 0 |
| Queue Length 95th (f) |  | 111 |  | 47 | 7 | 251 | 0 | 6 | \#776 | 0 |
| Internal Link Dist (ft) |  | 499 |  | 616 |  | 2169 |  |  | 546 |  |
| Turn Bay Length (tt) |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 390 |  | 162 | 325 | 1280 | 956 | 668 | 1208 | 1129 |
| Starvation Cap Reductn |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  | 0 | 0 | , | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.57 |  | 0.36 | 0.07 | 0.47 | 0.03 | 0.03 | 0.87 | 0.00 |

## Intersection Summary

## 2020 No Build Weekday Morning Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road
Area Type:
Other

Cycle Length: 80
Actuated Cycle Length: 71.1

## Natural Cycle: 75

Control Type: Actuated-Uncoordinated
\# 95th percentile volume exceeds capacity, queue may be fonger.
Queue shown is maximum after two cycles.
Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


## 2020 No Build Weekday Morning Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | \% | 7 | - |  | 4 | $\dagger$ | 7 | * | $\downarrow$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\ddagger$ |  | \% | $\uparrow$ | 「 | \% | $\uparrow$ | 「 |
| Trafic Volume (vph) | 19 | 43 | 132 | 25 | 8 | 15 | 20 | 556 | 28 | 17 | 993 | 5 |
| Future Volume (vph) | 19 | 43 | 132 | 25 | 8 | 15 | 20 | 556 | 28 | 17 | 993 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Utill Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.91 |  |  | 0.96 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 1.00 |  |  | 0.97 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Sald. Flow (prot) |  | 1807 |  |  | 1841 |  | 1687 | 1810 | 1302 | 1805 | 1792 | 1615 |
| Flt Permitted |  | 0.96 |  |  | 0.46 |  | 0.08 | 1.00 | 1.00 | 0.37 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1744 |  |  | 867 |  | 148 | 1810 | 1302 | 706 | 1792 | 1615 |
| Peak-hour factor, PHF | 0.87 | 0.87 | 0.87 | 0.82 | 0.82 | 0.82 | 0.93 | 0.93 | 0.93 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 22 | 49 | 152 | 30 | 10 | 18 | 22 | 598 | 30 | 18 | 1056 | 5 |
| RTOR Reduction (vph) | 0 | 97 | 0 | 0 | 15 | 0 | 0 | 0 | 10 | 0 | 0 | 2 |
| Lane Group Flow (vph) | 0 | 126 | 0 | 0 | 43 | 0 | 22 | 598 | 20 | 18 | 1056 | 3 |
| Heavy Vehicles (\%) | 0\% | 0\% | 2\% | 0\% | 0\% | 9\% | 7\% | 5\% | 24\% | 0\% | 6\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 8.6 |  |  | 8.6 |  | 50.7 | 48.3 | 48.3 | 48.1 | 47.0 | 47.0 |
| Effective Green, g (s) |  | 10.6 |  |  | 10.6 |  | 54.7 | 50.3 | 50.3 | 52.1 | 49.0 | 49.0 |
| Actuated g/C Ratio |  | 0.14 |  |  | 0.14 |  | 0.72 | 0.66 | 0.66 | 0.69 | 0.64 | 0.64 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Gpp Cap (vph) |  | 243 |  |  | 120 |  | 195 | 1197 | 861 | 528 | 1155 | 1041 |
| v/s Ratio Prot |  |  |  |  |  |  | c0.01 | 0.33 |  | 0.00 | c0.59 |  |
| v/s Ratio Perm |  | c0.07 |  |  | 0.05 |  | 0.07 |  | 0.02 | 0.02 |  | 0.00 |
| v/c Ratio |  | 0.52 |  |  | 0.35 |  | 0.11 | 0.50 | 0.02 | 0.03 | 0.91 | 0.00 |
| Uniform Delay, d1 |  | 30.3 |  |  | 29.6 |  | 11.8 | 6.5 | 4.4 | 4.2 | 11.7 | 4.8 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 1.9 |  |  | 1.8 |  | 0.3 | 0.3 | 0.0 | 0.0 | 11.1 | 0.0 |
| Delay (s) |  | 32.2 |  |  | 31.4 |  | 12.0 | 6.8 | 4.4 | 4.2 | 22.7 | 4.8 |
| Level of Service |  | C |  |  | C |  | B | A | A | A | C | A |
| Approach Delay (s) |  | 32.2 |  |  | 31.4 |  |  | 6.9 |  |  | 22.3 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 18.7 |  | HCM 2000 | evel of S | Service |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.79 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 76.0 |  | um of lost | ime (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 70.4\% |  | CU Level of | Service |  |  | C |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) <br> c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

## 2020 No Build Weekday Evening Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ |  |  |  | 4 | 4 | $\dagger$ | P | v | $\downarrow$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | \$ |  | \% | $\uparrow$ | 「 | 4 | 4 | 「 |
| Traffic Volume (vph) | 16 | 15 | 42 | 50 | 31 | 36 | 121 | 950 | 28 | 24 | 657 | 28 |
| Future Volume (vph) | 16 | 15 | 42 | 50 | 31 | 36 | 121 | 950 | 28 | 24 | 657 | 28 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width ( f ) | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (t) | 0 |  | 0 | 0 |  | 0 | 100 |  | 100 | 60 |  | 60 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (t) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( ft ) |  | 579 |  |  | 696 |  |  | 2249 |  |  | 626 |  |
| Travel Time (s) |  | 13.2 |  |  | 15.8 |  |  | 51.1 |  |  | 14.2 |  |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.75 | 0.75 | 0.75 | 0.90 | 0.90 | 0.90 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 4\% | 0\% | 2\% | 0\% | 0\% | 2\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 87 | 0 | 0 | 156 | 0 | 134 | 1056 | 31 | 27 | 747 | 32 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(ft) |  | 0 |  |  | 0 |  |  | 12 |  |  | 12 |  |
| Link Offset(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(ft) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | , |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% |  | 20.0\% | 20.0\% |  | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| v/c Ratio |  | 0.29 |  |  | 0.58 |  | 0.29 | 0.84 | 0.03 | 0.09 | 0.68 | 0.03 |
| Control Delay |  | 17.9 |  |  | 34.5 |  | 4.4 | 19.9 | 0.0 | 3.6 | 15.5 | 0.1 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 17.9 |  |  | 34.5 |  | 4.4 | 19.9 | 0.0 | 3.6 | 15.5 | 0.1 |
| Queue Length 50th (ft) |  | 13 |  |  | 51 |  | 14 | 238 | 0 | 3 | 236 | 0 |
| Queue Length 95th (t) |  | 51 |  |  | 97 |  | 27 | \#759 | 0 | 8 | 356 | 0 |
| Internal Link Dist ( t ) |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |

Lanes, Volumes, Timings
AJA

|  | 4 | $\rightarrow$ | $\geqslant$ | 7 | 4 | 4 | 4 | $\dagger$ | 7 | $\checkmark$ | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Turn Bay Length (ti) |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 319 |  |  | 287 |  | 488 | 1254 | 1127 | 343 | 1231 | 1109 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.27 |  |  | 0.54 |  | 0.27 | 0.84 | 0.03 | 0.08 | 0.61 | 0.03 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: <br> Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 72.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


## 2020 No Build Weekday Evening Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


|  | 4 | $\rightarrow$ | \% | 7 | 4 | 4 | 4 | 4 | / | ( | $\pm$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | $\ddagger$ |  | 7 | 4 | ${ }^{7}$ | \% | 4 | T |
| Traffic Volume (vph) | 12 | 13 | 79 | 33 | 11 | 35 | 70 | 615 | 25 | 20 | 677 | 17 |
| Future Volume (vph) | 12 | 13 | 79 | 33 | 11 | 35 | 70 | 615 | 25 | 20 | 677 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 100 |  | 100 | 60 |  | 60 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( ft ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 579 |  |  | 696 |  |  | 2249 |  |  | 626 |  |
| Travel Time (s) |  | 13.2 |  |  | 15.8 |  |  | 51.1 |  |  | 14.2 |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.87 | 0.87 | 0.87 | 0.89 | 0.89 | 0.89 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 119 | 0 | 0 | 91 | 0 | 79 | 691 | 28 | 25 | 846 | 21 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% |  | 20.0\% | 20.0\% |  | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| v/c Ratio |  | 0.33 |  |  | 0.34 |  | 0.17 | 0.49 | 0.02 | 0.04 | 0.70 | 0.02 |
| Contol Delay |  | 14.2 |  |  | 22.6 |  | 3.4 | 8.5 | 0.0 | 2.9 | 15.7 | 0.1 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 14.2 |  |  | 22.6 |  | 3.4 | 8.5 | 0.0 | 2.9 | 15.7 | 0.1 |
| Queue Length 50th ( ft ) |  | 11 |  |  | 20 |  | 7 | 90 | 0 | 2 | 275 | 0 |
| Queue Length 95th ( ft ) |  | 56 |  |  | 62 |  | 17 | 295 | 0 | 6 | 355 | 0 |
| Internal Link Dist (ft) |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |
| Turn Bay Length ( $t$ ) |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 434 |  |  | 334 |  | 501 | 1409 | 1229 | 663 | 1344 | 1189 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.27 |  |  | 0.27 |  | 0.16 | 0.49 | 0.02 | 0.04 | 0.63 | 0.02 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## 2020 No Build Saturday Midday Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road
Area Type: Other
Cycle Length: 80
Actuated Cycle Length: 64.4
Naturel Cycle: 60
Control Type: Actuated-Uncoordinated
Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


## 2020 No Build Saturday Midday Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | 7 | 7 | $\leftarrow$ |  | 4 | $\dagger$ | 1 | * | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | ¢ |  | \% | $\uparrow$ | F | \% | $\uparrow$ | F |
| Traffic Volume (vph) | 12 | 13 | 79 | 33 | 11 | 35 | 70 | 615 | 25 | 20 | 677 | 17 |
| Future Volume (vph) | 12 | 13 | 79 | 33 | 11 | 35 | 70 | 615 | 25 | 20 | 677 | 17 |
| Ideal Flow (Vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.90 |  |  | 0.94 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 0.99 |  |  | 0.98 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1809 |  |  | 1867 |  | 1805 | 1900 | 1615 | 1805 | 1881 | 1615 |
| Flt Permitted |  | 0.95 |  |  | 0.76 |  | 0.17 | 1.00 | 1.00 | 0.33 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1738 |  |  | 1450 |  | 319 | 1900 | 1615 | 625 | 1881 | 1615 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.87 | 0.87 | 0.87 | 0.89 | 0.89 | 0.89 | 0.80 | 0.80 | 0.80 |
| Adj. Flow (vph) | 14 | 15 | 90 | 38 | 13 | 40 | 79 | 691 | 28 | 25 | 846 | 21 |
| RTOR Reduction (vph) | 0 | 80 | 0 | 0 | 35 | 0 | 0 | 0 | 10 | 0 | 0 | 8 |
| Lane Group Flow (voh) | 0 | 39 | 0 | 0 | 56 | 0 | 79 | 691 | 18 | 25 | 846 | 13 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 6.0 |  |  | 6.0 |  | 48.7 | 43.4 | 43.4 | 42.1 | 40.1 | 40.1 |
| Effective Green, $g(s)$ |  | 8.0 |  |  | 8.0 |  | 52.7 | 45.4 | 45.4 | 46.1 | 42.1 | 42.1 |
| Actuated g/C Ratio |  | 0.12 |  |  | 0.12 |  | 0.76 | 0.65 | 0.65 | 0.66 | 0.61 | 0.61 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 200 |  |  | 167 |  | 398 | 1242 | 1056 | 483 | 1141 | 979 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  | c0.02 | c0.36 |  | 0.00 | c0.45 |  |
| V/s Ratio Perm |  | 0.02 |  |  | c0.04 |  | 0.13 |  | 0.01 | 0.03 |  | 0.01 |
| v/c Ratio |  | 0.20 |  |  | 0.33 |  | 0.20 | 0.56 | 0.02 | 0.05 | 0.74 | 0.01 |
| Uniform Delay, d1 |  | 27.8 |  |  | 28.2 |  | 6.6 | 6.5 | 4.2 | 4.4 | 9.8 | 5.4 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.5 |  |  | 1.2 |  | 0.2 | 0.5 | 0.0 | 0.0 | 2.6 | 0.0 |
| Delay (s) |  | 28.3 |  |  | 29.4 |  | 6.9 | 7.1 | 4.2 | 4.4 | 12.4 | 5.4 |
| Level of Service |  | C |  |  | C |  | A | A | A | A | B | A |
| Approach Delay (s) |  | 28.3 |  |  | 29.4 |  |  | 6.9 |  |  | 12.0 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 11.7 |  | HCM 2000 | evel of S | Service |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.62 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 69.4 |  | Sum of lost | time (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 61.0\% |  | ICU Level of | Service |  |  | B |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

## 2030 Build Weekday Morning Peak Hour

1：NH Route 125 （Calef Highway）\＆Greenhill Road／Tolend Road

|  | 4 | $\rightarrow$ | $\bigcirc$ | $\downarrow$ | 4 | 4 | 4 | $\dagger$ | \％ | （ | $\dagger$ | $+$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | \＄ |  | 7 | 中 | 「 | 7 | 中 | F |
| Traffic Volume（vph） | 19 | 43 | 139 | 29 | 8 | 15 | 22 | 577 | 34 | 17 | 1043 | 5 |
| Future Volume（vph） | 19 | 43 | 139 | 29 | 8 | 15 | 22 | 577 | 34 | 17 | 1043 | 5 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（ft） | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length（ ft ） | 0 |  | 0 | 0 |  | 0 | 100 |  | 100 | 60 |  | 60 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ ft ） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（ ft ） |  | 579 |  |  | 696 |  |  | 2249 |  |  | 626 |  |
| Travel Time（s） |  | 13.2 |  |  | 15.8 |  |  | 51.1 |  |  | 14.2 |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.82 | 0.82 | 0.82 | 0.93 | 0.93 | 0.93 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles（\％） | 0\％ | 0\％ | 2\％ | 0\％ | 0\％ | 9\％ | 7\％ | 5\％ | 24\％ | 0\％ | 6\％ | 0\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 0 | 231 | 0 | 0 | 63 | 0 | 24 | 620 | 37 | 18 | 1110 | 5 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split（s） | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split（\％） | 20．0\％ | 20．0\％ |  | 20．0\％ | 20．0\％ |  | 17．5\％ | 62．5\％ | 62．5\％ | 17．5\％ | 62．5\％ | 62．5\％ |
| Maximum Green（ $s$ ） | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time（s） | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） |  | －2．0 |  |  | －2．0 |  | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |
| Total Lost Time（s） |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead／Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| v／c Ratio |  | 0.64 |  |  | 0.49 |  | 0.09 | 0.49 | 0.04 | 0.03 | 0.92 | 0.00 |
| Control Delay |  | 23.5 |  |  | 36.5 |  | 3.4 | 7.4 | 0.1 | 2.9 | 27.7 | 0.0 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 23.5 |  |  | 36.5 |  | 3.4 | 7.4 | 0.1 | 2.9 | 27.7 | 0.0 |
| Queue Length 50th（ft） |  | 40 |  |  | 16 |  | 2 | 91 | 0 | 2 | 280 | 0 |
| Queue Length 95th（ t ） |  | 114 |  |  | 52 |  | 7 | 265 | 0 | 6 | \＃835 | 0 |
| Internal Link Dist（ft） |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |
| Turn Bay Length（ft） |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity（vph） |  | 396 |  |  | 144 |  | 323 | 1278 | 955 | 651 | 1206 | 1127 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v／c Ratio |  | 0.58 |  |  | 0.44 |  | 0.07 | 0.49 | 0.04 | 0.03 | 0.92 | 0.00 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Lanes，Volumes，Timings
AJA
Area Type: Other
Cycle Length: $80 \quad$ Cength: 70.9
Actuated Cycle Letural Cycle: 90
Control Type: Actuated-Uncoordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


## 2030 Build Weekday Morning Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | * | $\rightarrow$ | 7 | 7 |  | 4 | 4 | $\dagger$ | 1 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\pm$ |  |  | \$ |  | 7 | $\uparrow$ | 「 | 7 | $\uparrow$ | T |
| Traffic Volume (vph) | 19 | 43 | 139 | 29 | 8 | 15 | 22 | 577 | 34 | 17 | 1043 | 5 |
| Future Volume (vph) | 19 | 43 | 139 | 29 | 8 | 15 | 22 | 577 | 34 | 17 | 1043 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.91 |  |  | 0.96 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 1.00 |  |  | 0.97 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1803 |  |  | 1848 |  | 1687 | 1810 | 1302 | 1805 | 1792 | 1615 |
| Flt Permitted |  | 0.96 |  |  | 0.40 |  | 0.08 | 1.00 | 1.00 | 0.36 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1746 |  |  | 759 |  | 142 | 1810 | 1302 | 679 | 1792 | 1615 |
| Peak-hour factor, PHF | 0.87 | 0.87 | 0.87 | 0.82 | 0.82 | 0.82 | 0.93 | 0.93 | 0.93 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 22 | 49 | 160 | 35 | 10 | 18 | 24 | 620 | 37 | 18 | 1110 | 5 |
| RTOR Reduction (vph) | 0 | 102 | 0 | 0 | 15 | 0 | 0 | 0 | 13 | , | 0 | 2 |
| Lane Group Flow (vph) | 0 | 129 | 0 | 0 | 48 | 0 | 24 | 620 | 24 | 18 | 1110 | 3 |
| Heavy Vehicles (\%) | 0\% | 0\% | 2\% | 0\% | 0\% | 9\% | 7\% | 5\% | 24\% | 0\% | 6\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | - |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 8.6 |  |  | 8.6 |  | 50.5 | 48.1 | 48.1 | 47.9 | 46.8 | 46.8 |
| Effective Green, g ( s ) |  | 10.6 |  |  | 10.6 |  | 54.5 | 50.1 | 50.1 | 51.9 | 48.8 | 48.8 |
| Actuated g/C Ratio |  | 0.14 |  |  | 0.14 |  | 0.72 | 0.66 | 0.66 | 0.68 | 0.64 | 0.64 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 244 |  |  | 106 |  | 191 | 1196 | 860 | 510 | 1153 | 1039 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  | c0.01 | 0.34 |  | 0.00 | c0.62 |  |
| v/s Ratio Perm |  | c0.07 |  |  | 0.06 |  | 0.08 |  | 0.02 | 0.02 |  | 0.00 |
| v/c Ratio |  | 0.53 |  |  | 0.45 |  | 0.13 | 0.52 | 0.03 | 0.04 | 0.96 | 0.00 |
| Uniform Delay, d1 |  | 30.3 |  |  | 29.9 |  | 14.3 | 6.6 | 4.4 | 4.3 | 12.6 | 4.8 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 2.1 |  |  | 3.0 |  | 0.3 | 0.4 | 0.0 | 0.0 | 18.1 | 0.0 |
| Delay (s) |  | 32.3 |  |  | 32.9 |  |  | 7.0 | 4.5 | 4.3 | 30.8 | 4.8 |
| Level of Service |  | C |  |  | C |  | B | A | A | A | C | A |
| Approach Delay (s) |  | 32.3 |  |  | 32.9 |  |  | 7.1 |  |  | 30.2 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 23.1 |  | HCM 2000 | evel of S | Service |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.83 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 75.8 |  | Sum of lost | time (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 73.4\% |  | CU Level of | Service |  |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

|  | 4 | $\rightarrow$ | $\uparrow$ | $\checkmark$ | 4 | 4 | ＋ | $\dagger$ | 1 | $t$ | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ＊ |  |  | $\dagger$ |  | ${ }^{7}$ | 个 | 「 | 7 | 中 | 「 |
| Traffic Volume（vph） | 16 | 15 | 46 | 56 | 31 | 36 | 129 | 1004 | 33 | 24 | 668 | 28 |
| Future Volume（vph） | 16 | 15 | 46 | 56 | 31 | 36 | 129 | 1004 | 33 | 24 | 668 | 28 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（ft） | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length（ft） | 0 |  | 0 | 0 |  | 0 | 100 |  | 100 | 60 |  | 60 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ ft ） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（ ft ） |  | 579 |  |  | 696 |  |  | 2249 |  |  | 626 |  |
| Travel Time（s） |  | 13.2 |  |  | 15.8 |  |  | 51.1 |  |  | 14.2 |  |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.75 | 0.75 | 0.75 | 0.90 | 0.90 | 0.90 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles（\％） | 0\％ | 0\％ | 0\％ | 0\％ | 0\％ | 4\％ | 0\％ | 2\％ | 0\％ | 0\％ | 2\％ | 0\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 0 | 92 | 0 | 0 | 164 | 0 | 143 | 1116 | 37 | 27 | 759 | 32 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split（s） | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split（\％） | 20．0\％ | 20．0\％ |  | 20．0\％ | 20．0\％ |  | 17．5\％ | 62．5\％ | 62．5\％ | 17．5\％ | 62．5\％ | 62．5\％ |
| Maximum Green（s） | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time（s） | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） |  | －2．0 |  |  | －2．0 |  | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |
| Total Lost Time（s） |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead／Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| v／c Ratio |  | 0.30 |  |  | 0.62 |  | 0.31 | 0.89 | 0.03 | 0.09 | 0.69 | 0.03 |
| Control Delay |  | 17.3 |  |  | 37.4 |  | 4.7 | 23.9 | 0.1 | 3.6 | 16.0 | 0.1 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 17.3 |  |  | 37.4 |  | 4.7 | 23.9 | 0.1 | 3.6 | 16.0 | 0.1 |
| Queue Length 50th（ ft ） |  | 14 |  |  | 56 |  | 15 | 272 | 0 | 3 | 245 | 0 |
| Queue Length 95th（ft） |  | 51 |  |  | 103 |  | 28 | \＃826 | 0 | 8 | 365 | 0 |
| Internal Link Dist（ft） |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |
| Turn Bay Length（ ft ） |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity（vph） |  | 321 |  |  | 278 |  | 476 | 1252 | 1126 | 341 | 1224 | 1103 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v／c Ratio |  | 0.29 |  |  | 0.59 |  | 0.30 | 0.89 | 0.03 | 0.08 | 0.62 | 0.03 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## 2020 Build Weekday Evening Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road
Area Type:
Other
Cycle Length: 80
Actuated Cycle Length: 73
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


## 2020 Build Weekday Evening Peak Hour

1：NH Route 125 （Calef Highway）\＆Greenhill Road／Tolend Road

|  | 4 | $\rightarrow$ | 7 | 7 |  |  | ＋ | $\dagger$ | 7 |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ＊ |  |  | $\uparrow$ |  | \％ | 中 | 「 | 7 | $\uparrow$ | 「 |
| Traffic Volume（Vph） | 16 | 15 | 46 | 56 | 31 | 36 | 129 | 1004 | 33 | 24 | 668 | 28 |
| Future Volume（vph） | 16 | 15 | 46 | 56 | 31 | 36 | 129 | 1004 | 33 | 24 | 668 | 28 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time（s） |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util．Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.92 |  |  | 0.96 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| FIt Protected |  | 0.99 |  |  | 0.98 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） |  | 1844 |  |  | 1881 |  | 1805 | 1863 | 1615 | 1805 | 1863 | 1615 |
| Flt Permitted |  | 0.90 |  |  | 0.82 |  | 0.21 | 1.00 | 1.00 | 0.09 | 1.00 | 1.00 |
| Satd．Flow（perm） |  | 1670 |  |  | 1573 |  | 390 | 1863 | 1615 | 167 | 1863 | 1615 |
| Peak－hour factor，PHF | 0.84 | 0.84 | 0.84 | 0.75 | 0.75 | 0.75 | 0.90 | 0.90 | 0.90 | 0.88 | 0.88 | 0.88 |
| Adj．Flow（vph） | 19 | 18 | 55 | 75 | 41 | 48 | 143 | 1116 | 37 | 27 | 759 | 32 |
| RTOR Reduction（vph） | 0 | 47 | 0 | 0 | 19 | 0 | 0 | － | 13 | 0 | 0 | 13 |
| Lane Group Flow（vph） | 0 | 45 | 0 | 0 | 145 | 0 | 143 | 1116 | 24 | 27 | 759 | 19 |
| Heavy Vehicles（\％） | 0\％ | 0\％ | 0\％ | 0\％ | 0\％ | 4\％ | 0\％ | 2\％ | 0\％ | 0\％ | 2\％ | 0\％ |
| Turn Type | Perm | NA |  | Perm | NA |  | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green，G（s） |  | 9.4 |  |  | 9.4 |  | 53.0 | 47.1 | 47.1 | 45.8 | 43.5 | 43.5 |
| Effective Green， g （s） |  | 11.4 |  |  | 11.4 |  | 57.0 | 49.1 | 49.1 | 49.8 | 45.5 | 45.5 |
| Actuated g／C Ratio |  | 0.15 |  |  | 0.15 |  | 0.74 | 0.64 | 0.64 | 0.65 | 0.59 | 0.59 |
| Clearance Time（s） |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension（s） |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） |  | 247 |  |  | 233 |  | 435 | 1191 | 1032 | 200 | 1103 | 956 |
| v／s Ratio Prot |  |  |  |  |  |  | c0．03 | c0．60 |  | 0.01 | 0.41 |  |
| v／s Ratio Perm |  | 0.03 |  |  | c0．09 |  | 0.21 |  | 0.01 | 0.08 |  | 0.01 |
| v／c Ratio |  | 0.18 |  |  | 0.62 |  | 0.33 | 0.94 | 0.02 | 0.14 | 0.69 | 0.02 |
| Uniform Delay，d1 |  | 28.6 |  |  | 30.7 |  | 6.9 | 12.5 | 5.1 | 14.3 | 10.8 | 6.5 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 |  | 0.4 |  |  | 5.1 |  | 0.4 | 13.5 | 0.0 | 0.3 | 1.8 | 0.0 |
| Delay（s） |  | 29.0 |  |  | 35.8 |  | 7.3 | 26.0 | 5.1 | 14.6 | 12.6 | 6.5 |
| Level of Service |  | C |  |  | D |  | A | C | A | B | B | A |
| Approach Delay（s） |  | 29.0 |  |  | 35.8 |  |  | 23.3 |  |  | 12.4 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 20.6 |  | HCM 2000 | evel of S | Service |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.85 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 76.8 |  | Sum of lost | time（s） |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 80．6\％ |  | ICU Level of | Service |  |  | D |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

## 2020 Build Saturday MIdday Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | 7 | 1 | $4$ | 4 | $4$ | 4 | \% | $1$ | $\pm$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | $\ddagger$ |  | 7 | 中 | T | 4 | 4 | 「 |
| Traffic Volume (vph) | 12 | 13 | 82 | 39 | 11 | 35 | 73 | 641 | 30 | 20 | 705 | 17 |
| Future Volume (vph) | 12 | 13 | 82 | 39 | 11 | 35 | 73 | 641 | 30 | 20 | 705 | 17 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length ( ft ) | 0 |  | 0 | 0 |  | 0 | 100 |  | 100 | 60 |  | 60 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( ft ) |  | 579 |  |  | 696 |  |  | 2249 |  |  | 626 |  |
| Travel Time (s) |  | 13.2 |  |  | 15.8 |  |  | 51.1 |  |  | 14.2 |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.87 | 0.87 | 0.87 | 0.89 | 0.89 | 0.89 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 122 | 0 | 0 | 98 | 0 | 82 | 720 | 34 | 25 | 881 | 21 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split ( s ) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% |  | 20.0\% | 20.0\% |  | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| v/c Ratio |  | 0.34 |  |  | 0.39 |  | 0.19 | 0.51 | 0.03 | 0.04 | 0.72 | 0.02 |
| Control Delay |  | 14.2 |  |  | 25.5 |  | 3.6 | 8.8 | 0.0 | 2.9 | 16.6 | 0.1 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 14.2 |  |  | 25.5 |  | 3.6 | 8.8 | 0.0 | 2.9 | 16.6 | 0.1 |
| Queue Length 50th ( ft ) |  | 12 |  |  | 27 |  | 8 | 103 | 0 | 2 | 308 | 0 |
| Queue Length 95th (t) |  | 56 |  |  | 69 |  | 17 | 315 | 0 | 6 | 382 | 0 |
| Internal Link Dist (ft) |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |
| Turn Bay Length ( ft ) |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 423 |  |  | 308 |  | 476 | 1402 | 1224 | 641 | 1306 | 1159 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.29 |  |  | 0.32 |  | 0.17 | 0.51 | 0.03 | 0.04 | 0.67 | 0.02 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Lanes, Volumes, Timings
AJA

Area Type:
Other
Cycle Length: 80
Actuated Cycle Length: 66.6
Natural Cycle: 60
Control Type: Actuated-Uncoordinated
Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


## 2020 Build Saturday MIdday Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | 7 |  | $\leftarrow$ |  | 4 | $\dagger$ | P |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  |  | $\uparrow$ |  | \% | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 12 | 13 | 82 | 39 | 11 | 35 | 73 | 641 | 30 | 20 | 705 | 17 |
| Future Volume (vph) | 12 | 13 | 82 | 39 | 11 | 35 | 73 | 641 | 30 | 20 | 705 | 17 |
| Ideal Flow (Vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Widh | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.90 |  |  | 0.94 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Fit Protected |  | 0.99 |  |  | 0.98 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1808 |  |  | 1872 |  | 1805 | 1900 | 1615 | 1805 | 1881 | 1615 |
| Flt Permitted |  | 0.95 |  |  | 0.72 |  | 0.15 | 1.00 | 1.00 | 0.31 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1734 |  |  | 1385 |  | 291 | 1900 | 1615 | 593 | 1881 | 1615 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.87 | 0.87 | 0.87 | 0.89 | 0.89 | 0.89 | 0.80 | 0.80 | 0.80 |
| Adj. Flow (vph) | 14 | 15 | 93 | 45 | 13 | 40 | 82 | 720 | 34 | 25 | 881 | 21 |
| RTOR Reduction (vph) | 0 | 82 | 0 | 0 | 33 | 0 | 0 | 0 | 12 | 0 | 0 | 8 |
| Lane Group Flow (vph) | 0 | 40 | 0 | 0 | 65 | 0 | 82 | 720 | 22 | 25 | 881 | 13 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | , |  | 1 | - |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 6.3 |  |  | 6.3 |  | 50.6 | 45.3 | 45.3 | 44.0 | 42.0 | 42.0 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 8.3 |  |  | 8.3 |  | 54.6 | 47.3 | 47.3 | 48.0 | 44.0 | 44.0 |
| Actuated g/C Ratio |  | 0.12 |  |  | 0.12 |  | 0.76 | 0.66 | 0.66 | 0.67 | 0.61 | 0.61 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 201 |  |  | 160 |  | 376 | 1255 | 1066 | 465 | 1155 | 992 |
| v/s Ratio Prot |  |  |  |  |  |  | c0.02 | c0.38 |  | 0.00 | c0.47 |  |
| v/s Ratio Perm |  | 0.02 |  |  | c0.05 |  | 0.14 |  | 0.01 | 0.03 |  | 0.01 |
| v/c Ratio |  | 0.20 |  |  | 0.41 |  | 0.22 | 0.57 | 0.02 | 0.05 | 0.76 | 0.01 |
| Uniform Delay, d1 |  | 28.6 |  |  | 29.4 |  | 7.4 | 6.6 | 4.2 | 4.5 | 10.0 | 5.4 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.5 |  |  | 1.7 |  | 0.3 | 0.6 | 0.0 | 0.0 | 3.0 | 0.0 |
| Delay (s) |  | 29.1 |  |  | 31.1 |  | 7.7 | 7.3 | 4.2 | 4.6 | 13.1 | 5.4 |
| Level of Service |  | C |  |  | C |  | A | A | A | A | B | A |
| Approach Delay (s) |  | 29.1 |  |  | 31.1 |  |  | 7.2 |  |  | 12.7 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 12.3 |  | HCM 2000 | evel of S | Service |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.65 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 71.6 |  | Sum of lost | me (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 62.8\% |  | ICU Level o | Service |  |  | B |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group


## Area Type: <br> Other

Cycle Length: 80
Actuated Cycle Length: 70.5
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


## 2030 No Build Weekday Morning Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | 7 | 7 | $\checkmark$ |  | 4 | $\dagger$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\$$ |  |  | $\$$ |  | \% | $\uparrow$ | 「 | 7 | 4 | 「 |
| Traffic Volume (Vph) | 21 | 48 | 146 | 28 | 9 | 17 | 22 | 643 | 31 | 19 | 1095 | 6 |
| Future Volume (vph) | 21 | 48 | 146 | 28 | 9 | 17 | 22 | 643 | 31 | 19 | 1095 | 6 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.91 |  |  | 0.96 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 1.00 |  |  | 0.97 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1807 |  |  | 1838 |  | 1687 | 1810 | 1302 | 1805 | 1792 | 1615 |
| Fit Permitted |  | 0.96 |  |  | 0.42 |  | 0.08 | 1.00 | 1.00 | 0.29 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1748 |  |  | 800 |  | 150 | 1810 | 1302 | 556 | 1792 | 1615 |
| Peak-hour factor, PHF | 0.87 | 0.87 | 0.87 | 0.82 | 0.82 | 0.82 | 0.93 | 0.93 | 0.93 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 24 | 55 | 168 | 34 | 11 | 21 | 24 | 691 | 33 | 20 | 1165 | 6 |
| RTOR Reduction (vph) | 0 | 96 | 0 | 0 | 18 | 0 | 0 | 0 | 12 | 0 | 0 | 2 |
| Lane Group Flow (vph) | 0 | 151 | 0 | 0 | 48 | 0 | 24 | 691 | 21 | 20 | 1165 | 4 |
| Heavy Vehicles (\%) | 0\% | 0\% | 2\% | 0\% | 0\% | 9\% | 7\% | 5\% | 24\% | 0\% | 6\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pmpt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | , |
| Actuated Green, G (s) |  | 8.9 |  |  | 8.9 |  | 47.4 | 45.2 | 45.2 | 47.4 | 45.2 | 45.2 |
| Effective Green, g (s) |  | 10.9 |  |  | 10.9 |  | 51.4 | 47.2 | 47.2 | 51.4 | 47.2 | 47.2 |
| Actuated g/C Ratio |  | 0.15 |  |  | 0.15 |  | 0.69 | 0.64 | 0.64 | 0.69 | 0.64 | 0.64 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 256 |  |  | 117 |  | 190 | 1149 | 827 | 455 | 1138 | 1025 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  | c0.01 | 0.38 |  | 0.00 | c0.65 |  |
| v/s Ratio Perm |  | c0.09 |  |  | 0.06 |  | 0.08 |  | 0.02 | 0.03 |  | 0.00 |
| v/c Ratio |  | 0.59 |  |  | 0.41 |  | 0.13 | 0.60 | 0.03 | 0.04 | 1.02 | 0.00 |
| Uniform Delay, d1 |  | 29.6 |  |  | 28.8 |  | 16.3 | 8.0 | 5.0 | 4.7 | 13.5 | 5.0 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 3.4 |  |  | 2.3 |  | 0.3 | 0.9 | 0.0 | 0.0 | 32.9 | 0.0 |
| Delay (s) |  | 33.0 |  |  | 31.1 |  | 16.6 | 8.9 | 5.0 | 4.8 | 46.4 | 5.0 |
| Level of Service |  | C |  |  | C |  | B | A | A | A | D | A |
| Approach Delay (s) |  | 33.0 |  |  | 31.1 |  |  | 9.0 |  |  | 45.5 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 31.6 |  | HCM 2000 | evel of S | Service |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.89 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 74.3 |  | Sum of lost | ime (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 77.0\% |  | ICU Level of | Service |  |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis
AJA

## 2030 No Build Weekday Evening Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | 7 | $\bigcirc$ | $4$ | 4 |  | 4 | 7 | , | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | $\ddagger$ |  | ${ }^{7}$ | 4 | 「 | 1 | 中 | \% |
| Traffic Volume (vph) | 18 | 17 | 47 | 56 | 35 | 40 | 134 | 1049 | 31 | 27 | 725 | 31 |
| Future Volume (vph) | 18 | 17 | 47 | 56 | 35 | 40 | 134 | 1049 | 31 | 27 | 725 | 31 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width ( ft ) | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 100 |  | 100 | 60 |  | 60 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( t ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 579 |  |  | 696 |  |  | 2249 |  |  | 626 |  |
| Travel Time (s) |  | 13.2 |  |  | 15.8 |  |  | 51.1 |  |  | 14.2 |  |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.75 | 0.75 | 0.75 | 0.90 | 0.90 | 0.90 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 4\% | 0\% | 2\% | 0\% | 0\% | 2\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 97 | 0 | 0 | 175 | 0 | 149 | 1166 | 34 | 31 | 824 | 35 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% |  | 20.0\% | 20.0\% |  | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| v/c Ratio |  | 0.32 |  |  | 0.65 |  | 0.37 | 0.94 | 0.03 | 0.11 | 0.81 | 0.04 |
| Control Delay |  | 18.4 |  |  | 39.6 |  | 5.7 | 28.9 | 0.1 | 3.7 | 21.0 | 0.1 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 18.4 |  |  | 39.6 |  | 5.7 | 28.9 | 0.1 | 3.7 | 21.0 | 0.1 |
| Queue Length 50th ( ft ) |  | 16 |  |  | 66 |  | 16 | 304 | 0 | 3 | 288 | 0 |
| Queue Length 95th (ft) |  | 54 |  |  | 110 |  | 29 | \#882 | 0 | 8 | 424 | 0 |
| Internal Link Dist (ft) |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |
| Turn Bay Length ( t ) |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 319 |  |  | 280 |  | 414 | 1247 | 1122 | 346 | 1189 | 1075 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.30 |  |  | 0.63 |  | 0.36 | 0.94 | 0.03 | 0.09 | 0.69 | 0.03 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 80
Actuated Cycle Length: 72.7
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


## 2030 No Build Weekday Evening Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | 7 | 1 |  |  | 4 | 4 | 1 | 4 | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\$$ |  |  | $\uparrow$ |  | 午 | $\uparrow$ | 7 | \% | $\uparrow$ | F |
| Traffic Volume (vph) | 18 | 17 | 47 | 56 | 35 | 40 | 134 | 1049 | 31 | 27 | 725 | 31 |
| Future Volume (vph) | 18 | 17 | 47 | 56 | 35 | 40 | 134 | 1049 | 31 | 27 | 725 | 31 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.92 |  |  | 0.96 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 0.99 |  |  | 0.98 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1849 |  |  | 1880 |  | 1805 | 1863 | 1615 | 1805 | 1863 | 1615 |
| Flt Permitted |  | 0.88 |  |  | 0.82 |  | 0.15 | 1.00 | 1.00 | 0.09 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1641 |  |  | 1572 |  | 283 | 1863 | 1615 | 174 | 1863 | 1615 |
| Peak-hour factor, PHF | 0.84 | 0.84 | 0.84 | 0.75 | 0.75 | 0.75 | 0.90 | 0.90 | 0.90 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph) | 21 | 20 | 56 | 75 | 47 | 53 | 149 | 1166 | 34 | 31 | 824 | 35 |
| RTOR Reduction (vph) | 0 | 48 | 0 | 0 | 20 | 0 | 0 | 0 | 12 | 0 | 0 | 15 |
| Lane Group Flow (vph) | 0 | 49 | 0 | 0 | 155 | 0 | 149 | 1166 | 22 | 31 | 824 | 20 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 4\% | 0\% | 2\% | 0\% | 0\% | 2\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 9.5 |  |  | 9.5 |  | 54.0 | 46.7 | 46.7 | 44.0 | 41.7 | 41.7 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 11.5 |  |  | 11.5 |  | 57.0 | 48.7 | 48.7 | 48.0 | 43.7 | 43.7 |
| Actuated g/C Ratio |  | 0.15 |  |  | 0.15 |  | 0.75 | 0.64 | 0.64 | 0.63 | 0.57 | 0.57 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 246 |  |  | 236 |  | 395 | 1185 | 1028 | 200 | 1064 | 922 |
| v/s Ratio Prot |  |  |  |  |  |  | c0.05 | c0.63 |  | 0.01 | 0.44 |  |
| v/s Ratio Perm |  | 0.03 |  |  | c0.10 |  | 0.23 |  | 0.01 | 0.09 |  | 0.01 |
| v/c Ratio |  | 0.20 |  |  | 0.66 |  | 0.38 | 0.98 | 0.02 | 0.15 | 0.77 | 0.02 |
| Uniform Delay, d1 |  | 28.5 |  |  | 30.6 |  | 9.1 | 13.5 | 5.1 | 15.9 | 12.6 | 7.1 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.4 |  |  | 6.5 |  | 0.6 | 22.2 | 0.0 | 0.4 | 3.6 | 0.0 |
| Delay (s) |  | 28.9 |  |  | 37.1 |  | 9.7 | 35.7 | 5.1 | 16.2 | 16.2 | 7.1 |
| Level of Service |  | C |  |  | D |  | A | D | A | B | B | A |
| Approach Delay (s) |  | 28.9 |  |  | 37.1 |  |  | 32.0 |  |  | 15.8 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 26.5 |  | HCM 2000 | Level of S | Service |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.89 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 76.5 |  | Sum of lost | time (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 82.9\% |  | CU Level of | Service |  |  | E |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

## 2030 No Build Saturday Midday Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ |  | 1 | $4$ | 4 |  | $\dagger$ | $\neq$ | $y$ | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | \$ |  | 7 | + | 「 | 1 | 4 | 「 |
| Traffic Volume (vph) | 13 | 14 | 87 | 37 | 12 | 39 | 77 | 679 | 28 | 22 | 747 | 19 |
| Future Volume (vph) | 13 | 14 | 87 | 37 | 12 | 39 | 77 | 679 | 28 | 22 | 747 | 19 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width ( ft ) | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 100 |  | 100 | 60 |  | 60 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( f ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 579 |  |  | 696 |  |  | 2249 |  |  | 626 |  |
| Travel Time (s) |  | 13.2 |  |  | 15.8 |  |  | 51.1 |  |  | 14.2 |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.87 | 0.87 | 0.87 | 0.89 | 0.89 | 0.89 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 130 | 0 | 0 | 102 | 0 | 87 | 763 | 31 | 28 | 934 | 24 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% |  | 20.0\% | 20.0\% |  | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| v/c Ratio |  | 0.37 |  |  | 0.42 |  | 0.21 | 0.54 | 0.03 | 0.05 | 0.75 | 0.02 |
| Control Delay |  | 14.5 |  |  | 26.0 |  | 3.8 | 9.3 | 0.0 | 2.9 | 18.2 | 0.1 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 14.5 |  |  | 26.0 |  | 3.8 | 9.3 | 0.0 | 2.9 | 18.2 | 0.1 |
| Queue Length 50th ( ft ) |  | 14 |  |  | 27 |  | 8 | 113 | 0 | 3 | 345 | 0 |
| Queue Length 95th ( ft ) |  | 59 |  |  | 70 |  | 18 | 348 | 0 | 7 | 431 | 0 |
| Internal Link Dist (ft) |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |
| Turn Bay Length ( t ) |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 412 |  |  | 291 |  | 441 | 1410 | 1230 | 609 | 1284 | 1141 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.32 |  |  | 0.35 |  | 0.20 | 0.54 | 0.03 | 0.05 | 0.73 | 0.02 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Lanes, Volumes, Timings
AJA
S: \Jobs\8188VAnalysis 18188 -2030SMNB.syn

Area Type:
Other
Cycle Length: 80
Actuated Cycle Length: 68.4
Natural Cycle: 60
Control Type: Actuated-Uncoordinated
Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


|  | 4 | $\rightarrow$ | 7 | 7 | $\leftarrow$ | 4 | 4 | $\uparrow$ | + | \% | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\$$ |  |  | $\oplus$ |  | \% | 4 | 7 | ${ }^{*}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 13 | 14 | 87 | 37 | 12 | 39 | 77 | 679 | 28 | 22 | 747 | 19 |
| Future Volume (vph) | 13 | 14 | 87 | 37 | 12 | 39 | 77 | 679 | 28 | 22 | 747 | 19 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.90 |  |  | 0.94 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 0.99 |  |  | 0.98 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1808 |  |  | 1867 |  | 1805 | 1900 | 1615 | 1805 | 1881 | 1615 |
| Flt Permitted |  | 0.95 |  |  | 0.70 |  | 0.13 | 1.00 | 1.00 | 0.29 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1723 |  |  | 1336 |  | 246 | 1900 | 1615 | 548 | 1881 | 1615 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.87 | 0.87 | 0.87 | 0.89 | 0.89 | 0.89 | 0.80 | 0.80 | 0.80 |
| Adj. Flow (vph) | 15 | 16 | 99 | 43 | 14 | 45 | 87 | 763 | 31 | 28 | 934 | 24 |
| RTOR Reduction (vph) | 0 | 88 | 0 | 0 | 37 | 0 | 0 | 0 | 10 | 0 | 0 | 9 |
| Lane Group Flow (vph) | 0 | 42 | 0 | 0 | 65 | 0 | 87 | 763 | 21 | 28 | 934 | 15 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | , |  | 1 | - |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 6.3 |  |  | 6.3 |  | 52.4 | 47.0 | 47.0 | 45.8 | 43.7 | 43.7 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 8.3 |  |  | 8.3 |  | 56.4 | 49.0 | 49.0 | 49.8 | 45.7 | 45.7 |
| Actuated g/C Ratio |  | 0.11 |  |  | 0.11 |  | 0.77 | 0.67 | 0.67 | 0.68 | 0.62 | 0.62 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 194 |  |  | 151 |  | 346 | 1268 | 1078 | 442 | 1171 | 1005 |
| v/s Ratio Prot |  |  |  |  |  |  | c0.03 | c0.40 |  | 0.00 | c0.50 |  |
| v/s Ratio Perm |  | 0.02 |  |  | c0.05 |  | 0.17 |  | 0.01 | 0.04 |  | 0.01 |
| v/c Ratio |  | 0.22 |  |  | 0.43 |  | 0.25 | 0.60 | 0.02 | 0.06 | 0.80 | 0.01 |
| Uniform Delay, d1 |  | 29.6 |  |  | 30.3 |  | 8.8 | 6.8 | 4.1 | 4.7 | 10.4 | 5.3 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.6 |  |  | 2.0 |  | 0.4 | 0.8 | 0.0 | 0.1 | 3.9 | 0.0 |
| Delay (s) |  | 30.2 |  |  | 32.3 |  | 9.2 | 7.6 | 4.1 | 4.7 | 14.3 | 5.3 |
| Level of Service |  | C |  |  | C |  | A | A | A | A | B | A |
| Approach Delay (s) |  | 30.2 |  |  | 32.3 |  |  | 7.6 |  |  | 13.8 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 13.1 |  | HCM 2000 | Level of S | Service |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratioActuated Cycle Length (s) |  |  | 0.68 |  |  |  |  |  |  |  |  |  |
|  |  |  | 73.4 |  | Sum of lost | time (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 65.3\% |  | CU Level of | Service |  |  | C |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

## 2030 Build Weekday Morning Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 |  | 7 | 7 |  | 4 | 4 | $\dagger$ | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | \$ |  | \% | 4 | 「 | 7 | 4 | 「 |
| Traffic Volume (vph) | 21 | 48 | 153 | 32 | , | 17 | 24 | 664 | 37 | 19 | 1145 | 6 |
| Future Volume (vph) | 21 | 48 | 153 | 32 | 9 | 17 | 24 | 664 | 37 | 19 | 1145 | 6 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.907 |  |  | 0.960 |  |  |  | 0.850 |  |  | 0.850 |
| Flt Protected |  | 0.995 |  |  | 0.973 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1804 | 0 | 0 | 1844 | 0 | 1687 | 1810 | 1302 | 1805 | 1792 | 1615 |
| Flt Permitted |  | 0.966 |  |  | 0.371 |  | 0.085 |  |  | 0.278 |  |  |
| Satd. Flow (perm) | 0 | 1752 | 0 | 0 | 703 | 0 | 151 | 1810 | 1302 | 528 | 1792 | 1615 |
| Satd. Flow (RTOR) |  | 118 |  |  | 21 |  |  |  | 123 |  |  | 123 |
| Adj. Flow (vph) | 24 | 55 | 176 | 39 | 11 | 21 | 26 | 714 | 40 | 20 | 1218 | 6 |
| Lane Group Flow (vph) | 0 | 255 | 0 | 0 | 71 | 0 | 26 | 714 | 40 | 20 | 1218 | 6 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | , |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% |  | 20.0\% | 20.0\% |  | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| v/c Ratio |  | 0.69 |  |  | 0.56 |  | 0.09 | 0.59 | 0.04 | 0.04 | 1.02 | 0.01 |
| Control Delay |  | 26.6 |  |  | 41.2 |  | 3.5 | 10.6 | 0.1 | 2.9 | 47.5 | 0.0 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 26.6 |  |  | 41.2 |  | 3.5 | 10.6 | 0.1 | 2.9 | 47.5 | 0.0 |
| Queue Length 50th (tt) |  | 50 |  |  | 18 |  | 3 | 115 | 0 | 2 | 371 | 0 |
| Queue Length 95th (tt) |  | \#138 |  |  | \#65 |  | 8 | 333 | 0 | 6 | \#950 | 0 |
| Internal Link Dist (ft) |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 398 |  |  | 138 |  | 328 | 1209 | 910 | 562 | 1195 | 1118 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.64 |  |  | 0.51 |  | 0.08 | 0.59 | 0.04 | 0.04 | 1.02 | 0.01 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Intersection Summary
Cycle Length: 80
Actuated Cycle Length: 70.4
Natural Cycle: 90
Control Type: Actuated-Uncoordinated

Lanes, Volumes, Timings
AJA
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


## 2030 Build Weekday Morning Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | 7 | 7 |  |  | 4 | 4 | 1 | - | $\frac{1}{*}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\pm$ |  |  | \$ |  | 7 | $\uparrow$ | 「 | 7 | $\uparrow$ | 「 |
| Traffic Volume (vph) | 21 | 48 | 153 | 32 | 9 | 17 | 24 | 664 | 37 | 19 | 1145 | 6 |
| Future Volume (vph) | 21 | 48 | 153 | 32 | 9 | 17 | 24 | 664 | 37 | 19 | 1145 | 6 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.91 |  |  | 0.96 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 1.00 |  |  | 0.97 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1804 |  |  | 1845 |  | 1687 | 1810 | 1302 | 1805 | 1792 | 1615 |
| Flt Permitted |  | 0.97 |  |  | 0.37 |  | 0.09 | 1.00 | 1.00 | 0.28 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1751 |  |  | 702 |  | 151 | 1810 | 1302 | 528 | 1792 | 1615 |
| Peak-hour factor, PHF | 0.87 | 0.87 | 0.87 | 0.82 | 0.82 | 0.82 | 0.93 | 0.93 | 0.93 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 24 | 55 | 176 | 39 | 11 | 21 | 26 | 714 | 40 | 20 | 1218 | 6 |
| RTOR Reduction (vph) | 0 | 101 | 0 | 0 | 18 | 0 | 0 | 0 | 15 | , | 0 | 2 |
| Lane Group Flow (vph) | 0 | 154 | 0 | 0 | 53 | 0 | 26 | 714 | 25 | 20 | 1218 | 4 |
| Heavy Vehicles (\%) | 0\% | 0\% | 2\% | 0\% | 0\% | 9\% | 7\% | 5\% | 24\% | 0\% | 6\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 8.9 |  |  | 8.9 |  | 47.2 | 45.0 | 45.0 | 47.2 | 45.0 | 45.0 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 10.9 |  |  | 10.9 |  | 51.2 | 47.0 | 47.0 | 51.2 | 47.0 | 47.0 |
| Actuated g/C Ratio |  | 0.15 |  |  | 0.15 |  | 0.69 | 0.63 | 0.63 | 0.69 | 0.63 | 0.63 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 257 |  |  | 103 |  | 191 | 1148 | 825 | 437 | 1136 | 1024 |
| v/s Ratio Prot |  |  |  |  |  |  | c0.01 | 0.39 |  | 0.00 | c0.68 |  |
| v/s Ratio Perm |  | c0.09 |  |  | 0.08 |  | 0.09 |  | 0.02 | 0.03 |  | 0.00 |
| v/c Ratio |  | 0.60 |  |  | 0.52 |  | 0.14 | 0.62 | 0.03 | 0.05 | 1.07 | 0.00 |
| Uniform Delay, d1 |  | 29.6 |  |  | 29.2 |  | 16.3 | 8.2 | 5.1 | 4.9 | 13.5 | 5.0 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 3.9 |  |  | 4.3 |  | 0.3 | 1.1 | 0.0 | 0.0 | 48.3 | 0.0 |
| Delay (s) |  | 33.5 |  |  | 33.5 |  | 16.6 | 9.2 | 5.1 | 4.9 | 61.9 | 5.0 |
| Level of Service |  | C |  |  | C |  | B | A | A | A | E | A |
| Approach Delay (s) |  | 33.5 |  |  | 33.5 |  |  | 9.3 |  |  | 60.7 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 39.8 |  | HCM 2000 | Level of | Service |  | D |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.93 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 74.1 |  | Sum of los | time (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 80.0\% |  | CU Level | Service |  |  | D |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) <br> c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

## 2030 Build Weekday Evening Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | + | 4 | 4 | 4 | $4$ | $\dagger$ | \% | $1$ | $\frac{1}{\square}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | \$ |  | ${ }^{7}$ | $\uparrow$ | 「 | ${ }^{7}$ | 4 | F |
| Traffic Volume (vph) | 18 | 17 | 51 | 62 | 35 | 40 | 142 | 1103 | 36 | 27 | 756 | 31 |
| Future Volume (vph) | 18 | 17 | 51 | 62 | 35 | 40 | 142 | 1103 | 36 | 27 | 756 | 31 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width ( ft ) | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Storage Length ( ft ) | 0 |  | 0 | 0 |  | 0 | 100 |  | 100 | 60 |  | 60 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( ft ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( ft ) |  | 579 |  |  | 696 |  |  | 2249 |  |  | 626 |  |
| Travel Time (s) |  | 13.2 |  |  | 15.8 |  |  | 51.1 |  |  | 14.2 |  |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.75 | 0.75 | 0.75 | 0.90 | 0.90 | 0.90 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 4\% | 0\% | 2\% | 0\% | 0\% | 2\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 102 | 0 | 0 | 183 | 0 | 158 | 1226 | 40 | 31 | 859 | 35 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial ( $s$ ) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% |  | 20.0\% | 20.0\% |  | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| v/c Ratio |  | 0.33 |  |  | 0.71 |  | 0.42 | 0.98 | 0.04 | 0.11 | 0.83 | 0.04 |
| Control Delay |  | 18.2 |  |  | 44.6 |  | 7.6 | 36.3 | 0.1 | 3.7 | 22.6 | 0.1 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 18.2 |  |  | 44.6 |  | 7.6 | 36.3 | 0.1 | 3.7 | 22.6 | 0.1 |
| Queue Length 50th (ft) |  | 18 |  |  | 76 |  | 17 | 350 | 0 | 3 | 310 | 0 |
| Queue Length 95th (f) |  | 55 |  |  | \#116 |  | 42 | \#947 | 0 | 8 | 458 | 0 |
| Internal Link Dist (ft) |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |
| Turn Bay Length (f) |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 318 |  |  | 267 |  | 392 | 1254 | 1128 | 338 | 1164 | 1055 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.32 |  |  | 0.69 |  | 0.40 | 0.98 | 0.04 | 0.09 | 0.74 | 0.03 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## 2030 Build Weekday Evening Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


## 2030 Build Weekday Evening Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | $\rangle$ | $\rightarrow$ |  | 7 |  |  | 4 | $\dagger$ | 7 | * | $\frac{1}{*}$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  |  | $\ddagger$ |  | ${ }^{4}$ | $\uparrow$ | F | ${ }^{*}$ | * | F |
| Traffic Volume (vph) | 18 | 17 | 51 | 62 | 35 | 40 | 142 | 1103 | 36 | 27 | 756 | 31 |
| Future Volume (vph) | 18 | 17 | 51 | 62 | 35 | 40 | 142 | 1103 | 36 | 27 | 756 | 31 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Utill. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.92 |  |  | 0.96 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 0.99 |  |  | 0.98 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1844 |  |  | 1882 |  | 1805 | 1863 | 1615 | 1805 | 1863 | 1615 |
| Flt Permitted |  | 0.88 |  |  | 0.79 |  | 0.13 | 1.00 | 1.00 | 0.09 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1640 |  |  | 1530 |  | 251 | 1863 | 1615 | 169 | 1863 | 1615 |
| Peak-hour factor, PHF | 0.84 | 0.84 | 0.84 | 0.75 | 0.75 | 0.75 | 0.90 | 0.90 | 0.90 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph) | 21 | 20 | 61 | 83 | 47 | 53 | 158 | 1226 | 40 | 31 | 859 | 35 |
| RTOR Reduction (vph) | 0 | 52 | 0 | 0 | 19 | 0 | 0 | 0 | 14 | 0 | 0 | 15 |
| Lane Group Flow (vph) | 0 | 50 | 0 | 0 | 164 | 0 | 158 | 1226 | 26 | 31 | 859 | 20 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 4\% | 0\% | 2\% | 0\% | 0\% | 2\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 9.6 |  |  | 9.6 |  | 55.4 | 48.0 | 48.0 | 45.2 | 42.9 | 42.9 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 11.6 |  |  | 11.6 |  | 58.3 | 50.0 | 50.0 | 49.2 | 44.9 | 44.9 |
| Actuated g/C Ratio |  | 0.15 |  |  | 0.15 |  | 0.75 | 0.64 | 0.64 | 0.63 | 0.58 | 0.58 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 244 |  |  | 227 |  | 375 | 1195 | 1036 | 197 | 1073 | 930 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  | c0.05 | c0.66 |  | 0.01 | 0.46 |  |
| v/s Ratio Perm |  | 0.03 |  |  | c0.11 |  | 0.26 |  | 0.02 | 0.09 |  | 0.01 |
| v/c Ratio |  | 0.21 |  |  | 0.72 |  | 0.42 | 1.03 | 0.02 | 0.16 | 0.80 | 0.02 |
| Uniform Delay, d1 |  | 29.1 |  |  | 31.6 |  | 10.4 | 14.0 | 5.1 | 16.3 | 13.0 | 7.1 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.4 |  |  | 10.8 |  | 0.8 | 32.8 | 0.0 | 0.4 | 4.4 | 0.0 |
| Delay (s) |  | 29.5 |  |  | 42.5 |  | 11.2 | 46.8 | 5.1 | 16.7 | 17.3 | 7.1 |
| Level of Service |  | C |  |  | D |  | B | D | A | B | B | A |
| Approach Delay (s) |  | 29.5 |  |  | 42.5 |  |  | 41.7 |  |  | 16.9 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | , |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 32.6 |  | HCM 2000 | Level of S | Service |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratioActuated Cycle Length (s) |  |  | 0.94 |  |  |  |  |  |  |  |  |  |
|  |  |  | 77.9 |  | Sum of lost | time (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 86.6\% |  | CU Level of | Service |  |  | E |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

## 2030 Build Saturday MIdday Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | \% | 4 | 4 | 4 | 4 | 4 | $p$ | 4 | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * 9 |  |  | * |  | ${ }^{7}$ | 4 | 「 | 7 | 4 | T |
| Traffic Volume (vph) | 13 | 14 | 90 | 43 | 12 | 39 | 80 | 705 | 33 | 22 | 775 | 19 |
| Future Volume (vph) | 13 | 14 | 90 | 43 | 12 | 39 | 80 | 705 | 33 | 22 | 775 | 19 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.896 |  |  | 0.944 |  |  |  | 0.850 |  |  | 0.850 |
| Flt Protected |  | 0.994 |  |  | 0.978 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1805 | 0 | 0 | 1871 | 0 | 1805 | 1900 | 1615 | 1805 | 1881 | 1615 |
| Flt Permitted |  | 0.947 |  |  | 0.670 |  | 0.113 |  |  | 0.270 |  |  |
| Satd. Flow (perm) | 0 | 1720 | 0 | 0 | 1282 | 0 | 215 | 1900 | 1615 | 513 | 1881 | 1615 |
| Satd. Flow (RTOR) |  | 102 |  |  | 38 |  |  |  | 123 |  |  | 123 |
| Adj. Flow (vph) | 15 | 16 | 102 | 49 | 14 | 45 | 90 | 792 | 37 | 28 | 969 | 24 |
| Lane Group Flow (vph) | 0 | 133 | 0 | 0 | 108 | 0 | 90 | 792 | 37 | 28 | 969 | 24 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 16.0 | 16.0 | 11.0 | 16.0 | 16.0 |
| Total Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 14.0 | 50.0 | 50.0 | 14.0 | 50.0 | 50.0 |
| Total Split (\%) | 20.0\% | 20.0\% |  | 20.0\% | 20.0\% |  | 17.5\% | 62.5\% | 62.5\% | 17.5\% | 62.5\% | 62.5\% |
| Maximum Green (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 8.0 | 44.0 | 44.0 | 8.0 | 44.0 | 44.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | -2.0 |  |  | -2.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Min | Min | None | Min | Min |
| v/c Ratio |  | 0.38 |  |  | 0.47 |  | 0.23 | 0.56 | 0.03 | 0.05 | 0.78 | 0.02 |
| Control Delay |  | 14.4 |  |  | 29.2 |  | 4.1 | 9.7 | 0.0 | 3.0 | 19.4 | 0.1 |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 14.4 |  |  | 29.2 |  | 4.1 | 9.7 | 0.0 | 3.0 | 19.4 | 0.1 |
| Queue Length 50th ( ft ) |  | 14 |  |  | 32 |  | 9 | 128 | 0 | 3 | 382 | 0 |
| Queue Length 95th (ft) |  | 59 |  |  | 77 |  | 19 | 372 | 0 | 7 | 463 | 0 |
| Internal Link Dist (ft) |  | 499 |  |  | 616 |  |  | 2169 |  |  | 546 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  | 100 |  | 100 | 60 |  | 60 |
| Base Capacity (vph) |  | 404 |  |  | 270 |  | 413 | 1410 | 1230 | 583 | 1264 | 1125 |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.33 |  |  | 0.40 |  | 0.22 | 0.56 | 0.03 | 0.05 | 0.77 | 0.02 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 69.9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 60 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road


## 2030 Build Saturday MIdday Peak Hour

1: NH Route 125 (Calef Highway) \& Greenhill Road/Tolend Road

|  | 4 | $\rightarrow$ | 7 | 7 | $\leftarrow$ | 4 | 4 | 4 |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | $\uparrow$ |  | 7 | $\uparrow$ | 「 | \% | $\uparrow$ | F |
| Traffic Volume (vph) | 13 | 14 | 90 | 43 | 12 | 39 | 80 | 705 | 33 | 22 | 775 | 19 |
| Future Volume (vph) | 13 | 14 | 90 | 43 | 12 | 39 | 80 | 705 | 33 | 22 | 775 | 19 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.90 |  |  | 0.94 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 0.99 |  |  | 0.98 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1807 |  |  | 1870 |  | 1805 | 1900 | 1615 | 1805 | 1881 | 1615 |
| Flt Permitted |  | 0.95 |  |  | 0.67 |  | 0.11 | 1.00 | 1.00 | 0.27 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1721 |  |  | 1282 |  | 215 | 1900 | 1615 | 514 | 1881 | 1615 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.87 | 0.87 | 0.87 | 0.89 | 0.89 | 0.89 | 0.80 | 0.80 | 0.80 |
| Adj. Flow (vph) | 15 | 16 | 102 | 49 | 14 | 45 | 90 | 792 | 37 | 28 | 969 | 24 |
| RTOR Reduction (vph) | 0 | 90 | 0 | 0 | 34 | 0 | 0 | 0 | 12 | 0 | 0 | 9 |
| Lane Group Flow (vph) | 0 | 43 | 0 | 0 | 74 | 0 | 90 | 792 | 25 | 28 | 969 | 15 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Tum Type | Perm | NA |  | Perm | NA |  | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 6.6 |  |  | 6.6 |  | 53.6 | 48.2 | 48.2 | 47.2 | 45.0 | 45.0 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 8.6 |  |  | 8.6 |  | 57.6 | 50.2 | 50.2 | 51.2 | 47.0 | 47.0 |
| Actuated g/C Ratio |  | 0.11 |  |  | 0.11 |  | 0.77 | 0.67 | 0.67 | 0.68 | 0.63 | 0.63 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 197 |  |  | 147 |  | 322 | 1271 | 1080 | 423 | 1178 | 1012 |
| v/s Ratio Prot |  |  |  |  |  |  | c0.03 | 0.42 |  | 0.00 | c0.52 |  |
| v/s Ratio Perm |  | 0.02 |  |  | c0.06 |  | 0.19 |  | 0.02 | 0.04 |  | 0.01 |
| v/C Ratio |  | 0.22 |  |  | 0.51 |  | 0.28 | 0.62 | 0.02 | 0.07 | 0.82 | 0.01 |
| Uniform Delay, d1 |  | 30.1 |  |  | 31.2 |  | 10.1 | 7.0 | 4.2 | 4.9 | 10.8 | 5.3 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.6 |  |  | 2.7 |  | 0.5 | 1.0 | 0.0 | 0.1 | 4.8 | 0.0 |
| Delay (s) |  | 30.7 |  |  | 33.9 |  | 10.6 | 8.0 | 4.2 | 5.0 | 15.5 | 5.3 |
| Level of Service |  | C |  |  | C |  | B | A | A | A | B | A |
| Approach Delay (s) |  | 30.7 |  |  | 33.9 |  |  | 8.1 |  |  | 15.0 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 14.0 |  | HCM 2000 | Level of S | Service |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.72 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 75.0 |  | Sum of lost | lime (s) |  |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 67.3\% |  | CU Level of | Service |  |  | C |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

NH Route 125 at Scruton Pond Road


## 2019 Existing Weekday Evening Peak Hour

2: NH Route 125 (Calef Highway) \& Scrunton Pond Road





HCM LOS
F

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 757 | -125 | - | - |  |
| HCM Lane V/C Ratio | 0.027 | -0.768 | - | - |  |
| HCM Control Delay (s) | 9.9 | 0 | 94.1 | - | - |
| HCM Lane LOS | A | A | F | - | - |
| HCM 95th \%bile Q(veh) | 0.1 | - | 4.5 | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 12.6 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | A | F |  |
| Traffic Vol, veh/h | 59 | 39 | 5 | 593 | 1128 | 12 |
| Future Vol, veh/h | 59 | 39 | 5 | 593 | 1128 | 12 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 83 | 83 | 86 | 86 | 94 | 94 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 6 | 5 | 0 |
| Mvmt Flow | 71 | 47 | 6 | 690 | 1200 | 13 |


| Major/Minor | Minor2 | Major1 | Major2 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 1909 | 1207 | 1213 | 0 | - | 0 |
| $\quad$ Stage 1 | 1207 | - | - | - | - | - |
| $\quad$ Stage 2 | 702 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.2 | 4.1 | - | - | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - | - |
| Pot Cap-1 Maneuver | 76 | 226 | 582 | - | - | - |
| $\quad$ Stage 1 | 286 | - | - | - | - | - |
| $\quad$ Stage 2 | 495 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 75 | 226 | 582 | - | - | - |
| Mov Cap-2 Maneuver | 75 | - | - | - | - | - |
| $\quad$ Stage 1 | 281 | - | - | - | - | - |
| Stage 2 | 495 | - | - | - | - | - |
|  |  |  |  |  |  |  |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s 215.9 | 0.1 | 0 |  |

HCMLOS F

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 582 | -102 | - | - |  |
| HCM Lane V/C Ratio | 0.01 | -1.158 | - | - |  |
| HCM Control Delay (s) | 11.2 | 0 | 215.9 | - | - |
| HCM Lane LOS | B | A | F | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 7.7 | - | - |

## 2020 No Build Weekday Evening Peak Hour

2: NH Route 125 (Calef Highway) \& Scrunton Pond Road



## 2020 No Build Saturday Midday Peak Hour

2: NH Route 125 (Calef Highway) \& Scrunton Pond Road


| Major/Minor | Minor2 | Major1 | Major2 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 1669 | 902 | 927 | 0 | - | 0 |
| $\quad$ Stage 1 | 902 | - | - | - | - | - |
| $\quad$ Stage 2 | 767 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.2 | 4.1 | - | - | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - | - |
| Pot Cap-1 Maneuver | 107 | 339 | 746 | - | - | - |
| $\quad$ Stage 1 | 399 | - | - | - | - | - |
| $\quad$ Stage 2 | 462 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 102 | 339 | 746 | - | - | - |
| Mov Cap-2 Maneuver | 102 | - | - | - | - | - |
| $\quad$ Stage 1 | 380 | - | - | - | - | - |
| Stage 2 | 462 | - | - | - | - | - |



## 2030 Build Weekday Morning Peak Hour

2: NH Route 125 (Calef Highway) \& Scrunton Pond Road

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 16.6 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | A | F |  |
| Traffic Vol, veh/h | 59 | 40 | 7 | 622 | 1189 | 12 |
| Future Vol, veh/h | 59 | 40 | 7 | 622 | 1189 | 12 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 83 | 83 | 86 | 86 | 94 | 94 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 6 | 5 | 0 |
| Mvmt Flow | 71 | 48 | 8 | 723 | 1265 | 13 |


| Major/Minor | Minor2 | Major1 | Major2 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 2011 | 1272 | 1278 | 0 | - | 0 |
| $\quad$ Stage 1 | 1272 | - | - | - | - | - |
| $\quad$ Stage 2 | 739 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.2 | 4.1 | - | - | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - | - |
| Pot Cap-1 Maneuver | -66 | 207 | 550 | - | - | - |
| $\quad$ Stage 1 | 266 | - | - | - | - | - |
| $\quad$ Stage 2 | 476 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | -64 | 207 | 550 | - | - | - |
| Mov Cap-2 Maneuver | -64 | - | - | - | - | - |
| $\quad$ Stage 1 | 260 | - | - | - | - | - |
| Stage 2 | 476 | - | - | - | - | - |
|  |  |  |  |  |  |  |


$\xrightarrow{\text { Notes }} \stackrel{\text { Volume exceeds capacity }}{\sim} \$$ : Delay exceeds $300 s \quad+$ : Computation Not Defined $\quad *:$ All major volume in platoon

## 2020 Build Weekday Evening Peak Hour

## 2: NH Route 125 (Calef Highway) \& Scrunton Pond Road




|  | Intersection |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 7.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | M |  |  | 4 | t |  |
| Traffic Vol, veh/h | 57 | 17 | 21 | 701 | 782 | 43 |
| Future Vol, veh/h | 57 | 17 | 21 | 701 | 782 | 43 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | \# 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 74 | 74 | 92 | 92 | 85 | 85 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 0 | 1 | 0 |
| Mvmt Flow | 77 | 23 | 23 | 762 | 920 | 51 |





| Major/Minor | Minor2 | Major1 |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2104 | 1331 | 1338 | 0 | - | 0 |
| Stage 1 | 1331 | - | - | - | - |  |
| Stage 2 | 773 | - | - | - | - |  |
| Critical Hdwy | 6.4 | 6.2 | 4.1 | - | - |  |
| Critical Hdwy Stg 1 | 5.4 | . | - | - | - |  |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - |  |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - |  |
| Pot Cap-1 Maneuver | - 57 | 191 | 522 | - | - |  |
| Stage 1 | 249 | - | - | - | - |  |
| Stage 2 | 459 | - | - | - | - |  |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | $\sim 56$ | 191 | 522 | - | - | - |
| Mov Cap-2 Maneuver | $\sim 56$ | - | - | - | - |  |
| Stage 1 | 243 |  | - | - | - | - |
| Stage 2 | 459 | - | - | - | - |  |



## Notes

$\sim:$ Volume exceeds capacity $\$$ : Delay exceeds $300 \mathrm{~s} \quad+$ : Computation Not Defined *: All major volume in platoon

## 2030 No Build Weekday Evening Peak Hour

## 2: NH Route 125 (Calef Highway) \& Scrunton Pond Road





## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

2030 No Build Saturday Midday Peak Hour
2: NH Route 125 (Calef Highway) \& Scrunton Pond Road


| Major/Minor | Minor2 | Major1 |  |  |  |  |  | Major2 |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- | :---: | :---: | :---: |
| Conflicting Flow All | 1840 | 995 | 1023 | 0 | - | 0 |  |  |  |
| $\quad$ Stage 1 | 995 | - | - | - | - | - |  |  |  |
| $\quad$ Stage 2 | 845 | - | - | - | - | - |  |  |  |
| Critical Hdwy | 6.4 | 6.2 | 4.1 | - | - | - |  |  |  |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - | - |  |  |  |
| Pot Cap-1 Maneuver | 84 | 300 | 686 | - | - | - |  |  |  |
| $\quad$ Stage 1 | 361 | - | - | - | - | - |  |  |  |
| Stage 2 | 425 | - | - | - | - | - |  |  |  |

Platoon blocked, \%
Mov Cap-1 Maneuver ~79 300686 - . .

| Mov Cap-2 Maneuver | $\sim 79$ | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stage 1 | 339 | - | - | - | - | - |
| Stage 2 | 425 | - | - | - | - | - |



## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds $300 s \quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

## 2030 Build Weekday Morning Peak Hour

## 2: NH Route 125 (Calef Highway) \& Scrunton Pond Road

|  | Intersection |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 34.1 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | 4 | $\dagger$ |  |
| Traffic Vol, veh/h | 66 | 45 | 8 | 682 | 1306 | 13 |
| Future Vol, veh/h | 66 | 45 | 8 | 682 | 1306 | 13 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | \# 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 83 | 83 | 86 | 86 | 94 | 94 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 6 | 5 | 0 |
| Mumt Flow | 80 | 54 | 9 | 793 | 1389 | 14 |




| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 7.6 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | * |  |  | $\uparrow$ | F |  |
| Traffic Vol, veh/h | 27 | 12 | 21 | 1195 | 743 | 74 |
| Future Vol, veh/h | 27 | 12 | 21 | 1195 | 743 | 74 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, | \# 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 57 | 57 | 92 | 92 | 93 | 93 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 0 | 1 | 0 |
| Mumt Flow | 47 | 21 | 23 | 1299 | 799 | 80 |


| Major/Minor | Minor2 | Major1 | Major2 |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Conflicting Flow All | 2184 | 839 | 879 | 0 | - |
| $\quad$ Stage 1 | 839 | - | - | - | - |
| $\quad$ Stage 2 | 1345 | - | - | - | - |
|  | - |  |  |  |  |
| Critical Hdwy | 6.4 | 6.2 | 4.1 | - | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - |
| Pot Cap-1 Maneuver | 51 | 369 | 777 | - | - |
| $\quad$ Stage 1 | 427 | - | - | - | - |
| $\quad$ Stage 2 | 245 | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - |
| Mov Cap-1 Maneuver | -46 | 369 | 777 | - | - |
| Mov Cap-2 Maneuver | $\sim 46$ | - | - | - |  |
| $\quad$ Stage 1 | 382 | - | - | - | - |
| Stage 2 | 245 | - | - | - |  |




| MajorMinor | Minor2 | Major1 |  | Major2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Conflicting Flow All | 1925 | 1039 | 1067 | 0 | - | 0 |
| $\quad$ Stage 1 | 1039 | - | - | - | - | - |
| $\quad$ Stage 2 | 886 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.2 | 4.1 | - | - | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | 2.2 | - | - | - |
| Pot Cap-1 Maneuver | -74 | 283 | 661 | - | - | - |
| $\quad$ Stage 1 | 344 | - | - | - | - | - |
| $\quad$ Stage 2 | 406 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | -69 | 283 | 661 | - | - | - |
| Mov Cap-2 Maneuver | -69 | - | - | - | - | - |
| $\quad$ Stage 1 | 320 | - | - | - | - | - |
| Stage 2 | 406 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s 288.6 | 0.3 | 0 |  |
| HCM LOS | F |  |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | :--- | :--- |
| Capacity (veh/h) | 661 | - | 84 | - | - |
| HCM Lane V/C Ratio | 0.038 | -1.303 | - | - |  |
| HCM Control Delay (s) | 10.7 | 0 | 288.6 | - | - |
| HCM Lane LOS | B | A | F | - | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 8.2 | - | - |

## Notes

$\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad \mathbf{~}$ : Computation Not Defined $\quad$ : All major volume in platoon

NH Route 125 at NH Route 9

2019 Existing Weekday Morning Peak Hour
3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | $\cdots$ |  | P | $\underline{4}$ | $\downarrow$ | J | $\cdots$ | 4 | $\dagger$ | 7 | - |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | \% | $\uparrow$ | ${ }^{7}$ | ${ }_{1}$ | 中 ${ }^{\text {c }}$ |  | ${ }^{7}$ | + | T | 7 | 4 | 「 |
| Traffic Volume (vph) | 53 | 460 | 196 | 181 | 875 | 49 | 63 | 565 | 169 | 180 | 142 | 80 |
| Future Volume (vph) | 53 | 460 | 196 | 181 | 875 | 49 | 63 | 565 | 169 | 180 | 142 | 80 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length ( ft ) | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( ft ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time (s) |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.95 | 0.95 | 0.95 | 0.86 | 0.86 | 0.86 | 0.66 | 0.66 | 0.66 |
| Heavy Vehicles (\%) | 7\% | 5\% | 1\% | 5\% | 4\% | 16\% | 2\% | 1\% | 1\% | 8\% | 5\% | 1\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 58 | 505 | 215 | 191 | 973 | 0 | 73 | 657 | 197 | 273 | 215 | 121 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split (\%) | 22.4\% | 22.4\% | 22.4\% | 22.4\% | 22.4\% |  | 22.4\% | 32.9\% | 32.9\% | 22.4\% | 32.9\% | 32.9\% |
| Maximum Green ( s ) | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | -2.0 | -4.0 | -4.0 | -2.0 | -4.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v/c Ratio | 0.41 | 1.31 | 0.51 | 0.72 | 0.92 |  | 0.46 | 1.07 | 0.34 | 0.85 | 0.29 | 0.17 |
| Control Delay | 75.9 | 202.9 | 33.0 | 75.7 | 65.3 |  | 75.7 | 104.8 | 18.7 | 82.1 | 30.9 | 6.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 75.9 | 202.9 | 33.0 | 75.7 | 65.3 |  | 75.7 | 104.8 | 18.7 | 82.1 | 30.9 | 6.2 |
| Queue Length 50th ( ft ) | 56 | ~659 | 100 | 184 | 513 |  | 71 | $\sim 744$ | 59 | 262 | 137 | 3 |
| Queue Length 95th (ft) | 107 | \#943 | 198 | 274 | \#685 |  | 122 | \#981 | 126 | 269 | 160 | 14 |
| Internal Link Dist (ft) |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length (ft) | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity (vph) | 359 | 385 | 420 | 353 | 1057 |  | 376 | 613 | 581 | 355 | 751 | 729 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.16 | 1.31 | 0.51 | 0.54 | 0.92 |  | 0.19 | 1.07 | 0.34 | 0.77 | 0.29 | 0.17 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## Area Type:

Other
Cycle Length: 161
Actuated Cycle Length: 150.8
Natural Cycle: 120
Control Type: Actuated-Uncoordinated
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


## 2019 Existing Weekday Morning Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

c Critical Lane Group

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | $\dagger$ |  | Pa | 4 | $\downarrow$ | $\downarrow$ | $\cdots$ | , | $\rangle$ | $\dagger$ | $k$ | $\psi$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ | 7 | ${ }^{7}$ | 性 |  | ${ }_{1}$ | $\uparrow$ | F' | ${ }_{1}$ | $\uparrow$ | 「 |
| Traffic Volume (vph) | 194 | 903 | 106 | 81 | 483 | 97 | 81 | 165 | 102 | 254 | 469 | 128 |
| Future Volume (vph) | 194 | 903 | 106 | 81 | 483 | 97 | 81 | 165 | 102 | 254 | 469 | 128 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (f) | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length ( t ) | 150 |  | 150 | 150 |  | , | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( ft ) |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time (s) |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.93 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 1\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 213 | 992 | 116 | 87 | 623 | 0 | 88 | 179 | 111 | 276 | 510 | 139 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | , | . |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Solit (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split (\%) | 22.4\% | 22.4\% | 22.4\% | 22.4\% | 22.4\% |  | 22.4\% | 32.9\% | 32.9\% | 22.4\% | 32.9\% | 32.9\% |
| Maximum Green (s) | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | -2.0 | -4.0 | -4.0 | -2.0 | -4.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v/c Ratio | 0.66 | 1.68 | 0.20 | 0.45 | 0.73 |  | 0.45 | 0.39 | 0.24 | 0.74 | 0.81 | 0.23 |
| Control Delay | 60.9 | 341.9 | 9.9 | 64.5 | 51.2 |  | 64.2 | 45.5 | 8.2 | 61.6 | 51.1 | 9.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 60.9 | 341.9 | 9.9 | 64.5 | 51.2 |  | 64.2 | 45.5 | 8.2 | 61.6 | 51.1 | 9.5 |
| Queue Length 50th (ft) | 175 | -1263 | 9 | 72 | 258 |  | 73 | 127 | 0 | 226 | 386 | 13 |
| Queue Length 95th (t) | 274 | \#1675 | 58 | 136 | 371 |  | 137 | 220 | 47 | 356 | \#637 | 67 |
| Internal Link Dist ( t ) |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length ( t ) | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity (vph) | 462 | 592 | 573 | 446 | 903 |  | 462 | 744 | 681 | 457 | 720 | 675 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.46 | 1.68 | 0.20 | 0.20 | 0.69 |  | 0.19 | 0.24 | 0.16 | 0.60 | 0.71 | 0.21 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## 2019 Existing Weekday Evening Peak Hour

## 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

## Area Type: <br> Other

Cycle Length: 161
Actuated Cycle Length: 127.7
Natural Cycle: 130
Control Type: Actuated-Uncoordinated

- Volume exceeds capacity, queve is theoretically infinite.

Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capzcity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | \% |  |  | 4 | $\downarrow$ | $\cdots$ | $\cdots$ | $\checkmark$ | 7 | $\square$ | $k$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | \% | $\uparrow$ | " | \% | 怆 |  | \% | $\uparrow$ | 7 | 7 | $\uparrow$ | 「 |
| Traffic Volume (vph) | 194 | 903 | 106 | 81 | 483 | 97 | 81 | 165 | 102 | 254 | 469 | 128 |
| Future Volume (vph) | 194 | 903 | 106 | 81 | 483 | 97 | 81 | 165 | 102 | 254 | 469 | 128 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1805 | 1900 | 1615 | 1745 | 3491 |  | 1805 | 1900 | 1561 | 1787 | 1837 | 1546 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1805 | 1900 | 1615 | 1745 | 3491 |  | 1805 | 1900 | 1561 | 1787 | 1837 | 1546 |
| Peak-hour factor, PHF | 0.91 | 0.91 | 0.91 | 0.93 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 213 | 992 | 116 | 87 | 519 | 104 | 88 | 179 | 111 | 276 | 510 | 139 |
| RTOR Reduction (vph) | 0 | 0 | 70 | 0 | 10 | 0 | 0 | 0 | 84 | 0 | 0 | 76 |
| Lane Group Flow (vph) | 213 | 992 | 46 | 87 | 613 | 0 | 88 | 179 | 27 | 276 | 510 | 63 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 1\% |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Actuated Green, G (s) | 20.8 | 35.7 | 35.7 | 12.0 | 26.9 |  | 11.9 | 28.7 | 28.7 | 24.7 | 41.5 | 41.5 |
| Effective Green, g (s) | 22.8 | 39.7 | 39.7 | 14.0 | 30.9 |  | 13.9 | 30.7 | 30.7 | 26.7 | 43.5 | 43.5 |
| Actuated g/C Ratio | 0.18 | 0.31 | 0.31 | 0.11 | 0.24 |  | 0.11 | 0.24 | 0.24 | 0.21 | 0.34 | 0.34 |
| Clearance Time (s) | 6.0 | 8.0 | 8.0 | 6.0 | 8.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Gp Cap (vph) | 323 | 593 | 504 | 192 | 848 |  | 197 | 458 | 377 | 375 | 628 | 529 |
| v/s Ratio Prot | c0.12 | c0.52 |  | 0.05 | 0.18 |  | 0.05 | 0.09 |  | c0.15 | c0.28 |  |
| V/s Ratio Perm |  |  | 0.03 |  |  |  |  |  | 0.02 |  |  | 0.04 |
| v/c Ratio | 0.66 | 1.67 | 0.09 | 0.45 | 0.72 |  | 0.45 | 0.39 | 0.07 | 0.74 | 0.81 | 0.12 |
| Uniform Delay, d1 | 48.5 | 43.7 | 30.9 | 53.0 | 44.2 |  | 53.0 | 40.4 | 37.2 | 46.9 | 38.1 | 28.7 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 4.8 | 310.1 | 0.1 | 1.7 | 3.1 |  | 1.6 | 0.6 | 0.1 | 7.3 | 7.9 | 0.1 |
| Delay (s) | 53.3 | 353.8 | 31.0 | 54.7 | 47.2 |  | 54.6 | 40.9 | 37.3 | 54.2 | 46.0 | 28.8 |
| Level of Service | D | F | C | D | D |  | D | D | D | D | D | C |
| Approach Delay (s) |  | 277.0 |  |  | 48.2 |  |  | 43.0 |  |  | 45.9 |  |
| Approach LOS |  | F |  |  | D |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 137.6 |  | CM 2000 | evel of S | rvice |  | F |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 1.11 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 127.1 |  | m of lost | ime (s) |  |  | 16.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 94.5\% |  | Level of | Service |  |  | F |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

2019 Existing Saturday Midday Peak Hour
3：NH Route 125 （Calef Highway）\＆NH Route 9 （Littleworth Road）／NH Route 9 （Franklin Pierce Highw

|  | $\cdots$ | 4 | P | 澈 | $\pm$ | － | $\leqslant$ | \％ | \％ | $\checkmark$ | － | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | ${ }^{7}$ | 4 | T | ${ }_{1}$ | 中 $\%$ |  | 7 | 4 | 「 | ${ }_{1}$ | 中 | F |
| Traffic Volume（vph） | 112 | 466 | 106 | 105 | 579 | 125 | 112 | 247 | 157 | 146 | 198 | 102 |
| Future Volume（vph） | 112 | 466 | 106 | 105 | 579 | 125 | 112 | 247 | 157 | 146 | 198 | 102 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（ft） | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length（ f ） | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ ft ） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（ ft ） |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time（s） |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.80 | 0.80 | 0.80 | 0.89 | 0.89 | 0.89 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles（\％） | 0\％ | 1\％ | 0\％ | 0\％ | 1\％ | 0\％ | 0\％ | 0\％ | 0\％ | 0\％ | 1\％ | 0\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 118 | 491 | 112 | 131 | 880 | 0 | 126 | 278 | 176 | 162 | 220 | 113 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width（ft） |  | 12 |  |  | 12 |  |  | 12 |  |  | 12 |  |
| Link Offset（ft） |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width（ft） |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.04 | 1.00 | 1.00 | 1.00 | 1.00 | 1.04 | 1.00 | 1.04 | 1.04 |
| Turning Speed（mph） | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split（s） | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split（\％） | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ |  | 22．4\％ | 32．9\％ | 32．9\％ | 22．4\％ | 32．9\％ | 32．9\％ |
| Maximum Green（s） | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time（s） | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | －2．0 | －4．0 | －4．0 | －2．0 | －4．0 |  | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |
| Total Lost Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v／c Ratio | 0.47 | 0.85 | 0.20 | 0.50 | 0.79 |  | 0.48 | 0.65 | 0.40 | 0.55 | 0.49 | 0.24 |
| Control Delay | 51.1 | 52.3 | 9.5 | 50.9 | 40.8 |  | 50.9 | 45.9 | 16.6 | 50.1 | 39.3 | 7.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 51.1 | 52.3 | 9.5 | 50.9 | 40.8 |  | 50.9 | 45.9 | 16.6 | 50.1 | 39.3 | 7.2 |
| Queue Length 50th（ f ） | 73 | 304 | 5 | 81 | 274 |  | 78 | 169 | 33 | 100 | 126 | 0 |
| Queue Length 95th（ft） | 154 | \＃682 | 55 | 147 | \＃411 |  | 160 | 293 | 101 | 198 | 228 | 43 |
| Internal Link Dist（ ft ） |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |

## 2019 Existing Saturday Midday Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw


Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


2019 Existing Saturday Midday Peak Hour
3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | \% | $\dagger$ | par | $\leqslant$ | $\downarrow$ | W | $\checkmark$ | $\checkmark$ | خ | $\square$ | k | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NW |
| Lane Configurations | \% | $\uparrow$ | 7 | \% | $\uparrow t$ |  | \% | 4 | 「 | \% | $\uparrow$ | F |
| Traffic Volume (vph) | 112 | 466 | 106 | 105 | 579 | 125 | 112 | 247 | 157 | 146 | 198 | 102 |
| Future Volume (vph) | 112 | 466 | 106 | 105 | 579 | 125 | 112 | 247 | 157 | 146 | 198 | 102 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1805 | 1881 | 1615 | 1745 | 3485 |  | 1805 | 1900 | 1561 | 1805 | 1818 | 1561 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1805 | 1881 | 1615 | 1745 | 3485 |  | 1805 | 1900 | 1561 | 1805 | 1818 | 1561 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.80 | 0.80 | 0.80 | 0.89 | 0.89 | 0.89 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 118 | 491 | 112 | 131 | 724 | 156 | 126 | 278 | 176 | 162 | 220 | 113 |
| RTOR Reduction (vph) | 0 | 0 | 70 | 0 | 10 | 0 | 0 | 0 | 89 | 0 | 0 | 85 |
| Lane Group Flow (vph) | 118 | 491 | 42 | 131 | 870 | 0 | 126 | 278 | 87 | 162 | 220 | 28 |
| Heavy Vehicles (\%) | 0\% | 1\% | 0\% | 0\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Actuated Green, G (s) | 12.8 | 28.7 | 28.7 | 13.8 | 29.7 |  | 13.3 | 21.9 | 21.9 | 15.4 | 24.0 | 24.0 |
| Effective Green, g (s) | 14.8 | 32.7 | 32.7 | 15.8 | 33.7 |  | 15.3 | 23.9 | 23.9 | 17.4 | 26.0 | 26.0 |
| Actuated g/C Ratio | 0.14 | 0.31 | 0.31 | 0.15 | 0.32 |  | 0.14 | 0.23 | 0.23 | 0.16 | 0.25 | 0.25 |
| Clearance Time (s) | 6.0 | 8.0 | 8.0 | 6.0 | 8.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 252 | 581 | 499 | 260 | 1110 |  | 261 | 429 | 352 | 296 | 446 | 383 |
| v/s Ratio Prot | 0.07 | c0.26 |  | c0.08 | 0.25 |  | 0.07 | c0.15 |  | c0.09 | 0.12 |  |
| v/s Ratio Perm |  |  | 0.03 |  |  |  |  |  | 0.06 |  |  | 0.02 |
| v/c Ratio | 0.47 | 0.85 | 0.08 | 0.50 | 0.78 |  | 0.48 | 0.65 | 0.25 | 0.55 | 0.49 | 0.07 |
| Uniform Delay, d1 | 41.9 | 34.2 | 25.9 | 41.4 | 32.7 |  | 41.6 | 37.1 | 33.6 | 40.6 | 34.2 | 30.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.4 | 10.9 | 0.1 | 1.5 | 3.7 |  | 1.4 | 3.4 | 0.4 | 2.1 | 0.9 | 0.1 |
| Delay (s) | 43.3 | 45.1 | 26.0 | 42.9 | 36.4 |  | 43.0 | 40.5 | 33.9 | 42.7 | 35.1 | 30.7 |
| Level of Service | D | D | , | D | D |  | D | D | C | D | D | C |
| Approach Delay (s) |  | 41.8 |  |  | 37.3 |  |  | 39.1 |  |  | 36.6 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 38.7 | HCM 2000 Level of Service |  |  |  |  | D |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.67 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 105.8 |  | um of lost | me (s) |  |  | 16.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 64.8\% | ICU Level of Service |  |  |  |  | C |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

3：NH Route 125 （Calef Highway）\＆NH Route 9 （Littleworth Road）／NH Route 9 （Franklin Pierce Highw

|  | $\cdots$ |  | ［ |  | $\downarrow$ | W | $\leqslant$ | \％ | ¢ | $\square$ | K | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | 7 | 4 | 「 | ${ }^{7}$ | $\uparrow+$ |  | 4 | $\uparrow$ | 「 | ${ }_{1}$ | 中 | F |
| Traffic Volume（vph） | 52 | 492 | 185 | 236 | 911 | 66 | 108 | 543 | 164 | 174 | 137 | 107 |
| Future Volume（vph） | 52 | 492 | 185 | 236 | 911 | 66 | 108 | 543 | 164 | 174 | 137 | 107 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（ft） | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length（ft） | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（ft） |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time（s） |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.95 | 0.95 | 0.95 | 0.86 | 0.86 | 0.86 | 0.66 | 0.66 | 0.66 |
| Heavy Vehicles（\％） | 7\％ | 5\％ | 1\％ | 5\％ | 4\％ | 16\％ | 2\％ | 1\％ | 1\％ | 8\％ | 5\％ | 1\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 57 | 541 | 203 | 248 | 1028 | 0 | 126 | 631 | 191 | 264 | 208 | 162 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split（s） | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split（\％） | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ |  | 22．4\％ | 32．9\％ | 32．9\％ | 22．4\％ | 32．9\％ | 32．9\％ |
| Maximum Green（ $s$ ） | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time（s） | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | －2．0 | －4．0 | －4．0 | －2．0 | －4．0 |  | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |
| Total Lost Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v／c Ratio | 0.42 | 1.44 | 0.49 | 0.82 | 0.92 |  | 0.60 | 1.06 | 0.34 | 0.84 | 0.31 | 0.24 |
| Control Delay | 77.7 | 255.5 | 31.8 | 82.4 | 64.4 |  | 77.2 | 102.4 | 18.7 | 84.1 | 36.2 | 10.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 77.7 | 255.5 | 31.8 | 82.4 | 64.4 |  | 77.2 | 102.4 | 18.7 | 84.1 | 36.2 | 10.5 |
| Queue Length 50th（ft） | 58 | －782 | 93 | 249 | 556 |  | 128 | $\sim 745$ | 58 | 266 | 151 | 24 |
| Queue Length 95th（ft） | 106 | \＃1025 | 183 | \＃360 | \＃748 |  | 184 | \＃924 | 120 | 259 | 165 | 33 |
| Internal Link Dist（ft） |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length（ ft ） | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity（vph） | 350 | 375 | 412 | 345 | 1116 |  | 367 | 598 | 569 | 347 | 676 | 674 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v／c Ratio | 0.16 | 1.44 | 0.49 | 0.72 | 0.92 |  | 0.34 | 1.06 | 0.34 | 0.76 | 0.31 | 0.24 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## 2020 No Build Weekday Morning Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw
Area Type:
Other
Cycle Length: 161
Actuated Cycle Length: 154.6
Natural Cycle: 120
Control Type: Actuated-Uncoordinated
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


3：NH Route 125 （Calef Highway）\＆NH Route 9 （Littleworth Road）／NH Route 9 （Franklin Pierce Highw

| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\uparrow$ | 「 | ＊ | 中 ${ }^{\text {P }}$ |  | \％ | $\uparrow$ | 「 | \％ | $\uparrow$ | $\stackrel{ }{1}$ |
| Traffic Volume（vph） | 52 | 492 | 185 | 236 | 911 | 66 | 108 | 543 | 164 | 174 | 137 | 107 |
| Future Volume（vph） | 52 | 492 | 185 | 236 | 911 | 66 | 108 | 543 | 164 | 174 | 137 | 107 |
| Ideal Flow（vphol） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Total Lost time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1687 | 1810 | 1599 | 1662 | 3410 |  | 1770 | 1881 | 1546 | 1671 | 1749 | 1546 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd．Flow（perm） | 1687 | 1810 | 1599 | 1662 | 3410 |  | 1770 | 1881 | 1546 | 1671 | 1749 | 1546 |
| Peak－hour factor，PHF | 0.91 | 0.91 | 0.91 | 0.95 | 0.95 | 0.95 | 0.86 | 0.86 | 0.86 | 0.66 | 0.66 | 0.66 |
| Adj．Flow（vph） | 57 | 541 | 203 | 248 | 959 | 69 | 126 | 631 | 191 | 264 | 208 | 162 |
| RTOR Reduction（vph） | 0 | 0 | 80 | 0 | 3 | 0 | 0 | 0 | 79 | 0 | 0 | 77 |
| Lane Group Flow（vph） | 57 | 541 | 123 | 248 | 1025 | 0 | 126 | 631 | 112 | 264 | 208 | 85 |
| Heavy Vehicles（\％） | 7\％ | 5\％ | 1\％ | 5\％ | 4\％ | 16\％ | 2\％ | 1\％ | 1\％ | 8\％ | 5\％ | 1\％ |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Actuated Green，G（s） | 9.2 | 29.4 | 29.4 | 26.3 | 46.5 |  | 16.4 | 47.1 | 47.1 | 27.1 | 57.8 | 57.8 |
| Effective Green， g （s） | 11.2 | 33.4 | 33.4 | 28.3 | 50.5 |  | 18.4 | 49.1 | 49.1 | 29.1 | 59.8 | 59.8 |
| Actuatedg／C Ratio | 0.07 | 0.21 | 0.21 | 0.18 | 0.32 |  | 0.12 | 0.31 | 0.31 | 0.19 | 0.38 | 0.38 |
| Clearance Time（s） | 6.0 | 8.0 | 8.0 | 6.0 | 8.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 121 | 387 | 342 | 301 | 1104 |  | 208 | 592 | 486 | 311 | 670 | 593 |
| v／s Ratio Prot | 0.03 | c0．30 |  | c0．15 | c0．30 |  | 0.07 | c0．34 |  | c0．16 | 0.12 |  |
| v／s Ratio Perm |  |  | 0.08 |  |  |  |  |  | 0.07 |  |  | 0.05 |
| v／c Ratio | 0.47 | 1.40 | 0.36 | 0.82 | 0.93 |  | 0.61 | 1.07 | 0.23 | 0.85 | 0.31 | 0.14 |
| Uniform Delay，d1 | 69.5 | 61.2 | 52.1 | 61.4 | 51.0 |  | 65.3 | 53.4 | 39.5 | 61.3 | 33.6 | 31.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 2.9 | 194.1 | 0.6 | 16.5 | 13.1 |  | 4.9 | 55.8 | 0.2 | 18.9 | 0.3 | 0.1 |
| Delay（s） | 72.4 | 255.4 | 52.8 | 77.9 | 64.1 |  | 70.2 | 109.2 | 39.7 | 80.2 | 33.9 | 31.5 |
| Level of Service | E | F | D | E | E |  | E | F | D | F | C | C |
| Approach Delay（s） |  | 191.0 |  |  | 66.8 |  |  | 90.0 |  |  | 52.5 |  |
| Approach LOS |  | F |  |  | E |  |  | F |  |  | D |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 97.5 | HCM 2000 Level of Service | F |
| HCM 2000 Volume to Capacity ratio | 1.05 |  | 16.0 |
| Actuated Cycle Length（s） | 155.9 | Sum of lost time（s） | E |
| Intersection Capacity Utilization | $90.5 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |

## 2020 No Build Weekday Evening Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | $\cdots$ |  | pran | 4 | $\dagger$ | لا | $\checkmark$ | 4 | > | $\dagger$ | 㐫 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | ${ }^{*}$ | 4 | 1 | ${ }_{1}$ | 个 ${ }^{\text {P }}$ |  | 1 | 4 | 7 ${ }^{\text {P }}$ | ${ }^{1}$ | 4 | 1 |
| Traffic Volume (vph) | 191 | 931 | 104 | 102 | 511 | 127 | 101 | 160 | 99 | 249 | 458 | 163 |
| Future Volume (vph) | 191 | 931 | 104 | 102 | 511 | 127 | 101 | 160 | 99 | 249 | 458 | 163 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length (ft) | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( ft ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( ft ) |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time (s) |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.93 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 1\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 210 | 1023 | 114 | 110 | 686 | 0 | 110 | 174 | 108 | 271 | 498 | 177 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(ft) |  | 12 |  |  | 12 |  |  | 12 |  |  | 12 |  |
| Link Offset(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(ft) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.04 | 1.00 | 1.00 | 1.00 | 1.00 | 1.04 | 1.00 | 1.04 | 1.04 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split (\%) | 22.4\% | 22.4\% | 22.4\% | 22.4\% | 22.4\% |  | 22.4\% | 32.9\% | 32.9\% | 22.4\% | 32.9\% | 32.9\% |
| Maximum Green ( s ) | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | -2.0 | -4.0 | -4.0 | -2.0 | -4.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v/c Ratio | 0.66 | 1.78 | 0.20 | 0.52 | 0.78 |  | 0.51 | 0.38 | 0.23 | 0.74 | 0.83 | 0.30 |
| Control Delay | 62.0 | 387.0 | 10.2 | 64.8 | 53.4 |  | 64.6 | 44.9 | 7.6 | 63.1 | 53.6 | 14.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 62.0 | 387.0 | 10.2 | 64.8 | 53.4 |  | 64.6 | 44.9 | 7.6 | 63.1 | 53.6 | 14.2 |
| Queue Length 50th (ft) | 173 | ~1343 | 7 | 91 | 291 |  | 91 | 123 | 0 | 222 | 383 | 36 |
| Queue Length 95th (ft) | 275 | \#1810 | 59 | 165 | \#455 |  | 165 | 213 | 44 | 356 | \#633 | 106 |
| Internal Link Dist (ft) |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |

Lanes, Volumes, Timings
AJA

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | $\cdots$ |  | $0^{4}$ | $\underline{4}$ | 1 | W | 4 | 4 | $\dagger$ | $\uparrow$ | 匆 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Turn Bay Length (ft) | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity (vph) | 454 | 575 | 559 | 439 | 888 |  | 454 | 733 | 673 | 450 | 708 | 666 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.46 | 1.78 | 0.20 | 0.25 | 0.77 |  | 0.24 | 0.24 | 0.16 | 0.60 | 0.70 | 0.27 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 161 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 129.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maxim | ter two | es. |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

c Critical Lane Group

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | $\cdots$ | $\dagger$ | [ | 4 | $\frac{1}{\dagger}$ | b | $\cdots$ | \% | - | $\uparrow$ | - | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | ${ }_{1}$ | + | 「 | ${ }^{7}$ | +1 |  | ${ }^{7}$ | 4 | F' | ${ }^{7}$ | 4 | 7 |
| Traffic Volume (vph) | 109 | 486 | 104 | 126 | 604 | 144 | 135 | 239 | 153 | 141 | 192 | 124 |
| Future Volume (vph) | 109 | 486 | 104 | 126 | 604 | 144 | 135 | 239 | 153 | 141 | 192 | 124 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length ( ft ) | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( ft ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time (s) |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.80 | 0.80 | 0.80 | 0.89 | 0.89 | 0.89 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles (\%) | 0\% | 1\% | 0\% | 0\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 115 | 512 | 109 | 158 | 935 | 0 | 152 | 269 | 172 | 157 | 213 | 138 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split (\%) | 22.4\% | 22.4\% | 22.4\% | 22.4\% | 22.4\% |  | 22.4\% | 32.9\% | 32.9\% | 22.4\% | 32.9\% | 32.9\% |
| Maximum Green ( s ) | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | -2.0 | -4.0 | -4.0 | -2.0 | -4.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v/c Ratio | 0.47 | 0.90 | 0.19 | 0.55 | 0.81 |  | 0.53 | 0.65 | 0.40 | 0.54 | 0.53 | 0.32 |
| Control Delay | 51.8 | 57.8 | 9.2 | 51.1 | 40.7 |  | 50.9 | 47.0 | 16.7 | 50.9 | 43.1 | 11.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 51.8 | 57.8 | 9.2 | 51.1 | 40.7 |  | 50.9 | 47.0 | 16.7 | 50.9 | 43.1 | 11.9 |
| Queue Length 50th ( ft ) | 72 | 328 | 3 | 99 | 295 |  | 95 | 166 | 31 | 98 | 127 | 12 |
| Queue Length 95th ( ft ) | 152 | \#728 | 53 | 170 | 427 |  | 187 | 289 | 100 | 194 | 233 | 68 |
| Internal Link Dist (ft) |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length ( ft ) | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity (vph) | 549 | 572 | 562 | 531 | 1161 |  | 549 | 885 | 789 | 549 | 847 | 789 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.21 | 0.90 | 0.19 | 0.30 | 0.81 |  | 0.28 | 0.30 | 0.22 | 0.29 | 0.25 | 0.17 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Lanes, Volumes, Timings
AJA

## 2020 No Build Saturday Midday Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

## Area Type: <br> Other

Cycle Length: 161
Actuated Cycle Length: 107.4
Natural Cycle: 65
Control Type: Actuated-Uncoordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


## 2020 No Build Saturday Midday Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
AJA

## 2030 Build Weekday Morning Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | ' |  | Pat | 4 | $\frac{1}{7}$ | W | 4 | a | ¢ | $\uparrow$ | k | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | $\%$ | 4 | 「 | ${ }_{1}$ | + ${ }^{\text {a }}$ |  | ${ }^{7}$ | 4 | F | K | + | T |
| Traffic Volume (vph) | 52 | 523 | 185 | 243 | 930 | 77 | 118 | 543 | 164 | 174 | 137 | 115 |
| Future Volume (vph) | 52 | 523 | 185 | 243 | 930 | 77 | 118 | 543 | 164 | 174 | 137 | 115 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length ( ft ) | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( ft ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( ft ) |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time (s) |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.95 | 0.95 | 0.95 | 0.86 | 0.86 | 0.86 | 0.66 | 0.66 | 0.66 |
| Heavy Vehicles (\%) | 7\% | 5\% | 1\% | 5\% | 4\% | 16\% | 2\% | 1\% | 1\% | 8\% | 5\% | 1\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 57 | 575 | 203 | 256 | 1060 | 0 | 137 | 631 | 191 | 264 | 208 | 174 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split (\%) | 22.4\% | 22.4\% | 22.4\% | 22.4\% | 22.4\% |  | 22.4\% | 32.9\% | 32.9\% | 22.4\% | 32.9\% | 32.9\% |
| Maximum Green (s) | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | -2.0 | -4.0 | -4.0 | -2.0 | -4.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v/c Ratio | 0.42 | 1.54 | 0.49 | 0.83 | 0.95 |  | 0.62 | 1.06 | 0.34 | 0.84 | 0.31 | 0.26 |
| Control Delay | 77.8 | 295.2 | 32.0 | 83.5 | 67.6 |  | 77.3 | 104.0 | 18.8 | 84.5 | 37.2 | 10.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 77.8 | 295.2 | 32.0 | 83.5 | 67.6 |  | 77.3 | 104.0 | 18.8 | 84.5 | 37.2 | 10.8 |
| Queue Length 50th ( ft ) | 58 | $\sim 862$ | 94 | 258 | 581 |  | 139 | $\sim 752$ | 59 | 268 | 154 | 27 |
| Queue Length 95th (ft) | 106 | \#1104 | 183 | \#386 | \#787 |  | 197 | \#924 | 120 | 259 | 167 | 35 |
| Internal Link Dist (ft) |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length (ft) | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity (vph) | 349 | 374 | 411 | 343 | 1121 |  | 365 | 595 | 568 | 345 | 663 | 669 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.16 | 1.54 | 0.49 | 0.75 | 0.95 |  | 0.38 | 1.06 | 0.34 | 0.77 | 0.31 | 0.26 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Lanes, Volumes, Timings
AJA

## 2030 Build Weekday Morning Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw
Area Type:
Other
Cycle Length: 161
Actuated Cycle Length: 155.2
Natural Cycle: 130
Control Type: Actuated-Uncoordinated
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }_{1}$ | 中 | 「 | ${ }_{1}$ | 中 ${ }^{+}$ |  | 7 | ＋ | 「 | 7 | 中 |  |
| Traffic Volume（vph） | 52 | 523 | 185 | 243 | 930 | 77 | 118 | 543 | 164 | 174 | 137 | 115 |
| Future Volume（vph） | 52 | 523 | 185 | 243 | 930 | 77 | 118 | 543 | 164 | 174 | 137 | 115 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Total Lost time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1687 | 1810 | 1599 | 1662 | 3401 |  | 1770 | 1881 | 1546 | 1671 | 1749 | 1546 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd．Flow（perm） | 1687 | 1810 | 1599 | 1662 | 3401 |  | 1770 | 1881 | 1546 | 1671 | 1749 | 1546 |
| Peak－hour factor，PHF | 0.91 | 0.91 | 0.91 | 0.95 | 0.95 | 0.95 | 0.86 | 0.86 | 0.86 | 0.66 | 0.66 | 0.66 |
| Adj．Flow（vph） | 57 | 575 | 203 | 256 | 979 | 81 | 137 | 631 | 191 | 264 | 208 | 174 |
| RTOR Reduction（vph） | 0 | 0 | 80 | 0 | 3 | 0 | 0 | 0 | 79 | 0 | 0 | 84 |
| Lane Group Flow（vph） | 57 | 575 | 123 | 256 | 1057 | 0 | 137 | 631 | 112 | 264 | 208 | 90 |
| Heavy Vehicles（\％） | 7\％ | 5\％ | 1\％ | 5\％ | 4\％ | 16\％ | 2\％ | 1\％ | 1\％ | 8\％ | 5\％ | 1\％ |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Actuated Green，G（s） | 9.2 | 29.4 | 29.4 | 26.8 | 47.0 |  | 17.3 | 47.1 | 47.1 | 27.1 | 56.9 | 56.9 |
| Effective Green， g （ s ） | 11.2 | 33.4 | 33.4 | 28.8 | 51.0 |  | 19.3 | 49.1 | 49.1 | 29.1 | 58.9 | 58.9 |
| Actuated g／C Ratio | 0.07 | 0.21 | 0.21 | 0.18 | 0.33 |  | 0.12 | 0.31 | 0.31 | 0.19 | 0.38 | 0.38 |
| Clearance Time（s） | 6.0 | 8.0 | 8.0 | 6.0 | 8.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 120 | 386 | 341 | 306 | 1109 |  | 218 | 590 | 485 | 310 | 658 | 582 |
| v／s Ratio Prot | 0.03 | c0．32 |  | c0．15 | c0．31 |  | 0.08 | c0．34 |  | c0．16 | 0.12 |  |
| v／s Ratio Perm |  |  | 0.08 |  |  |  |  |  | 0.07 |  |  | 0.06 |
| v／c Ratio | 0.47 | 1.49 | 0.36 | 0.84 | 0.95 |  | 0.63 | 1.07 | 0.23 | 0.85 | 0.32 | 0.16 |
| Uniform Delay，d1 | 69.8 | 61.5 | 52.4 | 61.5 | 51.5 |  | 65.1 | 53.7 | 39.7 | 61.6 | 34.5 | 32.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 2.9 | 233.7 | 0.7 | 17.7 | 16.8 |  | 5.6 | 57.0 | 0.2 | 19.6 | 0.3 | 0.1 |
| Delay（s） | 72.7 | 295.2 | 53.0 | 79.2 | 68.3 |  | 70.7 | 110.7 | 39.9 | 81.1 | 34.8 | 32.4 |
| Level of Service | E | F | D | E | E |  | E | F | D | F | C | C |
| Approach Delay（s） |  | 221.2 |  |  | 70.5 |  |  | 90.9 |  |  | 53.1 |  |
| Approach LOS |  | F |  |  | E |  |  | F |  |  | D |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 106.2 | HCM 2000 Level of Service | F |
| HCM 2000 Volume to Capacity ratio | 1.08 |  | 16.0 |
| Actuated Cycle Length（s） | 156.4 | Sum of lost time（s） | F |
| Intersection Capacity Utilization | $92.5 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |

c Critical Lane Group

|  | 1 |  | $\square^{4}$ |  | $\downarrow$ | ＊ | $\cdots$ | \％ | ¢ | 7 | $\cdots$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | K | 4 | 「 | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  | 7 | 4 | 「 | ${ }^{1}$ | $\uparrow$ | F |
| Traffic Volume（vph） | 191 | 956 | 104 | 111 | 547 | 141 | 116 | 160 | 99 | 249 | 458 | 171 |
| Future Volume（vph） | 191 | 956 | 104 | 111 | 547 | 141 | 116 | 160 | 99 | 249 | 458 | 171 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 4900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（ft） | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length（ t ） | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ ft ） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（ft） |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time（s） |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.93 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles（\％） | 0\％ | 0\％ | 0\％ | 0\％ | 1\％ | 0\％ | 0\％ | 0\％ | 0\％ | 1\％ | 0\％ | 1\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 210 | 1051 | 114 | 119 | 740 | 0 | 126 | 174 | 108 | 271 | 498 | 186 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split（s） | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split（\％） | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ |  | 22．4\％ | 32．9\％ | 32．9\％ | 22．4\％ | 32．9\％ | 32．9\％ |
| Maximum Green（s） | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time（s） | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | －2．0 | －4．0 | －4．0 | －2．0 | －4．0 |  | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |
| Total Lost Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v／c Ratio | 0.67 | 1.87 | 0.21 | 0.54 | 0.85 |  | 0.55 | 0.37 | 0.23 | 0.75 | 0.83 | 0.32 |
| Control Delay | 63.2 | 426.0 | 10.6 | 65.7 | 57.8 |  | 65.3 | 44.5 | 7.4 | 64.7 | 55.3 | 15.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 63.2 | 426.0 | 10.6 | 65.7 | 57.8 |  | 65.3 | 44.5 | 7.4 | 64.7 | 55.3 | 15.5 |
| Queue Length 50th（ft） | 176 | －1428 | 8 | 100 | 326 |  | 106 | 124 | 0 | 225 | 389 | 42 |
| Queue Length 95th（ tt ） | 278 | \＃1909 | 59 | 177 | \＃525 |  | 186 | 213 | 44 | 362 | \＃646 | 118 |
| Internal Link Dist（ ft ） |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length（ ft ） | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity（vph） | 447 | 562 | 549 | 432 | 874 |  | 447 | 721 | 664 | 443 | 697 | 658 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v／c Ratio | 0.47 | 1.87 | 0.21 | 0.28 | 0.85 |  | 0.28 | 0.24 | 0.16 | 0.61 | 0.71 | 0.28 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## 2020 Build Weekday Evening Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw
Area Type:
Other

Cycle Length: 161
Actuated Cycle Length: 131.4
Natural Cycle: 130
Control Type: Actuated-Uncoordinated
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capecity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: $\quad$ 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


## 2020 Build Weekday Evening Peak Hour

3：NH Route 125 （Calef Highway）\＆NH Route 9 （Littleworth Road）／NH Route 9 （Franklin Pierce Highw

|  | ${ }^{7}$ | 4 | P | 4 | $\downarrow$ | $\cdots$ | $\leqslant$ | － | \％ | 4 | k | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | ${ }^{7}$ | 4 | 「 | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  | \％ | 4 | 「 | ${ }^{7}$ | 4 | 「 |
| Traffic Volume（vph） | 191 | 956 | 104 | 111 | 547 | 141 | 116 | 160 | 99 | 249 | 458 | 171 |
| Future Volume（vph） | 191 | 956 | 104 | 111 | 547 | 141 | 116 | 160 | 99 | 249 | 458 | 171 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Total Lost time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1805 | 1900 | 1615 | 1745 | 3471 |  | 1805 | 1900 | 1561 | 1787 | 1837 | 1546 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd．Flow（perm） | 1805 | 1900 | 1615 | 1745 | 3471 |  | 1805 | 1900 | 1561 | 1787 | 1837 | 1546 |
| Peak－hour factor，PHF | 0.91 | 0.91 | 0.91 | 0.93 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj．Flow（vph） | 210 | 1051 | 114 | 119 | 588 | 152 | 126 | 174 | 108 | 271 | 498 | 186 |
| RTOR Reduction（vph） | 0 | 0 | 72 | 0 | 14 | 0 | 0 | 0 | 81 | 0 | 0 | 77 |
| Lane Group Flow（vph） | 210 | 1051 | 42 | 119 | 726 | 0 | 126 | 174 | 27 | 271 | 498 | 109 |
| Heavy Vehicles（\％） | 0\％ | 0\％ | 0\％ | 0\％ | 1\％ | 0\％ | 0\％ | 0\％ | 0\％ | 1\％ | 0\％ | 1\％ |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Actuated Green，G（s） | 20.9 | 34.8 | 34.8 | 14.6 | 28.5 |  | 14.8 | 30.9 | 30.9 | 24.6 | 40.7 | 40.7 |
| Effective Green，g（s） | 22.9 | 38.8 | 38.8 | 16.6 | 32.5 |  | 16.8 | 32.9 | 32.9 | 26.6 | 42.7 | 42.7 |
| Actuated g／C Ratio | 0.17 | 0.30 | 0.30 | 0.13 | 0.25 |  | 0.13 | 0.25 | 0.25 | 0.20 | 0.33 | 0.33 |
| Clearance Time（s） | 6.0 | 8.0 | 8.0 | 6.0 | 8.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 315 | 563 | 478 | 221 | 861 |  | 231 | 477 | 392 | 363 | 599 | 504 |
| v／s Ratio Prot | c0．12 | c0．55 |  | 0.07 | 0.21 |  | 0.07 | 0.09 |  | c0．15 | c0．27 |  |
| v／s Ratio Perm |  |  | 0.03 |  |  |  |  |  | 0.02 |  |  | 0.07 |
| v／c Ratio | 0.67 | 1.87 | 0.09 | 0.54 | 0.84 |  | 0.55 | 0.36 | 0.07 | 0.75 | 0.83 | 0.22 |
| Uniform Delay，d1 | 50.4 | 46.1 | 33.3 | 53.6 | 46.8 |  | 53.5 | 40.4 | 37.3 | 49.0 | 40.8 | 32.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 5.3 | 396.8 | 0.1 | 2.5 | 7.6 |  | 2.6 | 0.5 | 0.1 | 8.1 | 9.6 | 0.2 |
| Delay（s） | 55.7 | 442.9 | 33.4 | 56.1 | 54.4 |  | 56.1 | 40.9 | 37.4 | 57.1 | 50.3 | 32.2 |
| Level of Service | E | F | C | E | D |  | E | D | D | E | D | C |
| Approach Delay（s） |  | 349.8 |  |  | 54.6 |  |  | 44.7 |  |  | 48.7 |  |
| Approach LOS |  | F |  |  | D |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  | 164.8 |  | HCM 2000 Level of Service |  |  |  |  | F |  |  |  |
| HCM 2000 Volume to Capacity ratio |  | 1.16 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 130.9 | Sum of lost time（s） |  |  |  |  | 16.0 |  |  |  |
| Intersection Capacity Utilization |  | 100．3\％ |  |  |  |  |  |  | G |  |  |  |
| Analysis Period（min） |  |  | 15 | ICU Level of Service |  |  |  |  |  |  |  |  |

c Critical Lane Group

## 2020 Build Saturday MIdday Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | $\ldots$ |  |  |  | $\frac{1}{\downarrow}$ | $\downarrow$ |  | $\checkmark$ | 7 | $\stackrel{\square}{5}$ | k | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | \% | $\uparrow$ | 「 | ${ }^{7}$ | 中t |  | 7 | $\uparrow$ | F | * | 4 | F |
| Traffic Volume (vph) | 109 | 510 | 104 | 133 | 625 | 156 | 148 | 239 | 153 | 141 | 192 | 132 |
| Future Volume (vph) | 109 | 510 | 104 | 133 | 625 | 156 | 148 | 239 | 153 | 141 | 192 | 132 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width ( ft ) | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length (t) | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (t) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( ft ) |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time (s) |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.80 | 0.80 | 0.80 | 0.89 | 0.89 | 0.89 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles (\%) | 0\% | 1\% | 0\% | 0\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 115 | 537 | 109 | 166 | 976 | 0 | 166 | 269 | 172 | 157 | 213 | 147 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split (\%) | 22.4\% | 22.4\% | 22.4\% | 22.4\% | 22.4\% |  | 22.4\% | 32.9\% | 32.9\% | 22.4\% | 32.9\% | 32.9\% |
| Maximum Green (s) | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | -2.0 | -4.0 | -4.0 | -2.0 | -4.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v/c Ratio | 0.47 | 0.95 | 0.19 | 0.57 | 0.83 |  | 0.56 | 0.65 | 0.40 | 0.55 | 0.55 | 0.35 |
| Control Delay | 52.2 | 66.0 | 9.3 | 51.3 | 42.2 |  | 51.1 | 47.4 | 16.8 | 51.3 | 44.8 | 13.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 52.2 | 66.0 | 9.3 | 51.3 | 42.2 |  | 51.1 | 47.4 | 16.8 | 51.3 | 44.8 | 13.6 |
| Queue Length 50th (ft) | 73 | 354 | 3 | 105 | 314 |  | 105 | 167 | 32 | 99 | 130 | 18 |
| Queue Length 95th (t) | 153 | \#789 | 53 | 179 | \#474 |  | 202 | 292 | 101 | 196 | 238 | 78 |
| Internal Link Dist (ft) |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length (ft) | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity (vph) | 545 | 568 | 559 | 527 | 1170 |  | 545 | 879 | 784 | 545 | 842 | 784 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | O | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.21 | 0.95 | 0.19 | 0.31 | 0.83 |  | 0.30 | 0.31 | 0.22 | 0.29 | 0.25 | 0.19 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Lanes, Volumes, Timings
AJA
S:Uobs181881Analysis|8188-2020SMBU.syn
Area Type: Other

Cycle Length: 161
Actuated Cycle Length: 108.2
Natural Cycle: 65
Control Type: Actuated-Uncoordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


2020 Build Saturday Mldday Peak Hour
3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | \% |  | P | , | $\downarrow$ | d | $\checkmark$ | k | $\rangle$ | $\square$ | k | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | \% | $\uparrow$ | " | * | 中 ${ }^{\text {a }}$ |  | ${ }^{7}$ | 4 | F | ${ }_{1}$ | 4 | F |
| Traffic Volume (vph) | 109 | 510 | 104 | 133 | 625 | 156 | 148 | 239 | 153 | 141 | 192 | 132 |
| Future Volume (vph) | 109 | 510 | 104 | 133 | 625 | 156 | 148 | 239 | 153 | 141 | 192 | 132 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1805 | 1881 | 1615 | 1745 | 3474 |  | 1805 | 1900 | 1561 | 1805 | 1818 | 1561 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1805 | 1881 | 1615 | 1745 | 3474 |  | 1805 | 1900 | 1561 | 1805 | 1818 | 1561 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.80 | 0.80 | 0.80 | 0.89 | 0.89 | 0.89 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 115 | 537 | 109 | 166 | 781 | 195 | 166 | 269 | 172 | 157 | 213 | 147 |
| RTOR Reduction (vph) | 0 | 0 | 71 | 0 | 11 | 0 | 0 | 0 | 90 | 0 | 0 | 90 |
| Lane Group Flow (vph) | 115 | 537 | 38 | 166 | 965 | 0 | 166 | 269 | 82 | 157 | 213 | 57 |
| Heavy Vehicles (\%) | 0\% | 1\% | 0\% | 0\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 |  |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Actuated Green, G (s) | 12.8 | 28.7 | 28.7 | 16.1 | 32.0 |  | 15.8 | 21.6 | 21.6 | 15.3 | 21.1 | 21.1 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 14.8 | 32.7 | 32.7 | 18.1 | 36.0 |  | 17.8 | 23.6 | 23.6 | 17.3 | 23.1 | 23.1 |
| Actuated g/C Ratio | 0.14 | 0.30 | 0.30 | 0.17 | 0.33 |  | 0.17 | 0.22 | 0.22 | 0.16 | 0.21 | 0.21 |
| Clearance Time (s) | 6.0 | 8.0 | 8.0 | 6.0 | 8.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 248 | 571 | 490 | 293 | 1161 |  | 298 | 416 | 342 | 289 | 389 | 334 |
| v/s Ratio Prot | 0.06 | c0.29 |  | c0.10 | c0. 28 |  | c0.09 | c0.14 |  | 0.09 | 0.12 |  |
| v/s Ratio Perm |  |  | 0.02 |  |  |  |  |  | 0.05 |  |  | 0.04 |
| v/c Ratio | 0.46 | 0.94 | 0.08 | 0.57 | 0.83 |  | 0.56 | 0.65 | 0.24 | 0.54 | 0.55 | 0.17 |
| Uniform Delay, d1 | 42.8 | 36.6 | 26.7 | 41.2 | 33.0 |  | 41.3 | 38.3 | 34.7 | 41.6 | 37.6 | 34.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.4 | 23.8 | 0.1 | 2.5 | 5.2 |  | 2.3 | 3.4 | 0.4 | 2.1 | 1.6 | 0.2 |
| Delay (s) | 44.2 | 60.4 | 26.8 | 43.7 | 38.2 |  | 43.6 | 41.7 | 35.0 | 43.6 | 39.2 | 34.7 |
| Level of Service | D | E | C | D | D |  | D | D | D | D | D | C |
| Approach Delay (s) |  | 53.1 |  |  | 39.0 |  |  | 40.3 |  |  | 39.3 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 42.9 |  | CM 2000 | evel of S | ervice |  | D |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.72 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 107.7 |  | um of lost | me (s) |  |  | 16.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 67.9\% |  | Level of | Service |  |  | C |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

C Critical Lane Group

HCM Signalized Intersection Capacity Analysis
AJA

## 2030 No Build Weekday Morning Peak Hour

3：NH Route 125 （Calef Highway）\＆NH Route 9 （Littleworth Road）／NH Route 9 （Franklin Pierce Highw

|  | $\cdots$ |  | $\mathrm{P}^{4}$ |  | $\frac{1}{1}$ | ال｜ |  |  | $\rangle$ | $\uparrow$ | $\cdots$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | 7 | 4 | 「 | k | 中 ${ }^{\text {W }}$ |  | ${ }^{7}$ | $\uparrow$ | 「 | ${ }_{1}$ | 4 | 「 |
| Traffic Volume（vph） | 57 | 540 | 206 | 255 | 1003 | 72 | 114 | 602 | 182 | 193 | 152 | 115 |
| Future Volume（vph） | 57 | 540 | 206 | 255 | 1003 | 72 | 114 | 602 | 182 | 193 | 152 | 115 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（ t ） | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length（ft） | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（ft） |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time（s） |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.95 | 0.95 | 0.95 | 0.86 | 0.86 | 0.86 | 0.66 | 0.66 | 0.66 |
| Heavy Vehicles（\％） | 7\％ | 5\％ | 1\％ | 5\％ | 4\％ | 16\％ | 2\％ | 1\％ | 1\％ | 8\％ | 5\％ | 1\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 63 | 593 | 226 | 268 | 1132 | 0 | 133 | 700 | 212 | 292 | 230 | 174 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split（s） | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split（\％） | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ |  | 22．4\％ | 32．9\％ | 32．9\％ | 22．4\％ | 32．9\％ | 32．9\％ |
| Maximum Green（s） | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time（s） | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | －2．0 | －4．0 | －4．0 | －2．0 | －4．0 |  | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |
| Total Lost Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v／c Ratio | 0.44 | 1.61 | 0.56 | 0.86 | 1.02 |  | 0.62 | 1.19 | 0.38 | 0.90 | 0.34 | 0.26 |
| Control Delay | 78.8 | 326.1 | 36.7 | 87.0 | 83.5 |  | 78.4 | 149.5 | 21.4 | 91.4 | 37.6 | 12.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 78.8 | 326.1 | 36.7 | 87.0 | 83.5 |  | 78.4 | 149.5 | 21.4 | 91.4 | 37.6 | 12.7 |
| Queue Length 50th（ ft ） | 64 | ～901 | 118 | 273 | －682 |  | 135 | ～903 | 77 | 302 | 172 | 35 |
| Queue Length 95th（ ft ） | 115 | \＃1143 | 214 | \＃416 | \＃881 |  | 193 | \＃1075 | 142 | 289 | 183 | 44 |
| Internal Link Dist（ft） |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length（ ft ） | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity（vph） | 343 | 368 | 406 | 338 | 1110 |  | 360 | 586 | 561 | 340 | 673 | 670 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v／c Ratio | 0.18 | 1.61 | 0.56 | 0.79 | 1.02 |  | 0.37 | 1.19 | 0.38 | 0.86 | 0.34 | 0.26 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Lanes，Volumes，Timings
AJA

## 2030 No Build Weekday Morning Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw
Area Type:
Other
Cycle Length: 161
Actuated Cycle Length: 157.5
Natural Cycle: 130
Control Type: Actuated-Uncoordinated
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


|  | $\cdots$ | $\uparrow$ | [ |  |  | W |  | + | 7 | $\square$ | $k$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | 7 | $\uparrow$ | \# | ${ }^{7}$ | 中t |  | \% | $\uparrow$ | 7 | 7 | $\uparrow$ | F |
| Traffic Volume (vph) | 57 | 540 | 206 | 255 | 1003 | 72 | 114 | 602 | 182 | 193 | 152 | 115 |
| Future Volume (vph) | 57 | 540 | 206 | 255 | 1003 | 72 | 114 | 602 | 182 | 193 | 152 | 115 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1687 | 1810 | 1599 | 1662 | 3410 |  | 1770 | 1881 | 1546 | 1671 | 1749 | 1546 |
| FIt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1687 | 1810 | 1599 | 1662 | 3410 |  | 1770 | 1881 | 1546 | 1671 | 1749 | 1546 |
| Peak-hour factor, PHF | 0.91 | 0.91 | 0.91 | 0.95 | 0.95 | 0.95 | 0.86 | 0.86 | 0.86 | 0.66 | 0.66 | 0.66 |
| Adj. Flow (vph) | 63 | 593 | 226 | 268 | 1056 | 76 | 133 | 700 | 212 | 292 | 230 | 174 |
| RTOR Reduction (vph) | 0 | 0 | 81 | 0 | 3 | 0 | 0 | 0 | 79 | 0 | 0 | 75 |
| Lane Group Flow (vph) | 63 | 593 | 145 | 268 | 1129 | 0 | 133 | 700 | 133 | 292 | 230 | 99 |
| Heavy Vehicles (\%) | 7\% | 5\% | 1\% | 5\% | 4\% | 16\% | 2\% | 1\% | 1\% | 8\% | 5\% | 1\% |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 |  |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Actuated Green, G (s) | 9.8 | 29.4 | 29.4 | 27.6 | 47.2 |  | 17.1 | 47.1 | 47.1 | 28.7 | 58.7 | 58.7 |
| Effective Green, $g(s)$ | 11.8 | 33.4 | 33.4 | 29.6 | 51.2 |  | 19.1 | 49.1 | 49.1 | 30.7 | 60.7 | 60.7 |
| Actuated g/C Ratio | 0.07 | 0.21 | 0.21 | 0.19 | 0.32 |  | 0.12 | 0.31 | 0.31 | 0.19 | 0.38 | 0.38 |
| Clearance Time (s) | 6.0 | 8.0 | 8.0 | 6.0 | 8.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 125 | 380 | 336 | 309 | 1099 |  | 212 | 581 | 478 | 323 | 668 | 590 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | 0.04 | c0.33 |  | c0.16 | c0.33 |  | 0.08 | c0.37 |  | c0.17 | 0.13 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  |  | 0.09 |  |  |  |  |  | 0.09 |  |  | 0.06 |
| v/c Ratio | 0.50 | 1.56 | 0.43 | 0.87 | 1.03 |  | 0.63 | 1.20 | 0.28 | 0.90 | 0.34 | 0.17 |
| Uniform Delay, d1 | 70.7 | 62.7 | 54.5 | 62.7 | 53.8 |  | 66.5 | 54.9 | 41.4 | 62.6 | 34.9 | 32.4 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.2 | 264.8 | 0.9 | 21.7 | 34.4 |  | 5.7 | 107.8 | 0.3 | 27.1 | 0.3 | 0.1 |
| Delay (s) | 73.9 | 327.5 | 55.4 | 84.4 | 88.2 |  | 72.2 | 162.6 | 41.8 | 89.7 | 35.2 | 32.5 |
| Level of Service | E | F | E | F | F |  | E | F | D | F | D | C |
| Approach Delay (s) |  | 239.7 |  |  | 87.5 |  |  | 126.6 |  |  | 57.4 |  |
| Approach LOS |  | F |  |  | F |  |  | F |  |  | , |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 125.8 |  | CM 2000 | evel of S | ervice |  | F |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 1.16 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 158.8 |  | um of lost | ime (s) |  |  | 16.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 98.3\% |  | CU Level | Service |  |  | F |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
AJA

## 2030 No Build Weekday Evening Peak Hour

3：NH Route 125 （Calef Highway）\＆NH Route 9 （Littleworth Road）／NH Route 9 （Franklin Pierce Highw

|  | $\cdots$ | $\dagger$ | $\rho^{3}$ |  | $\ddagger$ | \％ | $\cdots$ | ， | $\rangle$ | 7 | k | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | ${ }^{7}$ | 中 | 「 | 4 | 中t |  | 4 | 4 | 「 | 7 | 4 | 「 |
| Traffic Volume（vph） | 211 | 1026 | 216 | 110 | 562 | 137 | 109 | 177 | 110 | 275 | 507 | 123 |
| Future Volume（vph） | 211 | 1026 | 216 | 110 | 562 | 137 | 109 | 177 | 110 | 275 | 507 | 123 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（ft） | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length（ft） | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ ft ） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（ ft ） |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time（s） |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.93 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles（\％） | 0\％ | 0\％ | 0\％ | 0\％ | 1\％ | 0\％ | 0\％ | 0\％ | 0\％ | 1\％ | 0\％ | 1\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 232 | 1127 | 237 | 118 | 751 | 0 | 118 | 192 | 120 | 299 | 551 | 134 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（ $s$ ） | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split（s） | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split（\％） | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ |  | 22．4\％ | 32．9\％ | 32．9\％ | 22．4\％ | 32．9\％ | 32．9\％ |
| Maximum Green（s） | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time（s） | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | －2．0 | －4．0 | －4．0 | －2．0 | －4．0 |  | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |
| Total Lost Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v／c Ratio | 0.72 | 2.04 | 0.44 | 0.56 | 0.91 |  | 0.55 | 0.39 | 0.24 | 0.80 | 0.86 | 0.22 |
| Control Delay | 67.2 | 501.7 | 26.1 | 68.4 | 66.5 |  | 68.1 | 46.0 | 9.3 | 69.3 | 56.6 | 9.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 67.2 | 501.7 | 26.1 | 68.4 | 66.5 |  | 68.1 | 46.0 | 9.3 | 69.3 | 56.6 | 9.2 |
| Queue Length 50th（ ft ） | 199 | ～1589 | 96 | 102 | 343 |  | 102 | 146 | 3 | 251 | 455 | 11 |
| Queue Length 95th（ ft ） | 306 | \＃2050 | 197 | 176 | \＃534 |  | 176 | 235 | 56 | \＃421 | \＃755 | 63 |
| Internal Link Dist（ft） |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length（ ft ） | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity（vph） | 422 | 552 | 542 | 408 | 827 |  | 422 | 681 | 633 | 418 | 658 | 628 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v／c Ratio | 0.55 | 2.04 | 0.44 | 0.29 | 0.91 |  | 0.28 | 0.28 | 0.19 | 0.72 | 0.84 | 0.21 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Lanes，Volumes，Timings
AJA

## 2030 No Build Weekday Evening Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw
Area Type:
Other
Cycle Lengith: 161
Actuated Cycle Length: 137.5
Natural Cycle: 140
Control Type: Actuated-Uncoordinated
~ Volume exceeds capacity, queue is theorefically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


c Critical Lane Group

3：NH Route 125 （Calef Highway）\＆NH Route 9 （Littleworth Road）／NH Route 9 （Franklin Pierce Highw

|  | $k$ | ¢ | ［ |  | $\downarrow$ | W | $\cdots$ | $y$ | $\rangle$ | $F$ | $\cdots$ | $4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | ${ }^{4}$ | $\uparrow$ | F | ${ }^{7}$ | 中t |  | \％ | 中 | F＇ | 7 | 中 | 「 |
| Traffic Volume（vph） | 121 | 535 | 115 | 137 | 665 | 157 | 147 | 266 | 169 | 157 | 213 | 135 |
| Future Volume（vph） | 121 | 535 | 115 | 137 | 665 | 157 | 147 | 266 | 169 | 157 | 213 | 135 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（ft） | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length（ft） | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（ ft ） |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time（s） |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.80 | 0.80 | 0.80 | 0.89 | 0.89 | 0.89 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles（\％） | 0\％ | 1\％ | 0\％ | 0\％ | 1\％ | 0\％ | 0\％ | 0\％ | 0\％ | 0\％ | 1\％ | 0\％ |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 127 | 563 | 121 | 171 | 1027 | 0 | 165 | 299 | 190 | 174 | 237 | 150 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split（s） | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split（\％） | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ |  | 22．4\％ | 32．9\％ | 32．9\％ | 22．4\％ | 32．9\％ | 32．9\％ |
| Maximum Green（s） | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time（s） | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | －2．0 | －4．0 | －4．0 | －2．0 | －4．0 |  | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |
| Total Lost Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v／c Ratio | 0.50 | 1.04 | 0.22 | 0.59 | 0.93 |  | 0.57 | 0.68 | 0.42 | 0.58 | 0.55 | 0.33 |
| Control Delay | 55.3 | 89.9 | 11.9 | 54.5 | 53.1 |  | 54.4 | 48.9 | 18.9 | 54.2 | 44.1 | 13.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 55.3 | 89.9 | 11.9 | 54.5 | 53.1 |  | 54.4 | 48.9 | 18.9 | 54.2 | 44.1 | 13.2 |
| Queue Length 50th（ ft ） | 86 | $\sim 440$ | 10 | 115 | 370 |  | 111 | 196 | 43 | 117 | 149 | 20 |
| Queue Length 95th（ ft ） | 176 | \＃915 | 69 | 194 | \＃585 |  | 213 | 336 | 122 | 226 | 269 | 82 |
| Internal Link Dist（ft） |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length（ ft ） | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity（vph） | 521 | 543 | 539 | 504 | 1110 |  | 521 | 840 | 754 | 521 | 804 | 754 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v／c Ratio | 0.24 | 1.04 | 0.22 | 0.34 | 0.93 |  | 0.32 | 0.36 | 0.25 | 0.33 | 0.29 | 0.20 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## 2030 No Build Saturday Midday Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw
Area Type:
Other
Cycle Length: 161
Actuated Cycle Length: 113.7
Natural Cycle: 70
Control Type: Actuated-Uncoordinated
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw


C Critical Lane Group

HCM Signalized Intersection Capacity Analysis
AJA

## 2030 Build Weekday Morning Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | ${ }^{*}$ |  | pren |  |  | J |  | , | خ | 5 | k | $\dagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | \% | $\uparrow$ | F | \% | 中t |  | \% | $\uparrow$ | $\bar{\square}$ | \% | 4 | F |
| Traffic Volume (vph) | 57 | 571 | 206 | 262 | 1022 | 83 | 124 | 602 | 182 | 193 | 152 | 123 |
| Future Volume (vph) | 57 | 571 | 206 | 262 | 1022 | 83 | 124 | 602 | 182 | 193 | 152 | 123 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  | 0.989 |  |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1687 | 1810 | 1599 | 1662 | 3404 | 0 | 1770 | 1881 | 1546 | 1671 | 1749 | 1546 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 1687 | 1810 | 1599 | 1662 | 3404 | 0 | 1770 | 1881 | 1546 | 1671 | 1749 | 1546 |
| Satd. Flow (RTOR) |  |  | 102 |  | 5 |  |  |  | 115 |  |  | 130 |
| Adj. Flow (vph) | 63 | 627 | 226 | 276 | 1076 | 87 | 144 | 700 | 212 | 292 | 230 | 186 |
| Lane Group Flow (vph) | 63 | 627 | 226 | 276 | 1163 | 0 | 144 | 700 | 212 | 292 | 230 | 186 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | - |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split (\%) | 22.4\% | 22.4\% | 22.4\% | 22.4\% | 22.4\% |  | 22.4\% | 32.9\% | 32.9\% | 22.4\% | 32.9\% | 32.9\% |
| Maximum Green (s) | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | -2.0 | -4.0 | -4.0 | -2.0 | -4.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v/c Ratio | 0.44 | 1.71 | 0.56 | 0.87 | 1.04 |  | 0.64 | 1.20 | 0.38 | 0.90 | 0.35 | 0.28 |
| Control Delay | 78.9 | 366.7 | 36.8 | 88.9 | 89.5 |  | 78.4 | 151.1 | 21.5 | 91.8 | 38.6 | 13.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 78.9 | 366.7 | 36.8 | 88.9 | 89.5 |  | 78.4 | 151.1 | 21.5 | 91.8 | 38.6 | 13.0 |
| Queue Length 50th (ft) | 64 | -975 | 118 | 283 | $\sim 718$ |  | 147 | -903 | 77 | 302 | 174 | 38 |
| Queue Length 95th (ti) | 115 | \#1222 | 214 | \#436 | \#915 |  | 205 | \#1075 | 142 | 289 | 186 | 46 |
| Internal Link Dist (ft) |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length (tt) | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity (vph) | 342 | 367 | 405 | 337 | 1114 |  | 359 | 584 | 559 | 339 | 660 | 664 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.18 | 1.71 | 0.56 | 0.82 | 1.04 |  | 0.40 | 1.20 | 0.38 | 0.86 | 0.35 | 0.28 |

## Intersection Summary

Cycle Length: 161
Actuated Cycle Length: 157.9
Natural Cycle: 130
Control Type: Actuated-Uncoordinated

Lanes, Volumes, Timings
AJA

## 2030 Build Weekday Morning Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.


2030 Build Weekday Morning Peak Hour
3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | \% | $\uparrow$ | per | W | $\downarrow$ | l | $\checkmark$ | , | * | $\square$ | k | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | \% | $\uparrow$ | 「 | 7 | 中t |  | 7 | $\uparrow$ | 7 | \% | $\uparrow$ | $\stackrel{1}{7}$ |
| Traffic Volume (vph) | 57 | 571 | 206 | 262 | 1022 | 83 | 124 | 602 | 182 | 193 | 152 | 123 |
| Future Volume (vph) | 57 | 571 | 206 | 262 | 1022 | 83 | 124 | 602 | 182 | 193 | 152 | 123 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Sald. Flow (prot) | 1687 | 1810 | 1599 | 1662 | 3403 |  | 1770 | 1881 | 1546 | 1671 | 1749 | 1546 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1687 | 1810 | 1599 | 1662 | 3403 |  | 1770 | 1881 | 1546 | 1671 | 1749 | 1546 |
| Peak-hour factor, PHF | 0.91 | 0.91 | 0.91 | 0.95 | 0.95 | 0.95 | 0.86 | 0.86 | 0.86 | 0.66 | 0.66 | 0.66 |
| Adj. Flow (vph) | 63 | 627 | 226 | 276 | 1076 | 87 | 144 | 700 | 212 | 292 | 230 | 186 |
| RTOR Reduction (vph) | 0 | 0 | 81 | 0 | 3 | 0 | 0 | 0 | 80 | 0 | 0 | 81 |
| Lane Group Flow (vph) | 63 | 627 | 145 | 276 | 1160 | 0 | 144 | 700 | 132 | 292 | 230 | 105 |
| Heavy Vehicles (\%) | 7\% | 5\% | 1\% | 5\% | 4\% | 16\% | 2\% | 1\% | 1\% | 8\% | 5\% | 1\% |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | , |  |  | 8 |
| Actuated Green, G (s) | 9.8 | 29.3 | 29.3 | 28.0 | 47.5 |  | 18.1 | 47.1 | 47.1 | 28.7 | 57.7 | 57.7 |
| Effective Green, g (s) | 11.8 | 33.3 | 33.3 | 30.0 | 51.5 |  | 20.1 | 49.1 | 49.1 | 30.7 | 59.7 | 59.7 |
| Actuated g/C Ratio | 0.07 | 0.21 | 0.21 | 0.19 | 0.32 |  | 0.13 | 0.31 | 0.31 | 0.19 | 0.38 | 0.38 |
| Clearance Time (s) | 6.0 | 8.0 | 8.0 | 6.0 | 8.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (voh) | 125 | 378 | 334 | 313 | 1101 |  | 223 | 580 | 477 | 322 | 656 | 580 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | 0.04 | c0.35 |  | c0.17 | c0.34 |  | 0.08 | c0.37 |  | c0.17 | 0.13 |  |
| v/s Ratio Perm |  |  | 0.09 |  |  |  |  |  | 0.09 |  |  | 0.07 |
| v/c Ratio | 0.50 | 1.66 | 0.44 | 0.88 | 1.05 |  | 0.65 | 1.21 | 0.28 | 0.91 | 0.35 | 0.18 |
| Uniform Delay, d1 | 70.8 | 62.9 | 54.7 | 62.8 | 53.8 |  | 66.1 | 55.0 | 41.6 | 62.8 | 35.8 | 33.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.2 | 308.0 | 0.9 | 23.9 | 42.3 |  | 6.3 | 108.6 | 0.3 | 27.6 | 0.3 | 0.2 |
| Delay (s) | 74.0 | 370.9 | 55.6 | 86.7 | 96.1 |  | 72.4 | 163.6 | 41.9 | 90.4 | 36.1 | 33.5 |
| Level of Service | E | F | E | F | F |  | E | F | D | F | D | C |
| Approach Delay (s) |  | 272.7 |  |  | 94.3 |  |  | 126.7 |  |  | 57.8 |  |
| Approach LOS |  | F |  |  | F |  |  | F |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 136.0 |  | M 2000 | evel of S | rvice |  | F |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 1.19 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 159.1 |  | of lost | me (s) |  |  | 16.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 100.3\% |  | Level or | Service |  |  | G |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

## 2030 Build Weekday Evening Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | \% | $\dagger$ | P | L | $\frac{1}{\square}$ | $\cdots$ | $\cdots$ | , | \% | $\uparrow$ | * | $4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | ${ }^{7}$ | 4 | ${ }^{+1}$ | ${ }^{7}$ | 中 $\uparrow$ |  | ${ }^{7}$ | + | T | ${ }^{7}$ | 4 | 「 |
| Traffic Volume (vph) | 211 | 1051 | 216 | 119 | 598 | 151 | 124 | 177 | 110 | 275 | 507 | 131 |
| Future Volume (vph) | 211 | 1051 | 216 | 119 | 598 | 151 | 124 | 177 | 110 | 275 | 507 | 131 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Storage Length ( ft ) | 150 |  | 150 | 150 |  | 0 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( ft ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( ft ) |  | 283 |  |  | 2648 |  |  | 562 |  |  | 661 |  |
| Travel Time (s) |  | 6.4 |  |  | 60.2 |  |  | 12.8 |  |  | 15.0 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.93 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 1\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 232 | 1155 | 237 | 128 | 805 | 0 | 135 | 192 | 120 | 299 | 551 | 142 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split (s) | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split (\%) | 22.4\% | 22.4\% | 22.4\% | 22.4\% | 22.4\% |  | 22.4\% | 32.9\% | 32.9\% | 22.4\% | 32.9\% | 32.9\% |
| Maximum Green (s) | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | -2.0 | -4.0 | -4.0 | -2.0 | -4.0 |  | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v/c Ratio | 0.72 | 2.16 | 0.45 | 0.58 | 0.99 |  | 0.58 | 0.38 | 0.24 | 0.81 | 0.86 | 0.23 |
| Control Delay | 68.3 | 552.9 | 27.2 | 69.1 | 80.4 |  | 68.8 | 45.5 | 9.1 | 70.8 | 58.4 | 10.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 68.3 | 552.9 | 27.2 | 69.1 | 80.4 |  | 68.8 | 45.5 | 9.1 | 70.8 | 58.4 | 10.4 |
| Queue Length 50th (ft) | 201 | ~1674 | 99 | 112 | 381 |  | 118 | 147 | 3 | 255 | 464 | 16 |
| Queue Length 95th (ft) | 310 | \#2159 | 203 | 189 | \#607 |  | 198 | 234 | 55 | \#430 | \#771 | 72 |
| Internal Link Dist (ft) |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length (ft) | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity (vph) | 417 | 535 | 528 | 403 | 817 |  | 417 | 673 | 627 | 413 | 651 | 622 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.56 | 2.16 | 0.45 | 0.32 | 0.99 |  | 0.32 | 0.29 | 0.19 | 0.72 | 0.85 | 0.23 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## 2030 Build Weekday Evening Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw
Area Type: Other
Cycle Length: 161
Actuated Cycle Length: 139.1
Natural Cycle: 150
Control Type: Actuated-Uncoordinated
~ Volume exceeds capecity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


2030 Build Weekday Evening Peak Hour
3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

c Critical Lane Group

3：NH Route 125 （Calef Highway）\＆NH Route 9 （Littleworth Road）／NH Route 9 （Franklin Pierce Highw

|  | \％ | $\uparrow$ | P | 参 | $\frac{1}{\dagger}$ | W |  | $y$ | $\rangle$ | $\uparrow$ | k | $4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | ${ }^{7}$ | 4 | 7 | ${ }^{*}$ | 中 ${ }^{\text {d }}$ |  | ${ }^{4}$ | 中 | ri | ${ }^{7}$ | 4 | T |
| Traffic Volume（vph） | 121 | 559 | 115 | 144 | 686 | 169 | 160 | 266 | 169 | 157 | 213 | 143 |
| Future Volume（vph） | 121 | 559 | 115 | 144 | 686 | 169 | 160 | 266 | 169 | 157 | 213 | 143 |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  | 0.970 |  |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1805 | 1881 | 1615 | 1745 | 3474 | 0 | 1805 | 1900 | 1561 | 1805 | 1818 | 1561 |
| FIt Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（perm） | 1805 | 1881 | 1615 | 1745 | 3474 | 0 | 1805 | 1900 | 1561 | 1805 | 1818 | 1561 |
| Satd．Flow（RTOR） |  |  | 102 |  | 17 |  |  |  | 115 |  |  | 115 |
| Adj．Flow（vph） | 127 | 588 | 121 | 180 | 858 | 211 | 180 | 299 | 190 | 174 | 237 | 159 |
| Lane Group Flow（vph） | 127 | 588 | 121 | 180 | 1069 | 0 | 180 | 299 | 190 | 174 | 237 | 159 |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 |  | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 |  | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 |  | 11.0 | 18.0 | 18.0 | 11.0 | 18.0 | 18.0 |
| Total Split（s） | 36.0 | 36.0 | 36.0 | 36.0 | 36.0 |  | 36.0 | 53.0 | 53.0 | 36.0 | 53.0 | 53.0 |
| Total Split（\％） | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ | 22．4\％ |  | 22．4\％ | 32．9\％ | 32．9\％ | 22．4\％ | 32．9\％ | 32．9\％ |
| Maximum Green（s） | 30.0 | 28.0 | 28.0 | 30.0 | 28.0 |  | 30.0 | 47.0 | 47.0 | 30.0 | 47.0 | 47.0 |
| Yellow Time（s） | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust（s） | －2．0 | －4．0 | －4．0 | －2．0 | －4．0 |  | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 | －2．0 |
| Total Lost Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lead／Lag | Lead | Lag | Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min | Min | None | Min |  | None | None | None | None | None | None |
| v／c Ratio | 0.51 | 1.09 | 0.23 | 0.60 | 0.95 |  | 0.59 | 0.68 | 0.42 | 0.58 | 0.57 | 0.36 |
| Control Delay | 56.0 | 106.2 | 12.1 | 54.8 | 57.1 |  | 54.6 | 49.4 | 19.1 | 54.8 | 46.1 | 15.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 56.0 | 106.2 | 12.1 | 54.8 | 57.1 |  | 54.6 | 49.4 | 19.1 | 54.8 | 46.1 | 15.0 |
| Queue Length 50th（ft） | 87 | $\sim 486$ | 10 | 122 | 394 |  | 122 | 198 | 44 | 118 | 153 | 25 |
| Queue Length 95th（ft） | 177 | \＃977 | 69 | 204 | \＃623 |  | 231 | 339 | 123 | 228 | 275 | 93 |
| Internal Link Dist（ft） |  | 203 |  |  | 2568 |  |  | 482 |  |  | 581 |  |
| Turn Bay Length（ ft ） | 150 |  | 150 | 150 |  |  | 100 |  | 100 | 100 |  | 100 |
| Base Capacity（vph） | 517 | 539 | 535 | 500 | 1121 |  | 517 | 834 | 749 | 517 | 797 | 749 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v／c Ratio | 0.25 | 1.09 | 0.23 | 0.36 | 0.95 |  | 0.35 | 0.36 | 0.25 | 0.34 | 0.30 | 0.21 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 161 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 114.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |

Lanes，Volumes，Timings
AJA

## 2030 Build Saturday Mldday Peak Hour

3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highway)


3: NH Route 125 (Calef Highway) \& NH Route 9 (Littleworth Road)/NH Route 9 (Franklin Pierce Highw

|  | ${ }^{7}$ | 4 | P | $\checkmark$ | $\downarrow$ | $\checkmark$ | $\cdots$ | $\checkmark$ | 7 | 5 | k | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations | \% | $\uparrow$ | 「 | \% | $\uparrow \psi^{6}$ |  | \% | $\uparrow$ | 「 | ${ }^{4}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 121 | 559 | 115 | 144 | 686 | 169 | 160 | 266 | 169 | 157 | 213 | 143 |
| Future Volume (vph) | 121 | 559 | 115 | 144 | 686 | 169 | 160 | 266 | 169 | 157 | 213 | 143 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 12 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 11 | 12 | 11 | 11 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1805 | 1881 | 1615 | 1745 | 3475 |  | 1805 | 1900 | 1561 | 1805 | 1818 | 1561 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1805 | 1881 | 1615 | 1745 | 3475 |  | 1805 | 1900 | 1561 | 1805 | 1818 | 1561 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.80 | 0.80 | 0.80 | 0.89 | 0.89 | 0.89 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 127 | 588 | 121 | 180 | 858 | 211 | 180 | 299 | 190 | 174 | 237 | 159 |
| RTOR Reduction (vph) | 0 | 0 | 73 | 0 | 12 | 0 | 0 | 0 | 88 | 0 | 0 | 89 |
| Lane Group Flow (vph) | 127 | 588 | 48 | 180 | 1057 | 0 | 180 | 299 | 102 | 174 | 237 | 70 |
| Heavy Vehicles (\%) | 0\% | 1\% | 0\% | 0\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% |
| Turn Type | Prot | NA | Perm | Prot | NA |  | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Actuated Green, G (s) | 13.9 | 28.8 | 28.8 | 17.7 | 32.6 |  | 17.3 | 24.6 | 24.6 | 16.9 | 24.2 | 24.2 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 15.9 | 32.8 | 32.8 | 19.7 | 36.6 |  | 19.3 | 26.6 | 26.6 | 18.9 | 26.2 | 26.2 |
| Actuated g/C Ratio | 0.14 | 0.29 | 0.29 | 0.17 | 0.32 |  | 0.17 | 0.23 | 0.23 | 0.17 | 0.23 | 0.23 |
| Clearance Time (s) | 6.0 | 8.0 | 8.0 | 6.0 | 8.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 251 | 541 | 464 | 301 | 1115 |  | 305 | 443 | 364 | 299 | 417 | 358 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | 0.07 | c0.31 |  | c0.10 | c0.30 |  | c0.10 | c0.16 |  | 0.10 | 0.13 |  |
| v/s Ratio Perm |  |  | 0.03 |  |  |  |  |  | 0.07 |  |  | 0.05 |
| v/c Ratio | 0.51 | 1.09 | 0.10 | 0.60 | 0.95 |  | 0.59 | 0.67 | 0.28 | 0.58 | 0.57 | 0.20 |
| Uniform Delay, d1 | 45.4 | 40.6 | 29.8 | 43.5 | 37.8 |  | 43.7 | 39.8 | 35.8 | 43.9 | 38.9 | 35.4 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.6 | 64.4 | 0.1 | 3.2 | 15.9 |  | 3.0 | 4.0 | 0.4 | 2.9 | 1.8 | 0.3 |
| Delay (s) | 47.0 | 105.0 | 29.9 | 46.7 | 53.7 |  | 46.7 | 43.8 | 36.3 | 46.8 | 40.7 | 35.7 |
| Level of Service | D | F | C | D | D |  | D | D | D | D | D | D |
| Approach Delay (s) |  | 85.3 |  |  | 52.7 |  |  | 42.5 |  |  | 41.1 |  |
| Approach LOS |  | F |  |  | D |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 56.8 |  | CM 2000 | evel of S | ervice |  | E |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.78 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 114.0 |  | um of lost | me (s) |  |  | 16.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 73.4\% |  | CU Level of | Service |  |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement W | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | \% |  | F |  |  | 4 |
| Traffic Vol, veh/h | 14 | 15 | 614 | 23 | 32 | 1197 |
| Future Vol, veh/h | 14 | 15 | 614 | 23 | 32 | 1197 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stop | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 15 | 16 | 667 | 25 | 35 | 1301 |


| Major/Minor | Minor1 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 2051 | 680 | 0 | 0 | 692 | 0 |
| $\quad$ Stage 1 | 680 | - | - | - | - | - |
| $\quad$ Stage 2 | 1371 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | -4.12 | - |  |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | -2.218 | - |  |
| Pot Cap-1 Maneuver | 61 | 451 | - | - | 903 | - |
| $\quad$ Stage 1 | 503 | - | - | - | - | - |
| $\quad$ Stage 2 | 236 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 52 | 451 | - | - | 903 | - |
| Mov Cap-2 Maneuver | 52 | - | - | - | - | - |
| $\quad$ Stage 1 | 503 | - | - | - | - | - |
| Stage 2 | 203 | - | - | - | - | - |
|  |  |  |  |  |  |  |



|  |  | Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | \% |  | t |  |  | 4 |
| Traffic Vol, veh/h | 29 | 37 | 1162 | 21 | 24 | 665 |
| Future Vol, veh/h | 29 | 37 | 1162 | 21 | 24 | 665 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 32 | 40 | 1263 | 23 | 26 | 723 |





| Approach | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 35.4 | 0 | 0.3 |
| HCM LOS | E |  |  |


| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | - | 162 | 834 |
| HCM Lane V/C Ratio | - | - | - |  |
| HCM Control Delay (s) | - | - | 35.4 | 0.031 |







| Major/Minor | Minor1 | Major1 |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1826 | 846 | 0 | 0 | 857 | 0 |
| Stage 1 | 846 | - | - | - | - |  |
| Stage 2 | 980 | - | - | - | - |  |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 |  |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 |  |
| Pot Cap-1 Maneuver | 85 | 362 | - | - | 783 |  |
| Stage 1 | 421 | - | - | - | - |  |
| Stage 2 | 364 | - | - | - | - |  |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 79 | 362 | - | - | 783 |  |
| Mov Cap-2 Maneuver | 79 | - | - | - | - | - |
| Stage 1 | 421 |  | - | - | - | - |
| Stage 2 | 339 | - | - | - | - | - |


| Approach | WB | NB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 45.6 | 0 | 0.3 |
| HCM LOS | E |  |  |


| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | -132 | 783 | - |
| HCM Lane V/C Ratio | - | -0.338 | 0.033 | - |
| HCM Control Delay (s) | - | - | 45.6 | 9.8 |
| HCM Lane LOS | - | - | E | A |
| HCM 95th \%bile Q(veh) | - | - | 1.4 | 0.1 |
| H |  |  |  |  |

## 2030 Build Weekday Morning Peak Hour

5: NH Route 125 (Calef Highway) \& South Site Driveway



| Approach | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 90.1 | 0 | 0.2 |
| HCM LOS | F |  |  |


| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | - | - | 85 | 895 | - |
| HCM Lane V/C Ratio | - | - | 0.55 | 0.039 | - |
| HCM Control Delay (s) | - | - | 90.1 | 9.2 | 0 |
| HCM Lane LOS | - | - | F | A | A |
| HCM 95th \%tile Q(veh) | - | - | 2.4 | 0.1 | - |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 6.7 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | M |  | F |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 38 | 40 | 1143 | 35 | 27 | 667 |
| Future Vol, veh/h | 38 | 40 | 1143 | 35 | 27 | 667 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stop | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 41 | 43 | 1242 | 38 | 29 | 725 |


| Major/Minor | Minor1 | Major1 | Major2 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 2044 | 1261 | 0 | 0 | 1280 | 0 |
| $\quad$ Stage 1 | 1261 | - | - | - | - | - |
| $\quad$ Stage 2 | 783 | - | - | - | - | - |
| Critcal Hdwy | 6.42 | 6.22 | - | - | -12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | -2.218 | - |  |
| Pot Cap-1 Maneuver | 62 | 208 | - | - | 542 | - |
| $\quad$ Stage 1 | 267 | - | - | - | - | - |
| $\quad$ Stage 2 | 450 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - | - |  |
| Mov Cap-1 Maneuver | 56 | 208 | - | - | 542 | - |
| Mov Cap-2 Maneuver | 56 | - | - | - | - | - |
| $\quad$ Stage 1 | 267 | - | - | - | - | - |
| $\quad$ Stage 2 | 410 | - | - | - | - | - |


| Approach | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, $s$ | 162.8 | 0 | 0.5 |
| HCM LOS | F |  |  |


| Minor Lane/Major Mvmt | NBT | NBRWBL_n1 | SBL | SBT |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | -90 | 542 | - |
| HCM Lane V/C Ratio | - | -0.942 | 0.054 | - |
| HCM Control Delay (s) | - | -162.8 | 12 | 0 |
| HCM Lane LOS | - | - | F | B |
| HCM 95th \%tile Q(veh) | - | - | A.3 | 0.2 |

## 5: NH Route 125 (Calef Highway) \& South Site Driveway

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :--- |



## 2030 Build Weekday Morning Peak Hour

## 5: NH Route 125 (Calef Highway) \& South Site Driveway



## 2030 Build Weekday Evening Peak Hour

## 5: NH Route 125 (Calef Highway) \& South Site Driveway



| Major/Minor | Minor1 | Major1 | Major2 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 2135 | 1280 | 0 | 0 | 1299 | 0 |
| $\quad$ Stage 1 | 1280 | - | - | - | - | - |
| $\quad$ Stage 2 | 855 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | -2.218 | - |  |
| Pot Cap-1 Maneuver | 54 | 202 | - | - | 533 | - |
| $\quad$ Stage 1 | 261 | - | - | - | - | - |
| $\quad$ Stage 2 | 417 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 49 | 202 | - | - | 533 | - |
| Mov Cap-2 Maneuver | 49 | - | - | - | - | - |
| $\quad$ Stage 1 | 261 | - | - | - | - | - |
| $\quad$ Stage 2 | 376 | - | - | - | - | - |
|  |  |  |  |  |  |  |


| Approach | WB | NB | SB |
| :--- | ---: | :---: | ---: |
| HCM Control Delay, s 210.6 | 0 | 0.4 |  |
| HCM LOS | F |  |  |



|  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Intersection |  |  |  |  |  |  |
| Int Delay, s/veh | 2.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Yr |  | F |  |  | 4 |
| Traffic Vol, veh/h | 31 | 25 | 767 | 34 | 26 | 848 |
| Future Vol, veh/h | 31 | 25 | 767 | 34 | 26 | 848 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 34 | 27 | 834 | 37 | 28 | 922 |


|  | Minor1 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Major/Minor | Major1 | Major2 |  |  |  |  |
| Conflicting Flow All | 1831 | 853 | 0 | 0 | 871 | 0 |
| $\quad$ Stage 1 | 853 | - | - | - | - | - |
| $\quad$ Stage 2 | 978 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | -2.218 | - |  |
| Pot Cap-1 Maneuver | 84 | 359 | - | - | 774 | - |
| $\quad$ Stage 1 | 418 | - | - | - | - | - |
| $\quad$ Stage 2 | 364 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 78 | 359 | - | - | 774 | - |
| Mov Cap-2 Maneuver | 78 | - | - | - | - | - |
| $\quad$ Stage 1 | 418 | - | - | - | - | - |
| Stage 2 | 337 | - | - | - | - | - |
|  |  |  |  |  |  |  |


Guidelines for Major-Road Left-Turn Lane (NORTH).xls
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.
Guidelines for Major-Road Left-Turn Lane (NORTH).xls
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.
CALIBRATION CONSTANTS

Guidelines for Major-Road Left-Turn Lane (NORTH)
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.
2-lane roadway (English)
INPUT

Guidelines for Major-Road Left-Turn Lane (NORTH)
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

Guidelines for Major-Road Left-Turn Lane (NORTH)
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.
2-lane roadway (English) INPUT

Guidelines for Major-Road Left-Turn Lane (NORTH)
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.
2-lane roadway (English)

Guidelines for Major-Road Left-Turn Lane (SOUTH)
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.
Guidelines for Major-Road Left-Turn Lane (SOUTH)
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

 INPUT
Guidelines for Major-Road Left-Turn Lane (SOUTH)
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.
2-lane roadway (English)
INPUT

OUTPUT

CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, $\mathbf{s}:$ | 3.0 |
| Critical headway, $\mathbf{s}:$ | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, $\mathbf{s}:$ | 1.9 |

Guidelines for Major-Road Left-Turn Lane (SOUTH)
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.
2-lane roadway (English)

CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, $\mathbf{s}$ : | 3.0 |
| Critical headway, $\mathbf{s}:$ | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, $\mathbf{s}:$ | 1.9 |

Guidelines for Major-Road Left-Turn Lane (SOUTH)
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.
2-lane roadway (English)
INPUT

Guidelines for Major-Road Left-Turn Lane (SOUTH)
Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.
2-lane roadway (English)
INPUT

-
OUTPUT

Guidelines for Major-Road Right-Turn Lane (NORTH)
Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

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Guidelines for Major-Road Right-Turn Lane (NORTH)
Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

Guidelines for Major-Road Right-Turn Lane (NORTH)
Guidelines for Major-Road Right-Turn Lane (NORTH)

Guidelines for Major-Road Right-Turn Lane (SOUTH)
Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

Guidelines for Major-Road Right-Turn Lane (SOUTH)

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

Guidelines for Major-Road Right-Turn Lane (SOUTH)
Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

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Guidelines for Major-Road Right-Turn Lane (SOUTH)
Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.



[^0]:    ${ }^{1}$ Trip Generation, $10{ }^{\text {th }}$ Edition; Institute of Transportation Engineers; Washington, DC; 2017.

[^1]:    ${ }^{2}$ Manual on Uniform Traffic Control Devices (MUTCD); Federal Highway Administration; Washington, D.C.; 2009.

[^2]:    ${ }^{3}$ A minimum combined travel lane and paved shoulder width of 14 -feet is required to support bicycle travel in a shared traveled-way condition.

[^3]:    ${ }^{4}$ Ibid 1.

[^4]:    ${ }^{5}$ Ibid 1.
    ${ }^{6}$ Trip Generation Handbook, $3{ }^{\text {rd }}$ Edition, A Recommended Practice of the Institute of Transportation Engineers; Institute of Transportation Engineers; Washington, D.C.; September 2017.

[^5]:    ${ }^{7}$ The capacity analysis methodology is based on the concepts and procedures presented in the Highway Capacity Manual; Transportation Research Board; Washington, DC; 2010.

[^6]:    ${ }^{8}$ Highway Capacity Manual; Transportation Research Board; Washington, DC; 2010.

[^7]:    ${ }^{9}$ A Policy on Geometric Design of Highway and Streets, $7^{\text {th }}$ Edition; American Association of State Highway and Transportation Officials (AASHTO); 2018.

[^8]:    ${ }^{\text {a }}$ Recommended minimum values obtained from A Policy on Geometric Design of Highways and Streets, $7^{\text {th }}$ Edition; American Association of State Highway and Transportation Officials (AASHTO); 2018 and based on 60 mph approach speed along NH Route 125.
    ${ }^{\text {b }}$ Values shown are the intersection sight distance for a vehicle turning left or right exiting a roadway under STOP control such that motorists approaching the intersection on the major street should not need to adjust their travel speed to less than 70 percent of their initial approach speed.
    ${ }^{\text {c }}$ With regrading of the embankment along the east side of NH Route 125 north of the Project site roadway.

[^9]:    ${ }^{10}$ NCHRP Report 457 - Evaluating Intersection Improvement: An Engineering Study Guide, National Cooperative Highway Research Program; 2001.

[^10]:    ${ }^{11}$ Ibid 1.

[^11]:    ${ }^{12}$ Ibid 2.

[^12]:    N/S Street : Route 125 City/State : Barrington, NH

    Weather : Clear

[^13]:    1) LUC 853 (Convenience Market with Gasoline Pumps), 12 vehicle fueling positions (rate method)
    2) $\mathbf{1 0 \%}$ (AM) and $3 \%$ (PM) capture rate method calculated from SGP 2022 No-Build traffic projections
    3) Less $34 \%$ of donut shop trips due to the convenience store walk-in customers
    4) LUC 853 pass-by rate $=63 \%(\mathrm{AM}), 66 \%(\mathrm{PM})$; Donut Shop pass-by rate $=90 \%$ per scope meeting.
